

S1-Global Tuner Performance Study

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on behalf of INFN Milan team

- Main performances goals for tuning systems:
 - **Static or *Slow* tuning:**
 - Suitable tuning range according to cavity production frequency scatter. Typically 600 kHz for TESLA cavities.
 - Hz/step level frequency tuning resolution, with low hysteresis and mechanical backlash.
 - **Dynamic or *Fast* Tuning:**
 - Compensation of Lorentz Force induced Detuning or LFD during the flat-top or eventually during the full RF pulse

By design, S1-Global modules are rich in consolidated solutions as well as technical novelties and challenging issues.

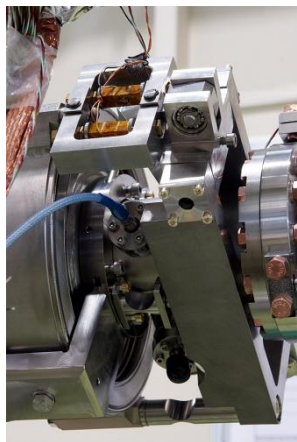
This is true also for tuning systems: apart from the well established DESY/Saclay tuner, the others, the Blade from INFN/FNAL and the ones from KEK, are here installed on a string for the very first time.



TESLA Cavity (DESY/FNAL)



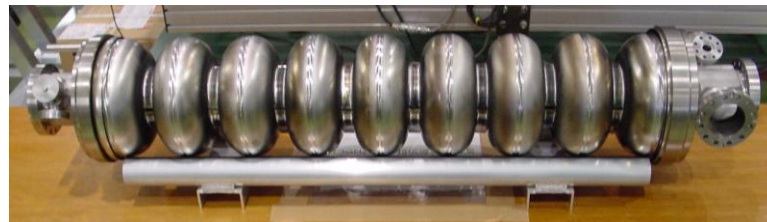
Blade Tuner (INFN/FNAL)



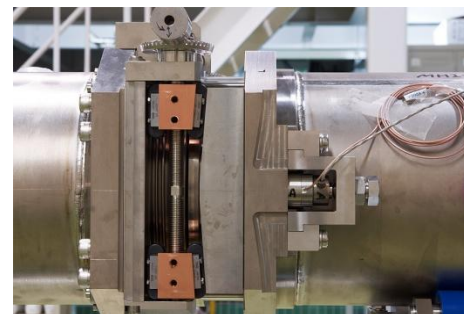
Saclay type Tuner (DESY)



TTF-III Coupler (DESY/FNAL)



Tesla-like (KEK)



Slide-Jack Tuner (KEK)



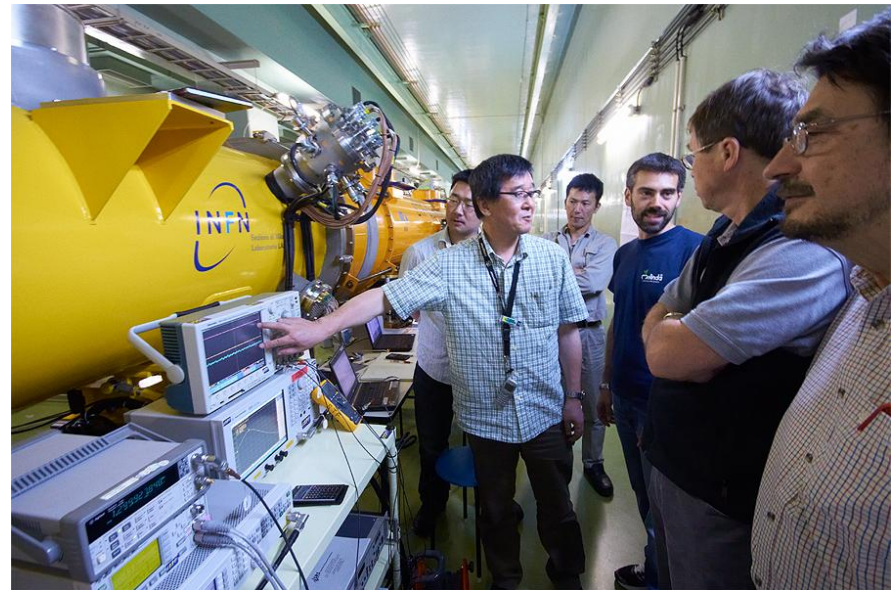
STF-II Coupler (KEK)



Tuning systems in details

- Cavities C1 and C2:
 - **Accel and AES TESLA cavities from FNAL**
 - **Helium tank from FNAL, specific design for coaxial tuner**
 - **Blade Tuner coaxial unit from INFN, revised ILC model**
 - **Motor drive unit with Phytron stepper motor and Harmonic Drive gear from FNAL**
 - **2 Noliac LV multilayer actuators from INFN**
- Cavities C3 and C4:
 - **“standard” DESY/FLASH TESLA cavity and helium tank system, fabricated by EZ**
 - **Lateral tuner with joint DESY/Saclay design**
 - **Motor drive unit composed by Phytron stepper motor and Harmonic Drive gear from DESY**
 - **2 Noliac LV multilayer actuators from DESY, packed in one single holder**
- Cavities A1 and A2:
 - **KEK TESLA-like cavities**
 - **KEK helium tank design for coaxial tuner**
 - **Slide Jack coaxial tuner mechanics from KEK**
 - **No drive unit installed. Tuner is manually driven from outside through a shaft.**
 - **One HV piezo from KEK**
- Cavities A3 and A4:
 - **The same than A1 and A2 cavity packages but with lateral tuner helium tank**
 - **KEK lateral Slide Jack tuner installed**

- A joint team from KEK, INFN and FNAL operated at S1-Global site:
 - **Module C tuners installation on February 2010, 2 Blade units and 2 DESY-Saclay units.**
 - **Low Power, CW, cold test of module C and A tuning systems on July 2010**





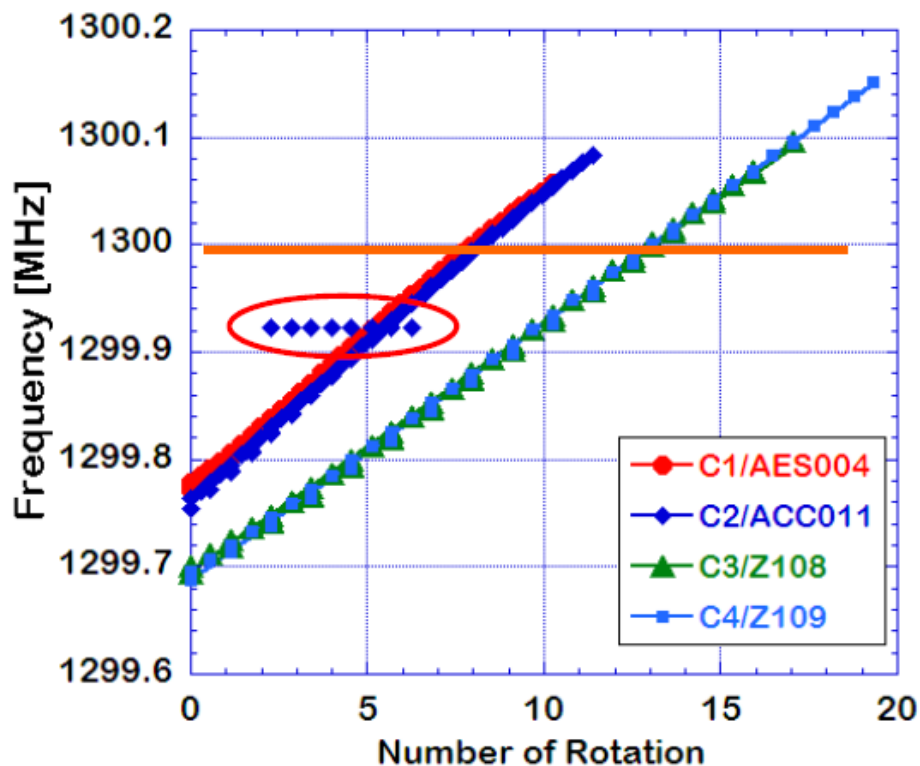
Room temperature measurement

- Once tuner systems have been installed on mod. C, they have been subjected to a basic functionality check:
 - **Important cross-check prior to cold mass enclosing**
 - **2 failing piezo actuators in cavities C3 and C4 (DESY-Saclay tuners) discovered:**
 - Discharge observed at a voltage lower than nominal.
 - The issue has been identified as **superficial discharge due to impurities** and solved through an accurate acetone cleaning of piezo ceramic surfaces.
 - **Finally, all 4 tuning systems performed as expected:**
 - The frequency shifts induced by both motor drive units and piezo actuators (static, 2 piezos) have been measured.

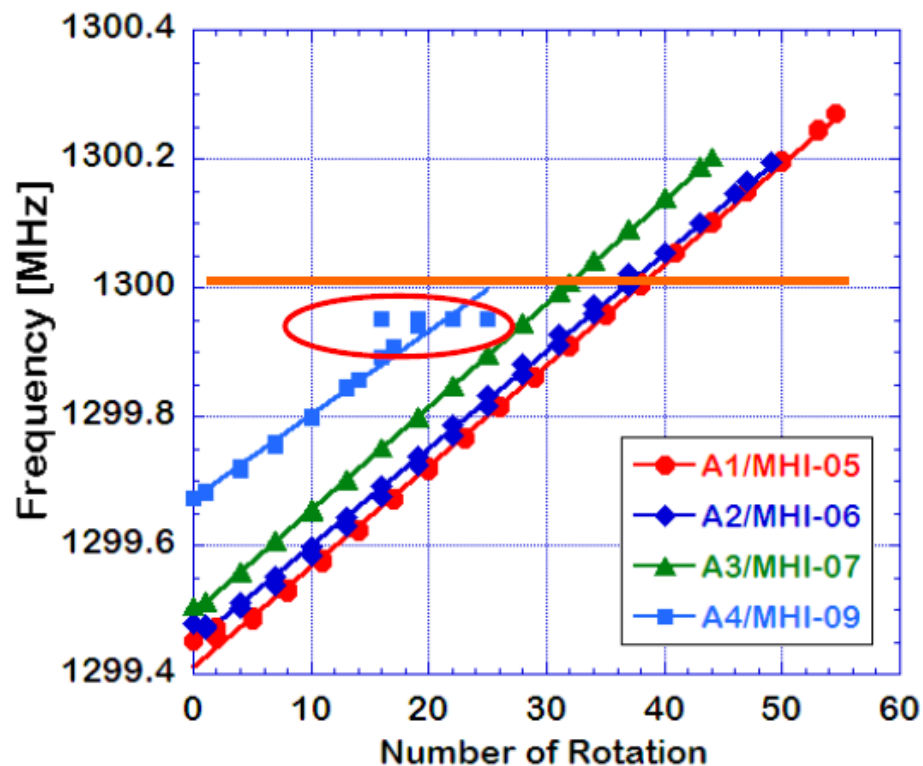
	C1 – Blade	C2 – Blade	C3 – Saclay	C4 - Saclay
Motor $\Delta v/\text{turn}$ [kHz]	31	26	17	20
Piezo $\Delta v/200V$ [kHz]	15	18	4	4

Static tuning range at cold

Cryomodule - C



Cryomodule - A



Trouble of two motor tuners occurred in C2/ACC011 (Blade) and A4/MHI-09 (Slide-Jack/end) !!



Static tuning range at cold

- For 6 out of 8 tuning systems installed the static tuning was confirmed in terms of range, hysteresis and capability to drive the cavity to operating frequency.
- Issue with Blade Tuner package in cavity C2:
 - Correctly performed a first tuning cycle around 1.3 GHz
 - Still unknown failure happened during the second cycle and frequency resulted to be stacked at about 1299.92 MHz.
- Issue with Slide Jack Tuner in A4:
 - Initially moved toward higher frequencies
 - Failure occurred in the driving shaft joint and frequency resulted to be stacked at 1299.95 MHz.



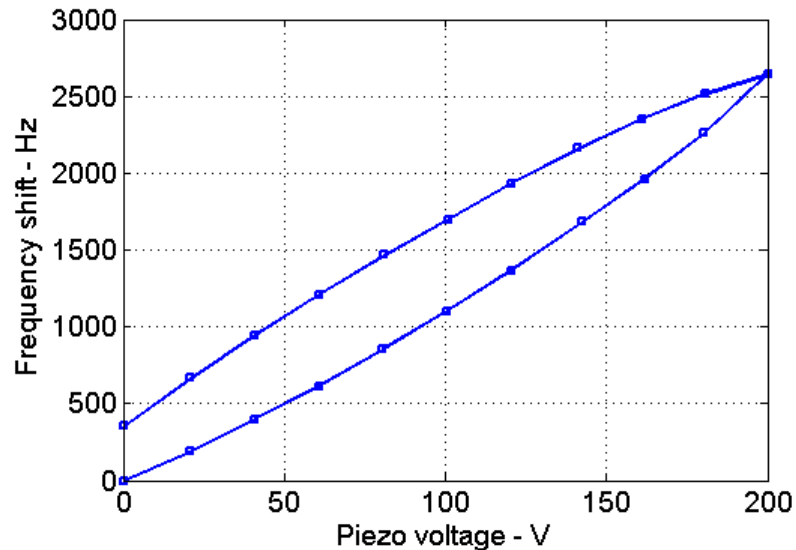
Piezo tuning range at cold

- Two main onset of measurements have been performed with fast actuators:
 - **DC piezo stroke, in different configurations. The cavity frequency shift is recorded as a function of the piezo DC driving voltage.**
 - This measurement allows for a direct evaluation of piezo integrity as well as the efficiency of their mechanical coupling to the cavity
 - **Pulsed piezo stroke. The dynamic frequency shift induced by a standard piezo pulse for LFD compensation is recorded.**
 - The pulse is a half-SIN waveform, 2.5 ms time width.
 - In this case the cavity intrinsic mechanical dynamic comes into the game, it's a meaningful evaluation of tuner LFD compensation capabilities.
- Measurements are performed with the cavity locked within a phase locked loop (PLL) with a 1kHz/V FM modulation factor:
 - **The modulation input signal is acquired, higher resolution and reproducibility is achieved if compared to direct NA measurements.**

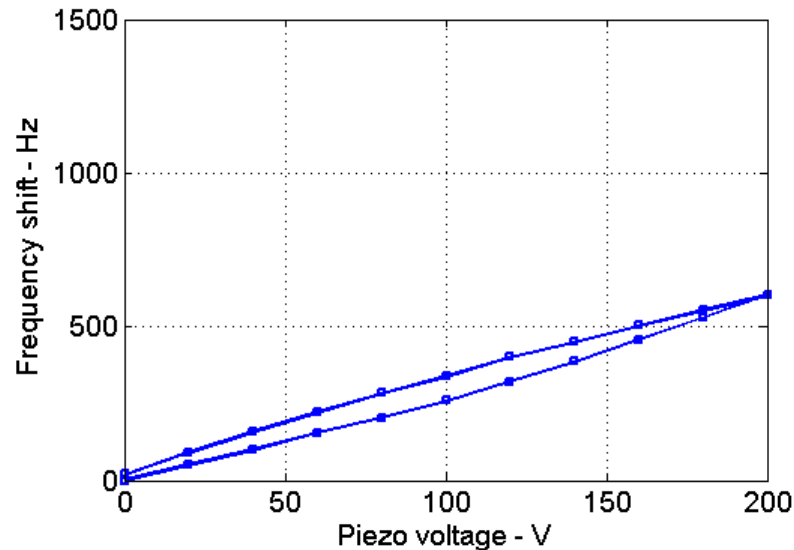


Piezo DC response – module C

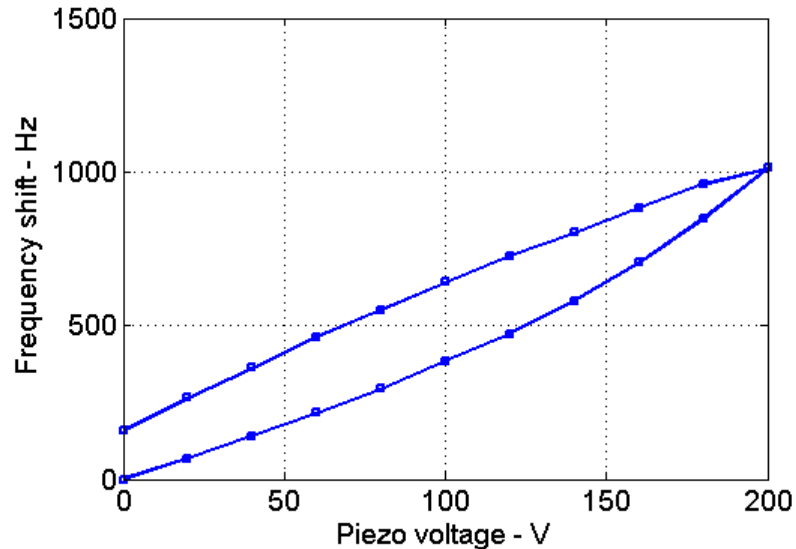
C1 - AES004 - Blade - Piezo 1+2



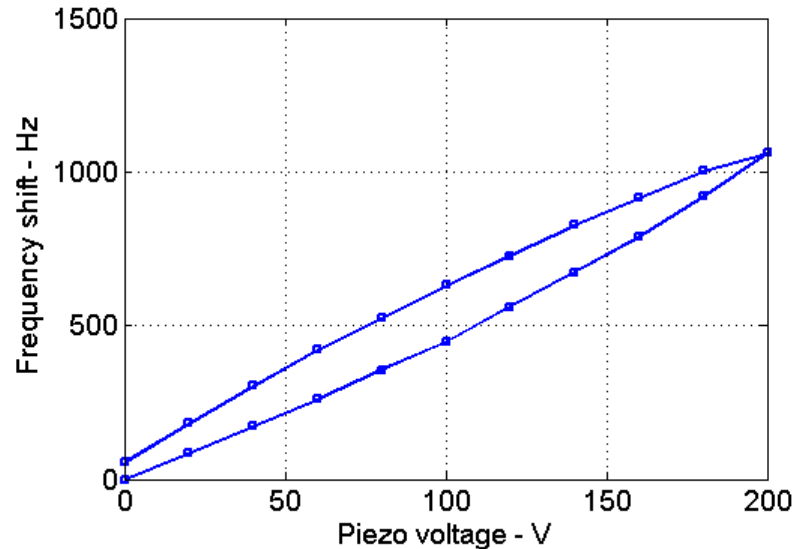
C2 - ACC011 - Blade - Piezo 1



C3 - Z108 - DESY - Piezo 2

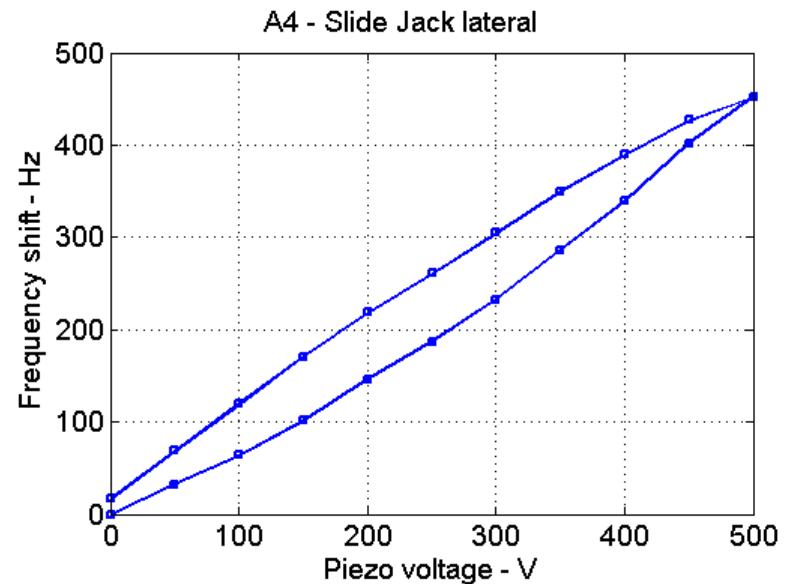
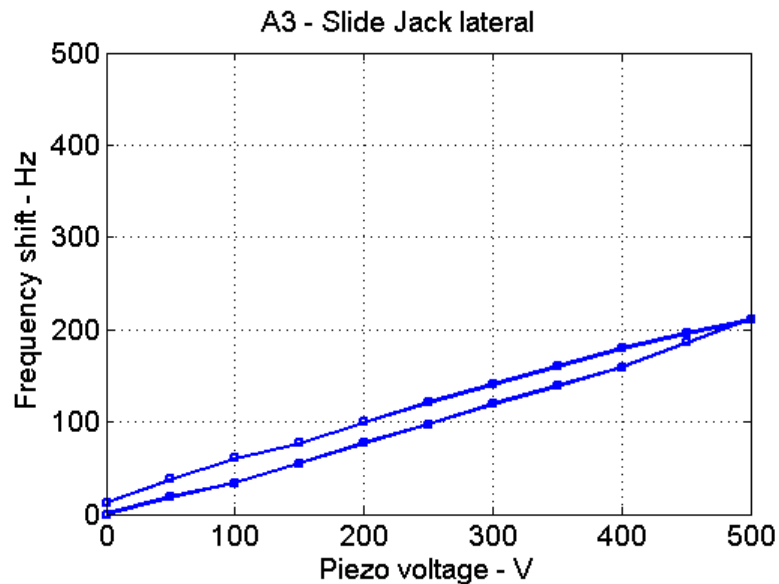
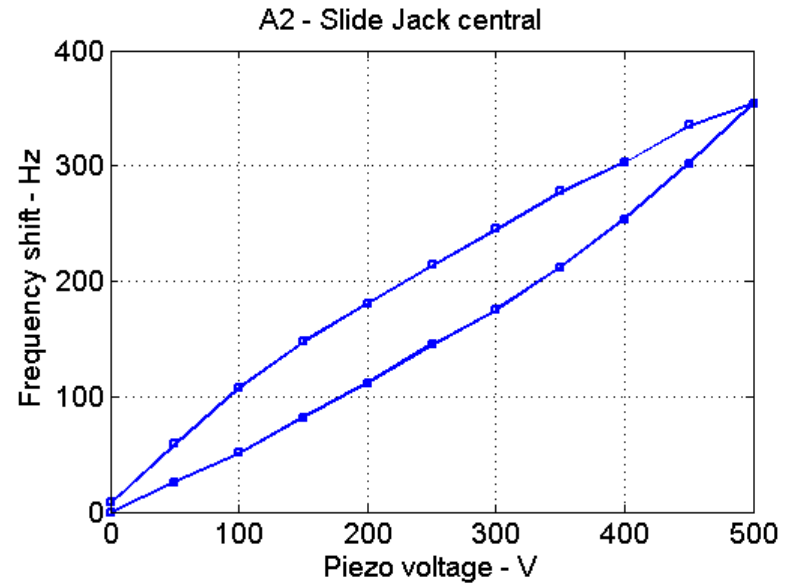
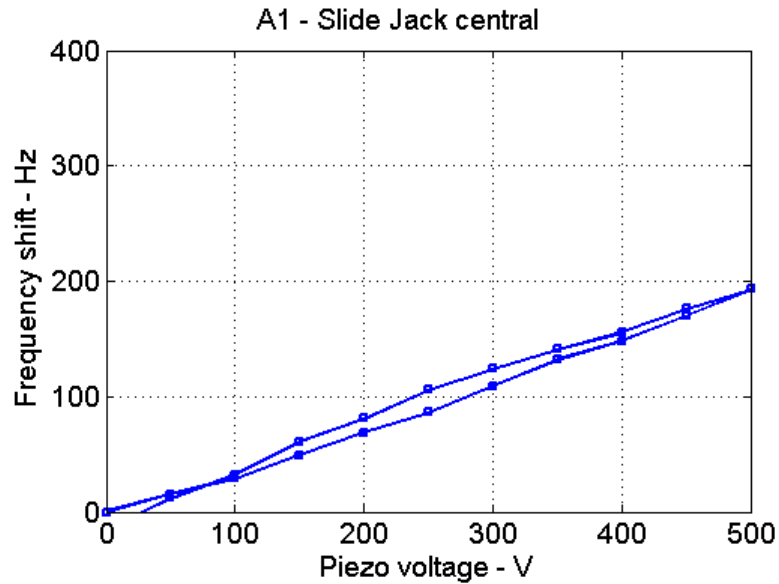


C4 - Z109 - DESY - Piezo 1





Piezo DC response – module A





DC response analyses results

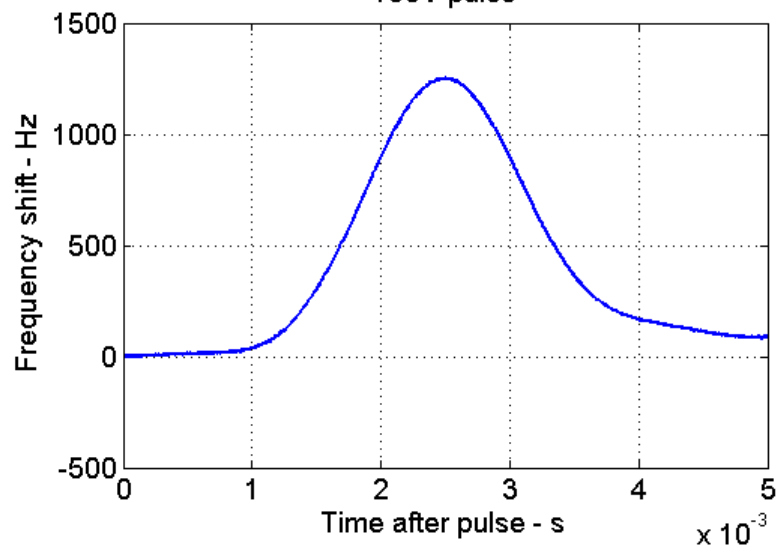
Table resumes piezo DC tuning results, the best piezo configuration is considered for module C cavities:

Cavity	Tuner	Maximum nominal piezo voltage [V]	Piezo configuration	Max applied voltage [V]	Frequency shift [Hz]
C1 – FNAL	Blade	200	1+2	200	2650
C2 – FNAL	Blade	200	1	200	610
C3 – DESY	DESY/Saclay	200	2	200	1010
C4 – DESY	DESY/Saclay	200	1	200	1060
A1 – KEK	Slide Jack cent.	500	-	500	190
A2 – KEK	Slide Jack cent.	500	-	500	350
A3 – KEK	Slide Jack lat.	500	-	500	210
A4 – KEK	Slide Jack lat.	500	-	500	450

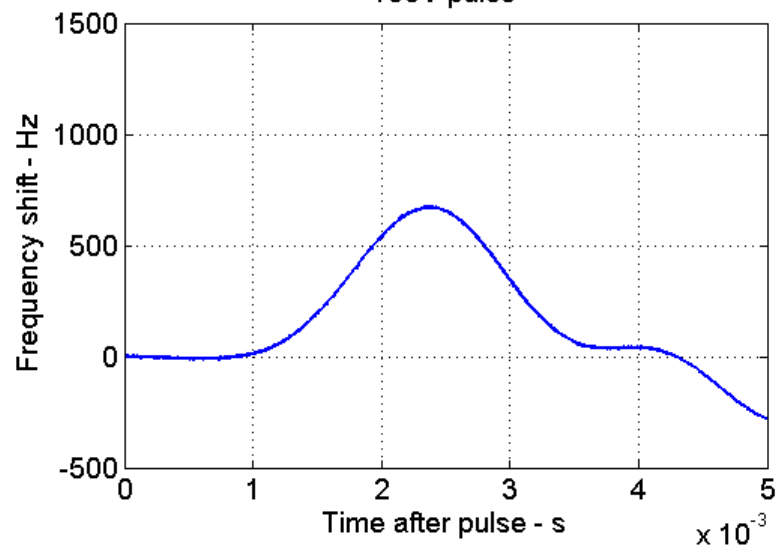


SIN pulse response – module C

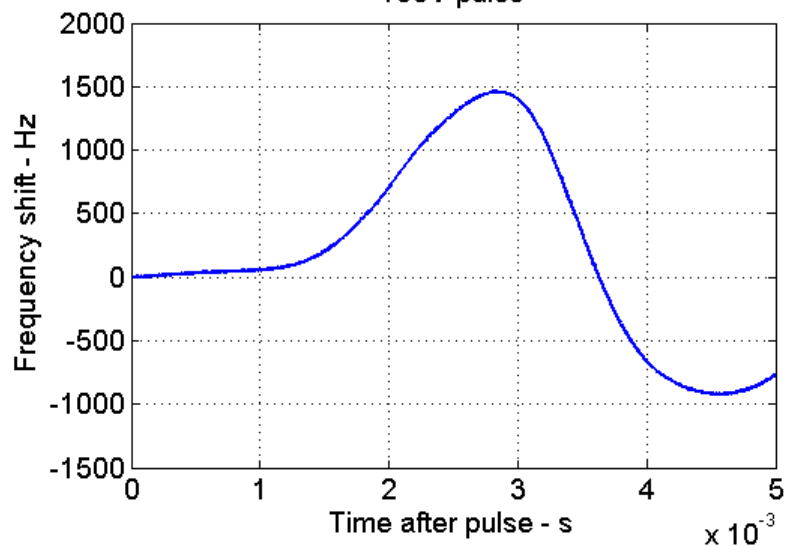
C1 - AES004 - Blade - Piezo 1+2
135V pulse



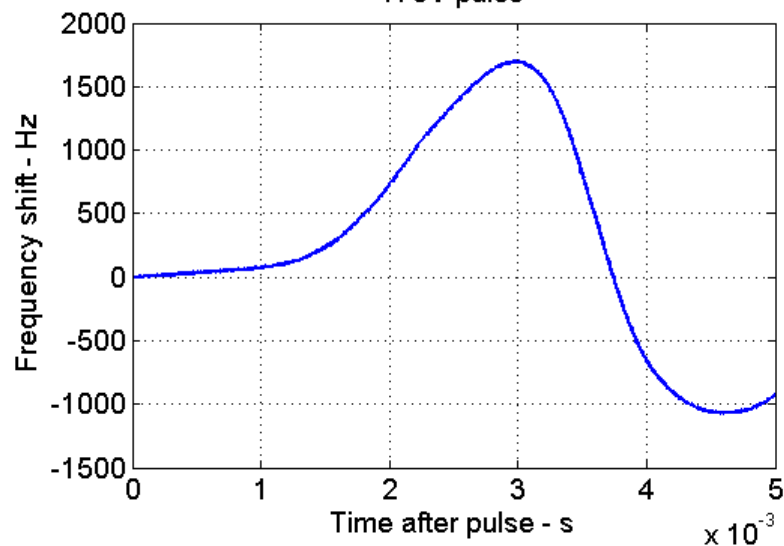
C2 - ACC011 - Blade - Piezo 1+2
100V pulse



C3 - Z108 - DESY - Piezo 2
180V pulse



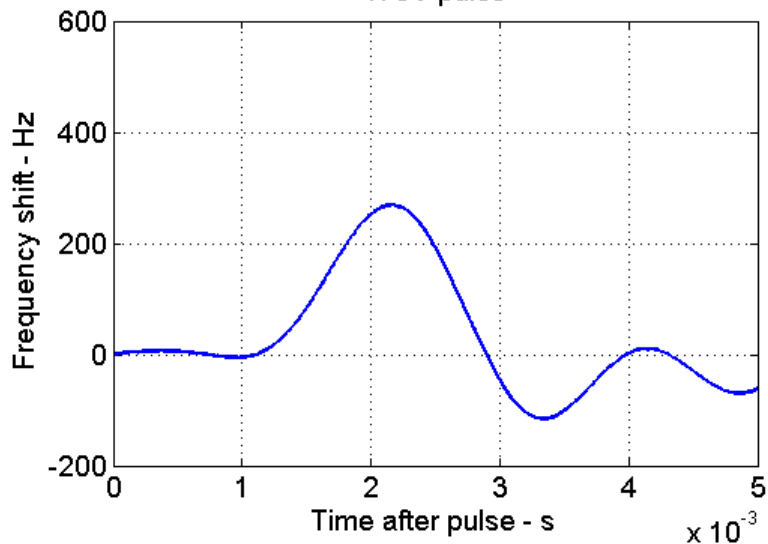
C4 - Z109 - DESY - Piezo 1
170V pulse



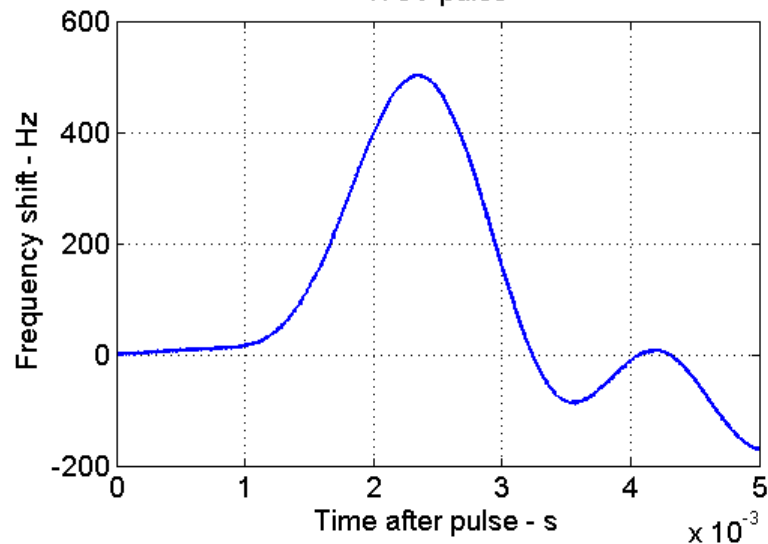


SIN pulse response – module A

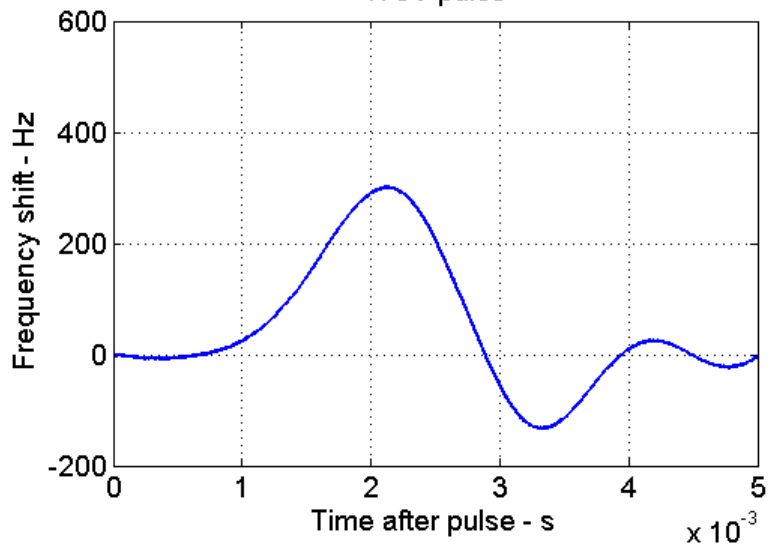
A1 - Slide Jack central
470V pulse



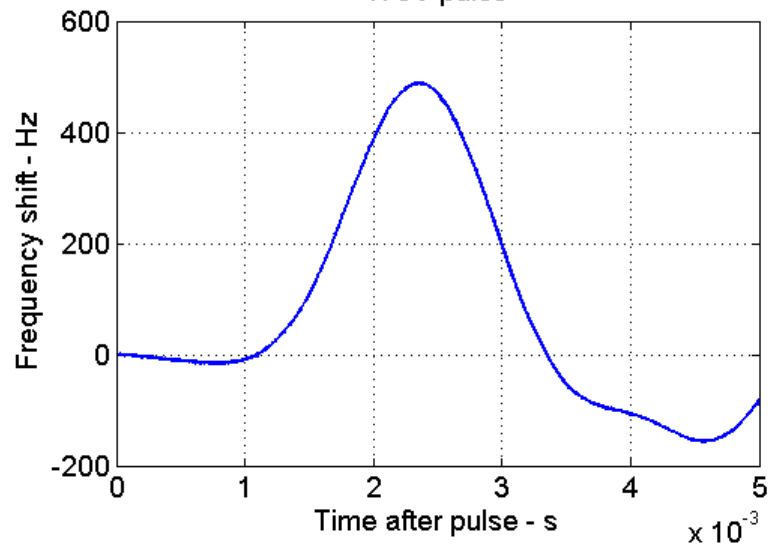
A2 - Slide Jack central
470V pulse



A3 - Slide Jack lateral
470V pulse

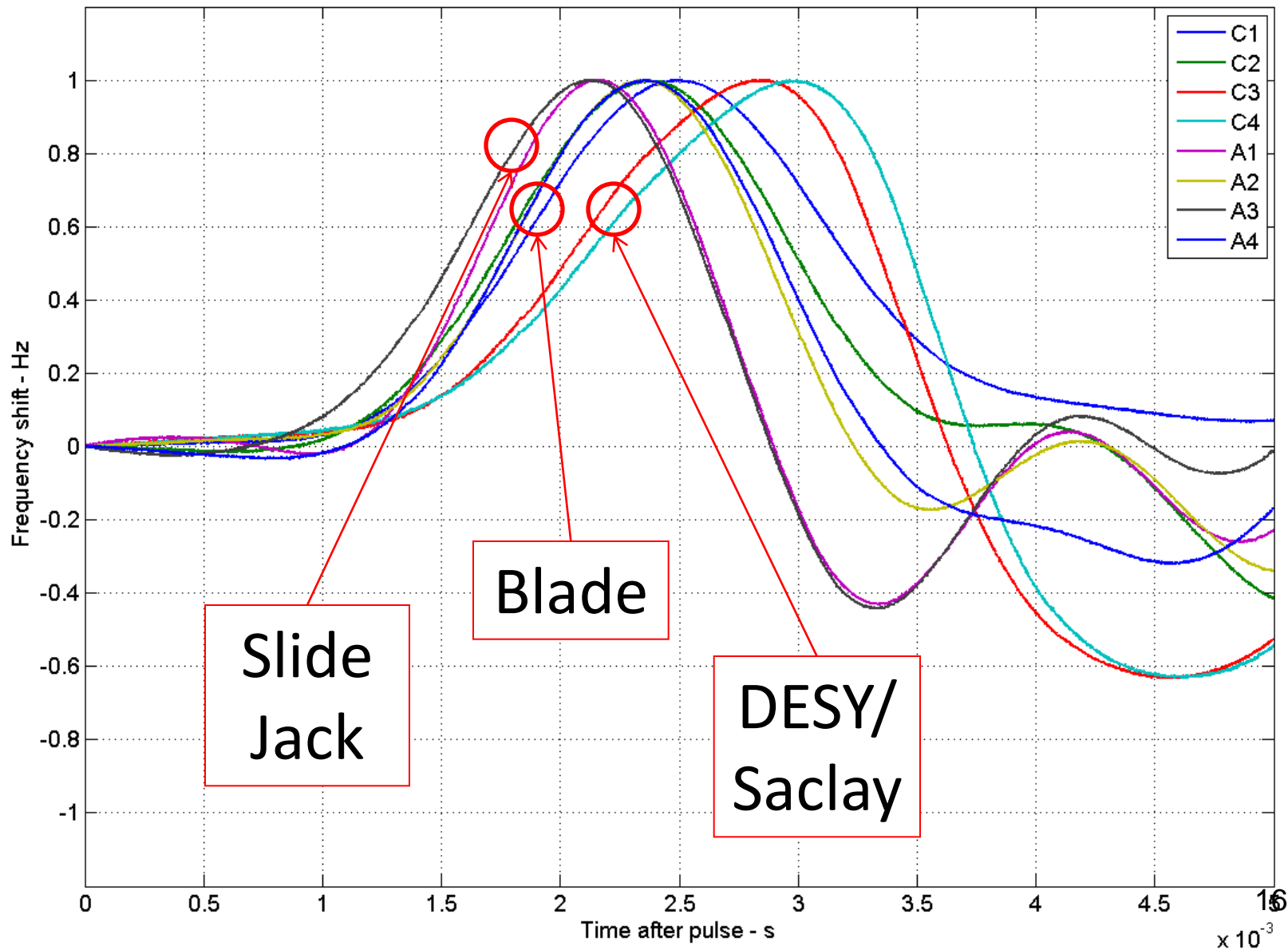


A4 - Slide Jack lateral
470V pulse



SIN pulse response – All

SIN pulse response - All tuners with scaling factor





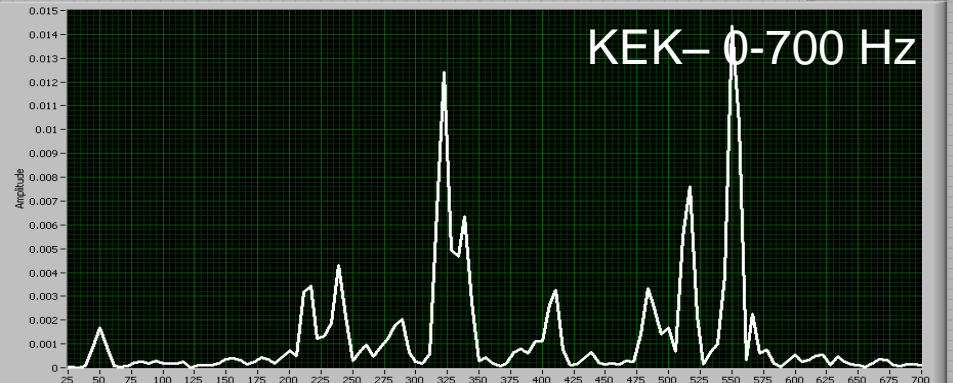
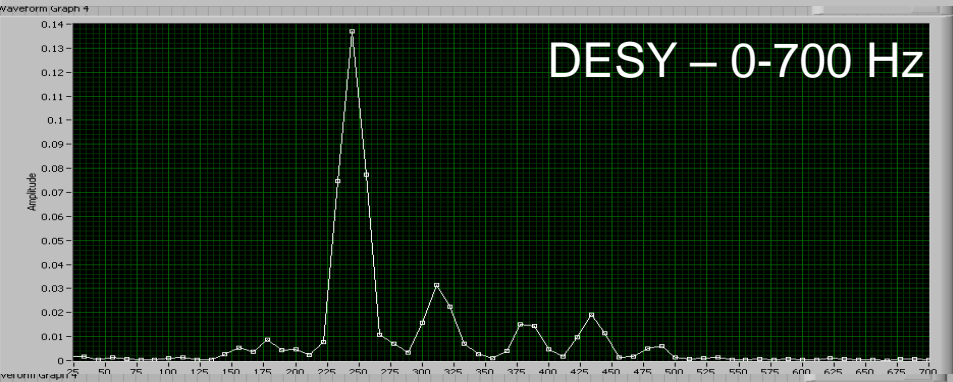
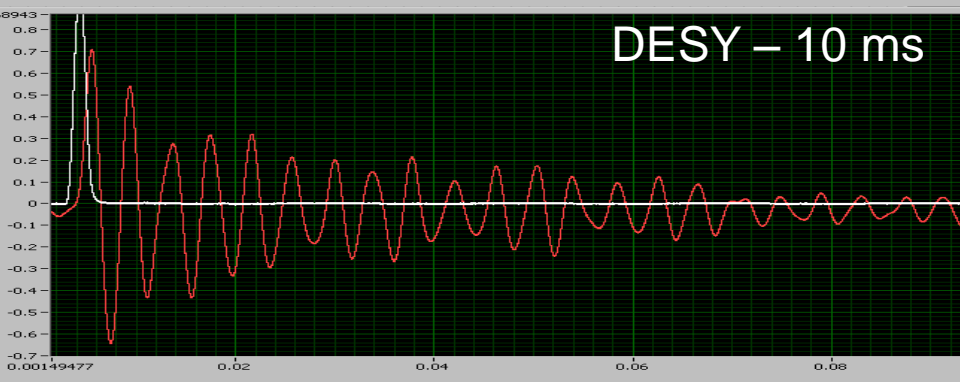
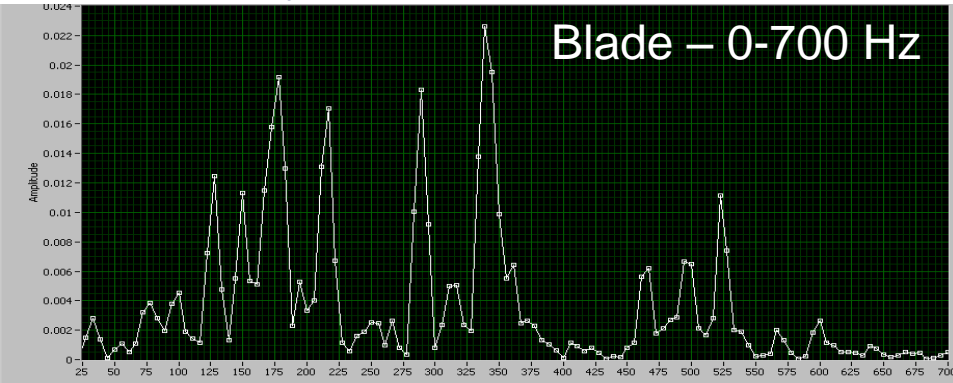
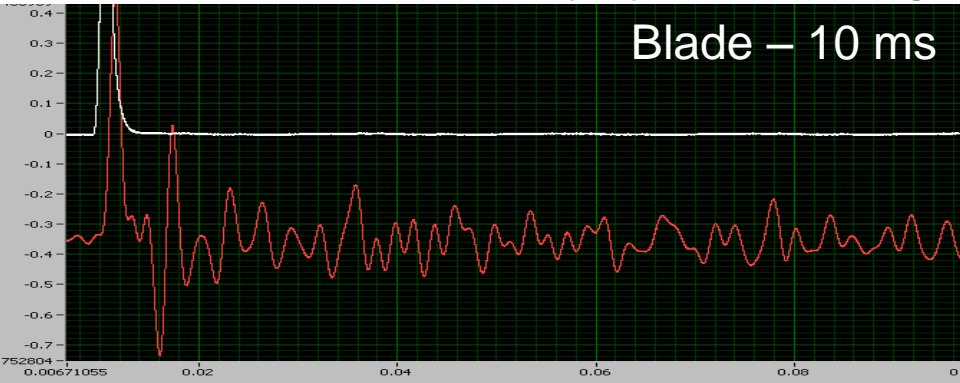
SIN pulse analyses results

Cavity - Tuner	Maximum piezo voltage [V]	Load C at 2 K [μ F]	Piezo conf.	SIN pulse amp. [V]	Max. Freq. shift in 1 ms [Hz]	Best lead time from pulse start [ms]	Dynamic / Static detuning ratio
C1-FNAL Blade	200	4.1	1+2	135	1040	1.31	0.6
C2-FNAL Blade	200	3.9	1+2	100	590	1.24	1
C3-DESY DESY/Saclay	200	2.0	2	180	1100	1.58	1.2
C4-DESY DESY/Saclay	200	1.9	1	170	1170	1.64	1.3
A1-KEK S. Jack cent.	500	0.19	-	470	270	1.10	1.5
A2-KEK S. Jack cent.	500	0.21	-	470	450	1.26	1.4
A3-KEK S. Jack lat.	500	0.20	-	470	270	1.03	1.3
A4-KEK S. Jack lat.	500	0.21	-	470	450	1.22	1.1



Additional dynamic analyses

On a larger time scale, piezo response analyses reveal details of intrinsic dynamics of different cavity systems through FFT (courtesy of Y. Pischalnikov):





Dynamic analyses comments - 1

- Plain piezo issues in C2 (still unexplained):
 - **Severe lack of mechanical coupling on both piezo**
 - **Piezo 2 discharging at lower voltage, not seen at RT.**
 - **Puzzling scenario: possibly correlated to static tuning failure?**
- Assuming DESY design as a reference, the other two systems rely on two different design concepts. These could be named as:
 - **“*Small external stiffness guideline*” for the Blade Tuner:**
 - Simple and light cavity constraints, and therefore the same for the tuner
 - achieve a large LFD compensation capability as required
 - **“*High external stiffness guideline*” for the Slide Jack Tuner:**
 - Strong and stiff cavity constraints, and therefore the same for the tuner
 - Minimize the amount of LFD to be compensated



Dynamic analyses comments - 2

- Collected data set is fully consistent with the scenario previously described:
 - **Very large DC stroke for the Blade Tuner piezo system (C1) if directly compared to module A tuners. Accordingly larger LFD expected (and measured, see next talk by Y. Pischnikov).**
 - **“Soft” Blade (and DESY actually) units systems act as low-bandwidth systems, with dominant modes placed at lower frequency and therefore longer rise-time.**
 - **“Stiff” KEK units act as high-bandwidth systems, with dominant modes at higher frequency and shorter rise-time.**
- Some other peculiarities emerged:
 - **Blade Tuner large DC tuning capabilities do not lead to equivalently high dynamic tuning capabilities. Both DESY and KEK systems took advantage in terms of static-to-dynamic detuning ratio:**
 - In DESY tuners case this is due to the purely harmonic response exhibited, sign of a clearly mechanically resonating cavity. This leads to a large dynamic overshoot when pulsing with piezo.
 - In KEK tuners case this is a direct effect of the system’s higher bandwidth.

- Globally speaking, all the four different tuning system design seemed to be able to accomplish their main goals:
 - **Statically tune the cavity with proper resolution**
 - **Ensure a dynamic piezo stroke sufficient to compensate the expected amount of LFD for that cavity, even in top-performance cavities**
- Severe failures emerged in some key components:
 - **Since motors, drives or piezo are well-known and (quite) affordable, the lack of experience with these brand new cavity systems could have played a major role.**
- High-power, pulsed RF test will clear the picture.
 - **See next talk from Y. Pischalnikov**