

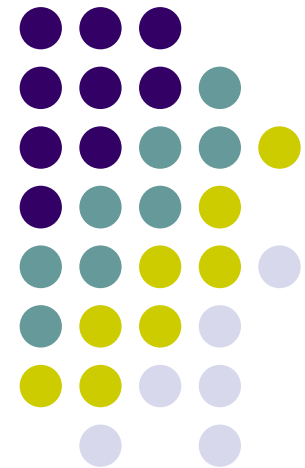
# Detector Integration of GLD and GLDc

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Nov. 16, 2007

Y. Sugimoto

KEK

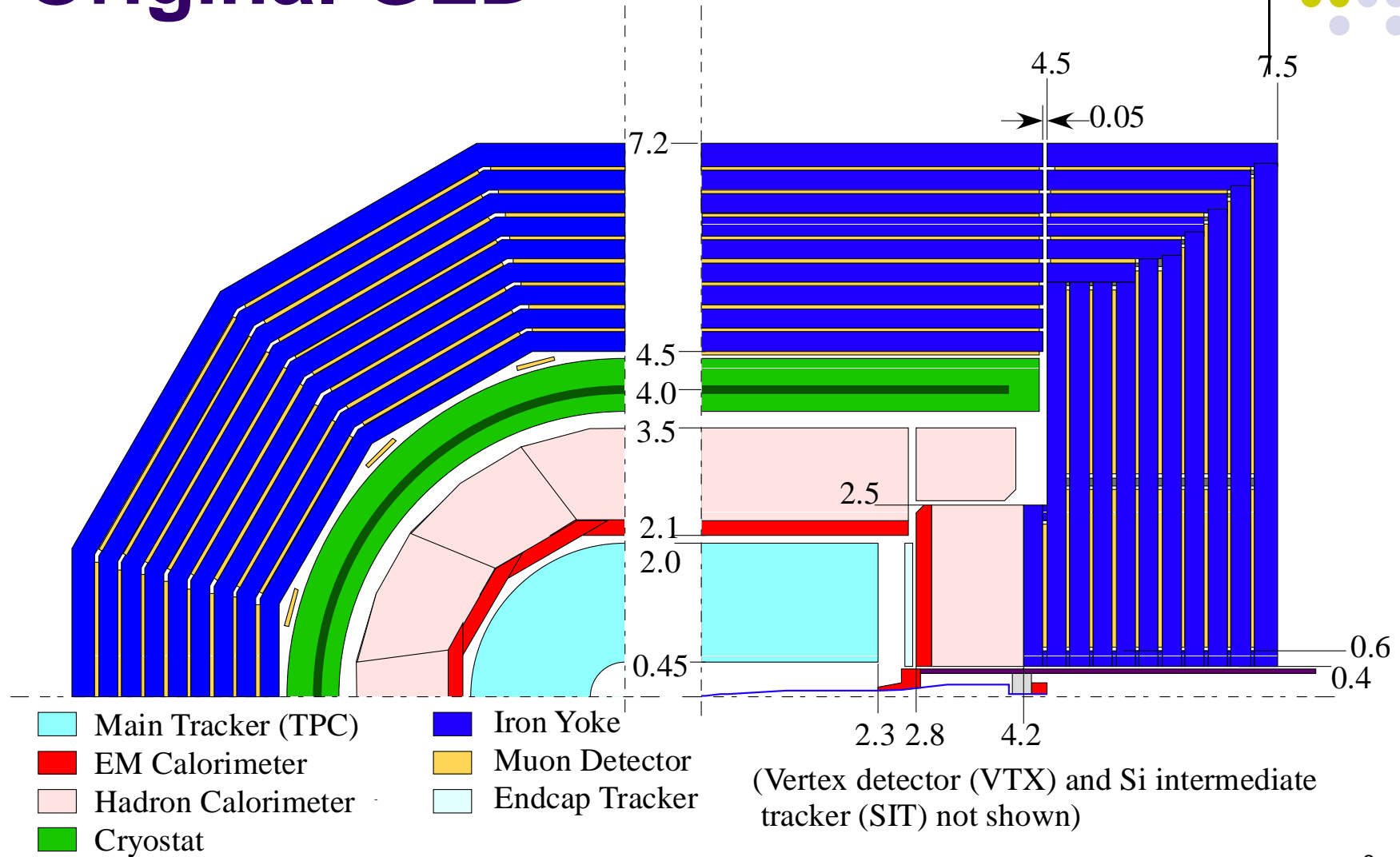
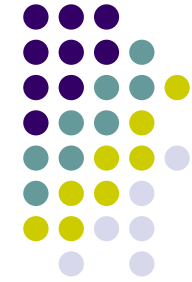


# Compact GLD Option

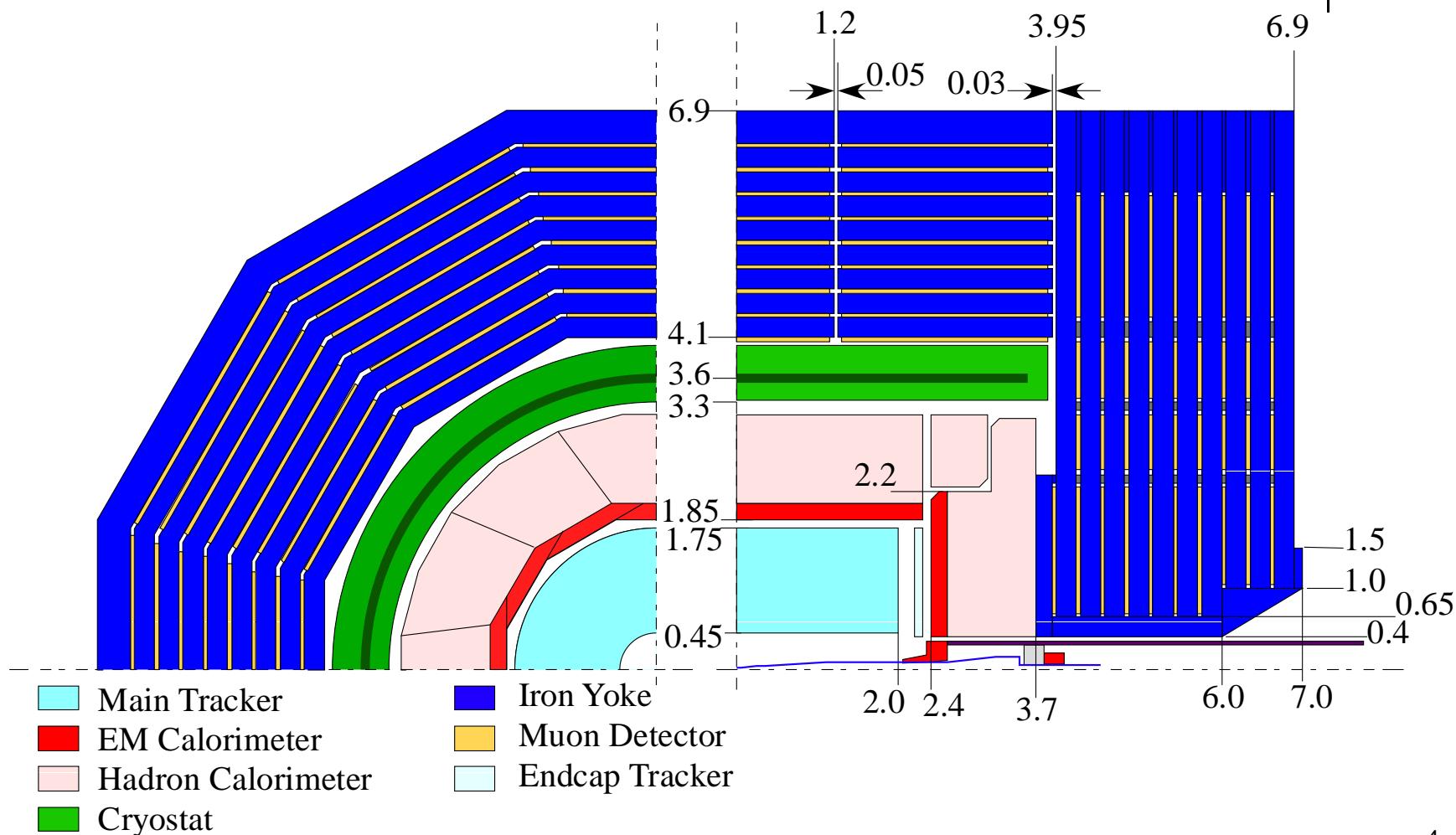


- Motivation
  - GLD and LDC will write a common Lol
  - The detector design should have common parameters
  - Common parameters should be determined based on detailed simulation study, but it will take a time  $\sim 0.5y(?)$
  - As a working assumption for the moment, a modified design of GLD with the central values for B and  $R_{CAL}$  between original GLD and LDC is made
    - $B = (3+4)/2 = 3.5$  T
    - $R_{CAL} = (2.1+1.6)/2 = 1.85$  m

# Original GLD



# Compact GLD - GLDc





# Parameters (1)

			GLD	GLDc
Iron Yoke	Barrel	Rout	7.2 m	6.9 m
		Rin	4.5 m	4.1 m
		Weight	6090 t	5080 t
	E.C.	Zin	4.2/4.5 m	3.7/3.95 m
		Zout	7.5 m	6.9 m
		Weight	3260 t / side	3050 t / side
Solenoid	B		3 T	3.5 T
	R		4 m	3.6 m
	Z		4 m	3.6 m
	Weight		~330 t	~300 t
	E		1.6 GJ	1.7 GJ
Stray field @Z=10m			70 G	120 G

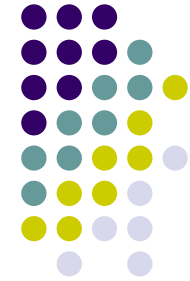


# Parameters (2)

		GLD	GLDc	
TPC	Rin (active region)	0.45 m	0.45 m	
	Rout	2.0 m	1.75 m	
	Zmax	2.3 m	2.0 m	
Barrel CAL	ECAL	Rin	2.1 m	1.85 m
		Rout	2.3 m	2.05 m
		BRin <sup>2</sup>	<b>13.2 Tm<sup>2</sup></b>	<b>12.0 Tm<sup>2</sup></b>
	HCAL	Rout	3.5 m	3.15 m
		Thickness	1.2 m	1.1 m
	Weight		1750 t	1130 t

BRin<sup>2</sup>=10.2 for LDC and 8.1 for SiD

# Parameters (3)



			GLD	GLDc
EC CAL	ECAL	Zmin	2.8 m	2.4 m
		Zmax	3.0 m	2.6 m
	HCAL	Zmax	4.2 m	3.7 m
		Thickness	1.2 m	1.1 m
	Weight		270 t / side	270 t / side
CAL	Total weight		2290 t	1670 t
Detector weight	Barrel yoke + solenoid		6.4 kt	5.4 kt
	Barrel total		8.2 kt	6.5 kt
	Endcap total		3.5 kt/side	3.3 kt/side
	Total weight		<b>15 kt</b>	<b>13 kt</b>



# Assembly

- GLD
  - Barrel part (Yoke+Sol.) > 6000 ton
  - For CMS style assembly (using 2000 ton crane to descend), it should be split into 5 rings and there will be many gaps
    - Large stray field
    - Difficulty in alignment of rings
  - In present design, GLD barrel yoke is split in R- and  $\phi$ -direction into 24 pieces
  - 400-t cranes in the underground exp hall and surface assembly hall
- GLDc
  - Barrel part (Yoke+Sol.) < 6000 ton
  - Pure CMS style assembly can be done by splitting the barrel part into 3 rings and splitting each end cap part into two halves
  - 50~100-t crane underground, 2000-t crane for the shaft, and 80-t crane in the surface assembly hall



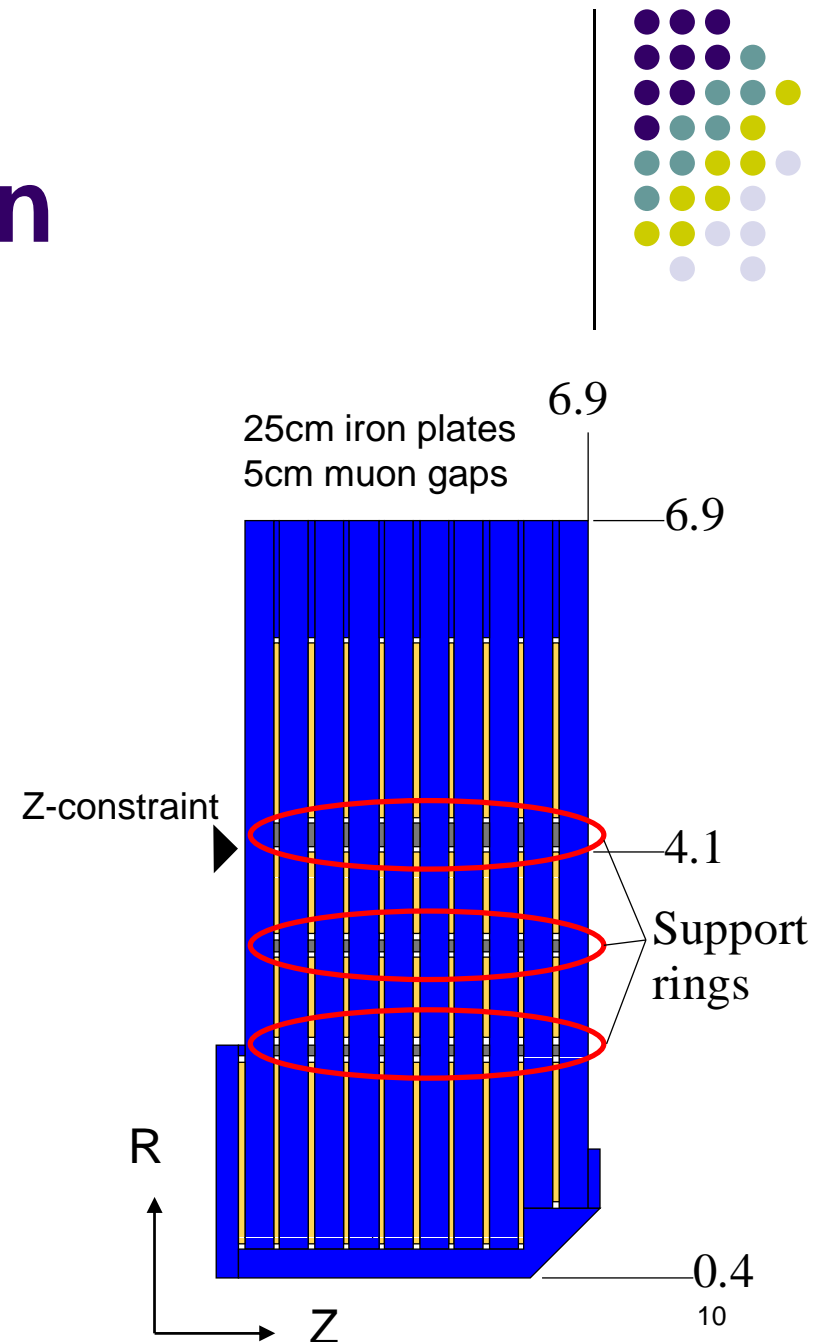
# Design of GLDc Endcap



- GLD/GLDc endcap yoke is vertically split
- Installation and maintenance of Muon detectors are done from the splitting plane ( $X=0$  plane) like Belle detector
- Support rings can be put between iron slabs to increase the rigidity of the endcap yoke
- Usually two halves may be connected tightly and split only for installation and maintenance of sub-detectors
- Endcap calorimeters can be arranged without dead space
- Because hadrons make shower in the endcap iron, small gap of muon detectors does not make inefficiency of muon identification

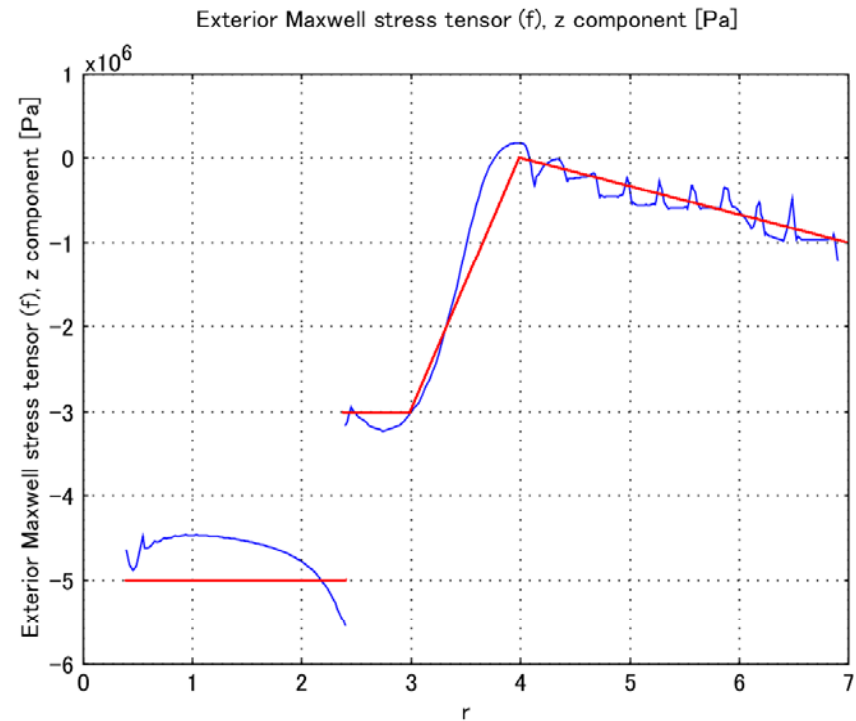
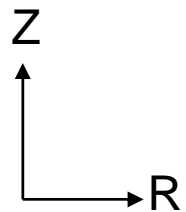
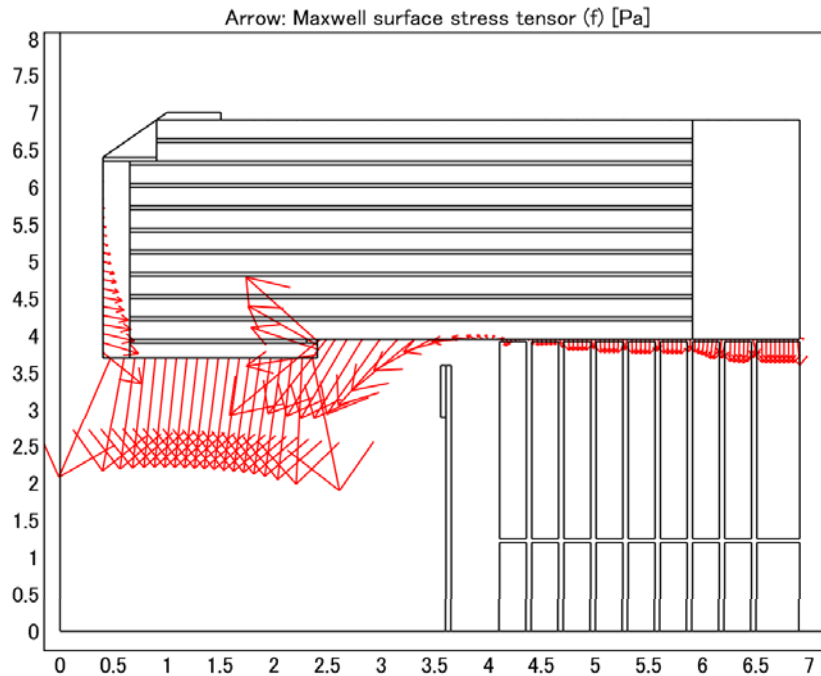
# Endcap Deformation

- Calculation by FEA method
  - Endcap is treated as a whole and surface force is calculated
  - The surface force at the front surface of the endcap is obtained as a function of R, and parameterized by a simple function
  - This simple function is used for the calculation of the deformation
  - Z-constraint only at R=4.1m (Inner radius of barrel yoke)
  - 3D model calculation



# Endcap Deformation

- Magnetic Force





# Endcap Deformation

- Results

	Angle	Support ring	$\Delta Z$		
			r=0.4 m	r=6.9 m	
3D	180	No	-21 mm	+11 mm	$\phi=0$
			-23 mm	-13 mm	$\phi=90$
3D	360	No	-12 mm	-3.9 mm	
3D	180	1 (r=4.1m)	-5.7 mm	-0.6 mm	$\phi=0$
			-5.9 mm	-0.5 mm	$\phi=90$
3D	360	1	-4.6 mm	-0.2 mm	
3D	180	2 (r=2.3, 4.1m)	-2.6 mm	+0.5 mm	$\phi=0$
			-2.7 mm	-0.7 mm	$\phi=90$
3D	360	2	-1.8 mm	-0.4 mm	
3D	180	3 (r=2.3, 3.2, 4.1m)	<b>-1.7 mm</b>	<b>+0.3 mm</b>	<b><math>\phi=0</math></b>
			<b>-1.8 mm</b>	<b>-0.7 mm</b>	<b><math>\phi=90</math></b>
3D	360	3	-1.1 mm	-0.4 mm	
2D	360	No	-90 mm	0 mm - Fix	SiD-like: 23x(10cm Fe + 5cm gap)

3D: 3-dimensional model

2D: Axial symmetric 2-dimensional model

180: Splitting endcap

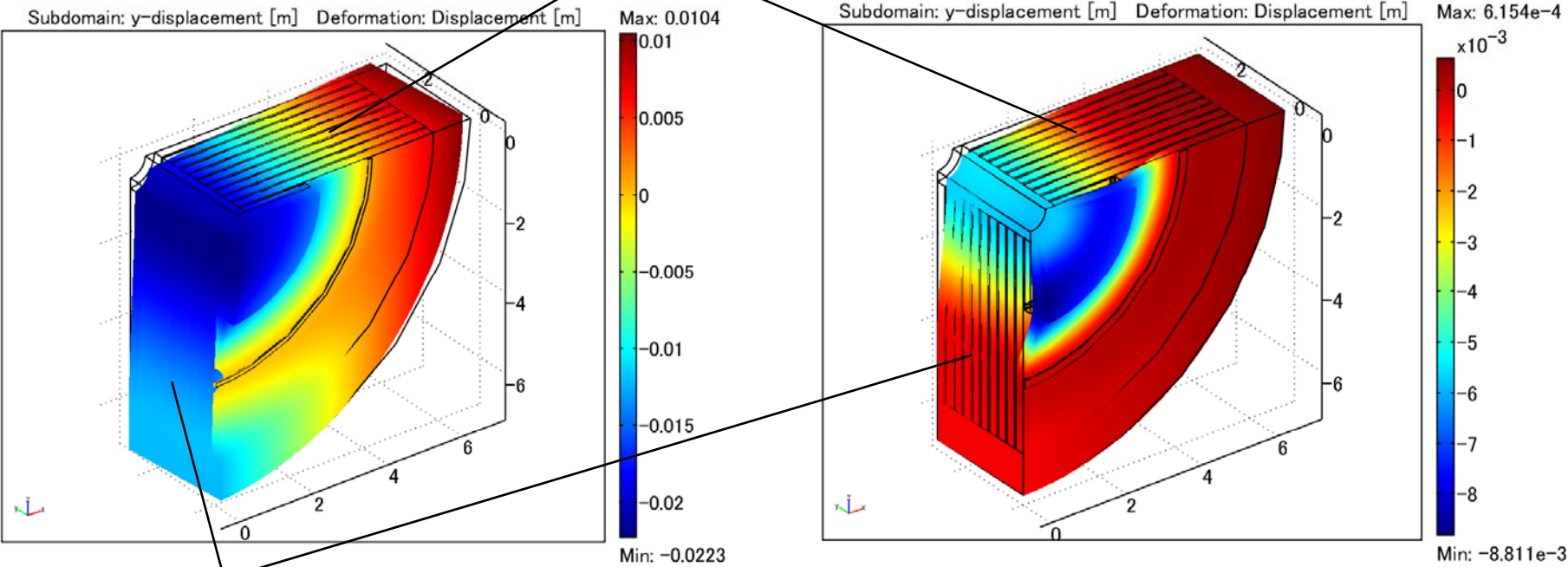
360: Non-splitting endcap

# Endcap Deformation



- No support ring
- One support ring/gap

Symmetry plane



Splitting plane

3D-180 degree model

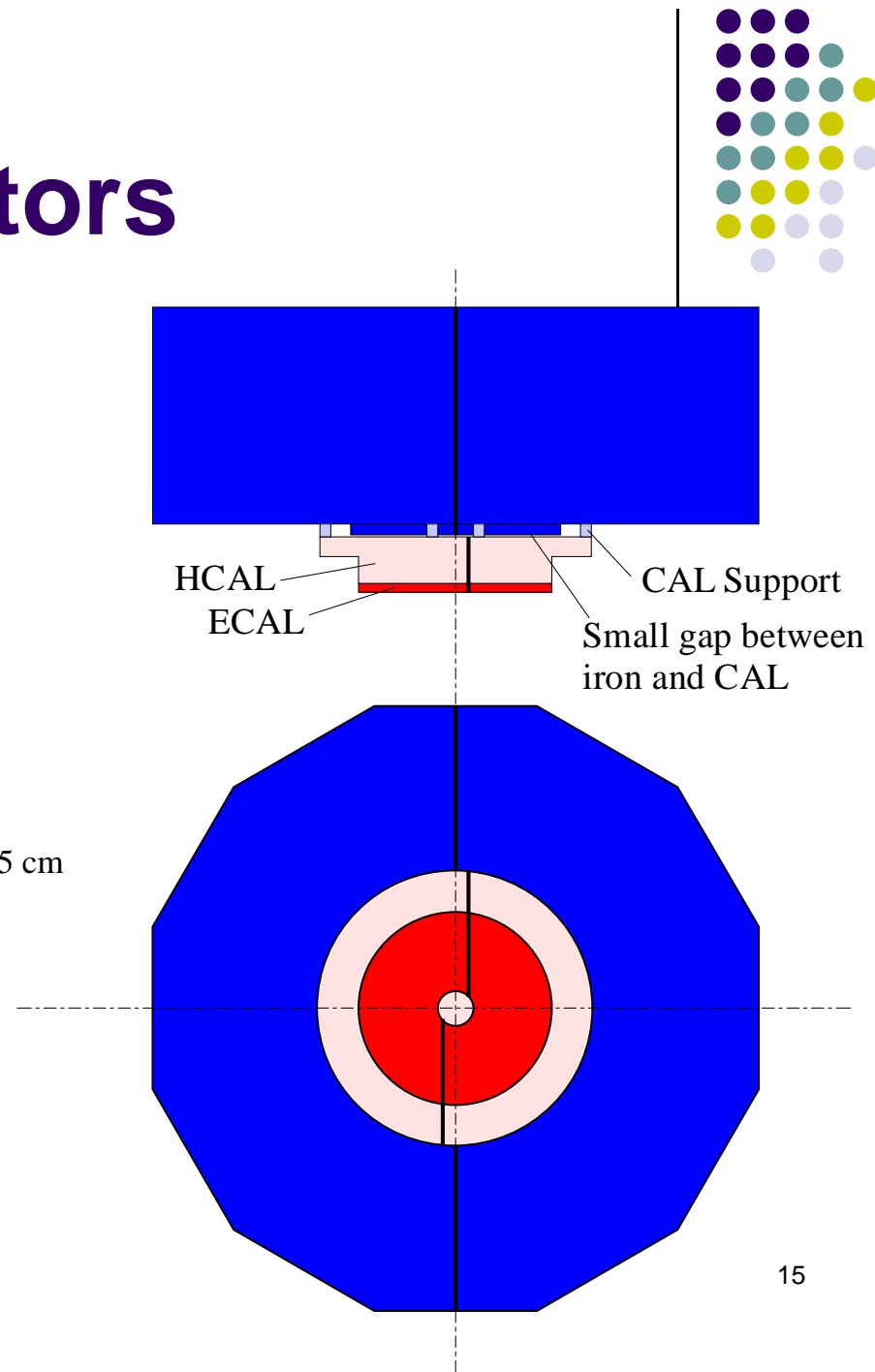
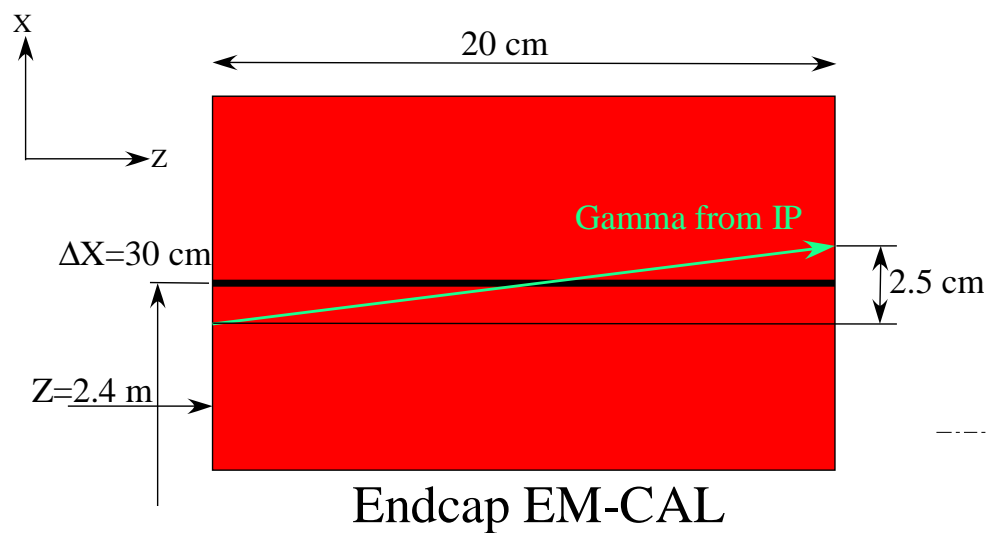
# Gap in sub-detectors



- Endcap calorimeters
  - Split along a plane which does not cross the IP ( $x=30\text{cm}$  plane, for example)
- Endcap muon detector
  - Split along the  $x=0$  plane (same as iron yoke)
  - Tracks entering the muon-detector gap can be detected by TPC and calorimeters
  - If the particle is a pion, it creates hadronic shower in iron yoke, and would be detected by muon detector even if there is small gap

# Gap in sub-detectors

- Endcap CAL



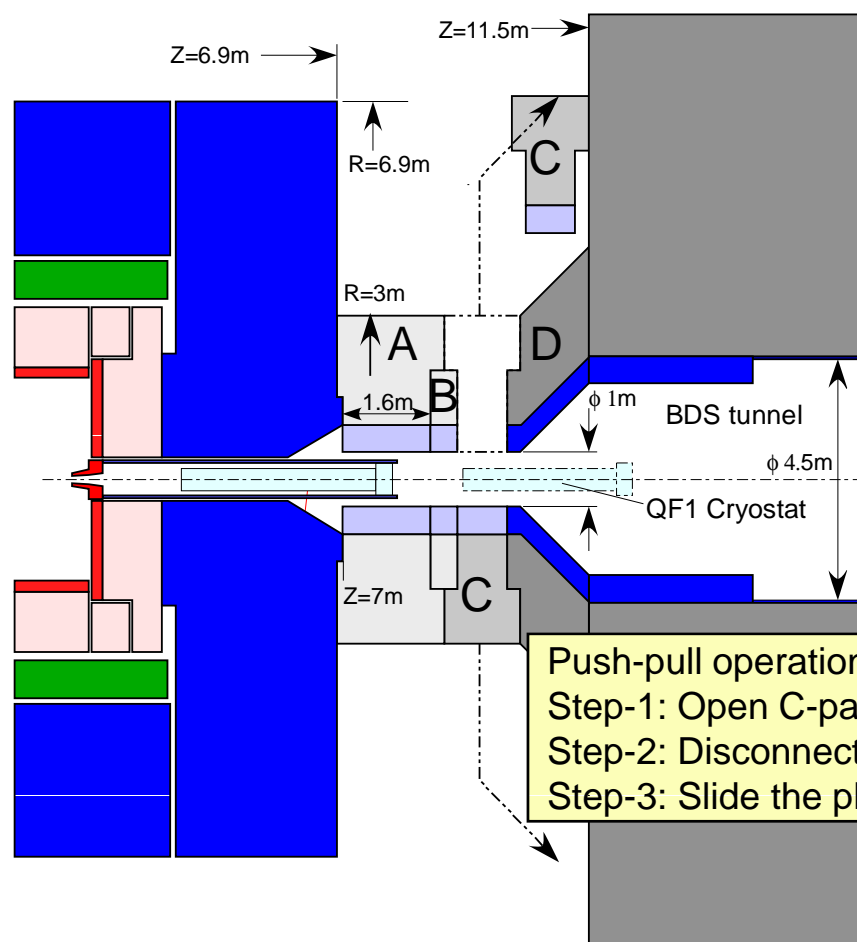




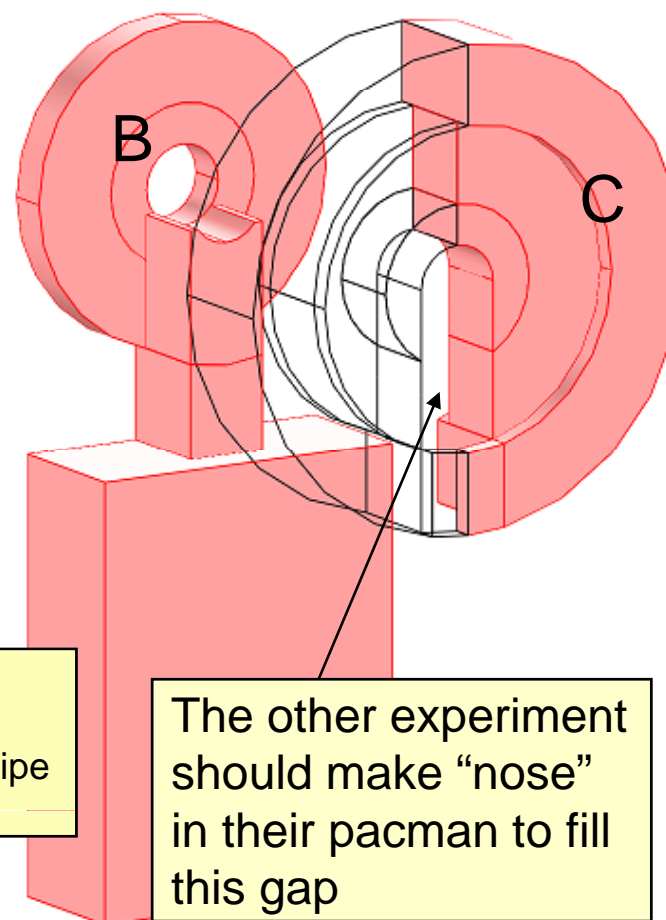


# Pacman design and FD support

- Plan view

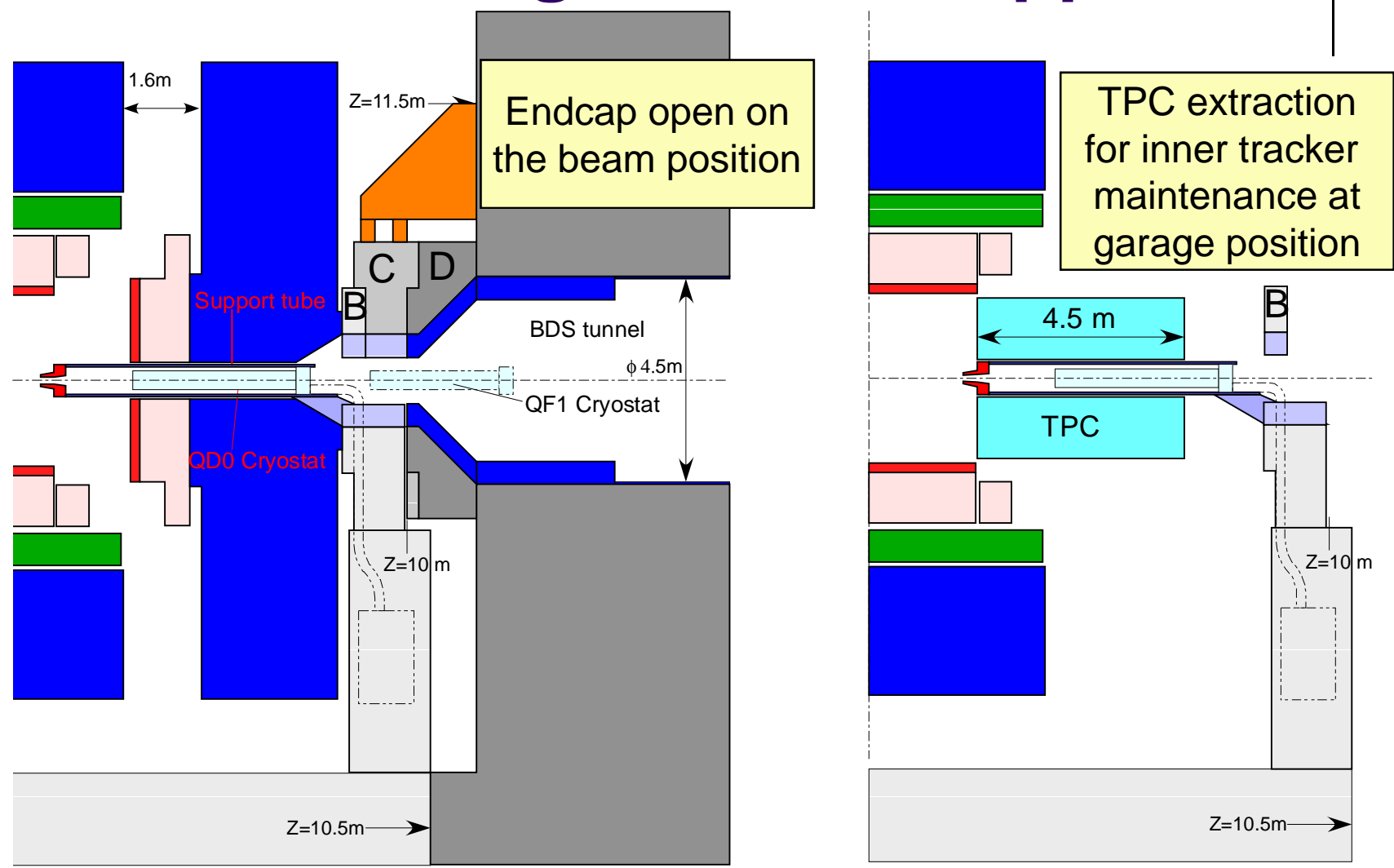


- 3D view



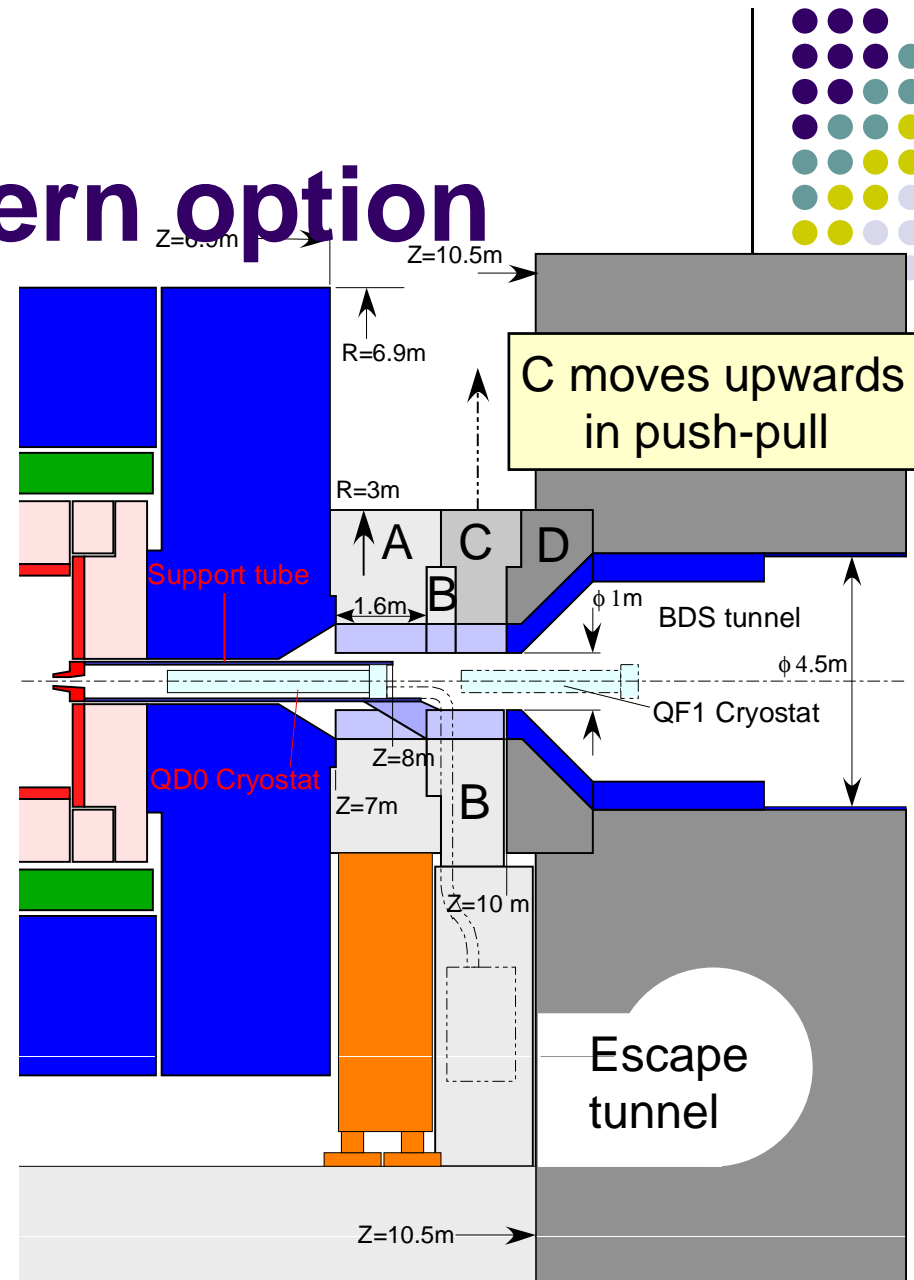


# Pacman design and FD support

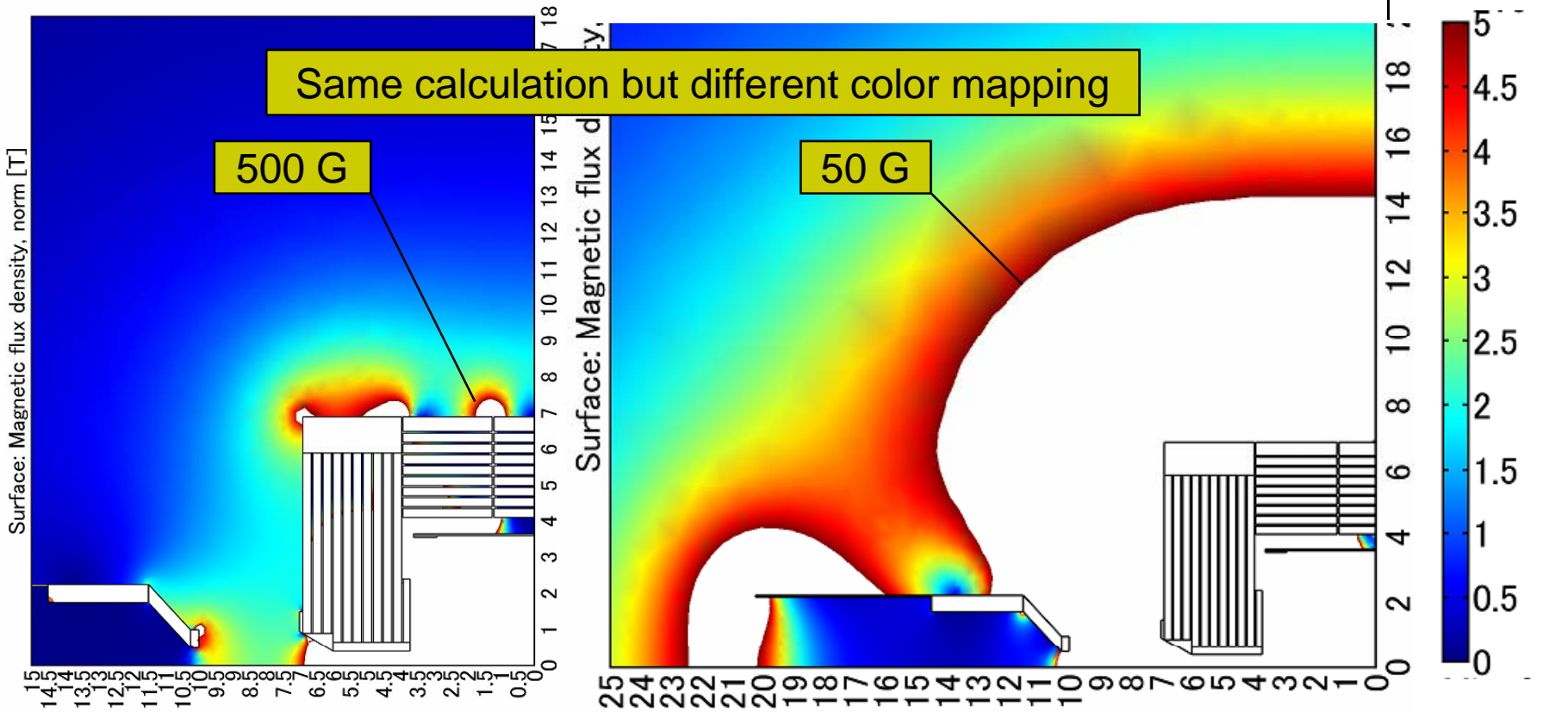


# Still smaller cavern option

- Forget about crane access
- Forget about safety issues
- Design with cavern floor width as small as 21m can be drawn with the support-tube scheme
  - Pacman “C” moves upwards (using a small gantry crane fixed to the wall?) in push-pull operation
  - There is no way for a person to run away from one side of the detector to the other side (escape tunnel ?)



# B field of GLDc



$B_0 = 3.5 \text{ T}$   
 $B(10.5\text{m} < Z < 20\text{m}) < 50 \text{ G}$   
 $B(R > 8\text{m}) < 500 \text{ G}$



# L\* for GLDc

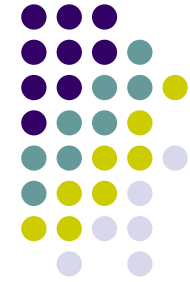
Component	Start	Length
End cap yoke	3.7 m	
BCAL	3.8 m (note-1)	0.2 m
BPM	4.0 m	0.2 m (??)
QD0 cryostat	4.2 m	0.264 m
QD0 coil (L*)	4.464 m	

L\* of ~4.5 m seems adequate

note-1:

By putting BCAL at  $Z > Z_{\text{endcap}}$ , strength of anti-DID can be reduced because R-component of solenoid B-field near the hole of end cap yoke can help guiding low energy pair-background into the beam exit hole

# Difference between GLD and LDC



- CMS style or not (same for GLDc)
- Thickness of iron return yoke
- Diameter of endcap hole
- Beam pipe shape
- Global shape: octagonal or dodecagonal
- $L^* \rightarrow$  Depends on  $Z_{\text{endcap}}$

# Thickness of iron return yoke



- GLD:2.7m, GLDc:2.8m, LDC:2.15m
  - GLD is designed to make stray field at  $Z=10\text{m}$  small enough (70/120 G for GLD/GLDc)
  - LDC design will cause large stray field outside the detector
  - If an electronics hut is built close to the detector, we should define a tolerable level of stray field (less than  $x$  gauss at  $R > R_{det} + y$ )
    - Electronics malfunction (saturation of ferrite core, etc.)
    - Safety (handling of tools, human health, etc.)
- Thickness of iron slabs
  - GLD: 25~30cm / LDC: 10cm
  - Deflection due to magnetic force should be estimated



# Diameter of endcap hole

- GLD:  $R=40\text{cm}$ 
  - Not changed from 2001 (JLC detector)
  - QD0
  - Compensation (Anti) solenoid
  - 10cm thick tungsten support tube
- LDC:  $R=30\text{cm}(?)$ 
  - No compensation solenoid
- Information from BDS group is necessary
  - Do we really need anti-solenoid?
  - What is the design of the anti-solenoid?
  - Do we need extra space around QD0 for alignment mechanism?





# Beam pipe shape

- GLD: Long straight section made of Al
- LDC: Long conical section made of Fe
- ➔ We (FCAL group?) need
  - Estimation of the wall thickness enough to support the pressure
  - Simulation study for lum. measurement
- Beam pipe near IP
  - Pair background simulation based on new machine parameters in RDR at 500 GeV **and 250 GeV** (We may have to ask GDE)



# Global shape

- GLD: Dodecagonal shape in order to reduce unnecessary gaps between TPC and ECAL, between HCAL and solenoid, and between solenoid and iron return yoke
- LDC: Octagonal shape
- For calorimeters, dodecagonal shape is better (see SiD study: M.Breidenbach at ALCPG2007)
- How should we decide for return yoke?



# Other Issues

- Issues not studied yet
  - Power consumption
  - Detector cooling
  - Cable/pipe extraction and handling
  - Detector alignment
  - Luminosity (run period) needed for track-based alignment
  - Support scheme of beam pipe/VTX/SIT
  - Vibration analysis
  - Seismic issues
  - Services for detector solenoid compatible with push-pull
  - Fire safety



# Next step

- Some issues can be studied only after detector parameters are defined, but we should start immediately studying on many issues in order to make a common design of ILD
  - Tolerable stray field of the detector solenoid
  - Structure of return yoke
  - Diameter of endcap hole
  - Pair background study with new machine parameters
  - Global shape of the detector
  - .....
  - .....