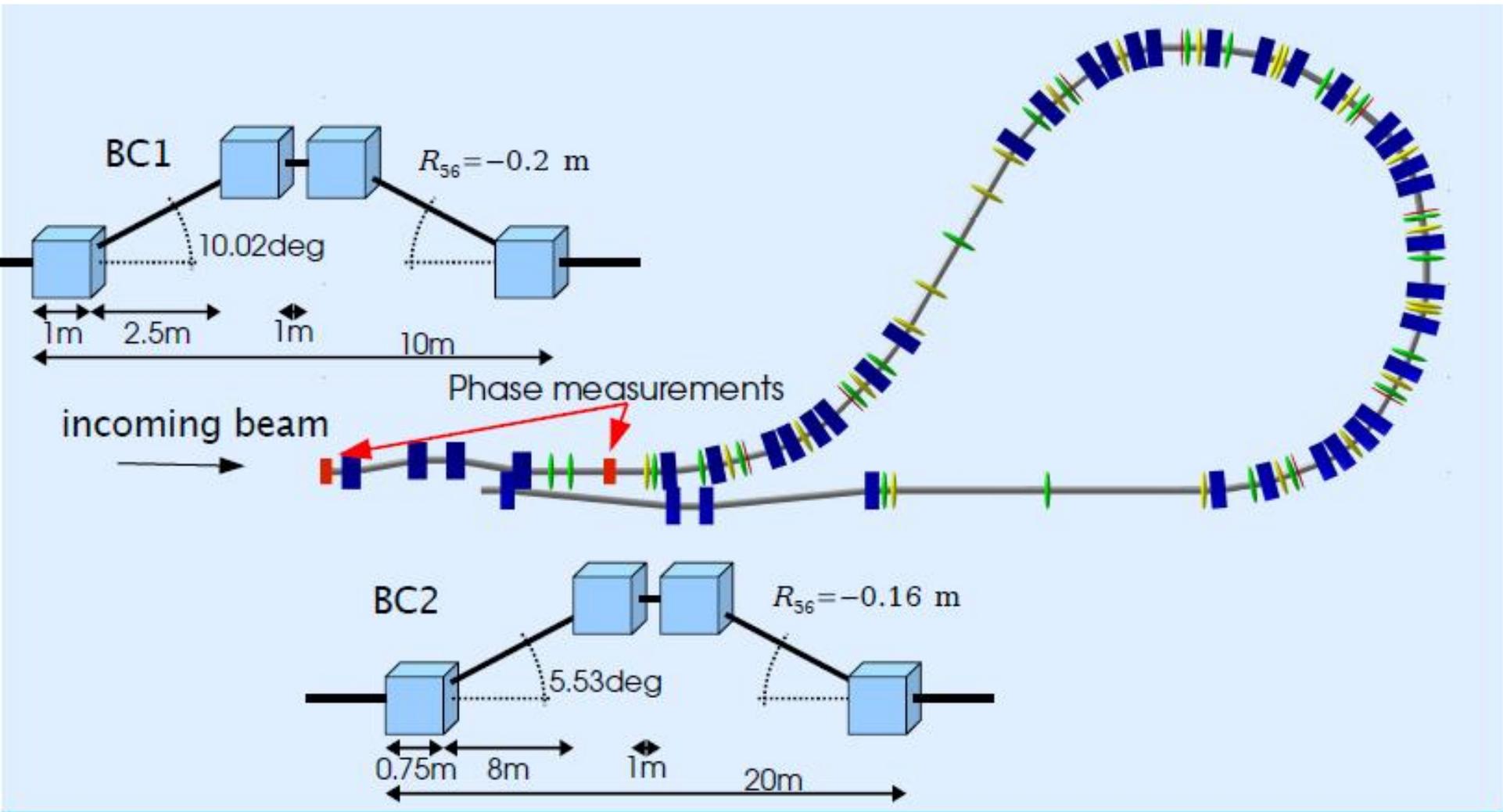


# Amplifiers for CLIC Drive Beam Phase Correction

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for Colin Perry

# Reminder of phase feed-forward concept



Frank Stulle, 13.08.2009

# Requirements & Assumptions - 1

Based on discussion in *August 2009*, we assumed:

## **Speed: 10ns**

- we shared the bandwidth limitation equally between kicker and amplifier
  - kicker active length is limited to 1.1m
- split amplifier bandwidth equally between amplifier modules and combining system
  - each needs a 70MHz bandwidth

## **Kickers: stripline kickers, 20mm clear aperture, 1m long**

- ~120 ohm impedance, balanced
  - each connected to amplifier with pair of coaxial cables
- fit maximum possible total length of kickers for minimum total power required
  - this means 4 at each bend (3, slightly longer, might be better)

## **Deflection: +/-720 $\mu$ rad at each bend**

- divided over 4 kickers = +/-180 $\mu$ rad at each

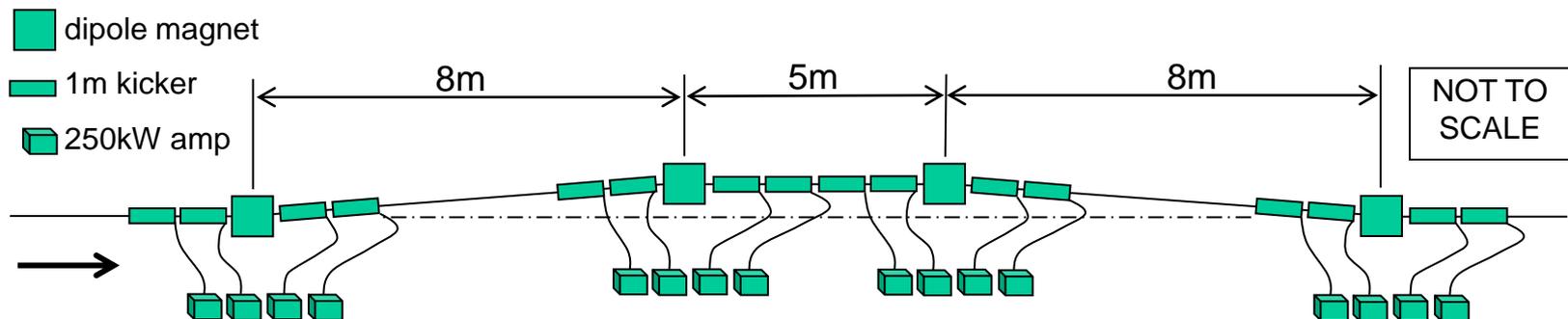
## **Amplifier architecture: modular, MOSFET**

- standard solution for fast, high-power amplifiers
- output from many low power modules have to be combined
- output voltage has to be stepped-up to provide the kV needed by the kicker
- the very low duty factor required (0.002%) is very unusual
  - it allows extremely high power densities and (relatively) low cost
- *note*: MOSFETs have almost entirely superceded bipolar transistors in this role

# A Preliminary System Concept

***It can be done – but looks very expensive.*** This is what we came up with:

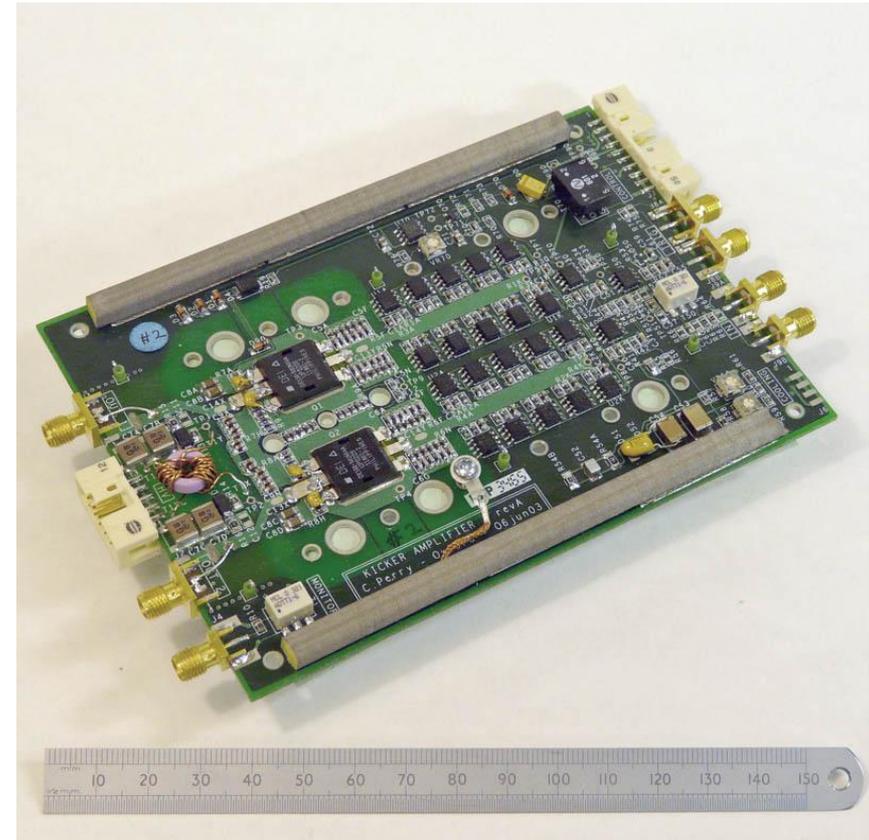
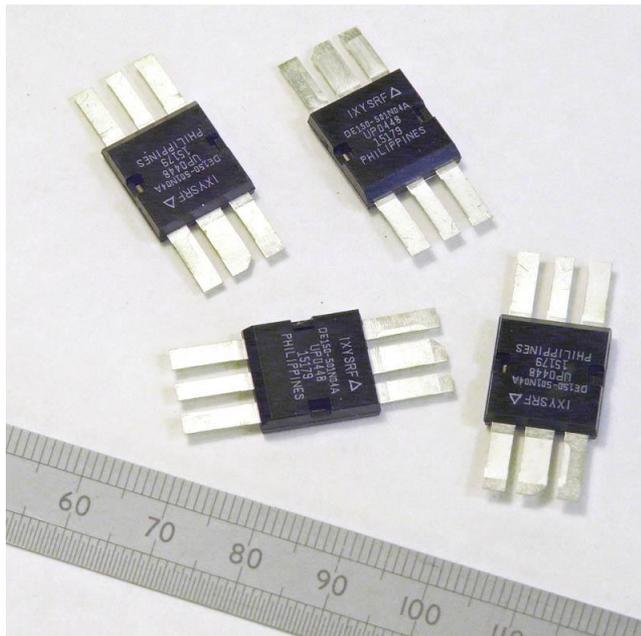
- 4 kickers at each bend
- 250kW peak power amplifier to each kicker
- 256 amplifier modules in each amplifier
- 1.2kW output each amplifier module (1kW after losses in combining etc)
- **amplifier size: 60 x 60 x 30cm** (=100 litres) min (double that is more comfortable)
- **amplifier cost: £75K per 250kW amplifier** (£300 per kW delivered to kicker)
- \*\*\* ***This is all very very approximate*** \*\*\*
- it makes no allowance for technological progress
- no single dominant cost, so estimates very rough until details worked out
- very dependent on high-volume costs: we have no sound basis for these
- 16 amplifiers & kickers / drive beam, 768 amplifiers total, 200MW total peak power
- **SYSTEM COST: £60M** (perhaps +/-£30M)



# Technicalities – Amplifier Modules – 1

## Module power is a matter of cost and size

- sweet spot looks today to be 1 to 2kW peak for 100MHz module bandwidth
- we are forced to low voltage, low impedance operation, and transforming the output



▲ 2kW peak output  
10ns amplifier module

◀ typical fast, high voltage MOSFETs  
(DE150-501N)

## Technicalities – Amplifier Modules – 2

|           |               |                  |             |              |            |              |              |                    |
|-----------|---------------|------------------|-------------|--------------|------------|--------------|--------------|--------------------|
| 1)        | Polyfet       | LR301            | Dual        | LDMOS        | 28V        | 0.6kW        | 0.15ns       |                    |
| 2)        | Polyfet       | SX501            | Dual        | VDMOS        | 28V        | 0.7kW        | 0.2ns        |                    |
| <b>3)</b> | <b>Freesc</b> | <b>MRF6VP11*</b> | <b>Dual</b> | <b>LDMOS</b> | <b>50V</b> | <b>1.5kW</b> | <b>0.2ns</b> | <b>\$170 @ 150</b> |
| 4)        | Polyfet       | SR746            | Dual        | VDMOS        | 50V        | 0.6kW        | 0.3ns        |                    |
| 5)        | IxysRF        | IXZ215N12L       | Single      | HV           | 55V        | 0.6kW        | 0.4ns        | 2 x \$32 @ 50      |
| 6)        | IxysRF        | IXZ210N50L       | Single      | HV           | 100V       | 1.0kW        | 0.8ns        | 2 x \$18 @ 50      |
| 7)        | IxysRF        | IXZ318N50        | Single      | HV           | 100V       | 2.0kW        | 1.0ns        | 2 x \$35 @ 25      |
| 8)        | IxysRF        | IXZ210N50L       | Single      | HV           | 200V       | 1.0kW        | 0.8ns        |                    |
| 9)        | IxysRF        | IXZ318N50        | Single      | HV           | 200V       | 4.0kW        | 1.6ns        | 2 x \$35 @ 25      |
| 10)       | IxysRF        | DE150-501N       | Single      | HV           | 220V       | 1.3kW        | 1.3ns        | 2 x \$28 @ 50      |

### Examples of possible MOSFETs and output stages based on them

- table gives supply voltage, peak output power, & a speed 'figure of merit'
- RF MOSFETs (1-4) tend to be expensive, low power, but fast
- HV MOSFETs (5-10) tend to be cheaper, higher power, but slower
- technically, #3 is the most attractive
- HV MOSFETs on 100V may be possible, but lower speed makes more demands on rest of system
- #10 is one we have used in two amplifier designs

# Technicalities – Transformation and Combining

The ~50V at the MOSFETs is a long way from the >2.5kV needed at kicker

- a lot of voltage step-up is needed & will have to be obtained in a series of stages

Standard RF combiners can't be used

- they can't give the bandwidth & they are too expensive

This is not trivial:

- we need a high upper frequency limit
- we need a good low frequency response: this is unusual
- we need good efficiency per stage
- first stage has to be small and cheap
- last stage has to handle high peak power and voltage

We use transmission-line transformers to step-up impedance and voltage

- voltage ratios of 1:3 or 1:4
- impedance transformation is from ~3 to 6 ohms to ~50 to 100 ohms (differential)
- higher ratios cannot give the bandwidth needed

Combining is by parallelling outputs

- typically, 16 at the higher impedance level to give 1 at the lower
- this does not have the isolation and protection from faults of 'proper' combiners
- passive protection (~10% power loss) serves to prevent faults propagating
- a redundant fuse-based disconnect system isolates failed amplifier modules

# System Issues

The obvious point of **cost** has been mentioned. Here are other important issues that have been addressed in this scheme:

**Size** - seems reasonable. But allowing a little more space may significantly reduce costs.

**Power consumption** - low enough to not give cooling problems nor significant electricity costs. Power stages would be enabled for at most 5us per bunch train.

- rough estimate: 500W per 250kW amplifier

**Reliability** - does not push things to their limit: saving money but impairing reliability is not acceptable

**Fault tolerance** - allows for modules failing without damaging others: it would continue to operate with a proportionate reduction in power

**Self-diagnosis** - system includes built-in test, and reporting of faults

**Ease of maintenance** - most faults require only plugging-in new small modules.

*Note:* very dense packaging tends to make this harder

**Response correction** - uncorrected response will not be sufficiently clean and accurate (many small reflections, non-linearities etc). Response would be continuously tested between bunch trains, and digital correction applied at input.

# Changed Requirements

In *February 2010* we learned requirements had changed somewhat:

- required kick angle at each bend was reduced to  $\pm 375 \mu\text{rad}$ 
  - this would have reduced power per kicker to 66kW peak
  - much more reasonable than the previous 250kW
- but energy spread of beam & dispersion of chicane increased kicker aperture
  - 0.5% rms energy spread, 1m dispersion
  - adds 5mm rms spread to beam width in middle section
  - to accept up to  $4\sigma$  in energy, extra 40mm aperture needed
  - allowing for beam deflection and a finite beam size, need 50mm aperture
  - brings power back up to 410kW peak
- allowing any sort of margin brings this to 600kW
  - eg for a slightly higher energy spread than assumed

Later it was indicated that full kick would not be essential at full bandwidth

- this may prove a useful dispensation, but doesn't have a radical effect

## A Technology Option: Vacuum Tubes - 1

Vacuum tubes should not be discounted.

- capable of high peak powers
- capable of the high voltages needed to drive kickers directly.

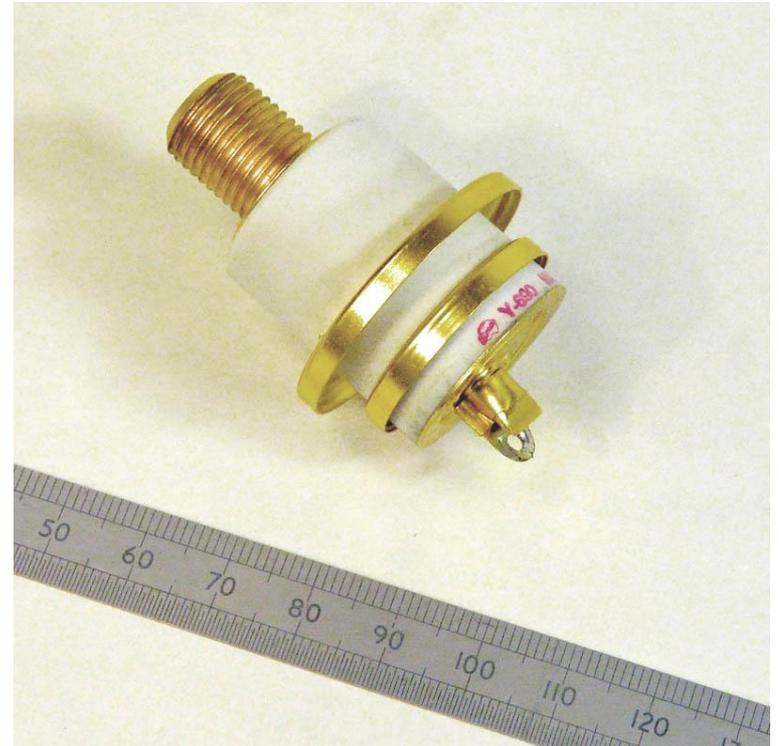
Y690 planar triode looks useable

- factory confirms it will remain available
- multiple tubes can provide high powers

We have a conceptual design for a 500kW peak power amplifier:

- 7 tubes with plates in parallel drive each kicker strip
- each tube has its own MOSFET driver
- believe we have a solution to critical problem of protecting driver from flashover
- could fit in 30 x 20 x 15cm (+50% for power supplies etc): total 14 litres
- cost: maybe around £40K

(We have used the tube. We only got 5kW peak, 40MHz from one, but should be able to push this to 35kW, 65MHz)



▲ Y690 Planar Triode

## A Technology Option: Vacuum Tubes - 2

Another possibility – the 3CPX10,000U7 pulse-rated triode

- this was suggested by an Eimac engineer
- it should remain available
- it is a large, transmitting type tube
- CPI would make a special with reduced cooling fins
- pair ought to do 500kW peak with 100MHz output stage bandwidth (perhaps even 750kW or so...)
- attractive as an output stage, but I don't yet see how to drive them
- might be hard to get overall bandwidth better than 60MHz
- amplifier would be larger than with Y690s: perhaps 45 x 30 x 30cm



▲ 4CX5000 – similar to the 3CPX10,000U7 but a bit taller and slimmer

# Engineering Improvements

**Better, cheaper parts** (esp MOSFETs) by the time system has to enter production

- gains likely to be modest

**Engineering for high-volume manufacture**

- get modules smaller & simpler than I assumed
- design for automated assembly

**Volume purchasing**

- I've *no idea* how parts costs fall in 100K+ quantities...

**Special MOSFETs**

- standard parts are in expensive & bulky high-power packages
- RF types are made and tested to meet demanding RF test specifications
- we need neither
- an existing die, packaged & tested to our requirements, *might* save costs

**Driver ASIC**

- an analog ASIC for the driver part of module could reduce size and cost
- feasible but difficult: analog ASICs are hard...

**Exploit reduced drive requirement at high frequencies?**

- *may* permit higher voltage, higher power, & cheaper output stages to be used
- not a safe assumption until fully worked out and demonstrated
- might offer a factor of 2 to 3 saving

*Note:* compound amplifiers (separate HF & LF parts) don't seem feasible

## Kicker Improvements

### **Optimized use of kickers – *probably worthwhile***

- required aperture varies between the kickers
- reducing aperture when possible reduces drive power
- modular amplifier allows configuration for different powers

Best compromise might be:

- halve the gap on kickers at first and last dipoles, and fit 2 kickers not 4
- keep drive power to each kicker the same
- saves 25% in amplifiers (number and total power) & reduces overall length

*Caution:* responses of kickers must match – easiest if kickers & amps are identical

### **Improved kicker design – *probably too difficult***

- stripline kickers are inefficient when aperture needed is longer across B
- ferrite yokes can confine magnetic field energy to useful region
- modest gain (factor of 2 in power?), but looks difficult and expensive

### **Separate fast and slow kickers – *doesn't seem to work out***

- exploit reduced kick required at high speeds
- separate fast (stripline) and slow (ferrite) kickers with their own amplifiers
- sound in principle, doesn't seem to work out in this case

### **Kicker with integrated drive amplifiers – *not meant seriously!***

Radical solution (impractical for CLIC): kicker with short sectional ferrite yokes slipped over ceramic beampipe. Each yoke has its own integrated driver. This can be a lot more efficient...

# The Future – System Design

In designing the drive beam phase correction system, bear in mind that:

- amplifier system cost will be **very** large
- it will be **very** sensitive to:
  - maximum kick angle
  - kicker aperture
- power and cost go roughly as the square of each of these factors
- requiring a conservative specification can be **very** expensive
  - eg fully correcting for more of the time
  - going from ' $2\sigma$ ' to ' $3\sigma$ ' (95% to 99.7% of the time) more than doubles the cost
- any reduction in initial drive beam phase errors will be enormously valuable

*Note:* the increased kicker aperture required by dispersion is a major cost driver.

And were there to be incoming dispersion in the opposite sense:

- maximum beam size would be reduced
- smaller aperture kickers could be used
- drive power needed would be decreased
- all the kicker/amplifier systems made identical with no loss of efficiency.

# The Future – Engineering Validation

*It would be important to validate the basic concepts of the amplifier system.*

amplifier output stage:

- can we actually get the predicted performance?

combining system:

- can we do this reliably?
- can we do it the final power levels needed?
- can we get adequate frequency response?

transformers and associated ferrites:

- will they work well enough?
- what are the detailed properties of the ferrites?
- how big and how expensive will they end up?

size and cost:

- push an amplifier module to a more-or-less finished design
- that would set an upper bound on size and cost
- amplifier module will dominate system cost

system concepts:

- functional test of a small-scale system would be an appropriate next stage
- eg: 16 amplifier modules and one combining stage, driving a kicker

# The Future – The Vacuum Tube Alternative

## ***Finally, a plea...***

The modular, solid-state amplifier system is very attractive. But not simple, and not cheap

Vacuum tube amplifiers *may* be able to provide high powers at considerably lower cost

If the drive power requirement increase any further, they may be the only affordable solution

But this is not a standard vacuum-tube application: there are several practical issues that may turn out to be show-stoppers

So without some real development work, they will not be available as an option

***There would be a real advantage in working on vacuum-tube amplifiers in parallel with solid-state designs***