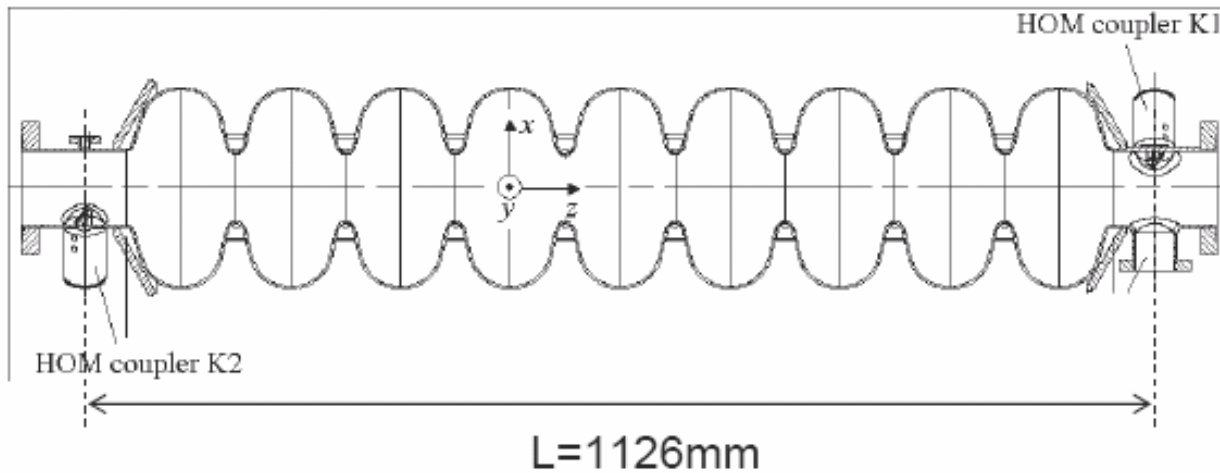




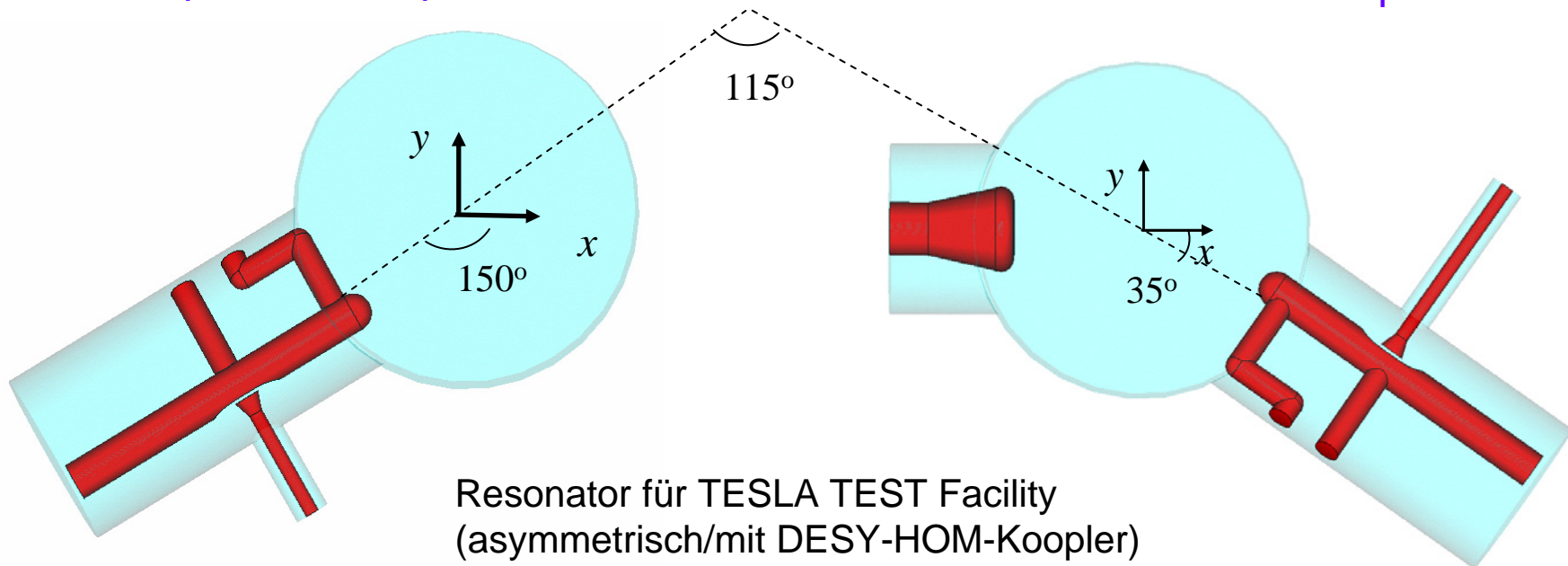
# Coupler Kick

Igor Zagorodnov and Martin Dohlus  
ILC Workshop, DESY  
31 May, 2007



upstream coupler

downstream couplers



Resonator für TESLA TEST Facility  
(asymmetrisch/mit DESY-HOM-Kooper)  
0 93 2214/0.000

# Outlook

- Coupler kick due to short-range wakefield (**coupler wake**)
- Coupler kick due to asymmetry of the external RF field (**coupler RF kick**)
- Comparison to the kick of the TESLA cavity (**cavity wake**)

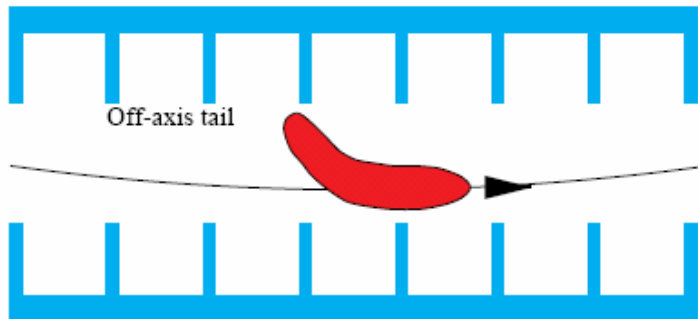
# Notation and Definitions

$\lambda(s)$  – Gaussian bunch with rms width  $\sigma$

$$k_{\perp} = \langle W \rangle = \int W(s) \lambda(s) ds \text{ – kick factor}$$

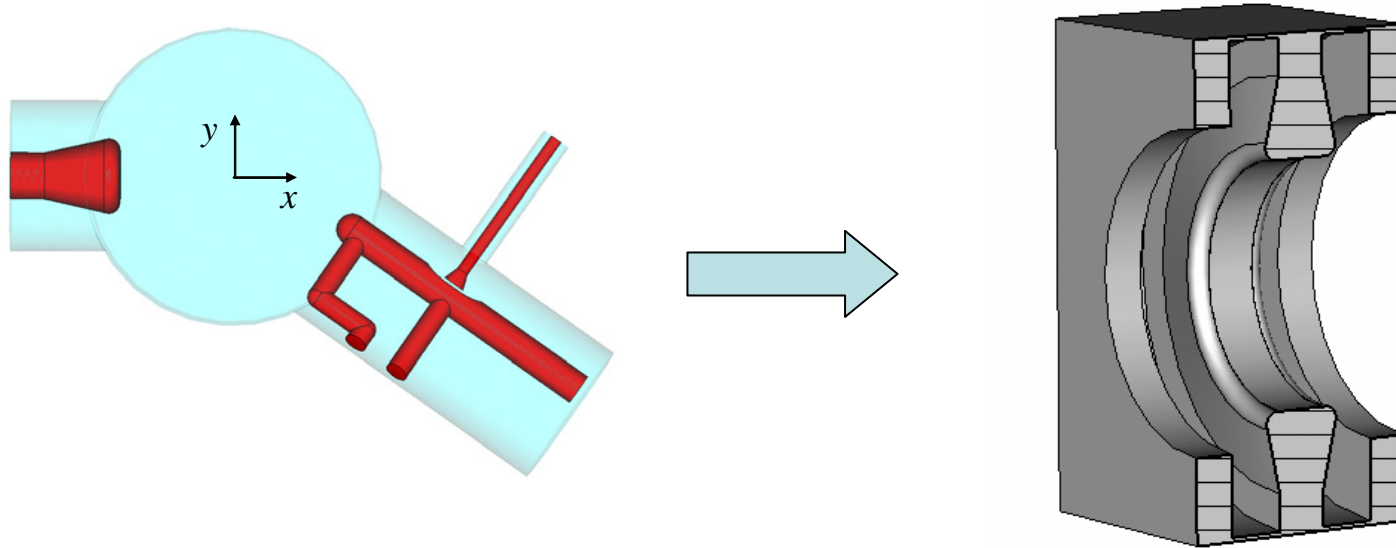
$$k_{\perp}^{\text{rms}} = \langle (W - k_{\perp})^2 \rangle^{0.5} = \left[ \int (W(s) - k_{\perp})^2 \lambda(s) ds \right]^{0.5} \text{ – rms kick factor}$$

It gives an estimation for the head-tail difference in the kick  
(banana shape)



The picture from  
R. Wanzenberg,  
Review of beam dynamics ...,  
Linac Conference, 1996

## Accuracy estimation / code benchmarking

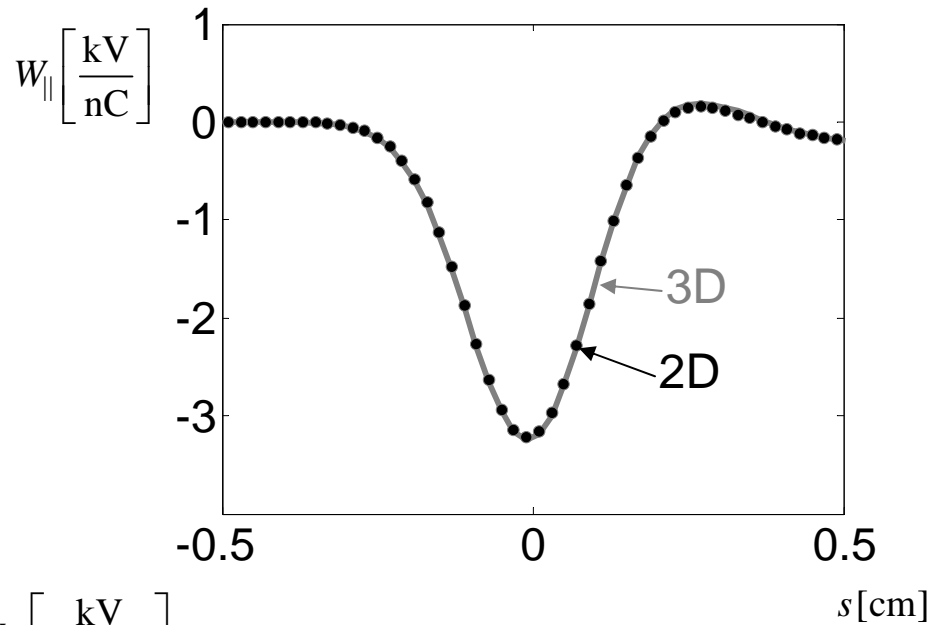
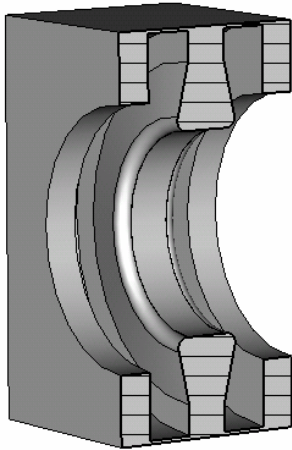


1. Zagorodnov I, Weiland T., *TE/TM Field Solver for Particle Beam Simulations without Numerical Cherenkov Radiation*// Physical Review – STAB,8, **2005**.

2. Zagorodnov I., *Indirect Methods for Wake Potential Integration* // Physical Review -STAB, 9, **2006**.

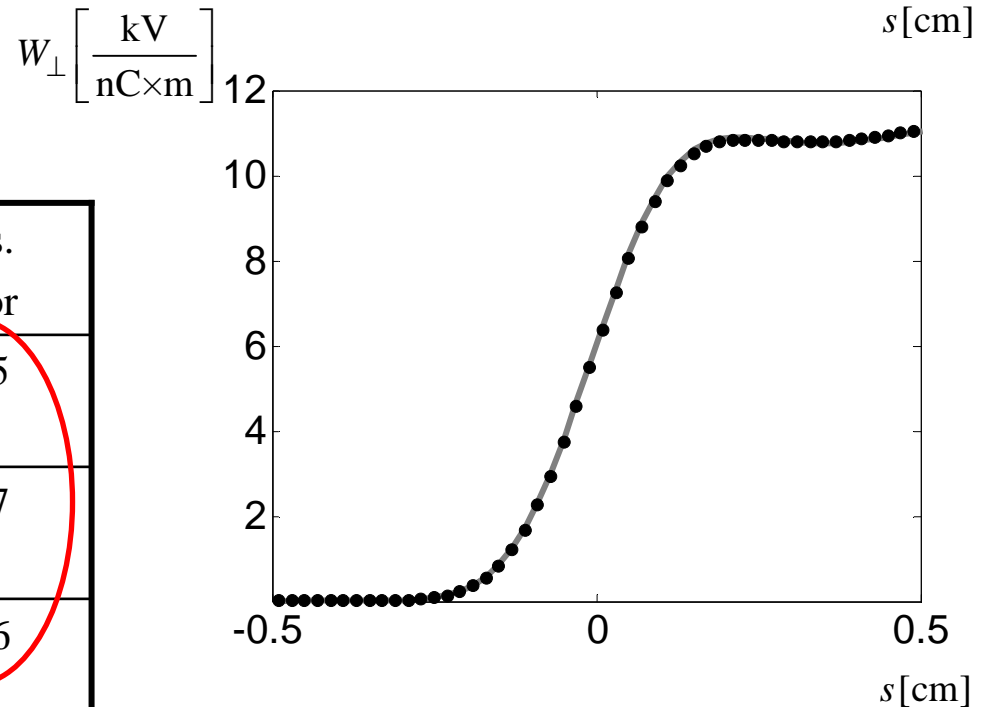
3. Bane K.L.F, Stupakov G., Zagorodnov I., *Impedance Calculations of Non-Axisymmetric Transitions Using the Optical Approximation*// Physical Review - STAB, submitted

# Accuracy estimation



Gaussian bunch with  $\sigma = 1$  mm

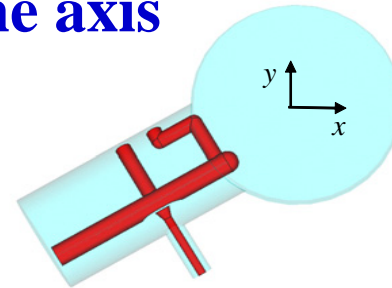
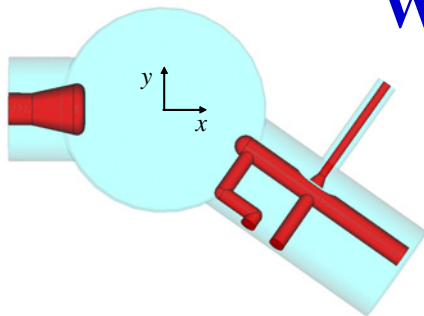
|                           | 2D,<br>$\sigma/h=5$ | 2D,<br>$\sigma/h=10$ | 3D,<br>$\sigma/h=5$ | Abs.<br>error |
|---------------------------|---------------------|----------------------|---------------------|---------------|
| $k_{  }$ ,<br>kV/nC       | 2.205               | 2.195                | 2.241               | 0.05          |
| $k_{tr}/ r $ ,<br>kV/nC/m | 5.820               | 5.817                | 5.89                | 0.07          |
| $ k_{tr}(0) $ ,<br>kV/nC  | 0                   | 0                    | 1e-6                | 1e-6          |



downstream couplers

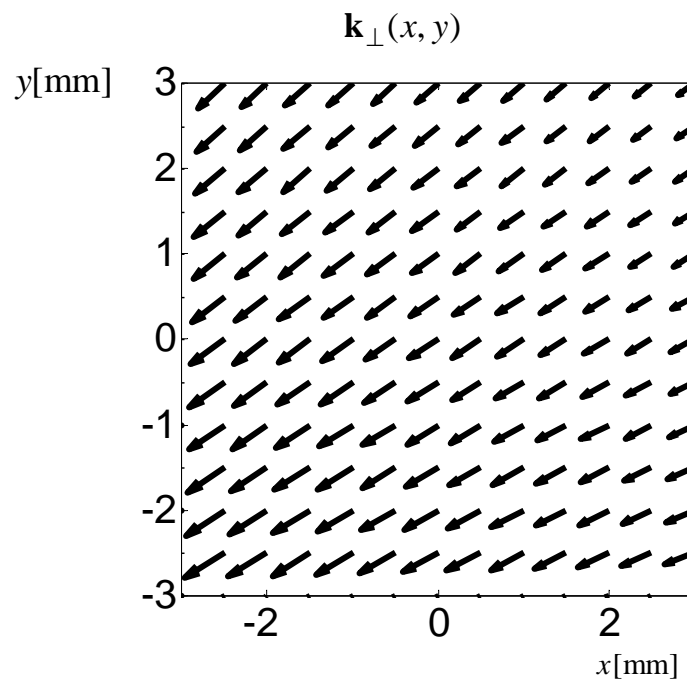
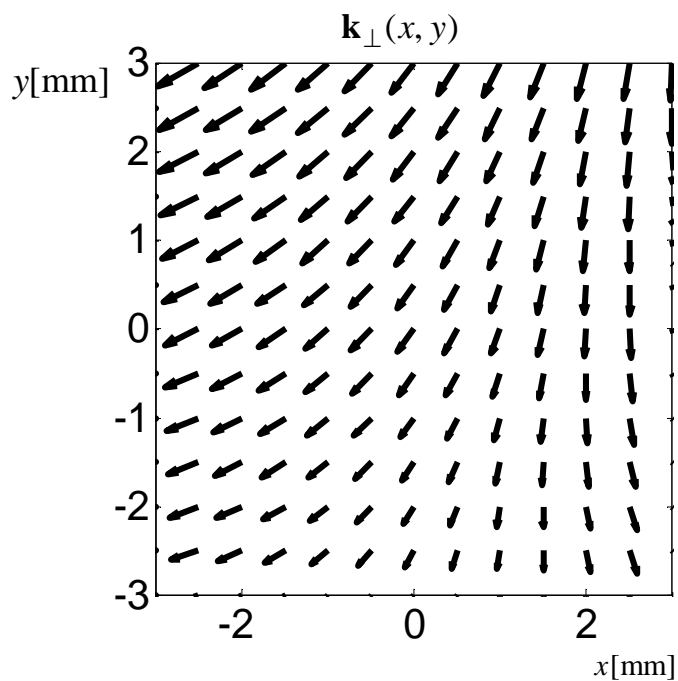
upstream coupler

## Wake kick near to the axis

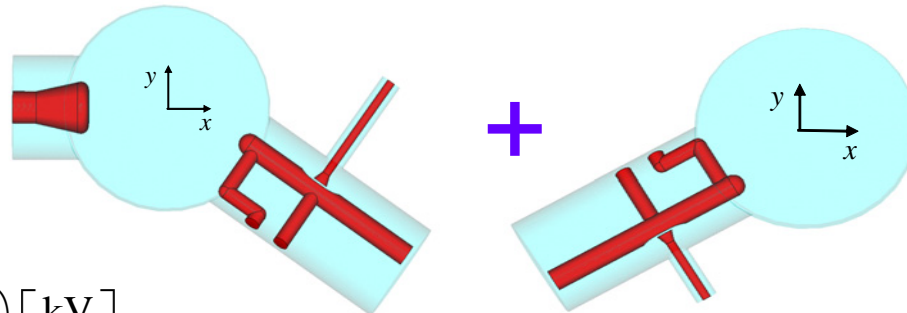


$$\mathbf{k}_{\perp}(x, y) = \begin{pmatrix} -0.0069 \\ -0.0094 \end{pmatrix} + \begin{pmatrix} 3.2 & -1.1 \\ -1.1 & -1.0 \end{pmatrix} \begin{pmatrix} x[\text{m}] \\ y[\text{m}] \end{pmatrix} \begin{bmatrix} \text{kV} \\ \text{nC} \end{bmatrix}$$

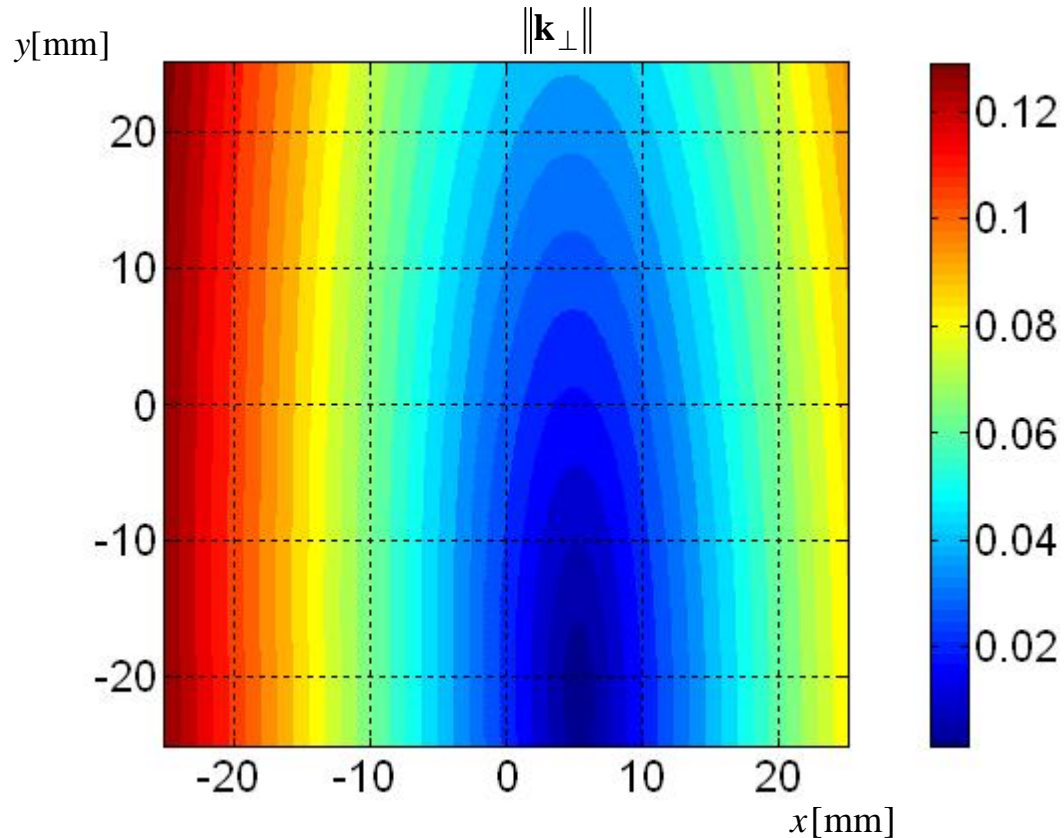
$$\mathbf{k}_{\perp}(x, y) = \begin{pmatrix} -0.0142 \\ -0.0095 \end{pmatrix} + \begin{pmatrix} 1.02 & 1.15 \\ 1.15 & 0.07 \end{pmatrix} \begin{pmatrix} x[\text{m}] \\ y[\text{m}] \end{pmatrix} \begin{bmatrix} \text{kV} \\ \text{nC} \end{bmatrix}$$



# Wake kick near to the axis



$$\mathbf{k}_{\perp}(x, y) = \begin{pmatrix} -0.021 \\ -0.019 \end{pmatrix} + \begin{pmatrix} 4.3 & 0.07 \\ 0.03 & -0.9 \end{pmatrix} \begin{pmatrix} x[\text{m}] \\ y[\text{m}] \end{pmatrix} \begin{bmatrix} \text{kV} \\ \text{nC} \end{bmatrix}$$



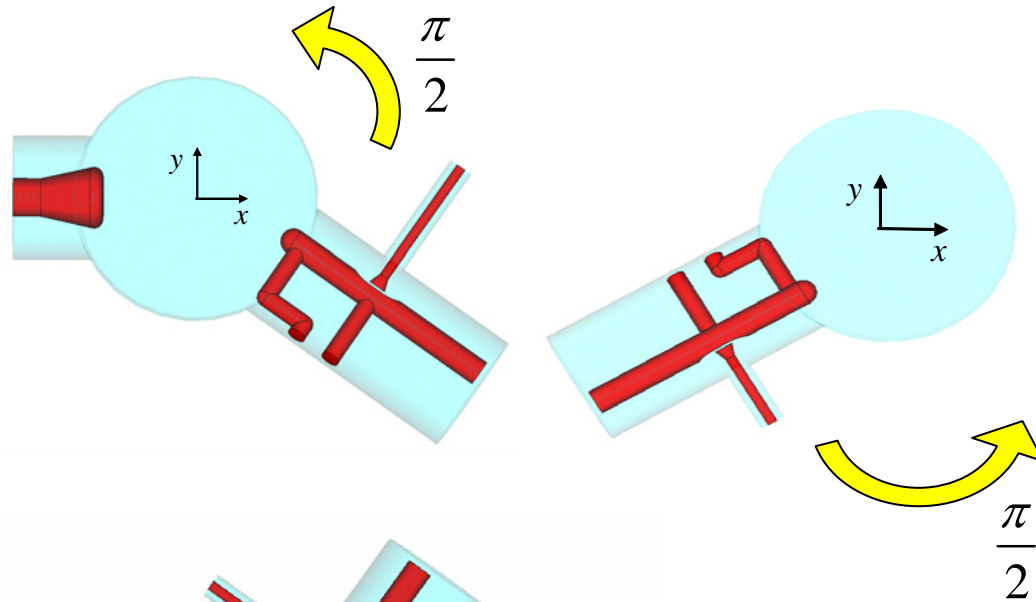
$$\mathbf{r}_c = \begin{pmatrix} 5.3 \\ -21.3 \end{pmatrix} \text{mm}$$

$$\|\mathbf{k}_{\perp}\|_{\min} = 5e-5 \frac{\text{kV}}{\text{nC}}$$

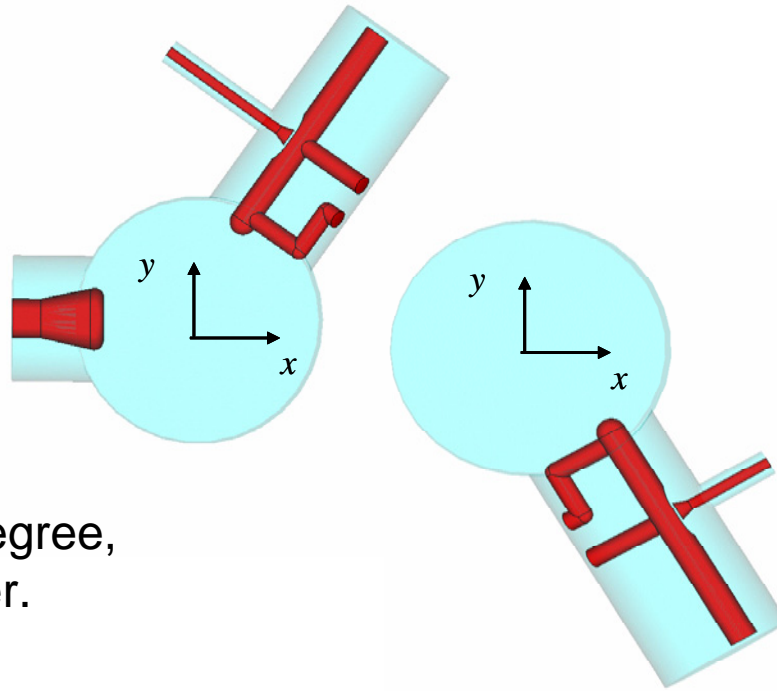


# How to compensate the wake kick on the axis?

old

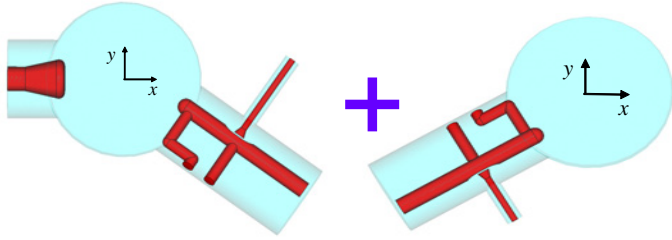


new



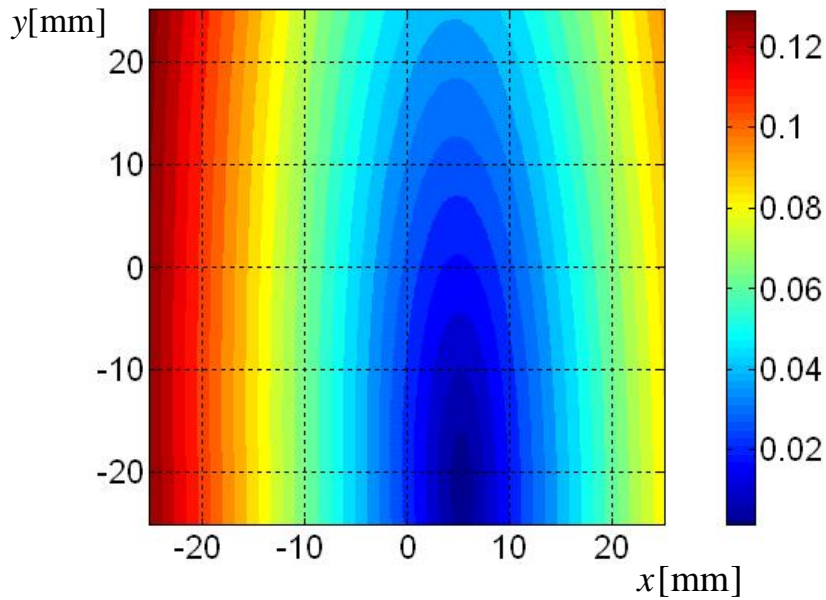
We have rotated by 90 degree,  
but 92.5 is possible better.

# Wake kick for the new orientation



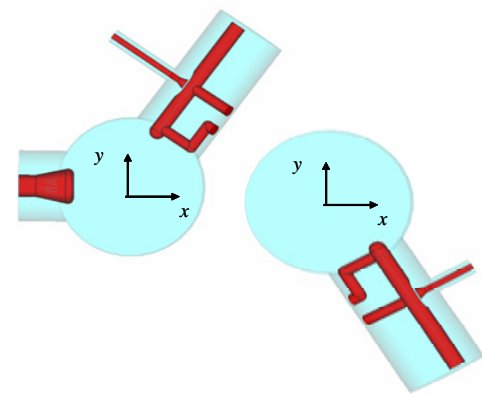
$$\mathbf{k}_{\perp}(x, y) = \begin{pmatrix} -0.021 \\ -0.019 \end{pmatrix} + \begin{pmatrix} 4.3 & 0.07 \\ 0.03 & -0.9 \end{pmatrix} \begin{pmatrix} x[\text{m}] \\ y[\text{m}] \end{pmatrix} \begin{bmatrix} \text{kV} \\ \text{nC} \end{bmatrix}$$

$\|\mathbf{k}_{\perp}\|$



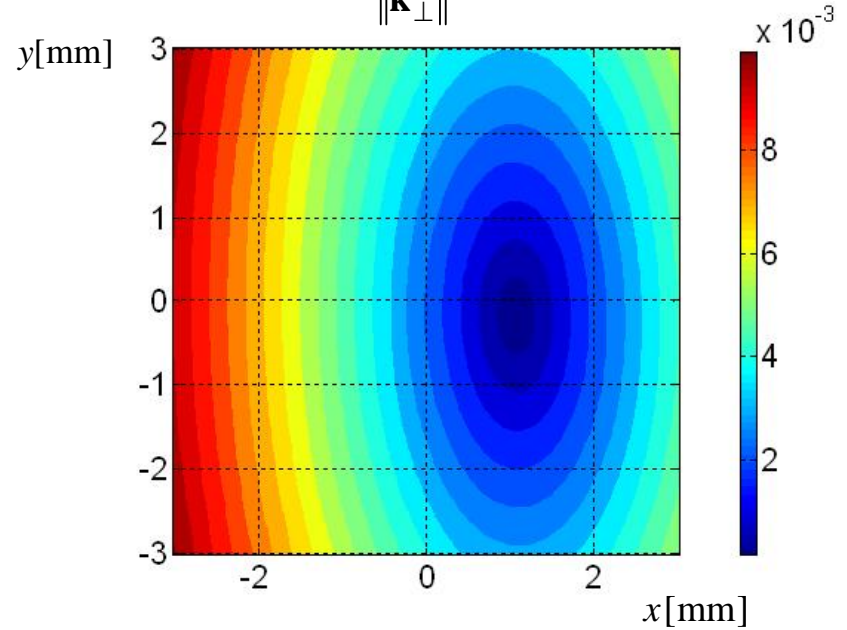
$$\|\mathbf{k}_{\perp}\|_{\min} = 5e-5 \frac{\text{kV}}{\text{nC}}$$

$$\mathbf{r}_c = \begin{pmatrix} 5.3 \\ -21.3 \end{pmatrix} \text{mm}$$



$$\mathbf{k}_{\perp}(x, y) = \begin{pmatrix} -0.0025 \\ -0.0002 \end{pmatrix} + \begin{pmatrix} 2.33 & 0.04 \\ -0.02 & 1.1 \end{pmatrix} \begin{pmatrix} x[\text{m}] \\ y[\text{m}] \end{pmatrix} \begin{bmatrix} \text{kV} \\ \text{nC} \end{bmatrix}$$

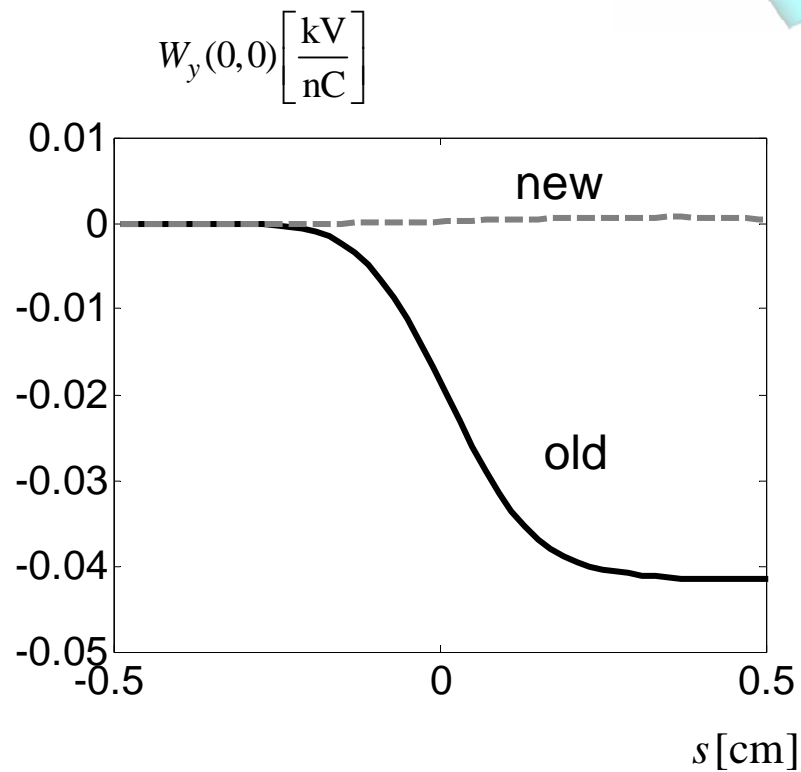
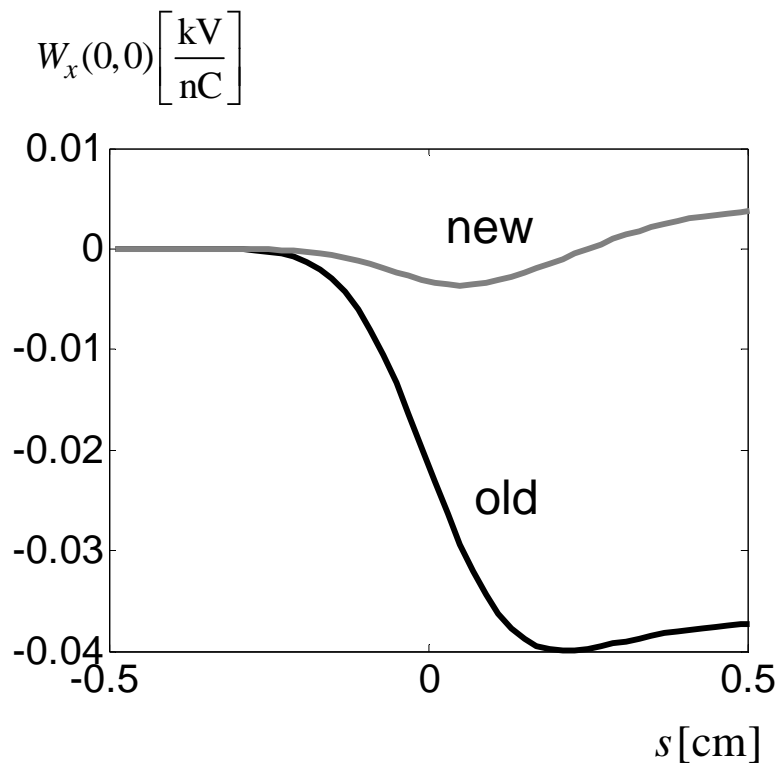
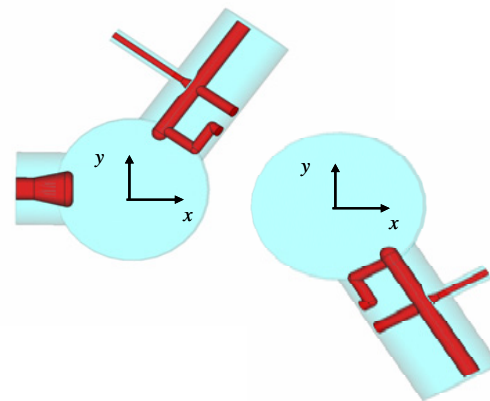
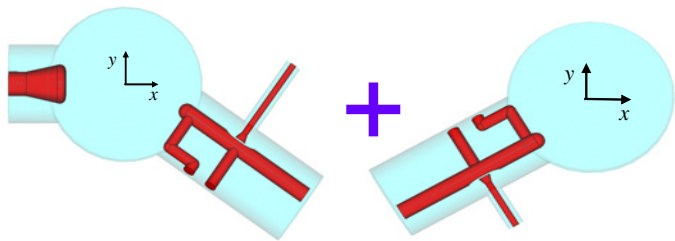
$\|\mathbf{k}_{\perp}\|$

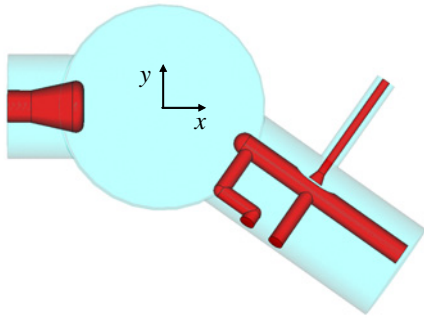


$$\|\mathbf{k}_{\perp}\|_{\min} = 8e-5 \frac{\text{kV}}{\text{nC}}$$

$$\mathbf{r}_c = \begin{pmatrix} 1.1 \\ -0.2 \end{pmatrix} \text{mm}$$

# Wake kick for the new orientation





downstream coupler,  
new,  $z_{\text{pen}}/\text{mm}=6$ , forward  
 $x/\text{mm} = \dots$   $y/\text{mm} = \dots$

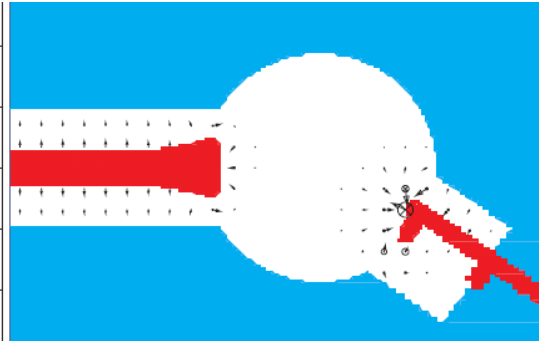
## RF kick

$$V_x(s) = \text{Re}(V_x \cdot V_z \cdot e^{-iks})$$

$$k_{\perp}^{0,rms} \approx \text{Im}(V_x \cdot V_z) \cdot k \cdot \sigma$$

$$V_z = 15\text{MV}$$

$$k = 2\pi \frac{1.3\text{GHz}}{c}$$



$$10^3 \cdot x_{\text{off}} = 0 \quad 10^3 \cdot y_{\text{off}} = 2$$

$$\frac{V_x}{10^{-6}} = -18.925 + 51.83i$$

$$\frac{V_y}{10^{-6}} = 39.418 + 8.879i$$

$$10^3 \cdot x_{\text{off}} = -2 \quad 10^3 \cdot y_{\text{off}} = 0$$

$$\frac{V_x}{10^{-6}} = -16.597 + 56.049i$$

$$\frac{V_y}{10^{-6}} = 27.217 + 4.356i$$

$$10^3 \cdot x_{\text{off}} = 0 \quad 10^3 \cdot y_{\text{off}} = 0$$

$$\frac{V_x}{10^{-6}} = -25.01 + 51.529i$$

$$\frac{V_y}{10^{-6}} = 32.166 + 5.242i$$

$$10^3 \cdot x_{\text{off}} = 2 \quad 10^3 \cdot y_{\text{off}} = 0$$

$$\frac{V_x}{10^{-6}} = -32.552 + 47.906i$$

$$\frac{V_y}{10^{-6}} = 38.866 + 6.337i$$

M. Dohlus, Field  
asymmetries & kicks, 2004.  
[http://www.desy.de/~dohlus/2004/2004.09.holgers\\_seminar/asym&kick\\_sep2004.pdf](http://www.desy.de/~dohlus/2004/2004.09.holgers_seminar/asym&kick_sep2004.pdf)

$$10^3 \cdot x_{\text{off}} = 0 \quad 10^3 \cdot y_{\text{off}} = -2$$

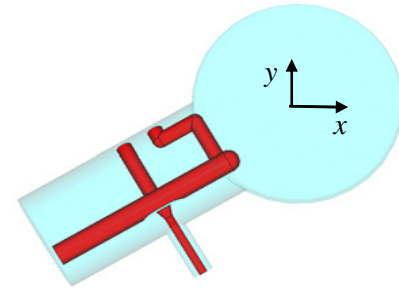
$$\frac{V_x}{10^{-6}} = -30.627 + 50.36i$$

$$\frac{V_y}{10^{-6}} = 24.394 + 1.725i$$

# RF kick

upstream coupler

x/mm = ... y/mm = ...



M. Dohlus, Field  
asymmetries & kicks, 2004.  
[http://www.desy.de/~dohlus/2004/2004.09.holgers\\_seminar/asym&kick\\_sep2004.pdf](http://www.desy.de/~dohlus/2004/2004.09.holgers_seminar/asym&kick_sep2004.pdf)

$$10^3 \cdot x_{\text{off}} = 0 \quad 10^3 \cdot y_{\text{off}} = 2$$
$$\frac{V_x}{10^{-6}} = -50.479 + 6.799i$$
$$\frac{V_y}{10^{-6}} = -42.924 - 2.275i$$

$$10^3 \cdot x_{\text{off}} = -2 \quad 10^3 \cdot y_{\text{off}} = 0$$
$$\frac{V_x}{10^{-6}} = -59.102 + 8.202i$$
$$\frac{V_y}{10^{-6}} = -48.701 - 3.873i$$

$$10^3 \cdot x_{\text{off}} = 0 \quad 10^3 \cdot y_{\text{off}} = 0$$
$$\frac{V_x}{10^{-6}} = -57.112 + 6.649i$$
$$\frac{V_y}{10^{-6}} = -41.413 - 3.469i$$

$$10^3 \cdot x_{\text{off}} = 2 \quad 10^3 \cdot y_{\text{off}} = 0$$
$$\frac{V_x}{10^{-6}} = -54.754 + 5.382i$$
$$\frac{V_y}{10^{-6}} = -35.112 - 3.051i$$

$$10^3 \cdot x_{\text{off}} = 0 \quad 10^3 \cdot y_{\text{off}} = -2$$
$$\frac{V_x}{10^{-6}} = -64.117 + 6.215i$$
$$\frac{V_y}{10^{-6}} = -38.919 - 4.676i$$

# TESLA Cavity in Cryomodule

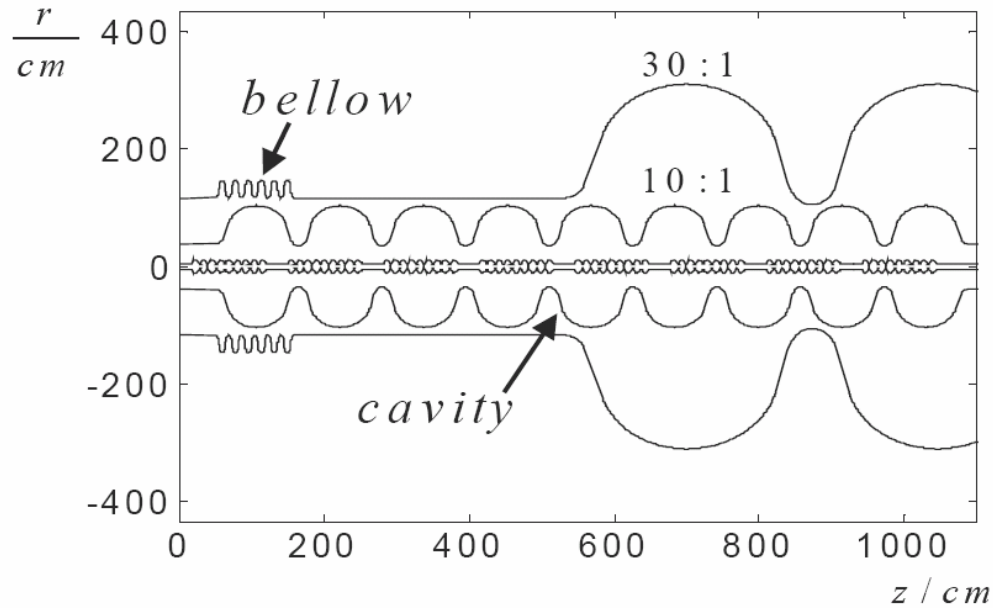


Fig1. Geometry of the TESLA cryomodule.

The TESLA linac consists of a long chain of cryomodules. The cryomodule of total length 12 m contains 8 cavities and 9 bellows as shown in Fig.1. The iris radius is 35 mm and beam tubes radius is 39 mm.

$$w_{\perp}(s) = 10^3 \left( 1 - \left( 1 + \sqrt{\frac{s}{s_1}} \right) \exp \left( -\sqrt{\frac{s}{s_1}} \right) \right) \left[ \frac{V}{pC \cdot m \cdot module} \right] \quad \text{where } s_0 = 1.74 \cdot 10^{-3} \text{ and } s_1 = 0.92 \cdot 10^{-3}$$

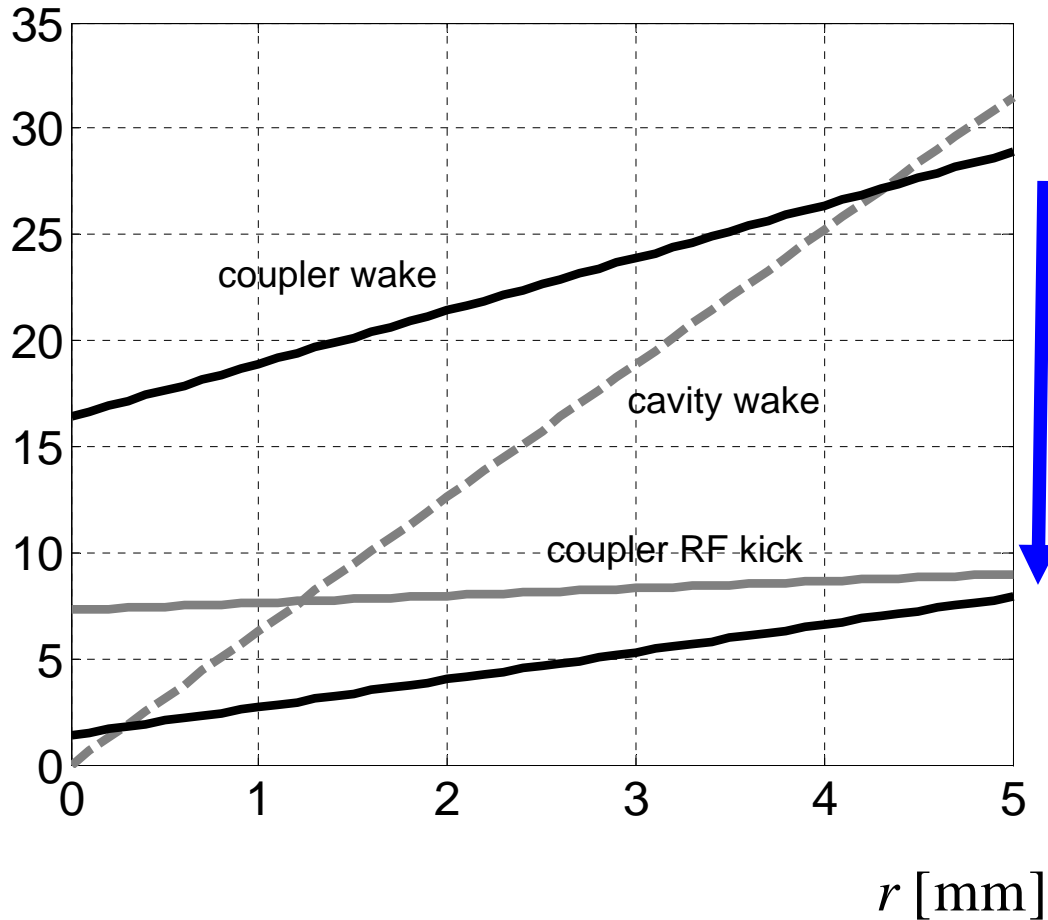
Zagorodnov I., Weiland T., *The Short-Range Transverse Wakefields in TESLA Accelerating Structure*// Proceedings of PAC 2003 Conference, USA, **2003**.

# Head-Tail Kick (ILC)

$\sigma = 300 \mu\text{m}$

$$k_{\perp}^{rms} \approx k_{\perp}^{0,rms} + k_{\perp}^{1,rms} r$$

$$k_{\perp}^{rms} \left[ \frac{V}{nC * \text{cavity}} \right]$$



## Head-Tail Kick (ILC)

$$k_{\perp}^{rms} \approx k_{\perp}^{0,rms} + k_{\perp}^{1,rms} r$$

$$k_{\perp}^{0,rms} \left[ \frac{V}{nC * cavity} \right]$$

| RMS bunch length, $\mu\text{m}$ | Coupler wake            | Coupler RF field | Cavity tilt by<br>1 mrad<br>(on crest / 10 grad) |
|---------------------------------|-------------------------|------------------|--|
| 300                             | Design= 16.4<br>New=1.4 | 7.3              | 0.35/10.7  |

$$k_{\perp}^{1,rms} \left[ \frac{V}{nC * mm * cavity} \right]$$

| RMS bunch length, $\mu\text{m}$ | Coupler wake            | Coupler RF field | Cavity wake |
|---------------------------------|-------------------------|------------------|-------------|
| 300                             | Design= 2.5<br>New= 1.3 | 0.34             | 6.3         |

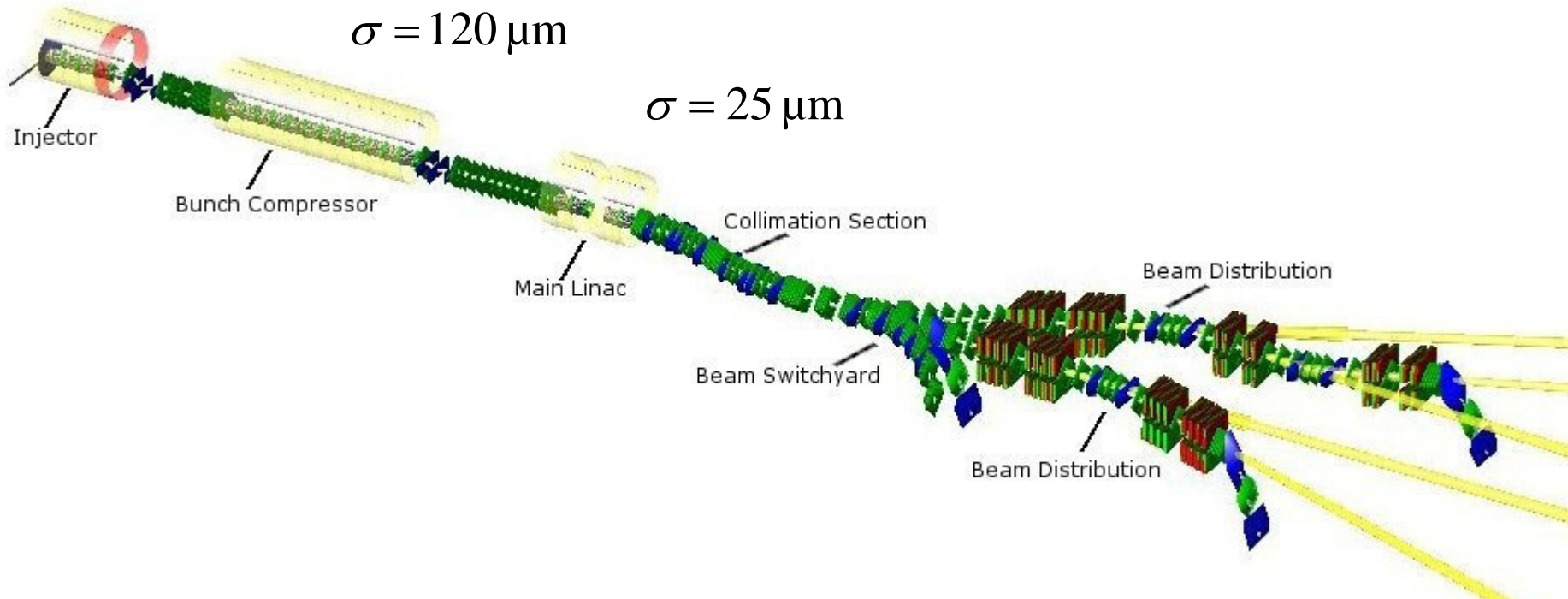


# European XFEL Project

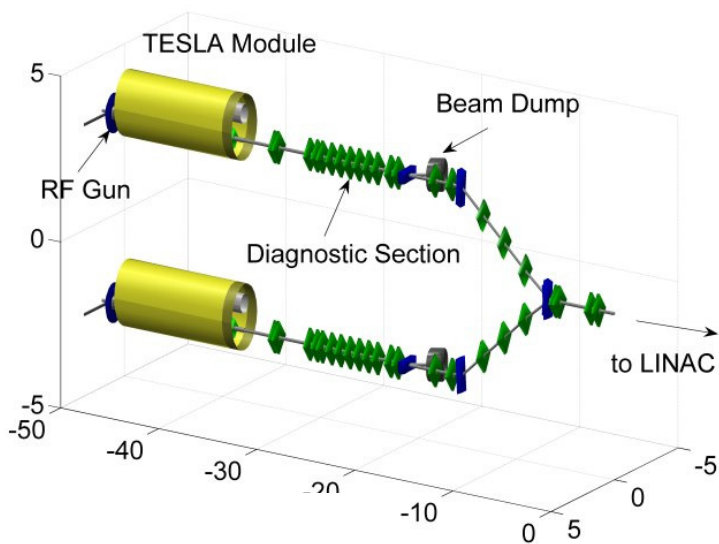
$\sigma = 2400 \mu\text{m}$

$\sigma = 120 \mu\text{m}$

$\sigma = 25 \mu\text{m}$

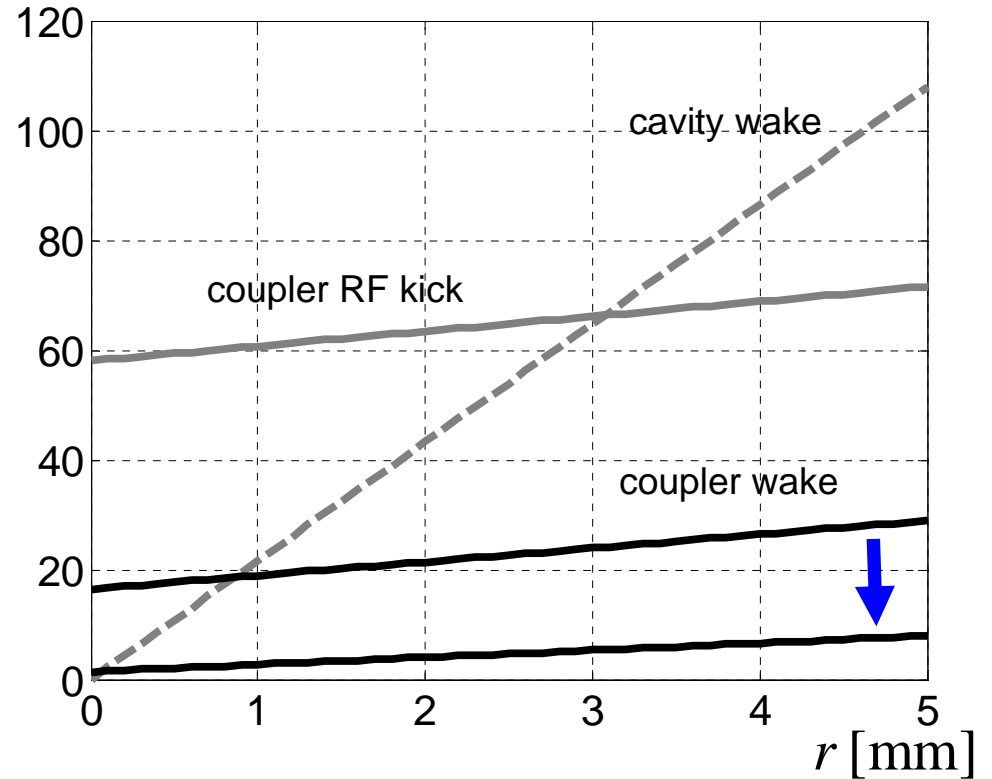


<http://www.desy.de/xfel-beam/index.html>



# Injector

$$k_{\perp}^{rms} \left[ \frac{V}{nC * cavity} \right]$$

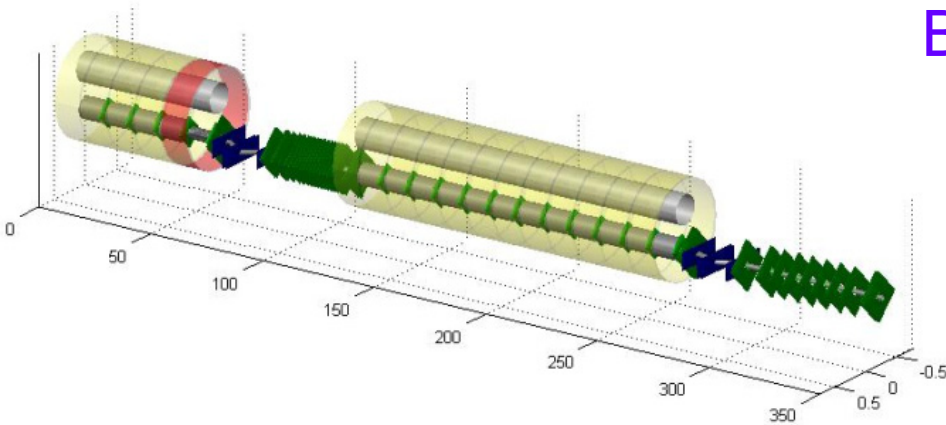


$\sigma = 2400 \mu\text{m}$

5\*8=40 couplers

Coupler RF kick is the most important. It can be reduced by alternative direction orientation of couplers.

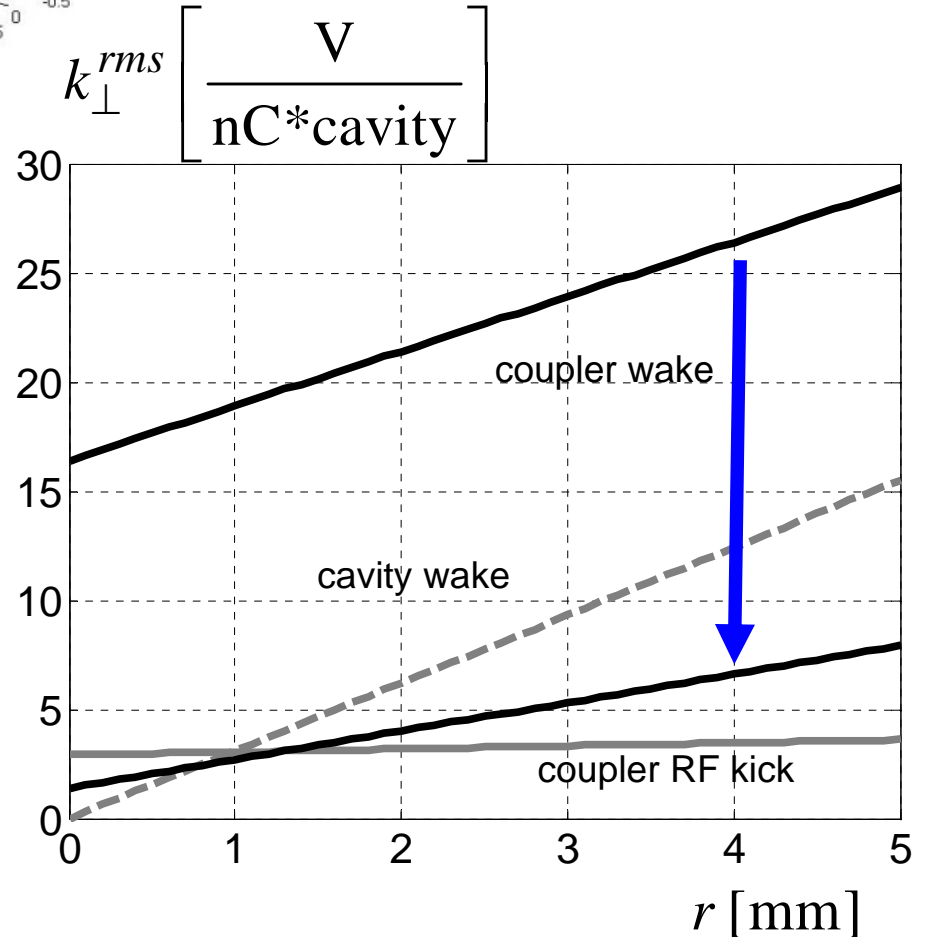
# Bunch Compressor



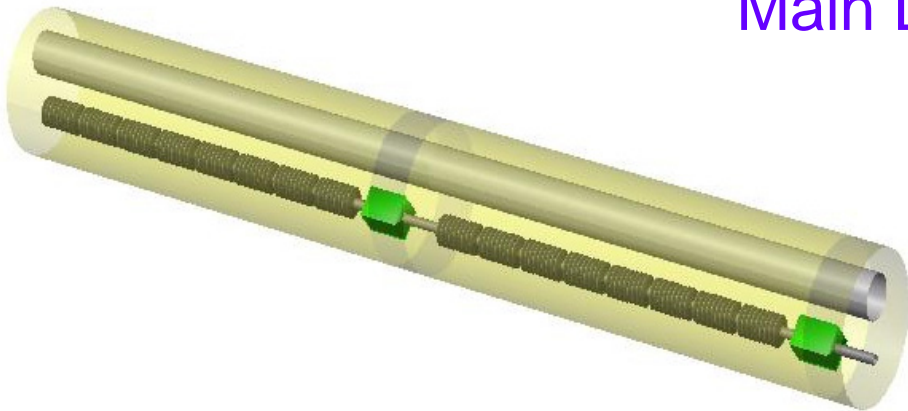
$$\sigma = 120 \mu\text{m}$$

12\*8=96 couplers

Coupler wake is the most important. It can be reduced with the new orientation of HOM couplers.



# Main Linac

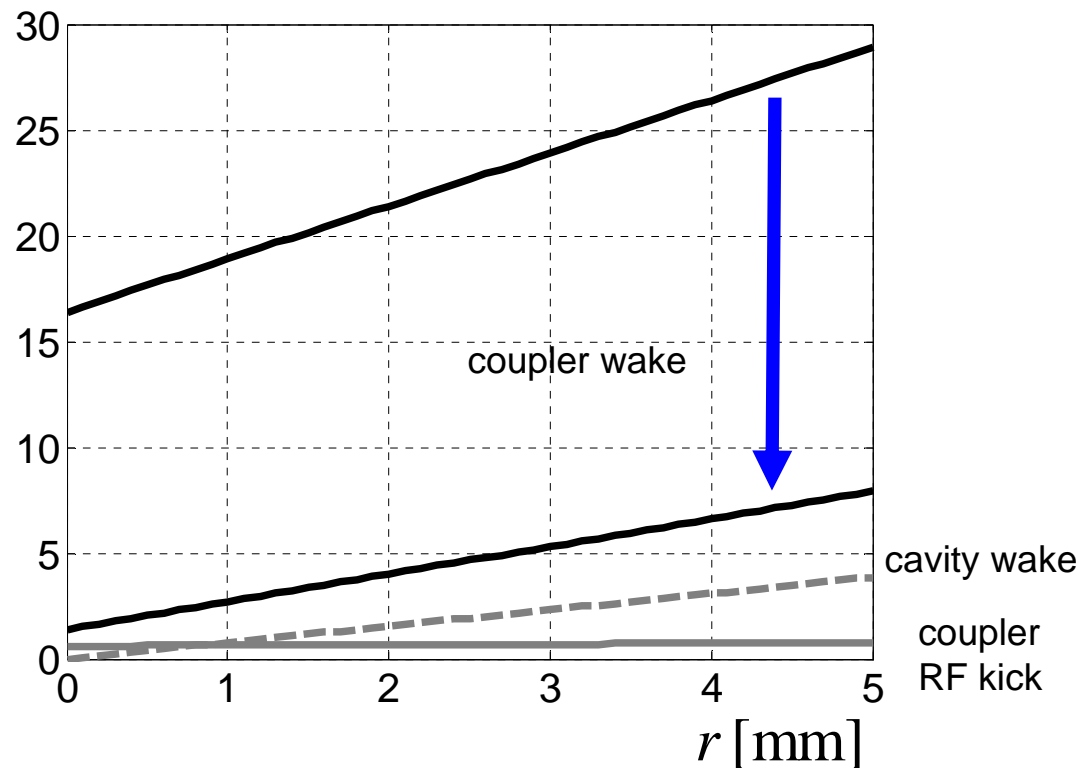


$$\sigma = 25 \mu\text{m}$$

100\*8=800 couplers

Coupler wake is the most important. It can be reduced with the new orientation of HOM couplers.

$$k_{\perp}^{rms} \left[ \frac{V}{nC * \text{cavity}} \right]$$

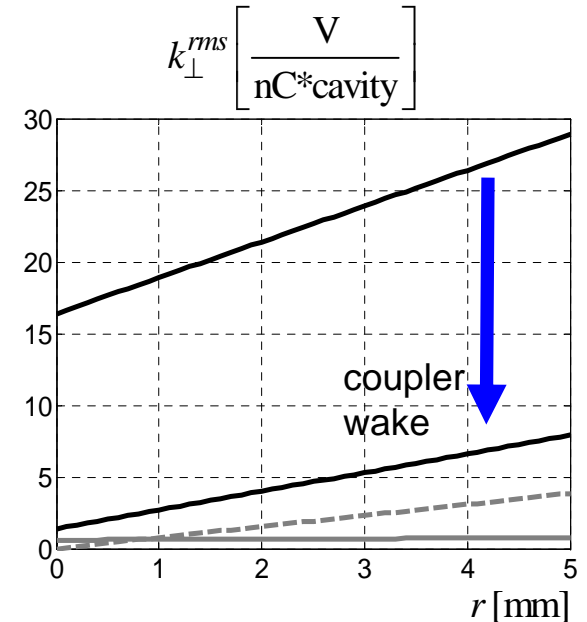
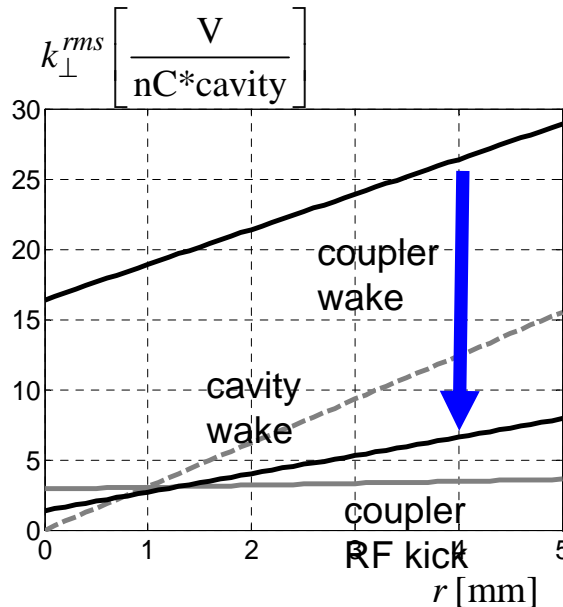
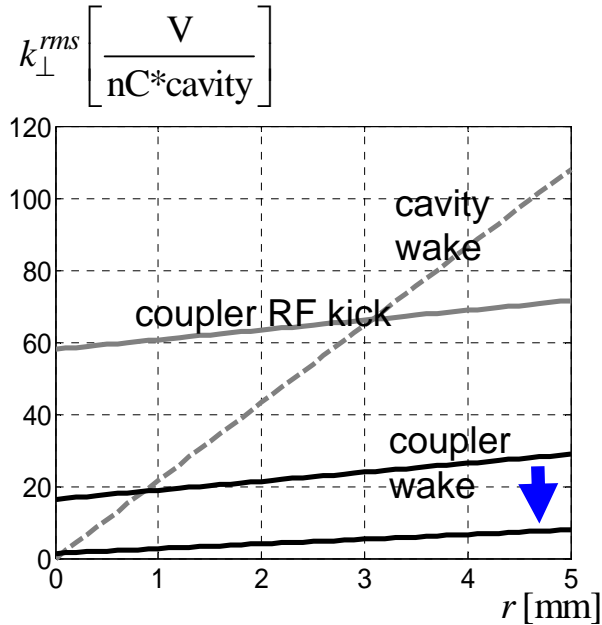


# Effect of new HOM couplers orientation

$\sigma = 2400 \mu\text{m}$

$\sigma = 120 \mu\text{m}$

$\sigma = 25 \mu\text{m}$



## Injector

Coupler RF kick is the most important. It can be reduced by alternative direction orientation of couplers.

## Bunch Compressor

Coupler wake kick is the most important. It can be reduced with the new orientation of HOM couplers.

## Main Linac

## Head-Tail Kick (rms kick)

$$k_{\perp}^{rms} \approx k_{\perp}^{0,rms} + k_{\perp}^{1,rms} r$$

$$k_{\perp}^{0,rms} \left[ \frac{V}{nC * cavity} \right]$$

| RMS bunch length $\sigma$ , $\mu\text{m}$ | Coupler wake, $O(1)$    | Coupler RF field, $O(\sigma)$ | Cavity tilt by 1 mrad (on crest / 10 grad) | Cavity wake |
|---|-------------------------|-------------------------------|--|-------------|
| 2400                                      | Design= 16.4<br>New=1.4 | 58                            | 23 / 88                                    | 0           |
| 120                                       |                         | 2.9                           | 0.06 / 4                                   |             |
| 25  |                         | 0.6                           | 0.002 / 0.9                                |             |

## Head-Tail Kick (rms kick)

$$k_{\perp}^{rms} \approx k_{\perp}^{0,rms} + k_{\perp}^{1,rms} r$$

$$k_{\perp}^{1,rms} \left[ \frac{V}{nC * mm * cavity} \right]$$

| RMS bunch length,<br>$\mu\text{m}$ | Coupler wake,<br>$O(1)$ | Coupler RF field,<br>$O(\sigma)$ | Cavity wake,<br>$O(\sigma)$ |
|------------------------------------|-------------------------|----------------------------------|-----------------------------|
| 2400                               | Design= 2.5<br>New= 1.3 | 2.7                              | 21.6                        |
| 120                                |                         | 0.14                             | 3.1                         |
| 25                                 |                         | 0.03                             | 0.77                        |

## Head-Tail Kick (rms kick)

1. Transverse Coupler Wake is capacitive (integral from bunch shape)

$$\mathbf{k}_{\perp} \approx \mathbf{k}_{\perp}^0 + \mathbf{k}_{\perp}^1 \mathbf{r} \quad k_{\perp}^{0,rms} \approx \frac{1}{\sqrt{3}} \|\mathbf{k}_{\perp}^0\| \quad k_{\perp}^{1,rms} \approx \frac{1}{\sqrt{3}} \|\mathbf{k}_{\perp}^1\|$$

2. RF Coupler Kick (on crest)

$$V_x(s) = \text{Re}(V_x \cdot V_z \cdot e^{-iks}) \quad V_z = 15\text{MV} \quad k = 2\pi \frac{1.3\text{GHz}}{c}$$
$$k_{\perp}^{0,rms} \approx \text{Im}(V_x \cdot V_z) \cdot k \cdot \sigma$$

3. Cavity tilt by angle  $\alpha$

$$V(s) = \text{Re}(0.5\alpha V_z \cdot e^{-i(ks-\varphi_0)})$$
$$k_{\perp}^{0,rms} \approx \left( \int [\text{Re}V(s) - \langle \text{Re}V(s) \rangle]^2 \lambda(s) ds \right)^{1/2}$$



# Conclusion

- The coupler **RF** kick is a main effect in the injector. It can be compensated by an alternative direction orientation of couplers.
- The coupler **wake** kick is a main effect after the 1st bunch compressor in XFEL project and for ILC bunch length of 300  $\mu\text{m}$ . Rotation of the HOM couplers by 90 degree allows to reduce the kick by factor 12.
- It is possible that the wake is overestimated. The cavity irises have smaller radius than the pipe. It could make the coupler kick weaker. The full structure modeling is desired.