

# Vibration Measurements at TTF

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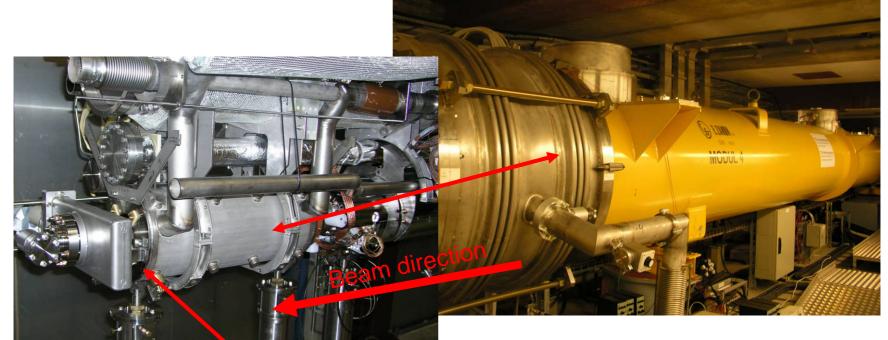
# Status from Vibration Measurements during Shutdown (Sep 2004)

- Measurements at ACC 4 only
  - Data acquisition close to sensors
  - Two sensors (cold) at the quadrupole vertical and transverse to the beam
  - □ Two sensors on top of the module
  - Two sensors on the ground/support
  - One geophone (vertical) at various places
- Measurements with various conditions
  - Comparison Piezo Geophone
  - Day, night weekend
  - Vacuum pumps on, off, pumps dismounted from trailer



Quadrupole at the End of the Cavity

String in a Module



Piezo sensors

Module 4 at ACC4 of TTF



### **Measurement Conditions**

- PC now close to sensors
- Preamplifier switched from acceleration to velocity
  - Implies a high pass at 1 Hz (.2 Hz in acc mode)
  - □ Low pass filter at 1 kHz
- Data analysis
  - Just FFT, ignoring non periodic effects, no corrections, no windowfunctions
  - Averaging over many measurements







## **Some Formulas**

$$\ddot{x}(t) = P \cdot u(t)$$

Piezo Sensor acceleration

$$P = 10^4 \cdot \frac{\mu m}{V}$$

$$\dot{x}(t) = G \cdot u(t)$$

Geophone velocity

$$P=10\cdot rac{\mu m}{V}$$
 gain switch=1 of  $V$ 

### **Fourier Transformations**

Windows (Hanning window) tested but not used

#### Fourier Integral

$$F(\omega) = \frac{1}{T} \int_0^T u(t) \cdot e^{-i\omega \cdot t} dt$$

#### **Power Spectrum**

$$P(\omega) = \frac{2}{T} \left| \int_0^T u(t) \cdot e^{-i \cdot \omega \cdot t} dt \right|^2$$

#### Fourier Transformation

$$U_{j} = \frac{1}{N} \sum_{k} u_{k} \cdot e^{-i \cdot \omega_{j} \cdot t_{k}} = \frac{1}{N} \sum_{k} u_{k} \cdot e^{-i \cdot \frac{2\pi}{N} \cdot j \cdot k}$$

$$k = 0, 1 \dots N - 1 \qquad j = 0, 1 \dots \frac{N}{2} - 1 \qquad u_{k} \in \mathbb{R}$$

### With this definition U<sub>i</sub> is only .5 of the real Amplitude

$$P_{j} = 2 \cdot T \cdot \left| U_{j} \right|^{2}$$
 depends on T!

### From Acceleration to Position

by double time integration which corresponds to by division by  $\omega^2$  of the Fourier coefficients

$$A_j o rac{U_j}{\omega^2}$$
  $P_j o rac{P_j}{\omega^2}$ 

## Variance and RMS

$$RMS = \sqrt{\sigma^2}$$

$$\sigma^2 = \frac{1}{T} \int_0^T u(t)^2 \cdot dt \qquad \text{wit}$$

with zero average

$$\sigma^2 = \frac{1}{2\pi} \int_0^\infty P(\omega) \cdot d\omega$$

$$\sigma^{2} = \frac{1}{2\pi} \int_{0}^{\infty} P(\omega) \cdot d\omega \qquad \qquad \sigma^{2} = \frac{d\omega}{2\pi} \sum_{j} 2 \cdot T \cdot \left| U_{j} \right|^{2} = \frac{1}{T} \sum_{j} P_{j} = 2 \sum_{j} \left| U_{j} \right|^{2}$$

Often one plots the RMS values as function of a lower frequency limit  $(\omega_0)$ 

$$\sigma^{2}(\omega_{0}) = \frac{1}{2\pi} \int_{\omega_{0}}^{\infty} P(\omega) \cdot d\omega$$

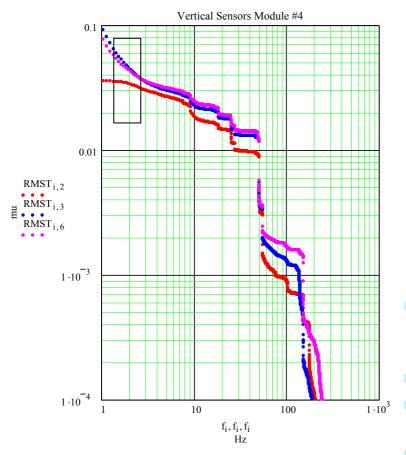
$$\sigma_{j}^{2} = \frac{1}{T} \sum_{l=j}^{\frac{N}{2}-1} P_{l} = 2 \sum_{l=j}^{\frac{N}{2}-1} |U_{l}|^{2}$$

$$RMS = \sqrt{\sigma^2}$$



## 2 Piezos and a Geophone on the Socket

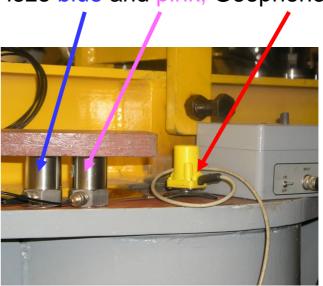
**RMS** average, Saturday midnight ± 1 hour



210804 2300 220804 0100

March 31, 2005

Piezo blue and pink, Geophone red



Good agreement between

- the two piezos
- piezo and geophone (20%)

Low RMS: 34 43 45 nm for f>2Hz

Comparable with ground motions measured by Ehrlichmann

 At low frequencies the noise signal is probably getting dominant



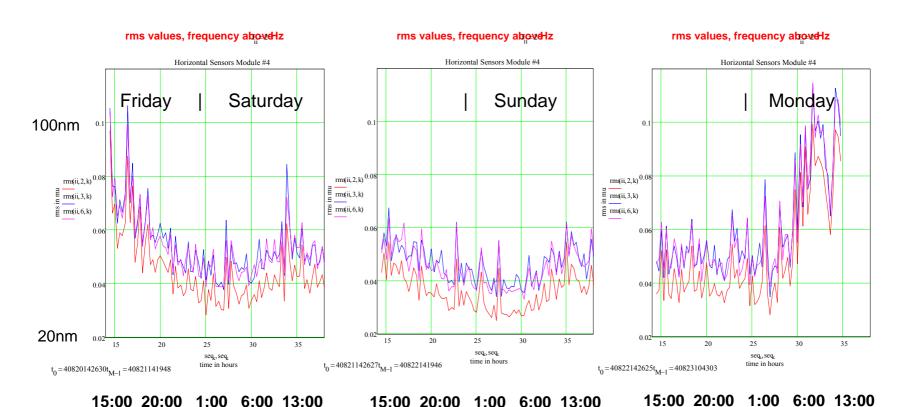
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## **Ground Vibration Time Dependence**

Friday to Monday, RMS f>2Hz

cultural noise

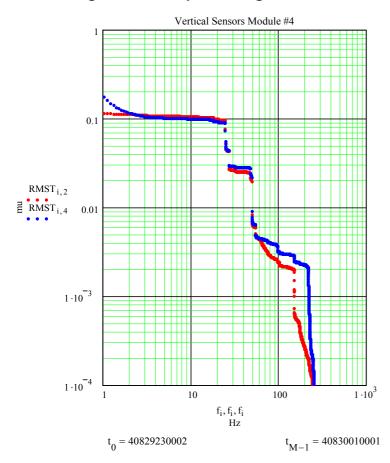


2 Piezos and a Geophone on the socket



# Comparison of Piezo and a Geophone on Top of the Module (vertical)

RMS average, satuday midnight ± 1 hour



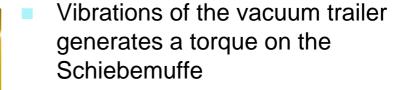
- Sensor positions on top of the module
- Good agreement, also Geophone and Piezo positions are not identical
- RMS: 115 nm for f>2Hz
- 2-3 time larger as at lower position (different weekend)





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## Check influence of the Pump Stand



Long lever arm

Vertical bellow fixed by bolts





## **Pump Stand Modifications**

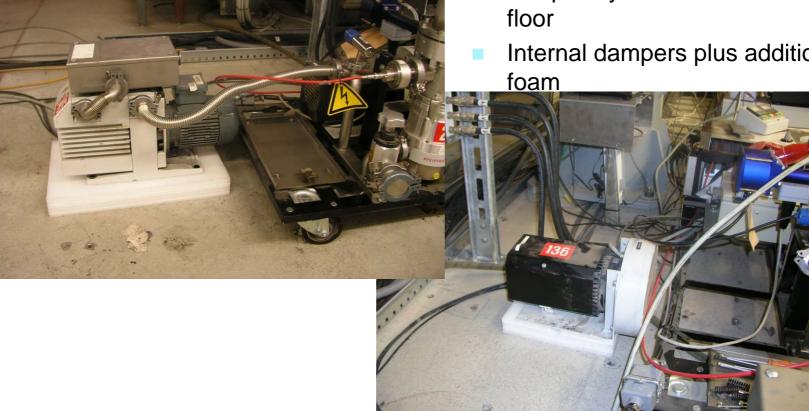
Pump moved from trailer to floor

Connected via a thin flexible line

Frequency converter moved to the floor

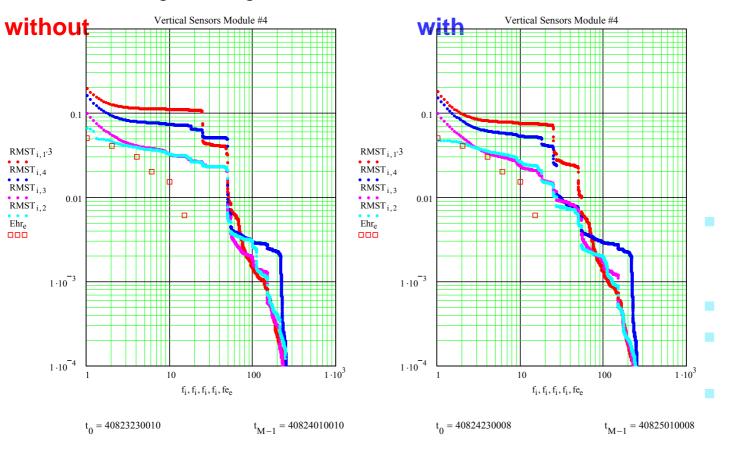
Internal dampers plus additional

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### Pump Stand without/with Modifications Vertical Sensors (2 different days)

RMS average, midnight ± 1 hour



#### Sensors:

Cold Top Socket Geophone Socket

### Different days

- Mon "without"
- Tue "with"

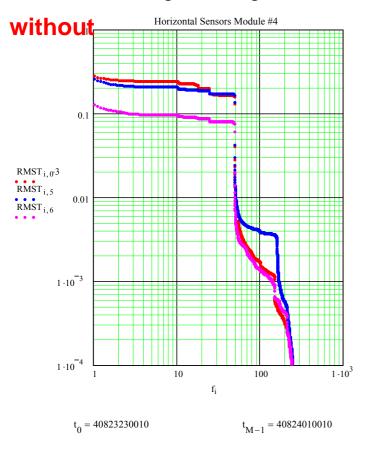
Cold Signal \*3
Some reduction
below 25 Hz

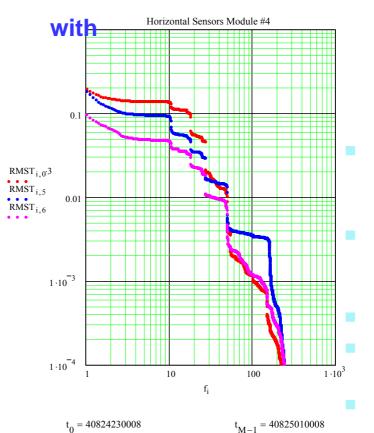
Large reduction between 25 and 50 Hz



### Pump Stand without/with Modifications Horizontal Sensors (2 different days)

RMS average, midnight ± 1 hour





Sensors:

Cold Top Socket

Different days

- Mon "without"
- Tue "with"

Horizontal vibrations much larger

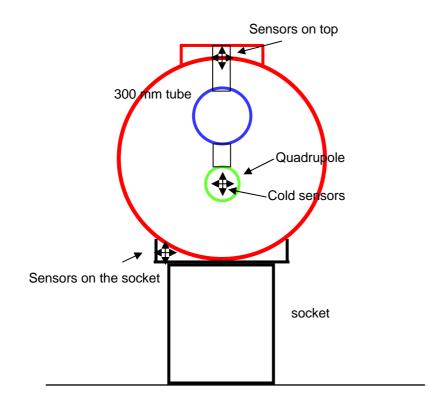
Cold Signal \*3

Some reduction below 25 Hz

Large reduction between 25 and 50 Hz

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### **Schematic View**



- The horizontal vibrations are larger (about factor 1.5)
- Cold mass essentially hanging
- Horizontal movements less constraint



## **Present Summary**

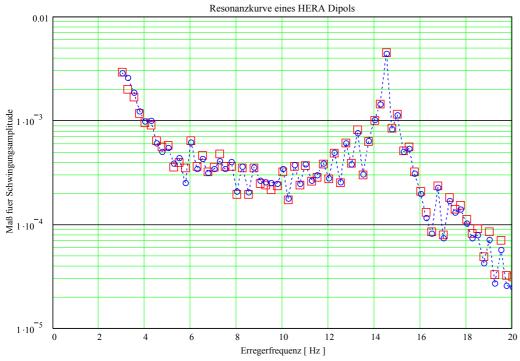
- Good agreement between the Geophone (our reference) and the Piezo in the frequency range from 2 to 100 Hz
  - at various positions
  - for averaged RMS and RMS vs. time
  - Cultural noise day/night/weekend
  - All in all data reliable
- Influence of vacuum pumps clearly seen
  - Effect vanishes after modifications
  - Pumps on/off not different anymore, which means turbo pump has no effect
- Next step
  - Analysis of data taken from forced vibrations using a motor with eccentric mass and tunable frequency
  - Analysis of data of pump stands optimizations



Forced Vibrations of a HERA Dipole

Cryostat up to 20Hz

$$Bint(i1, i2, i3, di) := \frac{f0}{\left(MF_{i3}\right)^2} \cdot \left(\sum_{i = i1 - di}^{i1 + di} B(i, i2, i3)\right)$$





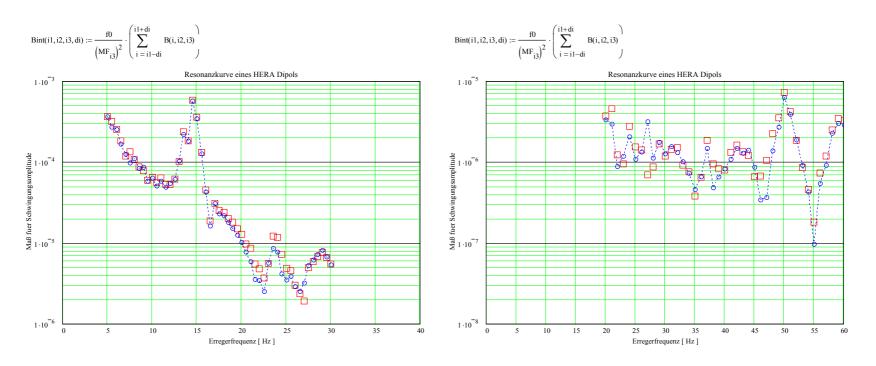




Strong resonance observed at about 14.5 Hz

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# Forced Vibration of a HERA Dipole Cryostat up to 60Hz



Different measurements with decreasing eccenter mass



# Forced Vibrations of a HERA Dipole Cryostat, RMS and Spectrum

