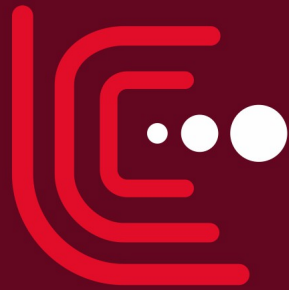


Summary of PosiPol2016



LINEAR COLLIDER COLLABORATION

Designing the world's next great particle accelerator

Masao KURIKI (Hiroshima University)



PosiPol2016

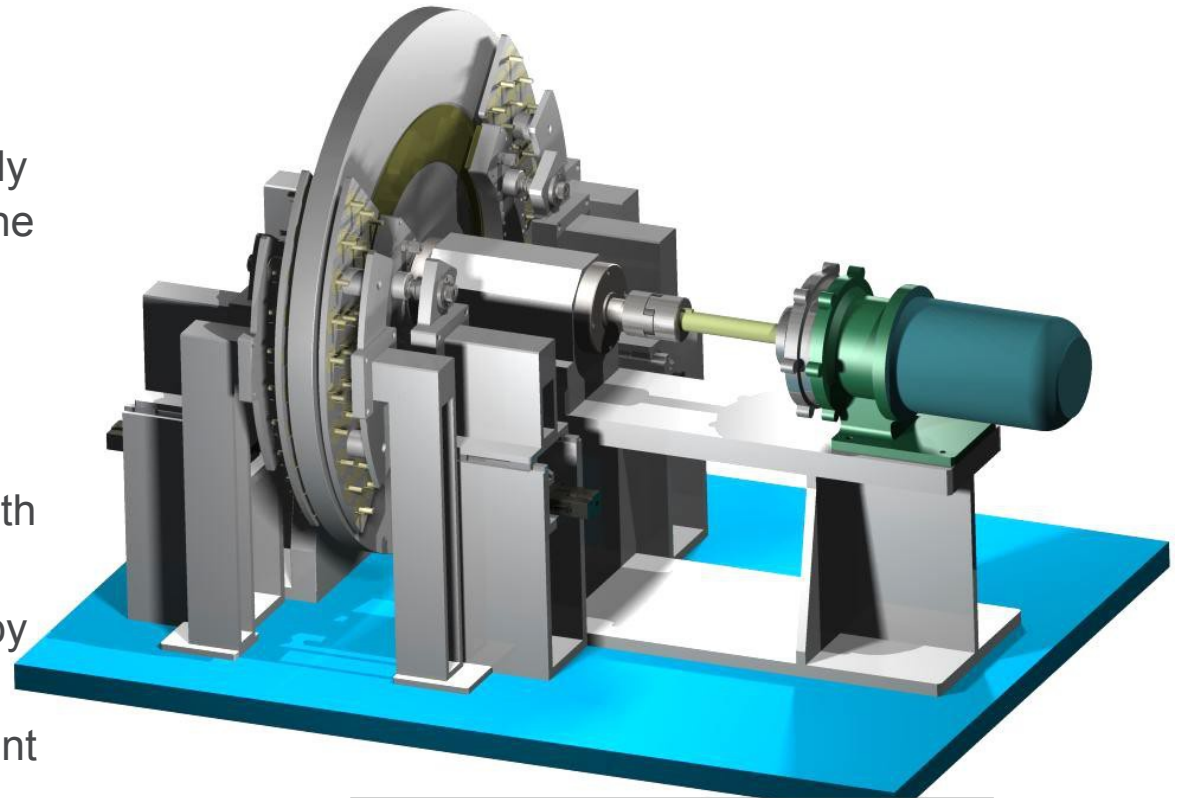
- 11th PosiPol WS
- 22 participants(16 EU, 1 US, 5 Japan) + online
- 2016/9/16-18 @ LAL-Orsay
- Laser Compton : 6
- E-Driven : 9
- Undulator : 7
- Other : 2



Active Sliding Contact Cooling Demo Conceptual Illustration

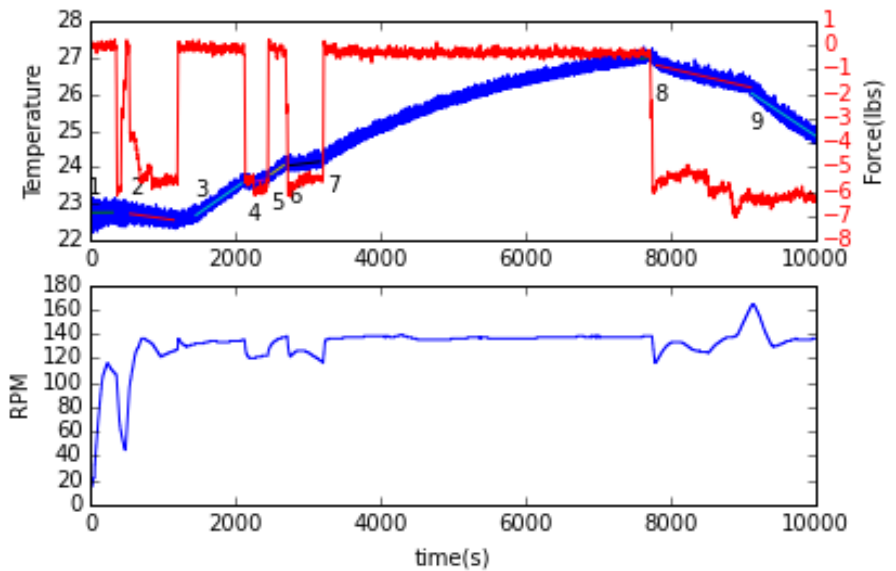
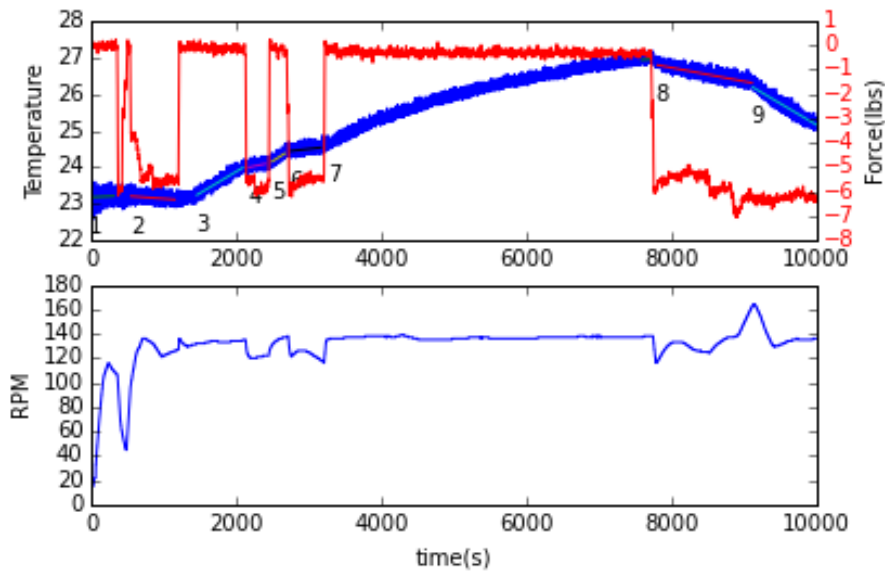
W. Liu

- Rotating 1meter diameter Target Wheel at 2000 rpm (100 m/s) while extracting ~10kW by using active sliding contact cooling.
- Target wheel is driven by a magnetically coupled drive motor which separates the motor from the vacuum.
- Stability of wheel controlled by heavy duty machine spindle.
- Temperature of wheel controlled by 4 Active Sliding Contact Cooling Pads with lubricant.
- Cooling Pad's temperature controlled by water/coolant.
- Heat applied to wheel using UHV radiant filament heaters.



Full Size Target Wheel Ready for Operations in Vacuum

Cooling Demonstration in Air



| stage | heater | Cooling pads | dT/dt (oc/s) | | Estimated cooling /heating power (W) | |
|-------|------------|--------------|--------------|------------|--------------------------------------|--------------------|
| | | | Upstream | Downstream | Upstream | Downstream |
| 1 | Off | Removed | 9.36E-05 | 2.29E-05 | --- | --- |
| 2 | Off | Applied | -1.51E-04 | -2.83E-04 | -14.6 | -27.4 |
| 3 | On, medium | Removed | 1.17E-03 | 1.38E-03 | 113.5 | 133.8 |
| 4 | On, medium | Applied | 4.18E-04 | 4.40E-04 | -72.9(equivalent) | -91.2(equivalent) |
| 5 | On, medium | Removed | 1.26E-03 | 1.41E-03 | 122.2 | 136.7 |
| 6 | On, medium | Applied | 2.26E-04 | 2.51E-04 | -100.3(equivalent) | -112.4(equivalent) |
| 7 | On, medium | Removed | 1.01E-03 | 1.24E-03 | 97.8 | 120.2 |
| 8 | On, medium | Applied | -3.73E-04 | -4.66E-04 | -36.2(net) | -45.2(net) |
| 9 | Off | Applied | -1.16E-03 | -1.32E-03 | -112.5 | -128.0 |



Cooling of the ILC e⁺ target by thermal radiation

S. Riemann

Ecm and luminosity determine energy deposition in target

∅ = 1m; 2000rpm, 0.4X0 Ti6Al4V

(Pe⁺ ≤30%)

| -Ebeam [GeV] | - Edep [kW] | -∞Tmax/pulse [K] | - dpa | -∞Tmax/pulse [K] | |
|---------------------------------|-------------|------------------|---------|----------------------|-------------------|
| | | | | - Nominal luminosity | - High luminosity |
| -120 A. Ushakov, 2015 | - 5.0 | - 66 | - 0.035 | - - | - - |
| -175 (ILC EDMS) | - 3.9 | - 125 | - 0.06 | - - | - - |
| -250 (ILC EDMS) | - 2.0 | - 130 | | - 4.1 | - 195 |
| -250 A. Ushakov, Update 2015 | - 2.3 | - 85 | - 0.05 | - 4.6 | - 128 |

Edep ≤ 7kW → cooling by thermal radiation is an option

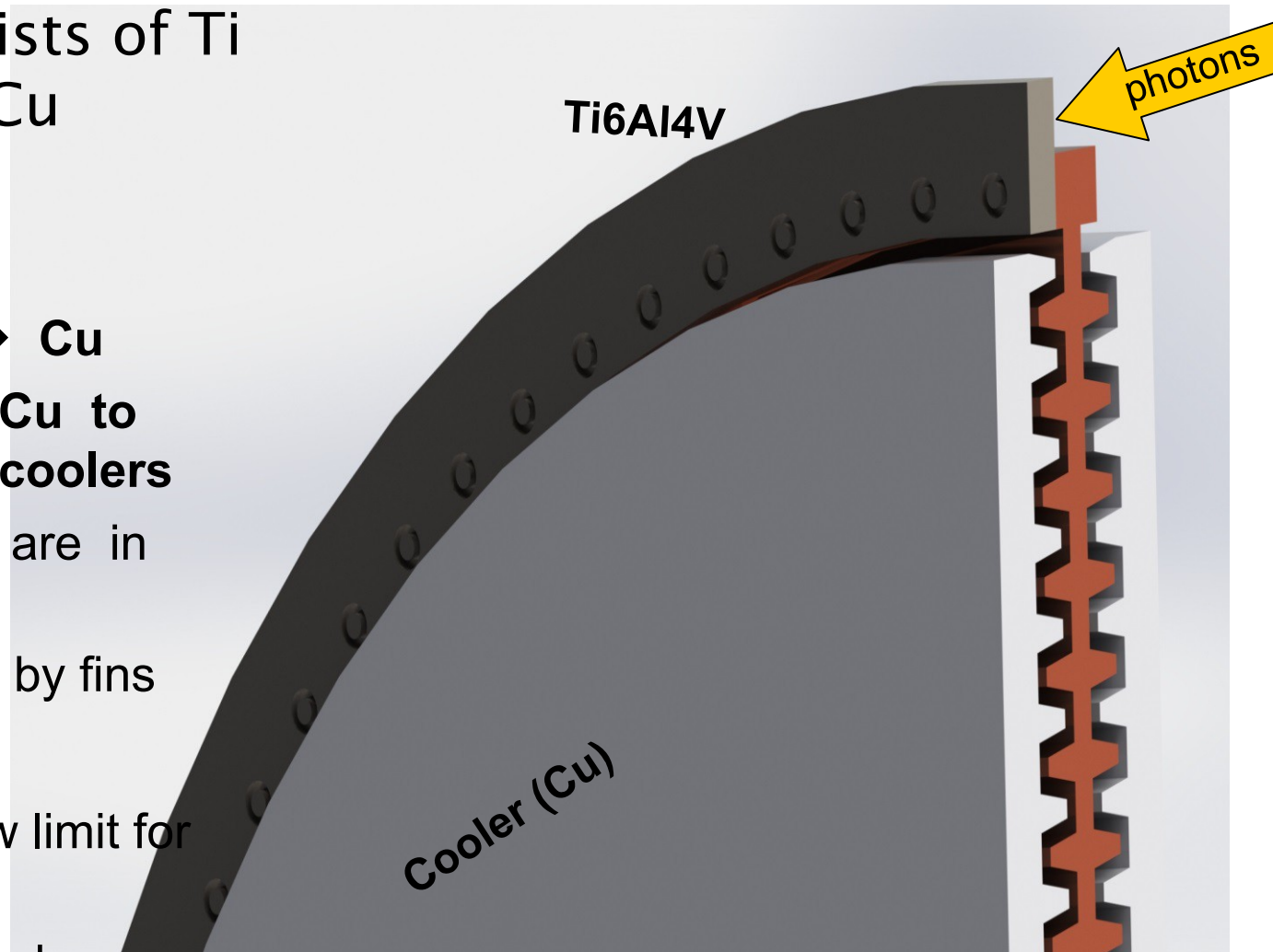
Radiative cooling model

- Rotating wheel consists of Ti rim (e⁺ target) and Cu (radiator)
- Heat path:
 - thermal conduction Ti → Cu
 - Thermal radiation from Cu to stationary water cooled coolers
- Target, radiator and cooler are in vacuum
- Radiating area is adjusted by fins

Goal:

keep target temperature below limit for failure of Ti6Al4V

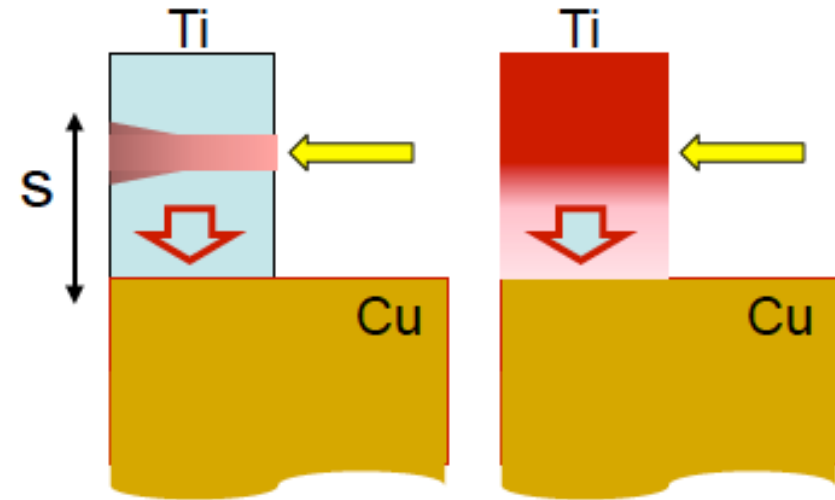
Reliable fatigue limit at elevated temperatures?





Heat transfer target to radiator

- Spinning target \Leftrightarrow ~ 6.5 s between load cycles
 - Heat moves $\sqrt{\lambda t / \rho c} \sim 0.5$ cm in 6.5sec
 - accumulation of heat in the target
- Temperature flow to radiator depends on s
 - Average heat transfer through rim



$$\frac{dQ}{dt} = \lambda \cdot A_{\text{contact}}^{\text{Ti-Cu}} \frac{dT}{ds} \sim \lambda / s \cdot A_{\text{contact}}^{\text{Ti-Cu}} (T_{\text{Ti}} - T_{\text{Cu}})$$

$$A_{\text{contact}} \sim 470 \text{cm}^2, \lambda \sim 10 \text{W}/(\text{m K})$$

$$dQ/dt = 2.3 \text{kW}: T_{\text{max-ave}} (\text{Ti}) - T_{\text{contact}} \sim 100 \text{K} (s=1.5 \text{cm}) \\ \sim 150 \text{K} (s=2.5 \text{cm})$$

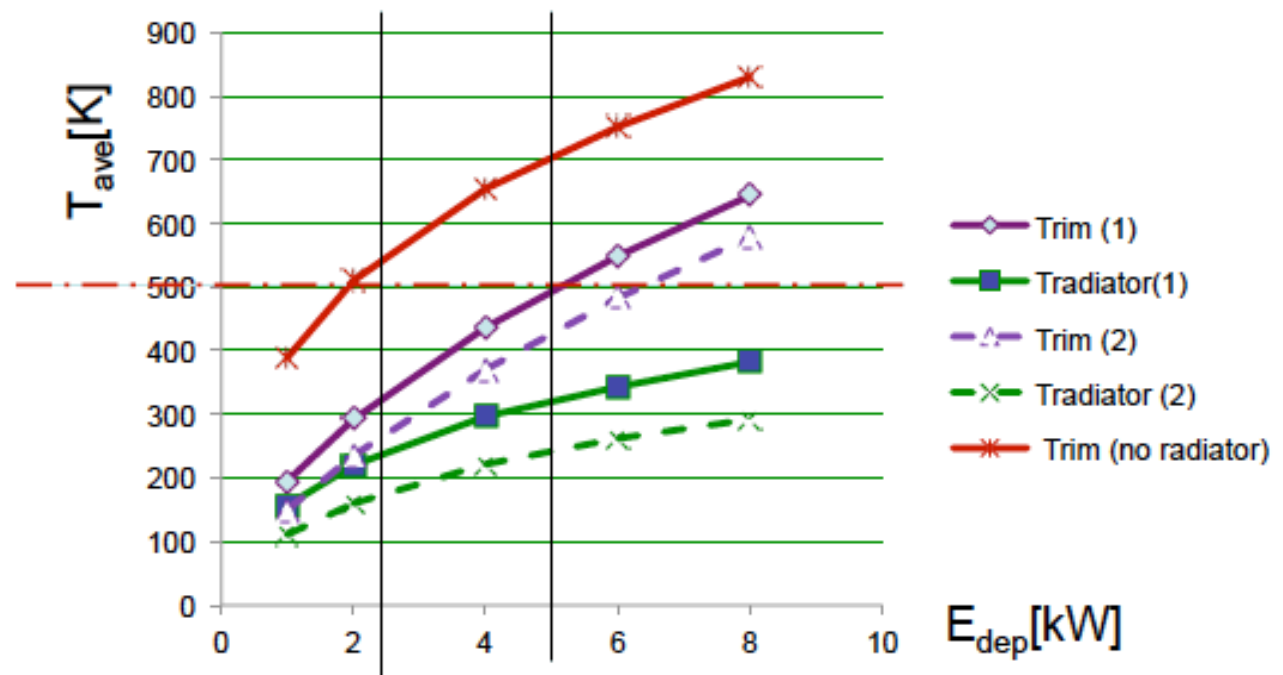
- Additional cyclic temperature rise by pulse (80...200K)
- Cyclic peak temperatures in target can exceed 500°C , in particular for large s
 - need design with short heat transfer path through Ti rim to keep the average T_{target} as low as possible
 - for high power deposition (\Leftrightarrow high lumi) even average temperature could be $>500^\circ\text{C}$



Estimated average temperature in T rim and Cu radiator

Consider thermal radiation from rim and radiator

- Case (1): rim 0.082m^2 + radiator 1m^2
- Case (2): rim 0.082m^2 + radiator 2m^2
- Case (3): Only rim, 0.16m^2 ; no radiator
- Emissivity $\varepsilon=0.6$

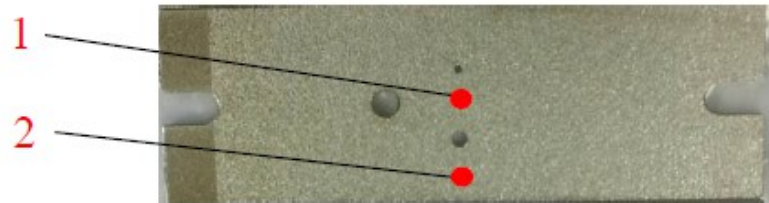


- Estimates give the principal behavior and only approximate temp values. Real temperatures need simulations, they depend on radiator design and Ti-Cu contact



Target Material Test at MAMI, Mainz

A. Ignatenko



| Target | Hit point | Regime | Beam time | Load cycles | Years of ILC operation* |
|--------|-----------|----------------------------------|-------------|-------------------|-------------------------|
| #1 | 1 | 100 Hz, 2 ms, 10 μ A average | 18 h 28 min | $6.82 \cdot 10^6$ | 2.46 |
| #1 | 2 | 67 Hz, 3 ms, 10 μ A average | 5h 4 min | $1.24 \cdot 10^6$ | 0.45 |
| #2 | 1 | 67 Hz, 3 ms, 10 μ A average | 5h 4 min | $1.24 \cdot 10^6$ | 0.45 |
| #3 | 1 | 100 Hz, 2 ms, 10 μ A average | 14 h 22 min | $5.17 \cdot 10^6$ | 1.87 |

*1 year of ILC operation: 5000 h, 5 Hz, each point is irradiated every 6.5 s

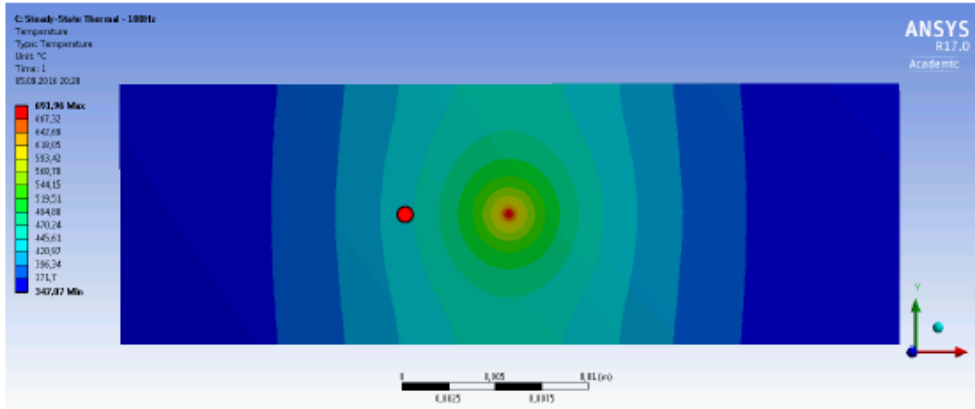




ANSYS simulation, target #1

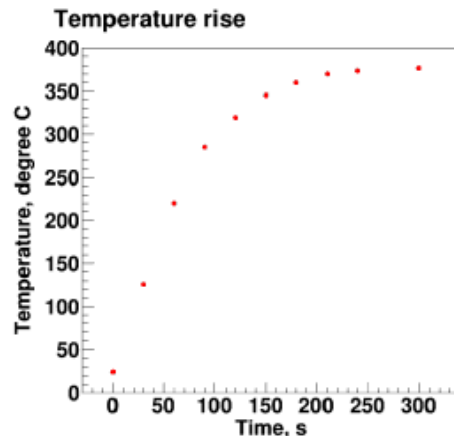
| | |
|-----------|-----------|
| Target | #1 |
| Thickness | 1 mm |
| Surface | Rough |
| Fixation | Not fixed |
| Cooling | Radiation |

Neglect low thermal conductivity to the holder via ceramics etc
 Consider cooling by radiation from the surface only



Max. average T = 691 °C
 Max. T rise / pulse (@ 700 °C) = 82 °C
 Max. T in target #1: 691 + 82 °C

Distribution of the average temperature ($\epsilon=0.5$)*



→ $\epsilon \gtrsim 0.5$

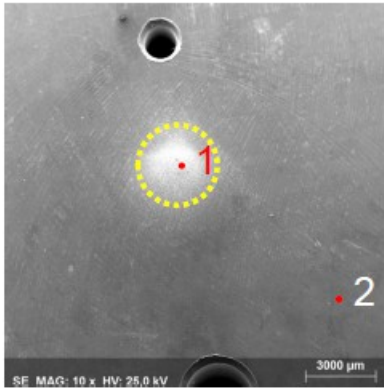
* Here and later:
 • Ambient T = 22 °C
 • Ti6Al4V properties according to
 K.C. Mills, 2002, Recommended Values of Thermophysical Properties
 For Selected Commercial Alloys, p. 217, as referenced by J. Yang

Real temperature measurement in ●



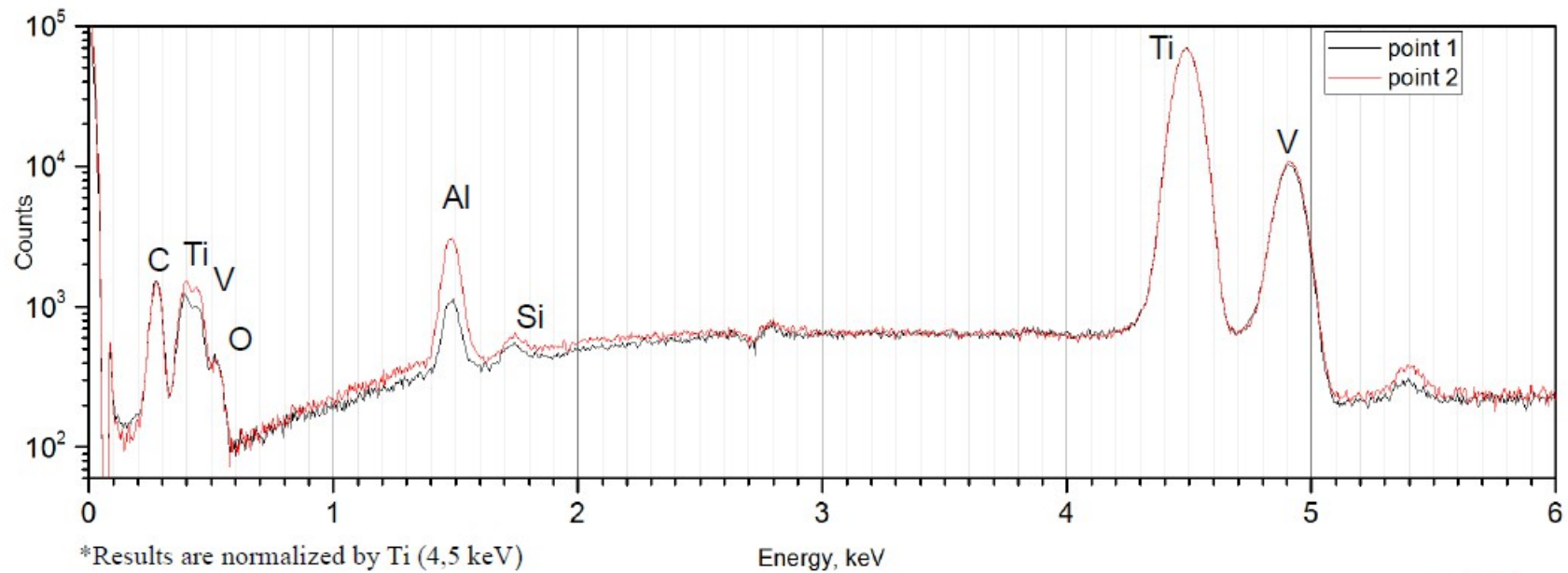


Target #3, SEM image (Yegor Tamashevich)



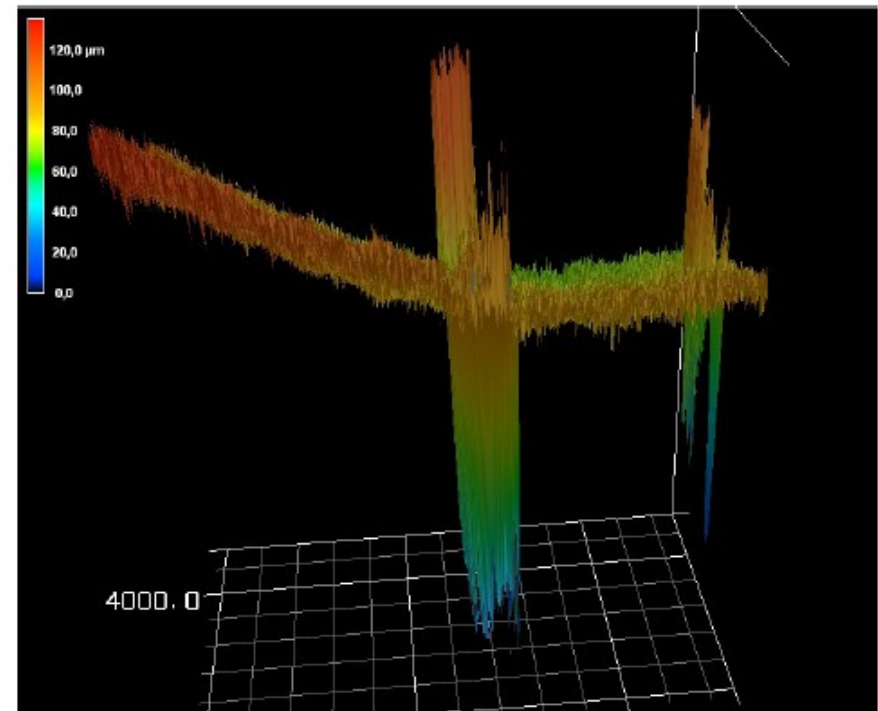
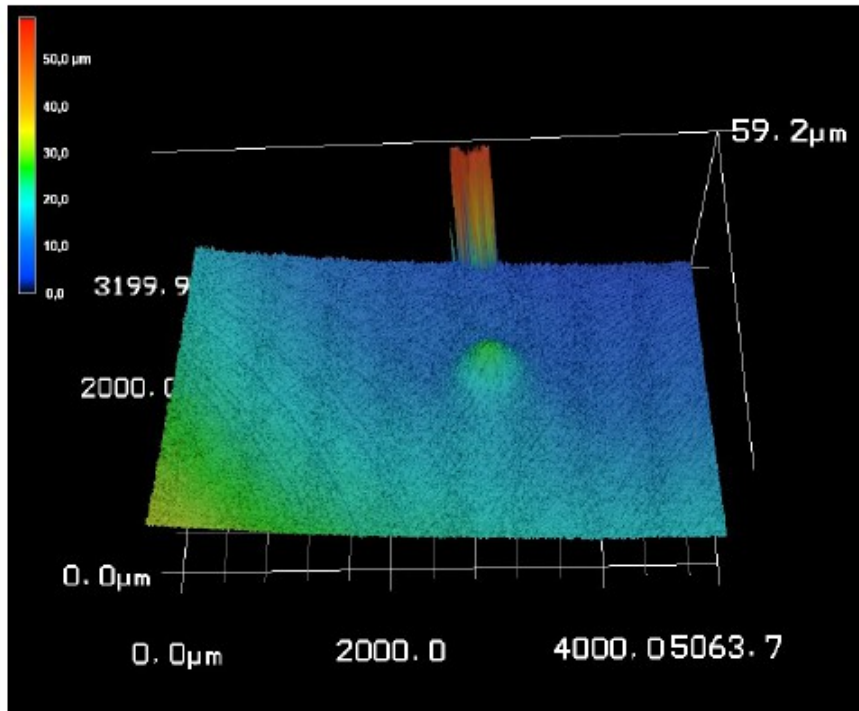
Point 1 – Beam spot area
Point 2 – Un-irradiated area

Aluminum concentration is lower in the beam spot area





Target #3, surface investigation, exit side



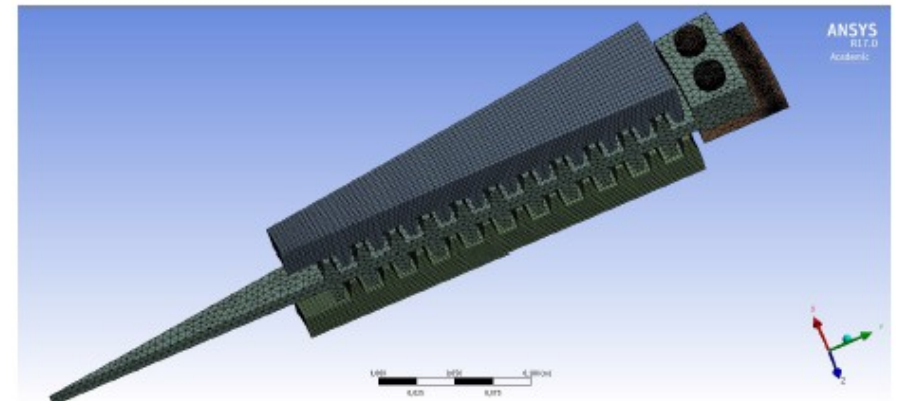
Plastic deformation after irradiation, 1 peak observed in the beam spot: $\sim 25 \mu\text{m}$ from the surrounding to the top of the peak



Thermomechanicle Examination :F. Dietrich

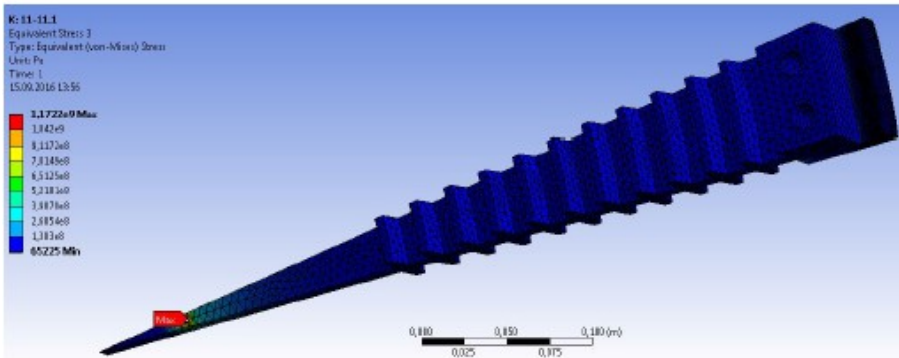
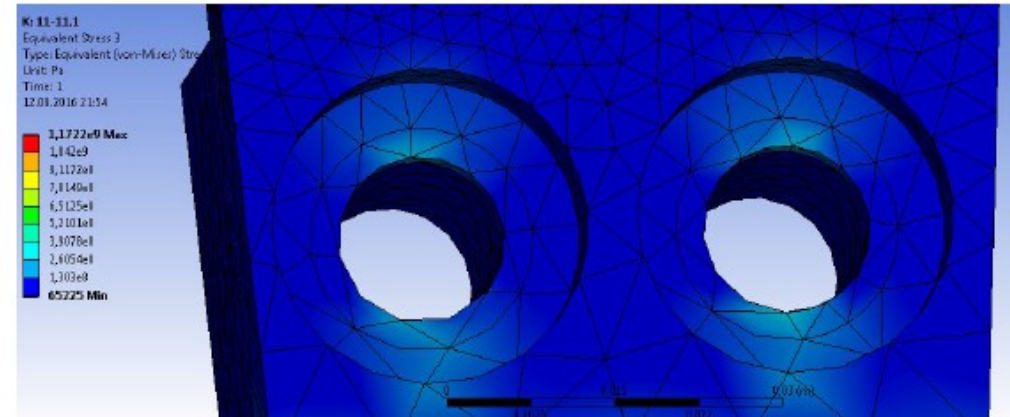
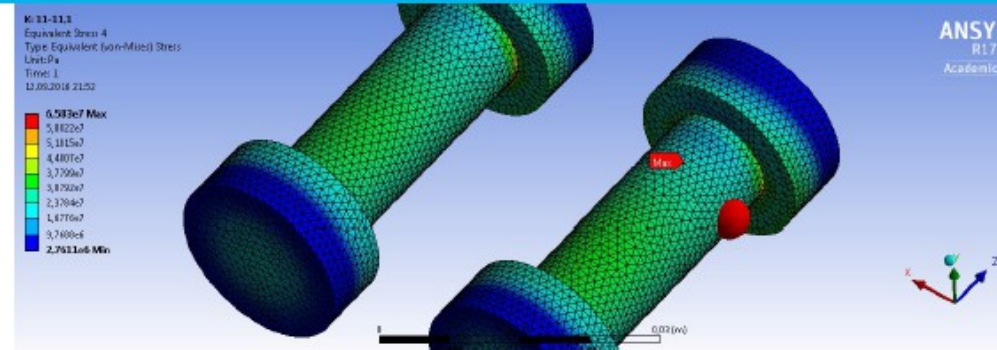
Modified Model – simulation set up

- > the new Model is simulated with an energy deposition of 2.3 kW
- > there is only a static thermal simulation
- > there is now a static structural analysis
 - including a constant rotational force
 - the wheel has fixed faces under the fins
 - Screw were fixed with Bolt pretensions and frictional connections
- > 3 Simulations were done
 - M12 with 11.1 mm thickness
 - M12 with 14.8 mm thickness
 - M5 with 14.8 mm Thickness



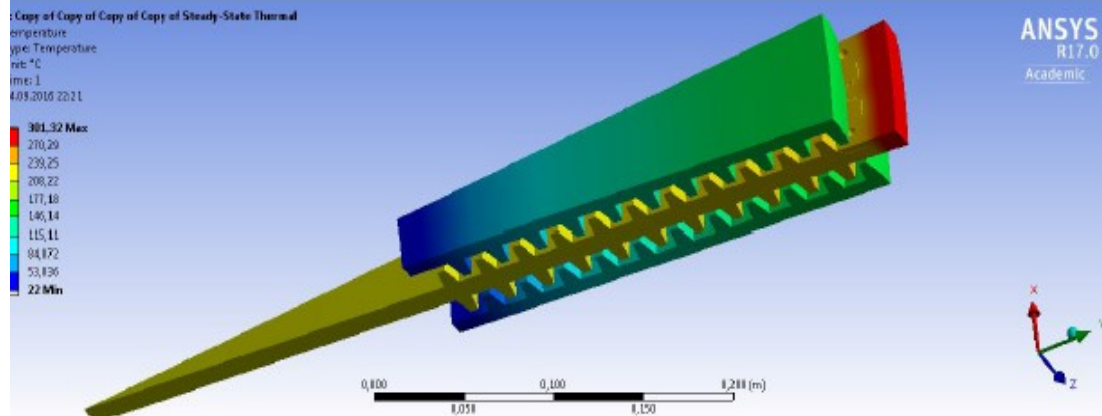
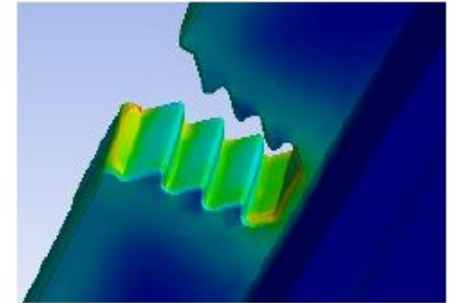
New Model – result

- Max. temperature: 282.71°C (555.86 K)
 - located in the middle of the beam spot
- Max von Mises stress: 1,17GPa
 - at the fixed surface (maybe artificial)
- Max. von Mises stress at the screws 65,83MPa
- Max. von Mises stress at the contact surface is 203,8MPa



Fire-tree-root – results

- > Max equilibrium temperature is 301.31 °C (574.46K)
 - located over the fire tree ,at the exit side, in the middle of the beam spot
- > Static simulation shows max. von Mises Stress of 66,08 MPa
 - locates at the bottom of the fire-tree notch



ANSYS
R17.0
Academic

Static Structural
Equivalent Stress
Units: Equivalent (von Mises) Stress
Units: Pa
mm: 1
4/9/2016 22:21

6.6083e8 Max
5.974e8
5.1328e8
4.4875e8
3.6713e8
2.8371e8
2.2828e8
1.4686e8
7.3434e7
10526 Min

