

Review of Spin Rotators for LC

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October 18-22, 2010

IWLC2010 - CERN, Geneva

- Spin dynamics and design criteria
- Spin rotator location
- Spin rotator options
- CLIC case: two options
- Summary and conclusions

Spin Dynamics Summary

⇒ The precession motion for the magnetic moment of an accelerating relativistic particle is given by the solution of the Thomas-BMT equation, see for instance Bryan W. Montague, Phys. Rep., **113**, No. 1, 8-13 (1984)

- Spin Precession

$$\phi_s = G \gamma_0 \alpha$$

- Mean polarization:

$$\langle P_z \rangle = P_0 e^{-\frac{(G\gamma_0\alpha\sigma_\delta)^2}{2}}$$

- Relative depolarization:

$$1 - \frac{\langle P_z \rangle}{P_0}$$

- Where

Symbol	Value	Description
G	0.00115965219	anomalous momentum of the electron
α	-	arc bending angle
γ_0	-	relativistic factor
σ_δ	-	energy spread

Spin Depolarization

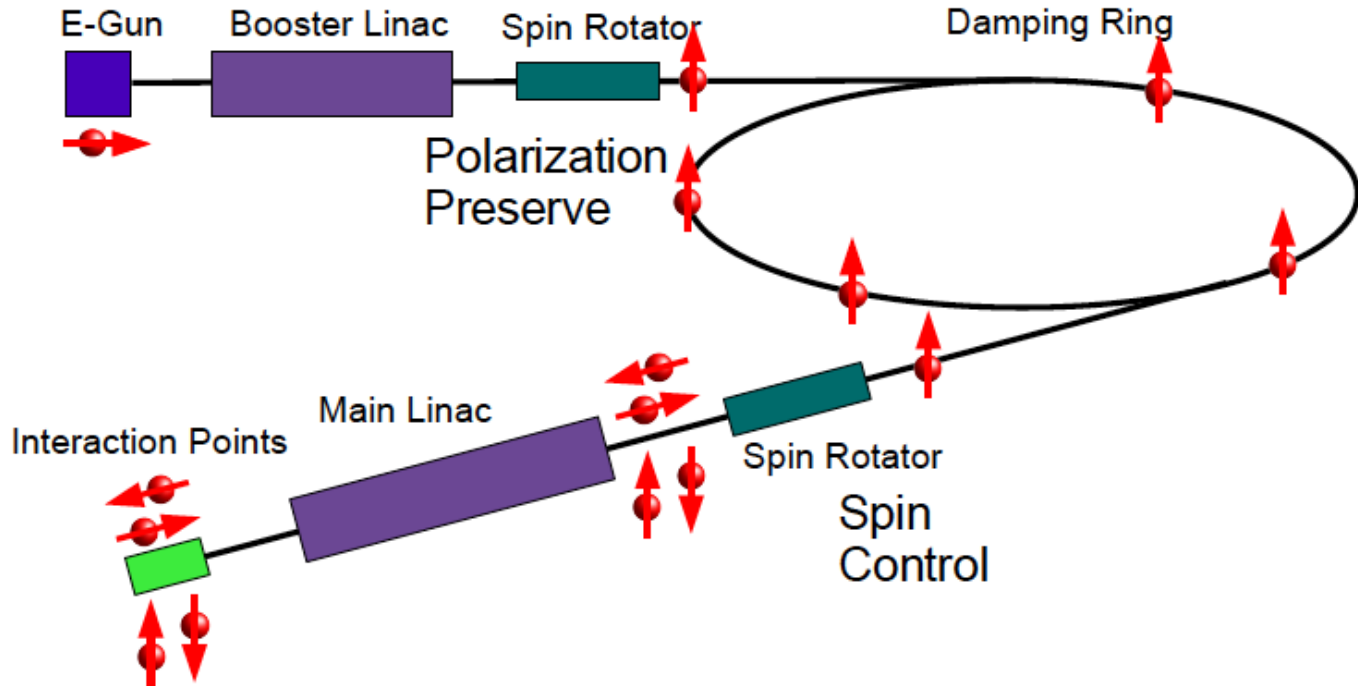
- In the damping rings, if the spin direction is not perpendicular to the horizontal plane, spin precesses during the storage
- Because the precession frequency depends on the beam energy, the precession phase is randomized by energy spread
- This randomization causes a significant depolarization. The spin direction has to be perpendicular to the horizontal plane to avoid this depolarization effect by the precession

Spin Rotator Design Criteria

- Design Criteria (P. Emma for NLC, 1994)
 - *Spin should be orientable in any direction*
 - *Net momentum compaction must be small such that energy fluctuations do not become longitudinal position fluctuations (less than 100 μm bunch length @ IP for NLC)*
 - *It should be located such that total spin diffusion due to energy spread is small*
 - *System should not dilute significantly the beam transverse emittance (small energy spread)*
 - *System should be short, simple and robust*

Spin Rotator Location

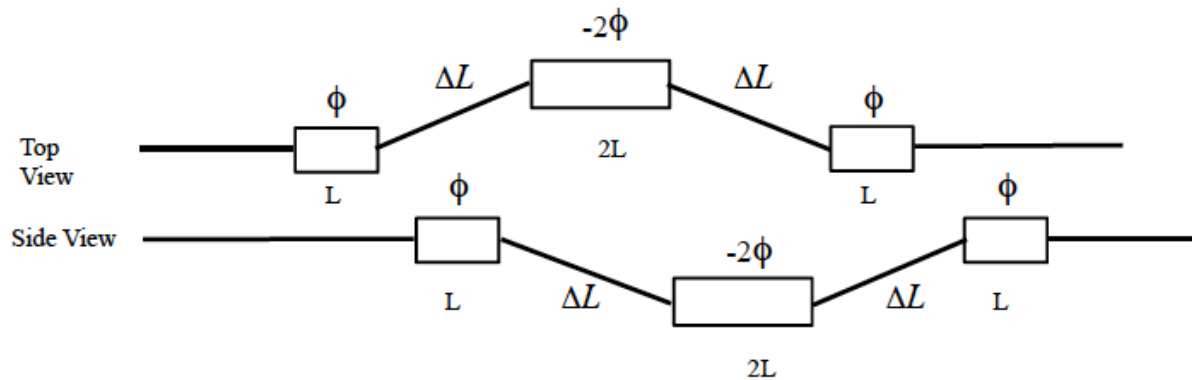
- Spin precesses around the magnetic field
- ⇒ Longitudinal Polarization should be perpendicular before DR injection
- ⇒ Polarization control after DR



Half Serpent Spin Rotator

⇒ Very simple schema: the system requires only nested horizontal and vertical chicane; but they inevitably dilute the transverse emittances through synchrotron radiation emission

⇒ But a vertical bending schemes are not feasible:



Disadvantages

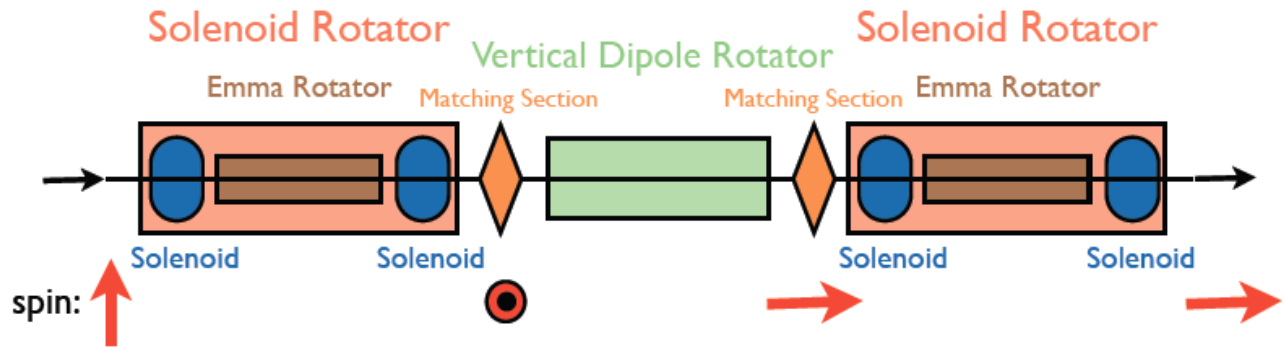
- Each vertical bend would have to be about 1000 meters long to keep vertical emittance from growing even 2%
- R_{56} 800 meters in such a setup – totally unacceptable
- Spin rotation is fixed, we want full variability in exiting polarization

Solenoid Based Spin Rotator

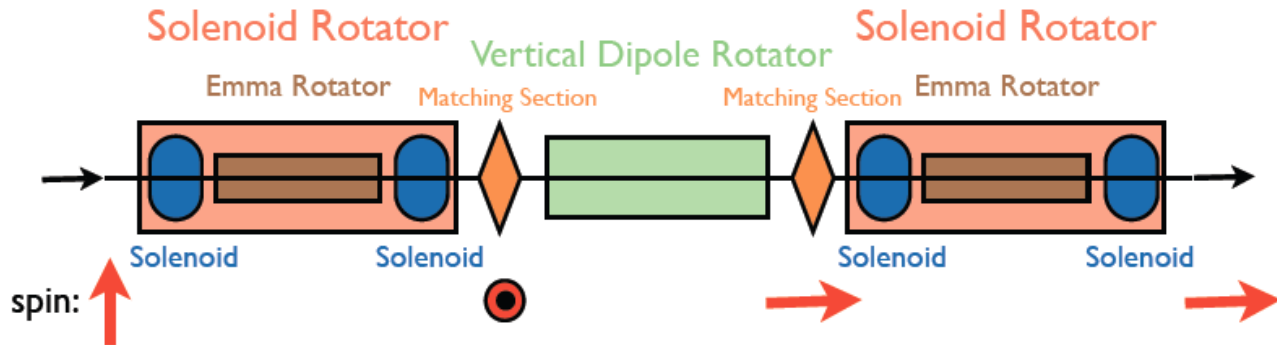
⇒ First designed by Paul Emma for NLC

- Spin Rotation is achieved by two solenoids with a bending magnet in between
- Each solenoid is split in two parts separated by a *reflector* $\begin{pmatrix} I_2 & 0 \\ 0 & -I_2 \end{pmatrix}$ to correct for couplings ⇒ there are four solenoids in total
- The central bending section must rotate the spin by 90 degrees
- This configuration allows arbitrary spin orientation

⇒ **Sketch**



Emma Rotator

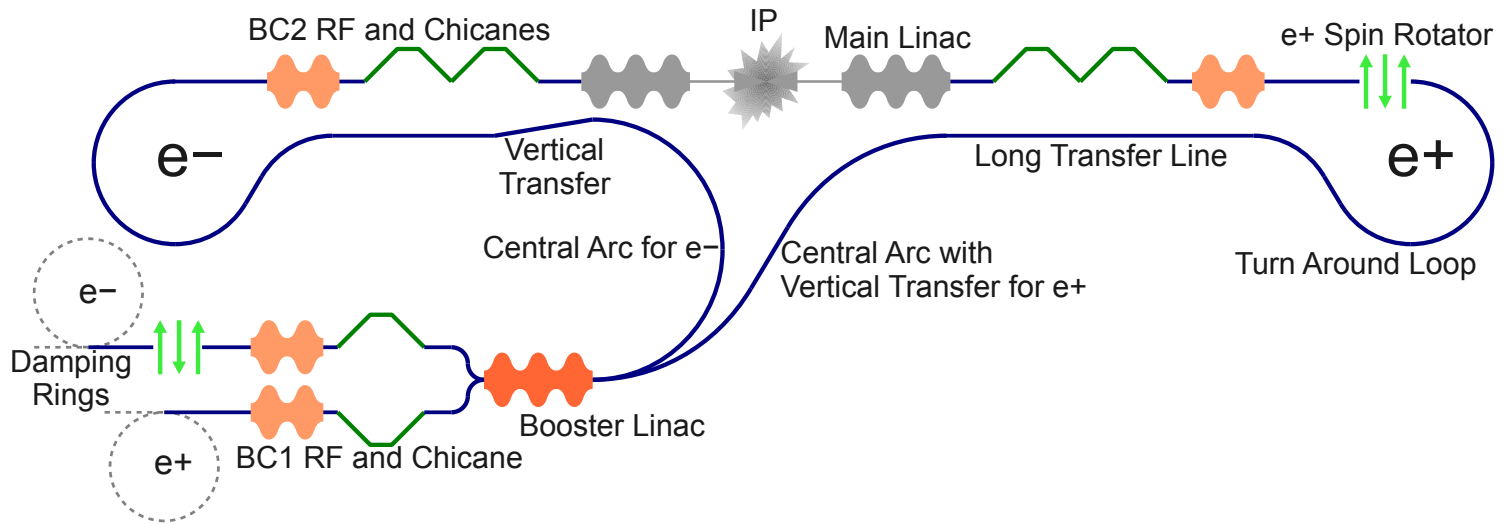


Description

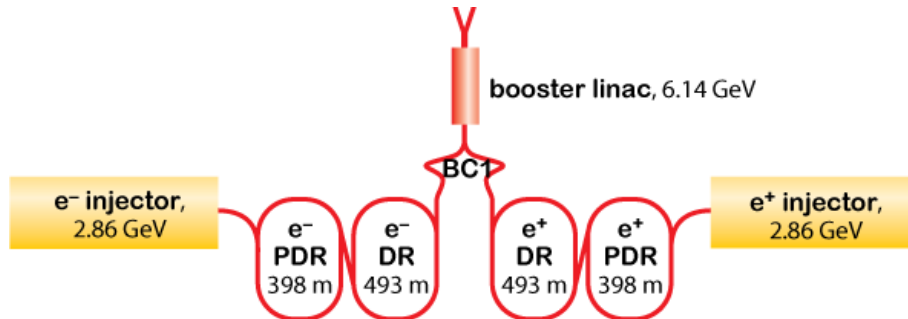
- Reflector beamline : four FODO cells with 90 degrees phase advance in X and 45 degrees phase advance in Y
- Bend section : mini arc composed by three FODO cells with 90 degrees phase advance in X and Y (can be shortened)

Spin Rotator Location in CLIC

CLIC RTML layout (F.Stulle)



Previous layout



Spin Precession and Depolarization in CLIC

region	E_0 [GeV]	σ_δ	$\alpha_{\text{electrons}}$ [rad]	$\alpha_{\text{positrons}}$ [rad]
exit of damping rings to bc1	2.86	0.13%	0	0
exit of bc1 to booster	2.86	1.04%	0	0
exit of booster to bc2	9	0.33%	$\pi - \pi + \text{HV-doglegs} = 0$	$\pi + \text{HV-doglegs} = \pi$
exit of bc2 to bds	9	1.64%	0	0
exit of main linac to ip	1500	0.35%	$1 \cdot 10^{-3}$	$1 \cdot 10^{-3}$

region	E_0 [GeV]	σ_δ	$1 - \frac{\langle P_z \rangle}{P_0}$ [%]	$\phi_s = a \gamma_0 \alpha$ [deg]	n -turns
exit of damping rings to bc1	2.86	0.13%	0	0	0
exit of bc1 to booster	2.86	1.04%	0	0	0
exit of booster to bc2 entrance	9	0.33%	0 / 2.2	0 / 3676.4 \equiv 76.4	0 / 10.2
exit of bc2 to bds	9	1.64%	0	0	0
exit of main linac to ip	1500	0.35%	0.007	195	0.54

⇒ From the point of view of the spin dynamics, ideal location for the spin rotators would probably be: **before bc1** for the electrons, **before bc2** for the positrons

⇒ Notice that, in case of a symmetric RTML where both spin rotators are placed before bc1 and assuming that the beam experiences a total bending angle $\alpha = \pi/2_{\text{booster} \rightarrow \text{bc2}}$ for each line, the total depolarization per beam is 0.56% per line. (with a precession of 5.1 n-turns)

Solenoid Strength

- Each of the four solenoids must be capable of providing a maximum of ± 45 degrees spin rotation

$$\psi_{\text{spin}} = \pi/4, \quad \text{with} \quad \psi_{\text{beam}} = \psi_{\text{spin}}/2$$

- Solenoid strength

$$k = \frac{\psi_{\text{spin}}}{2L} = \frac{B_z}{2(B_0\rho)}$$

Assuming 2.6 meters long solenoids (like ILC)

$$k = \frac{\pi/4}{2} \frac{1}{(L = 2.6 \text{ m})} = 0.15104 \text{ m}^{-1}$$

⇒ The maximum longitudinal field is:

$$B_{z,\text{max}} = 2 \cdot k \cdot (B_0\rho) = 2 \cdot k \cdot \frac{E_0}{ec} = 2 \cdot 0.15104 \text{ m}^{-1} \cdot \frac{E_0}{ec}$$

required magnetic field at 2.86 or 9 GeV is:

$$B_{z,\text{max}} @ 2.86 \text{ GeV} = \mathbf{2.9 \text{ T}}$$

$$B_{z,\text{max}} @ 9 \text{ GeV} = \mathbf{9.1 \text{ T}}$$

Bending Arc

- The bending section should rotate the spin by 90 degrees

$$\phi_s = a \gamma_0 \alpha = \frac{\pi}{2}$$

$$\alpha @ 2.86 \text{ GeV} = \frac{\pi/2}{a (\gamma_0 = 2.86e3/0.511)} = 0.24202 \text{ rad} = 13.867 \text{ degrees}$$

$$\alpha @ 9 \text{ GeV} = \frac{\pi/2}{a (\gamma_0 = 9e3/0.511)} = 0.076908 \text{ rad} = 4.4065 \text{ degrees}$$

- Magnetic strength:

$$B\rho @ 2.86 \text{ GeV} = \frac{pc}{ec} = \frac{2.86 \text{ GV}}{c} = \frac{2.86 \text{ GV}}{2.997925 \cdot 10^8 \text{ m/s}} = 9.5 \text{ T m}$$

$$B\rho @ 9 \text{ GeV} = \frac{pc}{ec} = \frac{9 \text{ GV}}{c} = \frac{9 \text{ GV}}{2.997925 \cdot 10^8 \text{ m/s}} = 30 \text{ T m}$$

Bending Magnets and Longitudinal Motion

- Assuming to be using 6, 1 meter long magnets, this corresponds to a bending radius

$$\rho @ 2.86 \text{ GeV} = \frac{L}{\alpha} = \frac{6 \cdot 1 \text{ m}}{0.24202 \text{ rad}} = 24.792 \text{ m}$$

$$\rho @ 9 \text{ GeV} = \frac{L}{\alpha} = \frac{6 \cdot 1 \text{ m}}{0.076908 \text{ rad}} = 78.015 \text{ m}$$

⇒ Magnetic field

$$B @ 2.86 \text{ GeV} = \frac{9.5 \text{ T m}}{24.792 \text{ m}} = 0.38319 \text{ T}$$

$$B @ 9 \text{ GeV} = \frac{30 \text{ T m}}{78.015 \text{ m}} = 0.38454 \text{ T}$$

⇒ R_{56} for the bending section is:

$$R_{56} @ 2.86 \text{ GeV} = 60.0 \text{ mm}$$

$$R_{56} @ 9 \text{ GeV} = 6.0 \text{ mm}$$

ISR-Induced Emittance Growth

The effect of incoherent synchrotron radiation (ISR) emission on the emittance growth can be estimated using

$$\Delta\gamma\epsilon = 4 \times 10^{-8} E^6 [\text{GeV}] I_5 [\text{m}^{-1}]$$

where

$$I_5 = \frac{4L}{|\rho|^3} \cdot \frac{\eta^2 + (\eta\alpha + \eta'\beta)^2}{\beta}$$

⇒ **Case of $E=2.86$ GeV:** using $L=1$ m, $\rho = 24.8$ m, average dispersion and its derivative $\eta = 0.3$ m and $\eta'=0.15$ rad, horizontal twiss $\beta=22.5$ m and $\alpha = \pm 3.5$, and horizontal emittance $\gamma\epsilon = 0.68 \mu\text{m}$:

$$\frac{\Delta\gamma\epsilon}{\gamma\epsilon} = 0.7\%$$

⇒ **Case of $E=9$ GeV:** using $L=1$ m, $\rho = 78.0$ m, average dispersion and its derivative $\eta = 0.1$ m and $\eta'=0.05$ rad, horizontal twiss $\beta=22.5$ m and $\alpha = \pm 3.5$, and horizontal emittance $\gamma\epsilon = 0.68 \mu\text{m}$:

$$\frac{\Delta\gamma\epsilon}{\gamma\epsilon} = 0.003\%$$

Spin Rotator and Bunch Compressor

- P. Emma, 1994: *“the rotator system has very little impact on the performance of the bunch compressor”*
- Longitudinal transfer matrix of the bunch compressor

$$R_{\text{BC}} = \begin{pmatrix} 1 + fR_{56} & R_{56} \\ f & 1 \end{pmatrix}$$

- In case of full compression, ie. $1 + fR_{56} = 0$, adding the spin rotator changes the total transfer as follows

$$R_{\text{BC}} \cdot R_{\text{ROT}} = \begin{pmatrix} 1 + fR_{56} & R_{56} \\ f & 1 \end{pmatrix} \cdot \begin{pmatrix} 1 & \alpha \\ 0 & 1 \end{pmatrix} = \begin{pmatrix} 0 & R_{56} \\ f & 1 + \alpha f \end{pmatrix}$$

⇒ Bunch length after compression is unchanged by the rotator and the energy spread after compression is smaller ($f = 2 \text{ m}^{-1}$, $\alpha = -0.04 \text{ m}$):

$$\sigma_{z,f} = \sigma_{\delta,i} R_{56}, \quad \sigma_{\delta,f} = \sqrt{\sigma_{z,i}^2 f^2 + \sigma_{\delta,i}^2 (1 + \alpha f)}$$

- In our case, as bc1 **does not fully compress**,

$$R_{\text{BC}} \cdot R_{\text{ROT}} = \begin{pmatrix} 1 + fR_{56} & R_{56} + \alpha(1 + fR_{56}) \\ f & 1 + \alpha f \end{pmatrix}$$

⇒ Rotator might have an impact on the compression factor

$$\sigma_{z,f} = \sigma_{\delta,i} [R_{56} + \alpha(1 + fR_{56})]$$

$$\sigma_{\delta,f} = \sqrt{\sigma_{z,i}^2 f^2 + \sigma_{\delta,i}^2 (1 + \alpha f)}$$

Notice that if $\alpha f < 0$ the final energy spread gets reduced

⇒ This problem can be overcome using an isochronous arc.

Summary Table for CLIC

Relevant parameters with the spin rotator location, for **electrons** and **positrons**:

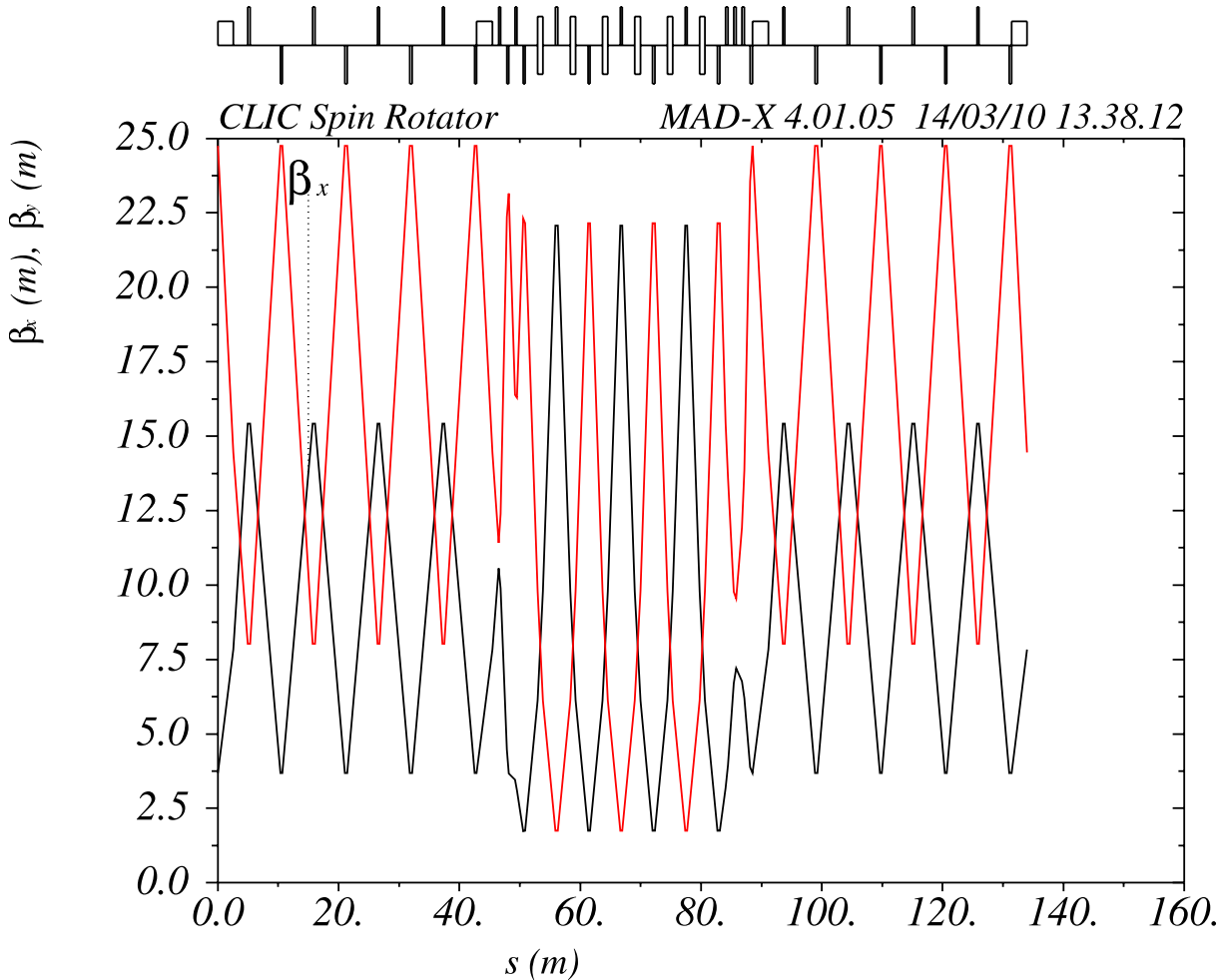
quantity	before bc1 ^(*)	before bc2	symm.rtml	unit	remarks
beam energy	2.86	9	2.86	GeV	
bending angle	0 (π)	0	$\pi/2$	rad	
spin depolarization	0 (2.2)	0	0.56	%	bds excluded
spin precession	0 (10.2)	0	5.1	turns	" "
solenoid field	2.9	9.1	like (*)	T	$L=2.6$ m
bending angle	13.9	4.4	like (*)	deg	$L=1$ m
bending magnet	0.38	0.38	like (*)	T	" "
R_{56}	60.0	6.0	like (*)	mm	
$\Delta\gamma\epsilon_x$ by synrad emission	0.7	0.003	like (*)	%	negligible
total length	134.0	longer	like (*)	m	scales with the energy

⇒ New RTML layout: potential problem might be the large solenoid field for the positrons; positron spin rotator before bc2 would be longer; positron spin rotator before bc1: 2.2% depolarization seems to me negligible

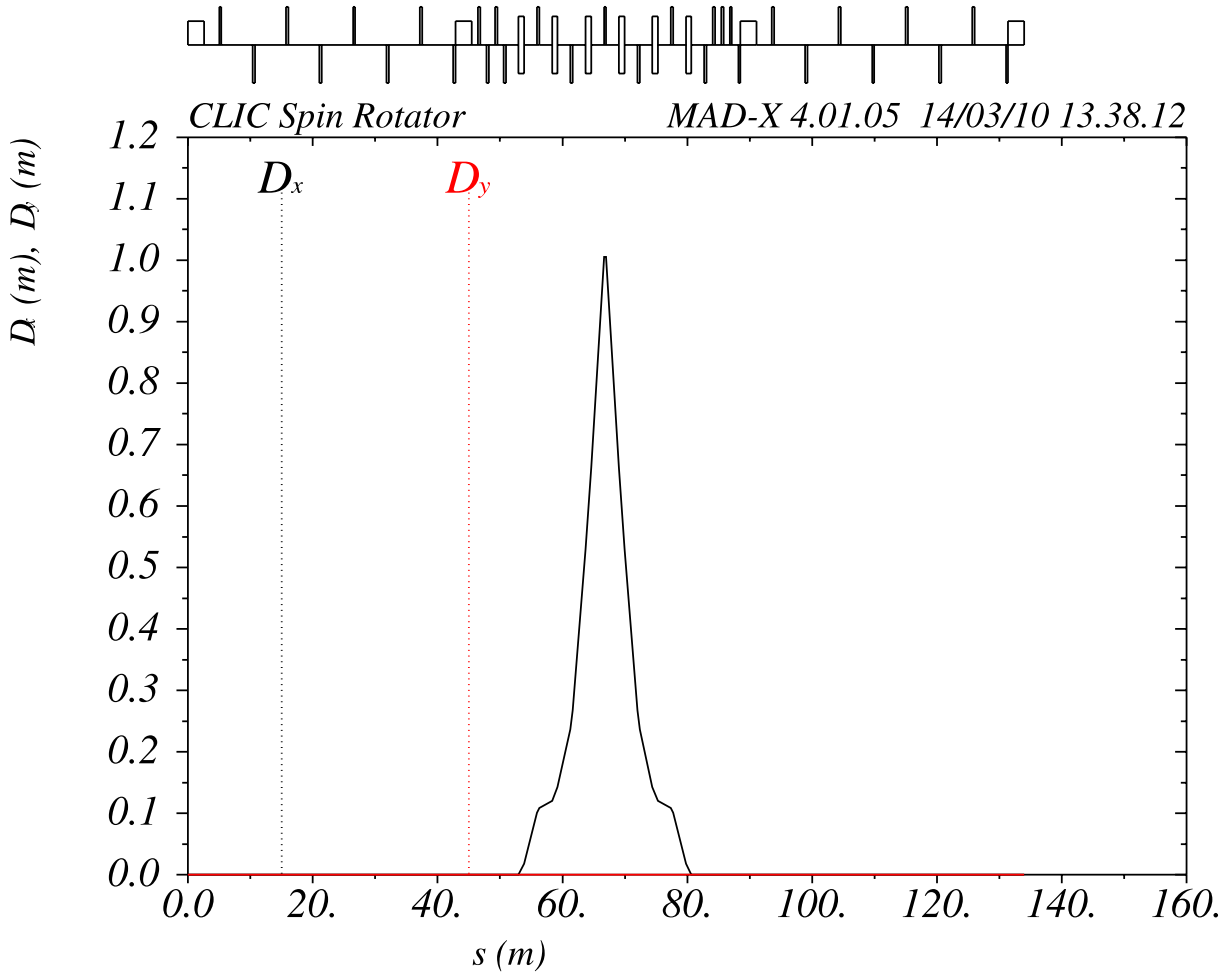
⇒ Old RTML layout (symmetric): no major problems, negligible depolarization

- Detailed beam dynamics studies have to be carried out
- Impact of R_{56} on the bunch compressor must be evaluated / use of an isochronous arc

Spin Rotator Optics



Spin Rotator Optics



Spin Rotator Optics

