Mechanical design studies of the pulsed solenoid for positron sources

Possible methods for manufacture

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polarized gamma photons with a titanium target.



A pulsed solenoid is used to match the emittance of the positron bunch with the acceptance of the accelerating-focusing channel.

Principal Layout: Ti-Wheel with a Diameter of 1.0 m, rotating at 100 m/s, 2000 rpm.



Cross-section of the vacuum chamber with rotation target wheel, magnetic bearing system, and pulsed solenoid

Diameter of wheel: 120 cm, 2000 rpm Tangential velocity at r=50 cm: 100 m/s The mass of the wheel 50 kg (without shaft) Ti-alloy target 7mm thickness The repetition rate of the beam pulses is 5 Hz Heat input around the wheel is about 2 kW Thermal radiation cooling from both sides of the target



Basic concept of the pulsed solenoid

The concept of the solenoid has already been developed and presented in the relevant papers [G. Moortgat-Pick, C. Tenholt, S. Riemann, G. Loisch]. From a mechanical point of view, the solenoid should have a conical shape with the corresponding geometrical dimensions.



Requirements

The solenoid will be made of a copper conductor with a cross-section of 9x9 mm and have a channel with a diameter of 6 mm for cooling. It must be equipped with current and water leads.



Three possible approaches for manufacturing the solenoid coil

- Using a standard conductor from the optics used in the accelerator (crosssection 9x9mm with a hole diameter of 6mm).
- Manufacturing a special conductor of the required cross-section using the extrusion method of copper.

• 3D printing with copper (proposed by Martin Lemke)



Coil turns turned at the angle of the solenoid cone





Design presented at FutureColider@DESY conference in January 2024





Focal plane parallel to the target plane



As a result, the prototypes proposed today looks like this:





Conclusions and plans:

The following ideas have been proposed, requiring further analysis:

- Turning the turns of the coil by an angle equal to the cone angle of the solenoid, which will reduce the coil's "looseness" and smooth the magnetic field gradient along the axis.
- 3D printed inter-turn transitions, allowing the turns to be placed in a plane parallel to the target plane.
- Two methods of fixing the solenoid turns are proposed, which are estimated to increase the operational lifespan by an order of magnitude

• Everything mentioned above requires magnetic and stress simulations, which are part of our future plans.

Thanks for your attention!

Contact

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BACKUP Slides

The problem of the mechanics of such a pulsed device is the result of the action of electrodynamic forces in the elements of the magnet, primarily in its conductive units. Pulsed mechanical action during operation of the magnet should not lead to unacceptable mechanical stress in its elements. Usually this problem can be solved by applying external mechanical connections.

In relation to PS, the problem of mechanical fastening of winding turns is exacerbated due to the impossibility of using organic insulation under conditions of intense flows of ionizing radiation. Here it is possible to use, in essence, only ceramic insulation, and in limited quantities.



Powering of the Cu-Conductor.

- length l=1 m,
- pulsed with half sine pulses of 4 ms, 50 kA peak at 5 Hz.
- Av. Ohmic resistance: 2.38 10⁻⁴ Ω .
- Av. d.c.Voltage: 12. V.
- Av. Pulsed power: 5.95 kW.
- PEDD(el): 1.86 J/g pulse, well below the accepted limit of 10 J/g.
- ΔT=4.66 K/pulse.
- Av. Power density: 83 W/cm^3.
- *Use high quality, oxygen free Copper with high electrical conductivity: σ =5.85 10^5 (1/ Ω m).

Cooling of the Conductor.

- Water flow with a velocity of 6 m/s through the conductor gives a mass flow of 0.17 l/s.
- • Pressure drop $\Delta P=6$ Bar/meter.
- ΔT in water over the conductor length of 1 m: 8.35 K.
- Water inlet at 20 oC.
- Peak temperature rise in the coil above the water temperature just after a pulse, during steady state cycling: 18.3 K.
- Peak temperature in the conductor: at the inlet 38.3 oC, at the outlet 46.7 oC.