

Mechanical studies of CRY-04

A. Basti INFN-PISA
in collaboration with INFN-Milano

Outline:

- ❖ We made a first simple FEM of CRY-4 module using beam elements.
 - We used the dimensions and weights of CRY-4 design supply by the INFN-Milano group (P.Pierini and N.Panzeri).

- ❖ We used this model to study the Vacuum Vessel support positions and the normal modes of vibration.

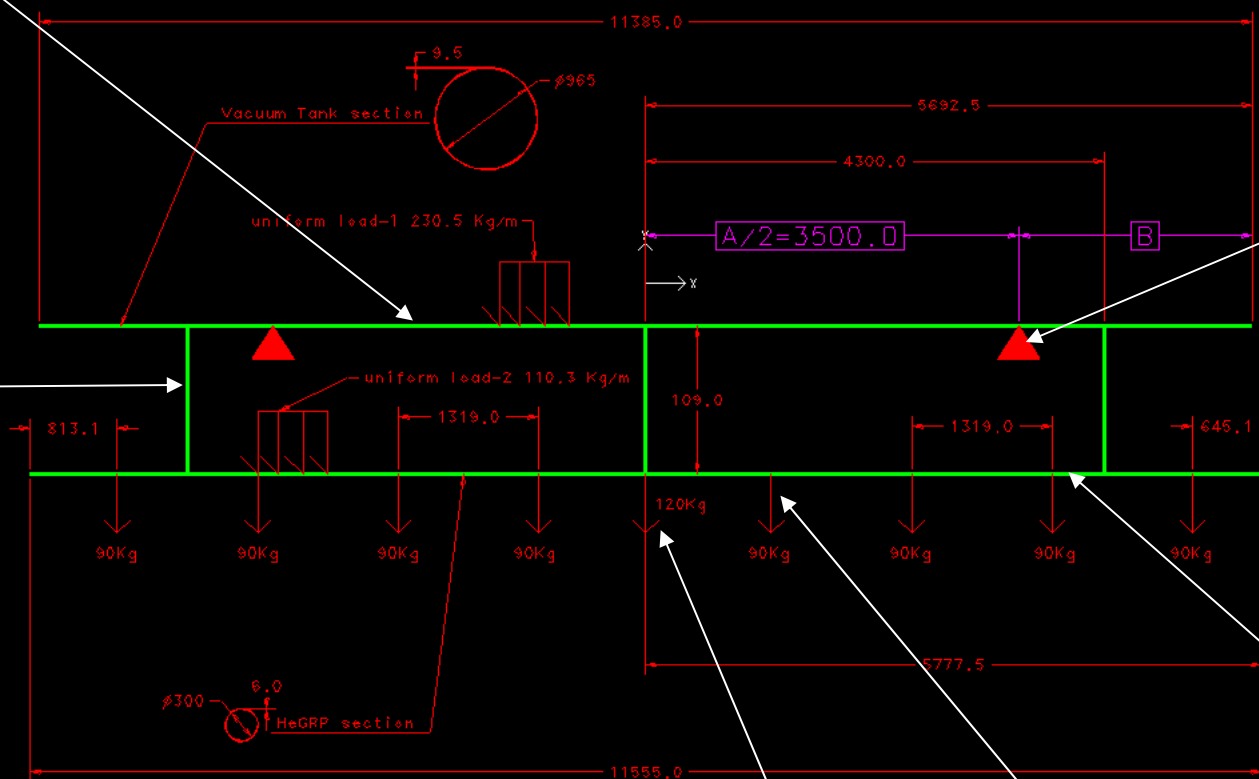
- ❖ Checks of ASME code compliance of Vacuum Vessel design.

Vacuum Vessel

CRYO-4 FEM BEAM MODEL-1

Vacuum Vessel supports

POST



uniform load-1 = vacuum tank weight 2625 kg
 uniform load-2 = HeGRP weight 530 Kg + shields weight 745 Kg
 90 Kg = cavity + shape weight
 120 Kg = quadrupole weight

Y

Z

Cavities

HeGRP

Quadrupole

Vacuum Vessel Supports

❖ Model:

- Horizontal vessel.
- Uniform vertical load applied (vessel weight + internal components).

❖ Solution:

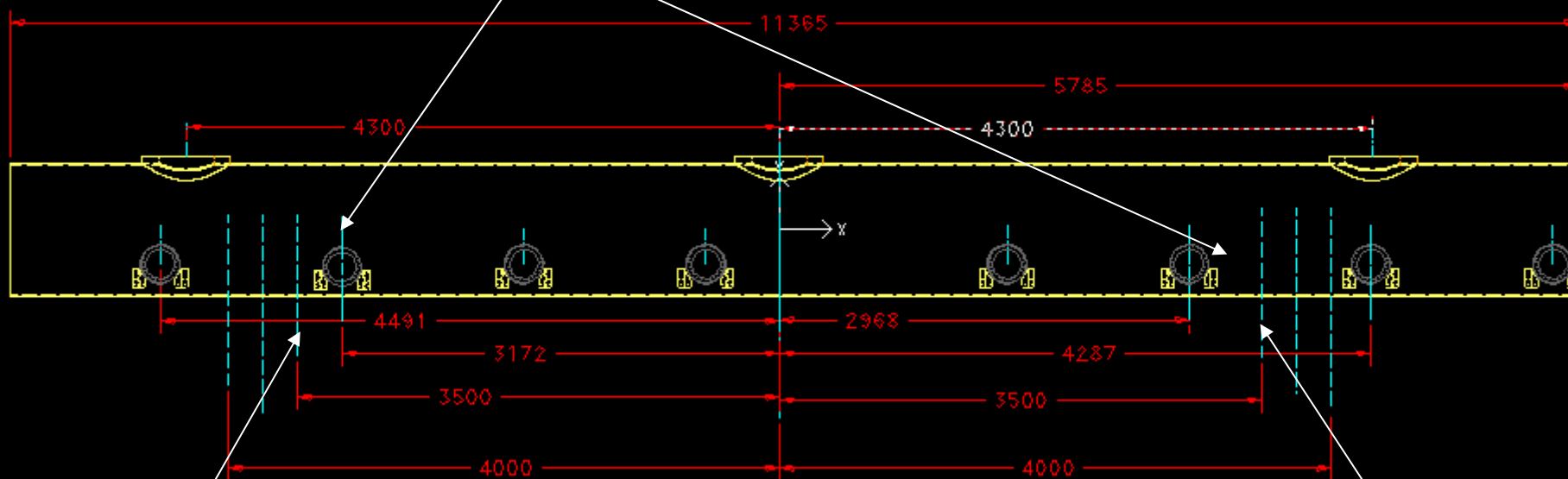
- two supports in symmetrical position with respect of central section. (isostatica solution, beam supported in two points).

❖ Optimization:

- Max bending moment equal in the centre and support sections.

CRY-4 Vacuum Vessel design

Analytical solution $A/2=3300$ mm



Vessel Support Position

Vessel Support Position

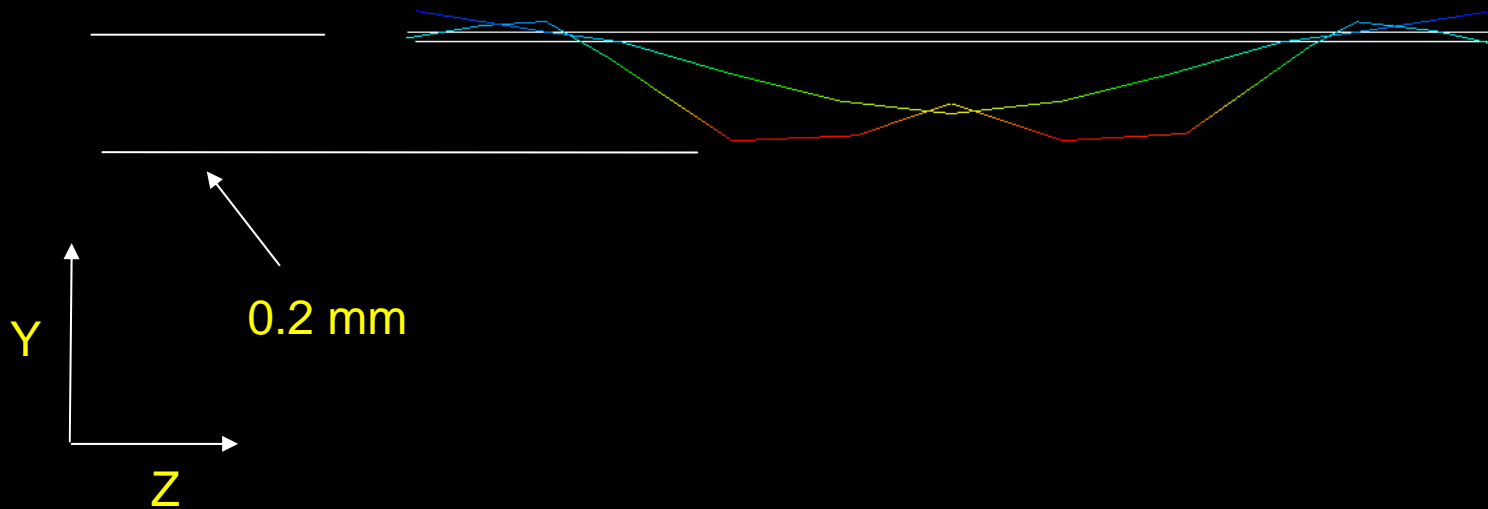
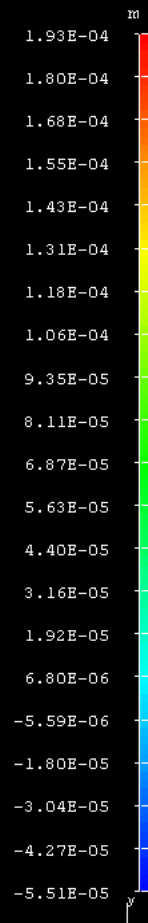
Using the FE model

- ❖ We use the FE beam model to calculate the displacements in the cases in which:
 - 1) we have only two support points,
 - at the distance from centre :
 - $A/2 = 3500$ mm
 - $A/2 = 3750$ mm
 - $A/2 = 4000$ mm
 - 2) We have three support points.
 - (one in the middle and two at 3500 from centre)

Displacements A/2=3500

```

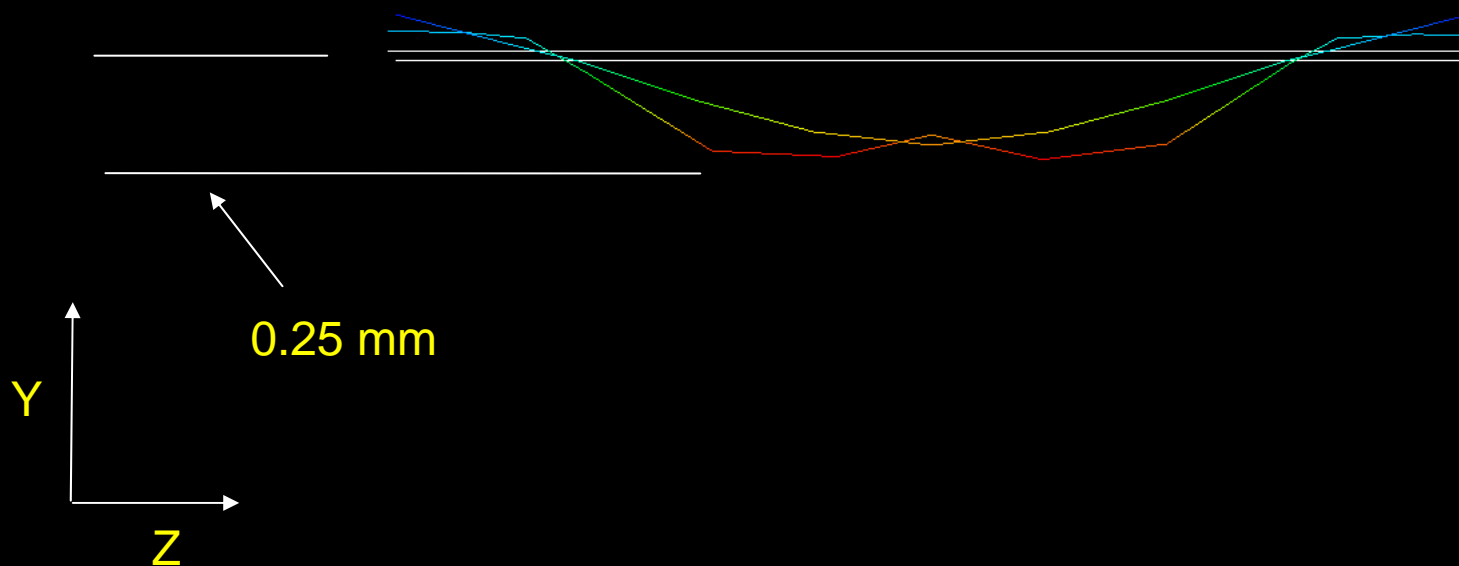
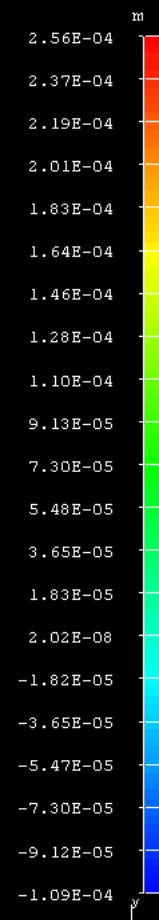
I-DEAS Visualizer
Display 1
Fem_statica
  B.C. 1,DISPLACEMENT_1,LOAD SET 1
D:\disegn11\CRY4revA_FEA.mfl
DISPLACEMENT Y Unaveraged Top shell
Min: -5.51E-05 m Max: 1.93E-04 m
  B.C. 1,DISPLACEMENT_1,LOAD SET 1
D:\disegn11\CRY4revA_FEA.mfl
DISPLACEMENT XYZ Magnitude
Min: 0.00E+00 m Max: 1.93E-04 m
Part Coordinate System
    
```



Displacements $A/2=3750$

```

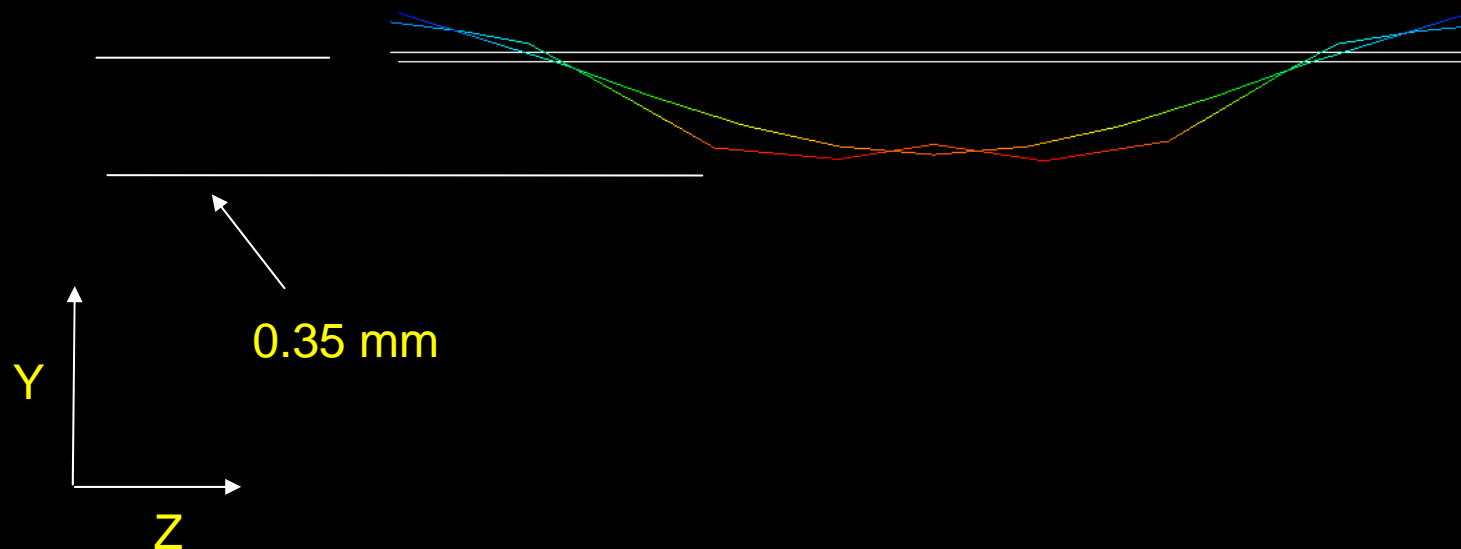
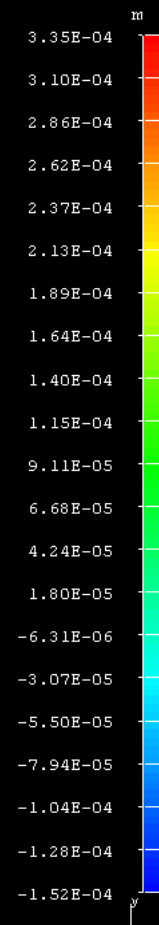
I-DEAS Visualizer
Display 1
Fem_statica
  B.C. 1,DISPLACEMENT_1,LOAD SET 1
  D:\disegnill\CRY4revA_FEA.mfl
  DISPLACEMENT Y Unaveraged Top shell
  Min: -1.09E-04 m Max: 2.56E-04 m
  B.C. 1,DISPLACEMENT_1,LOAD SET 1
  D:\disegnill\CRY4revA_FEA.mfl
  DISPLACEMENT XYZ Magnitude
  Min: 0.00E+00 m Max: 2.56E-04 m
  Part Coordinate System
    
```



Displacements A/2=4000

```

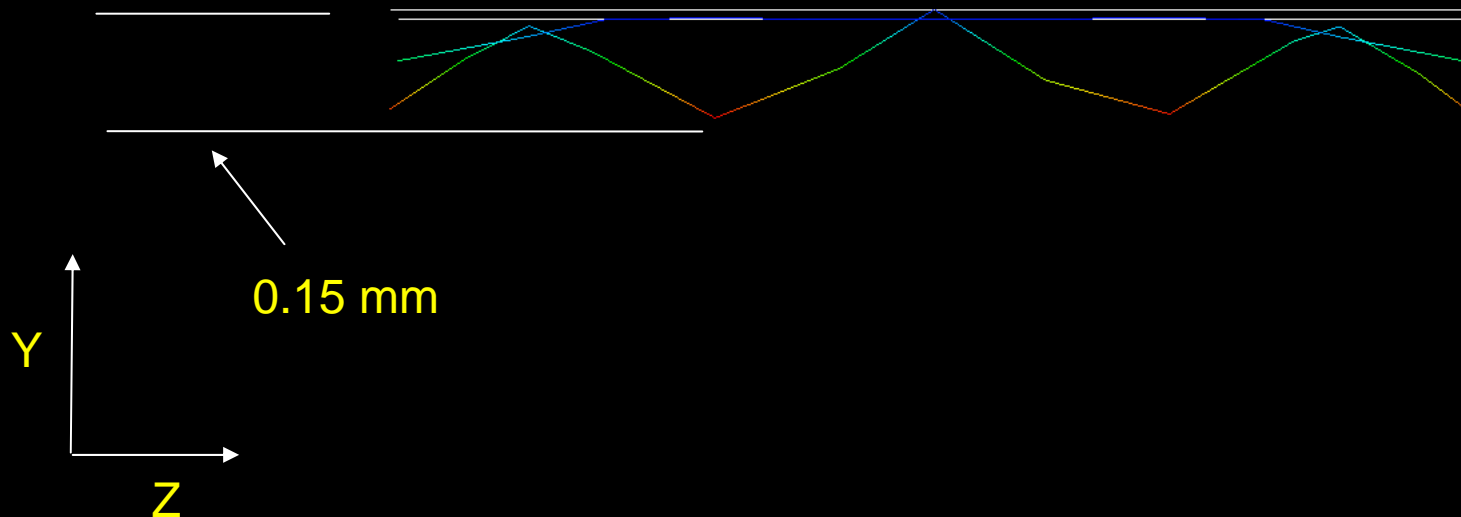
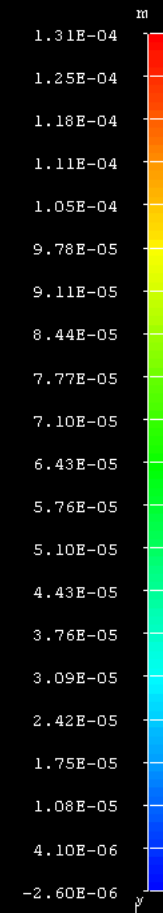
I-DEAS Visualizer
Display 1
Fem_statica
  B.C. 1,DISPLACEMENT_1,LOAD SET 1
  D:\disegnill\CRY4revA_FEA.mfl
  DISPLACEMENT Y Unaveraged Top shell
  Min: -1.52E-04 m Max: 3.35E-04 m
  B.C. 1,DISPLACEMENT_1,LOAD SET 1
  D:\disegnill\CRY4revA_FEA.mfl
  DISPLACEMENT XYZ Magnitude
  Min: 0.00E+00 m Max: 3.35E-04 m
  Part Coordinate System
    
```



Displacements - 3 support points

```

I-DEAS Visualizer
Display 1
Fem_statica
  B.C. 1,DISPLACEMENT_1,LOAD SET 1
  D:\disegn11\CRY4revA_FEA.mfl
DISPLACEMENT Y Unaveraged Top shell
Min: -2.60E-06 m Max: 1.31E-04 m
  B.C. 1,DISPLACEMENT_1,LOAD SET 1
  D:\disegn11\CRY4revA_FEA.mfl
DISPLACEMENT XYZ Magnitude
Min: 0.00E+00 m Max: 1.31E-04 m
Part Coordinate System
    
```



FEM Results:

	Max displacements
$A/2 = 3500$ mm	0.19 mm
$A/2 = 3750$ mm	0.25 mm
$A/2 = 4000$ mm	0.33 mm
Three points ($A/2=3500$)	0.13 mm

- ❖ The solution with three supports introduce several mechanical construction complication for a minimal gain.

Evaluation of normal mode of vibration

- ❖ We used the FE model to evaluate the normal modes in the case we have two support points ($A/2=3500$) and three support points.

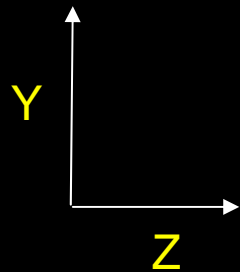
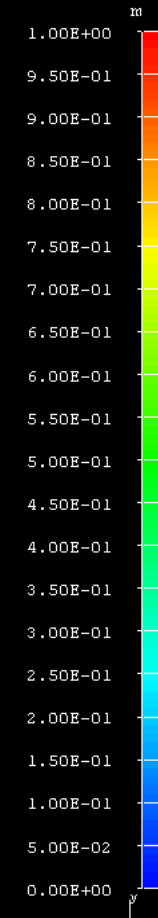
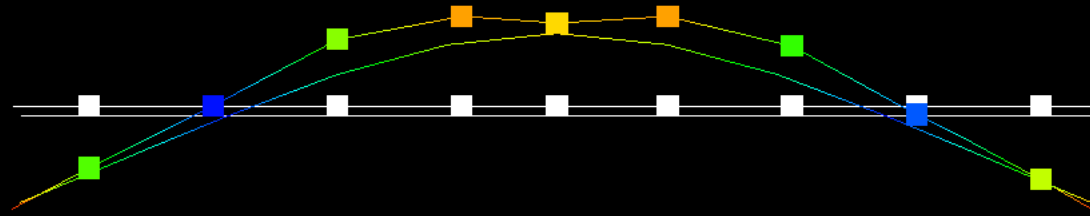
- ❖ In the FE model we have replaced the concentrate forces in the HeGRP nodes with lumped masses.

Normal Mode -1 (Y-Z plane) two support points

```

I-DEAS Visualizer
Display 1
Fem_frequenze_proprie
  B.C. 2,NORMAL_MODE 1,DISPLACEMENT_1
D:\disegn111\CRY4revA_FEA.mfl
DISPLACEMENT Magnitude Unaveraged Top shell
Min: 0.00E+00 m Max: 1.00E+00 m
  B.C. 2,NORMAL_MODE 1,DISPLACEMENT_1
D:\disegn111\CRY4revA_FEA.mfl
DISPLACEMENT XYZ Magnitude
Min: 0.00E+00 m Max: 1.00E+00 m
Part Coordinate System
Frequency: 3.49E+01 Hz
    
```

34.9 Hz

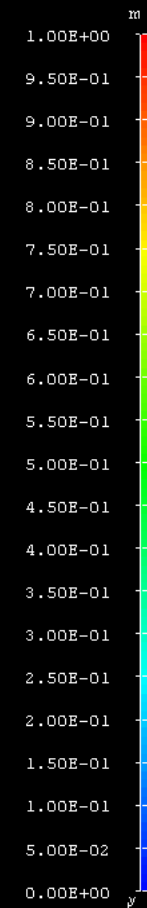
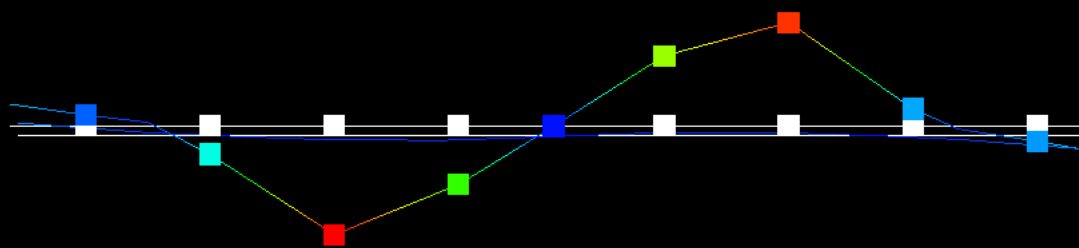
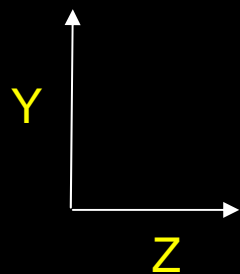


Normal Mode -3 (Y-Z plane) two support points

```

I-DEAS Visualizer
Display 1
Fem_frequenze_proprie
  B.C. 2,NORMAL_MODE 3,DISPLACEMENT_3
D:\disegn111\CRY4revA_FEA.mfl
DISPLACEMENT Magnitude Unaveraged Top shell
Min: 0.00E+00 m Max: 1.00E+00 m
  B.C. 2,NORMAL_MODE 3,DISPLACEMENT_3
D:\disegn111\CRY4revA_FEA.mfl
DISPLACEMENT XYZ Magnitude
Min: 0.00E+00 m Max: 1.00E+00 m
Part Coordinate System
Frequency: 6.14E+01 Hz
    
```

61.4 Hz

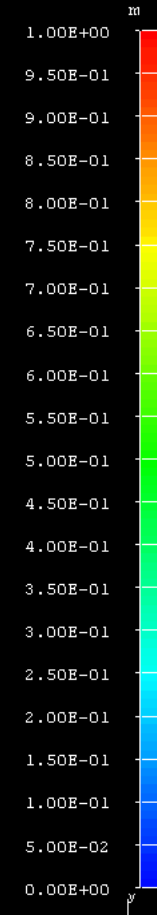
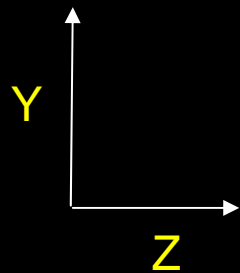
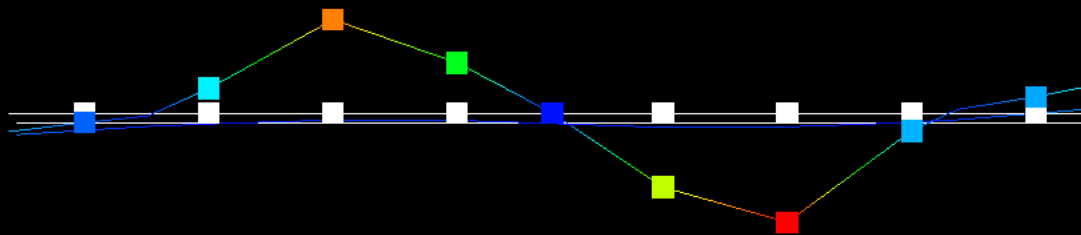


Normal Mode -1 (Y-Z plane) three support points

```

I-DEAS Visualizer
Display 1
Fem_frequenze_proprie
  B.C. 2,NORMAL_MODE 1,DISPLACEMENT_1
  D:\disegnill\CRY4revA_FEA.mfl
DISPLACEMENT Magnitude Unaveraged Top shell
Min: 0.00E+00 m Max: 1.00E+00 m
  B.C. 2,NORMAL_MODE 1,DISPLACEMENT_1
  D:\disegnill\CRY4revA_FEA.mfl
DISPLACEMENT XYZ Magnitude
Min: 0.00E+00 m Max: 1.00E+00 m
Part Coordinate System
Frequency: 6.14E+01 Hz
    
```

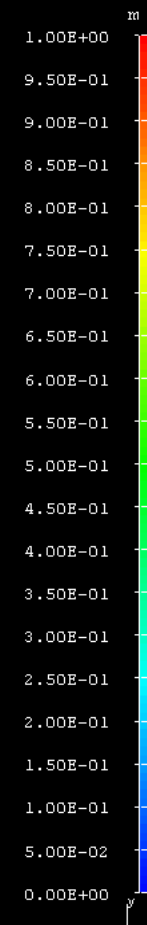
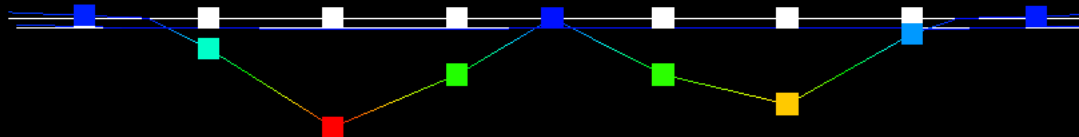
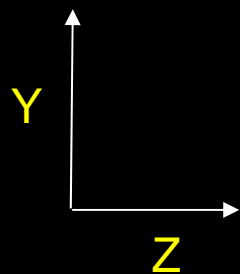
61.4 Hz



Normal Mode -3 (Y-Z plane) three support points

```
I-DEAS Visualizer
Display 1
Fem_frequenze_proprie
  B.C. 2,NORMAL_MODE 3,DISPLACEMENT_3
D:\disegn11\CRY4revA_FEA.mfl
DISPLACEMENT Magnitude Unaveraged Top shell
Min: 0.00E+00 m Max: 1.00E+00 m
  B.C. 2,NORMAL_MODE 3,DISPLACEMENT_3
D:\disegn11\CRY4revA_FEA.mfl
DISPLACEMENT XYZ Magnitude
Min: 0.00E+00 m Max: 1.00E+00 m
Part Coordinate System
Frequency: 6.24E+01 Hz
```

62.4 Hz



Normal Frequencies

Two supports

1	34.9 Hz	(Y-Z plane)
2	57.2 Hz	(X-Z plane)
3	61.4 Hz	(Y-Z plane)
4	61.8 Hz	(X-Z plane)
5	65.0 Hz	(Y-Z plane)
6	71.6 Hz	(X-Z plane)
7	86.6 Hz	(Y-Z plane)
8	92.2 Hz	(X-Z plane)
9	92.5 Hz	(Y-Z plane)
10	98.0 Hz	(X-Z plane)

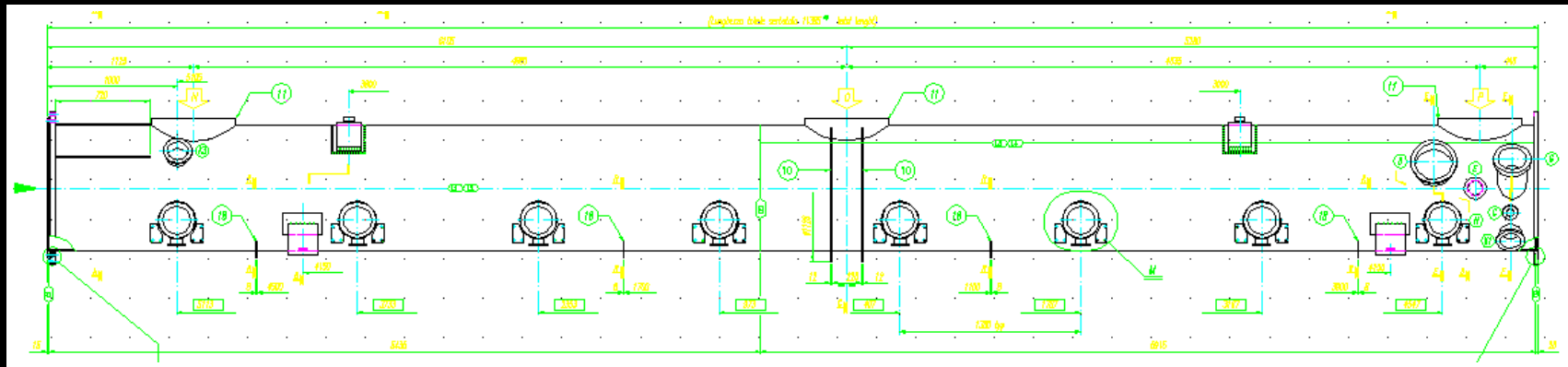
Three supports

1	61.4 Hz	(Y-Z plane)
2	62.3 Hz	(X-Z plane)
3	62.4 Hz	(Y-Z plane)
4	62.5 Hz	(X-Z plane)
5	70.2 Hz	(Y-Z plane)
6	75.4 Hz	(X-Z plane)
7	86.6 Hz	(Y-Z plane)
8	98.0 Hz	(X-Z plane)
9	124 Hz	(Y-Z plane)
10	134 Hz	(X-Z plane)

Checks of ASME code compliance of Vacuum Vessel design

- ❖ ASME Code Sect. VIII division 1.
- ❖ Reference drawing: Cry-3 module (released for prototype fabrication).
- ❖ Verifications done:
 - Max allowable pressure
 - Minimum thickness required for Vessel
 - Nozzle thickness check
 - Calculation of the opening reinforcing area

CRY-3 Vacuum Vessel design:



Material data:

(H II DIN 17155 corresponding SA516 gr. 60)

$Y_s := 32 \cdot 10^3 \text{ psi}$	$Y_s = 220.632 \times 10^6 \text{ Pa}$
$UTS := 60 \cdot 10^3 \text{ psi}$	$UTS = 413.685 \times 10^6 \text{ Pa}$
$E := 30 \cdot 10^6 \text{ psi}$	$E = 2.068 \times 10^{11} \text{ Pa}$

Geometric data:

- $Do = 952.6 \text{ mm}$ Outer Diameter
- $t = 9.52 \text{ mm}$ Thickness
- $L = 11385 \text{ mm}$ Length

Results:

- ❖ **Vacuum Vessel (considering the central ring as stiffener ring):**
 - Maximum Pressure $P_{\max} = 2.46 \text{ atm}$ ($P = 1 \text{ atm}$)
 - Minimum Thickness $T_{\min} = 6.5 \text{ mm}$ ($t = 9.52 \text{ mm}$)

- ❖ **Nozzle openings and reinforcing areas: (considering vessel extra thickness as reinforcing area)**

Nozzle Type	D_i Internal Diameter [mm]	t Actual thickness [mm]	t_r Required thickness [mm]	A_d Available Area [mm ²]	A_r Required Area [mm ²]
C	64	3	0.2	235.28	208
D	290	5	0.7	983.3	942.5
E	108.2	3.05	0.3	367.26	351.65
G	213	5	0.9	920.92	880.75
H	278	5	0.8	1150	1125
K1, K3	158.3	5	0.5	590.57	514.48

Conclusion

- ❖ The FE beam model is an useful model to study the CRY-4 design.
- ❖ We can use the standard solution (two supports) to support the vacuum vessel (like in the CRY-3 design).
- ❖ To minimize the displacements the distance of these two supports from the centre must be 3500 mm:
 - the max. calculated displacements are below 0.2 mm.
 - Neglected local vessel deformations.
 - System can be realigned after the installation.
 - Three supports are not needed.
- ❖ **Normal mode studies:**
 - Concerns about normal modes close to 60 Hz.
 - Needed more investigations.
- ❖ **Checks of ASME code compliance are almost completed.**
 - Easy to repeat these calculations for other vessel design.