



ILC Beam Dump Issues

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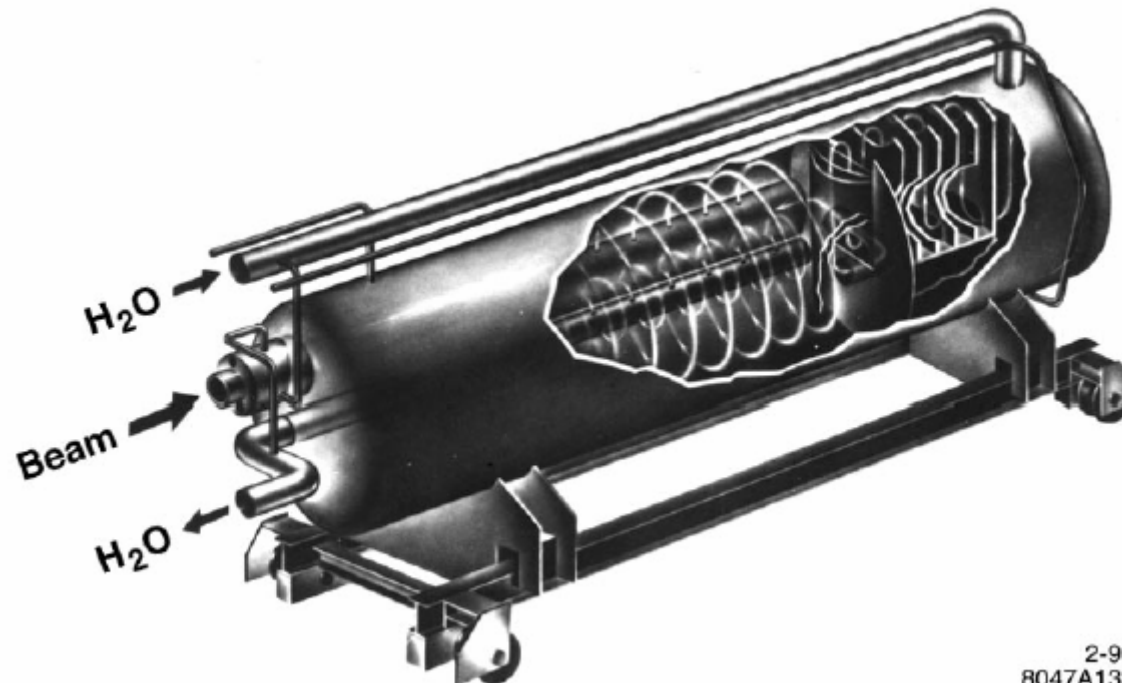
For SLAC BDS in particular, Clay Corvin, Eric Doyle & Dieter Walz

DESY/SLAC/UK Beam Dump Meeting @ DESY

16 February 2006

Historical Perspective

- **1996 - Dieter Walz, SLAC Dumps & Collimator guru, designs parameters of 10MW beam dump for NLC parameters based on existing 2MW water dump he built in 1967**
 - NLC ZDR, Ch.11A
 - <http://www.slac.stanford.edu/cgi-wrap/getdoc/slac-r-474-Ch11.pdf>



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Issues Raised

- **Water velocity ~ 1m/s so that in NLC case the water volume hit by the 192 bunch train moves at least 2σ during the interbunch 8.3ms period**
- **Temperature rise during that time sufficiently low to avoid boiling**
- **Size of tank adequate to absorb shower**
- **Window**
 - thin enough so that, assuming cooling by convection to water and some lateral conductive cooling, temperature rise during bunch train, less than stress limit
 - Small enough that thermal stress within limits for material
- **System to recover radioactive isotopes and hydrogen**

General Parameters

- **R=30cm where beam hits water flow**
- **Velocity(water) = 1-1.5 m/s**
- **Pressure water ~8atm so that T(boiling) ~ 160 °C**
- **Diameter vessel ~ 1.5m**
- **Length water ~ 6.5m (18 X_0)**
- **~ 1m high Z to absorb remainder of shower after water section**
- **30cm diameter 1mm thick Cu window**

Issues for ILC

- **Current/Area of undisturbed beam now higher**
 - especially before recent redesign of 20mrad extraction line
- **Bunch structure such that ~600 bunches pass before water moves ~200um at 1 m/s**
 - Peak temperature and thermal stress on window
- **Window size required set by size of disrupted beam**

At this time, emphasis has been on increasing bunch size so that energy absorbed by window during passage of ~600 bunches is < melting or fracture temperatures

We are just beginning an ANSYS analysis to evaluate window stress and temperature rise under various conditions

No results yet, but clearly a challenging problem

Beam Conditions at 20mrad Dumps

| CM Energy GeV | Parameters | Current uA | Power/Beam MW | Beamstrahlung MW | Undisrupted sig_x mm | sig_y mm |
|------------------|----------------|---------------|------------------|---------------------|----------------------------|-------------|
| 500 | Nominal | 45.1 | 11.3 | 0.3 | 0.87 | 0.10 |
| 500 | High | 45.1 | 11.3 | 0.8 | 1.25 | 0.12 |
| 1000 | Nominal | 36.1 | 18.0 | 0.9 | 0.51 | 0.35 |
| 1000 | High | 36.1 | 18.0 | 3.2 | 0.89 | 0.35 |

**Worst case for window:
(Current/beam area) 5x larger than in ZDR**

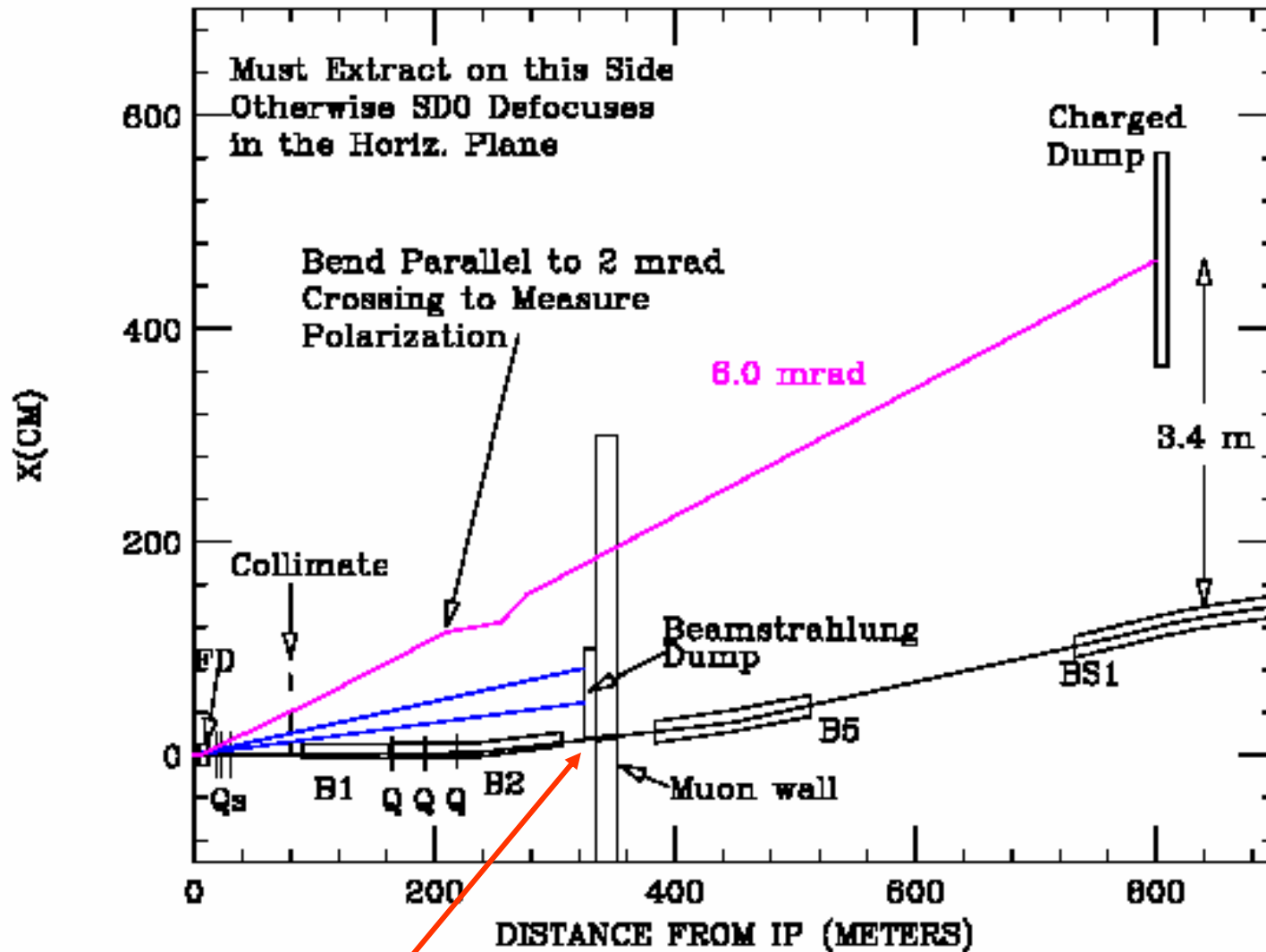
Notes from Beam Dump Meeting with Dieter Walz, April 21, 2005

- **Designing a survivable window is more of a challenge than designing a water dump to absorb 20 MW**
- **The ratio of current to beam area at the window is about 5x larger than in the 1996 ZDR. This factor leads to overheating of the window and the water which will cause immediate window failure.**
- **How to increase the beam size at the window?**
 - Safest** {
 1. Add ~100m drift to the extraction line
 2. Design the extraction line for larger beam at the dump
 3. Raster the beam with magnetic or electric fields
 4. Introduce metallic vapors into the beam pipe
 5. All of the above will require a donut collimator to catch the beamstrahlung and charged particle tails

Notes (continued)

- **Need to couple the beam line vacuum directly to the dump. This will necessitate putting fast valves into the extraction line.**
- **Offset the window with respect to the dump center to put the shower directly at the point of maximum water circulation. This requirement can be used to reduce the distance between the dump center and the incoming beam line.**
- **It would be prudent to include an automatic window exchange mechanism, a la Beam Dump East, since everything around the dump will be very hot.**
- **For the 2 mrad extraction line it should be relatively easy to put a beam pipe through the beamstrahlung dump for the incoming beam if that should prove necessary.**

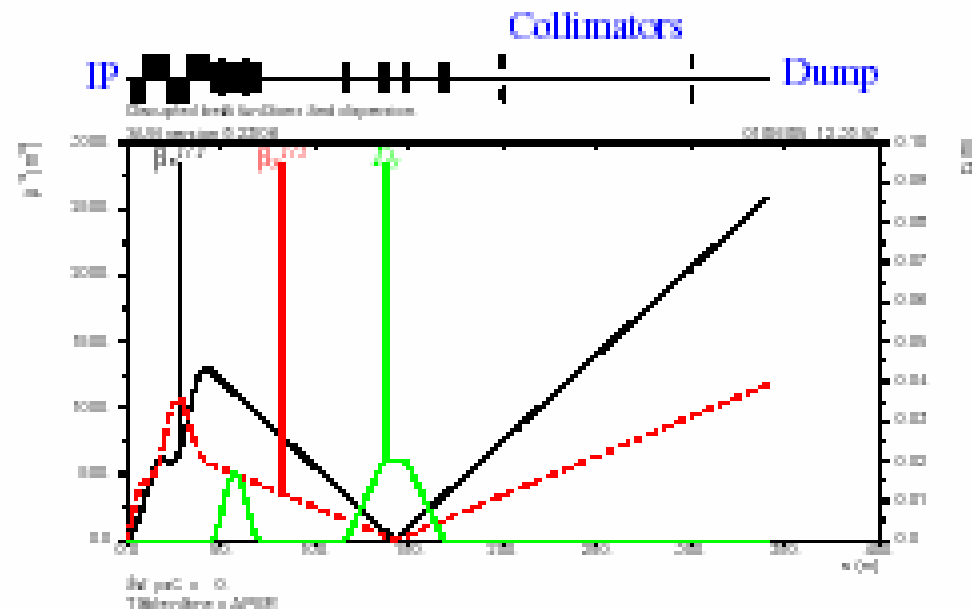
2 mrad Extraction Layout



Note proximity of beamstrahlung dump to the incoming beam – may need to put the incoming beam line pipe through the water tank.

20 MRAD EXTRACTION LINE WITH ENLARGED BEAM SIZE AT DUMP

- In the present optics, the undisrupted beam size at dump is too small for a practical dump design. At 0.5 TeV CM, the present value of undisrupted $\sigma_x \sigma_y = 0.87 \times 0.10 \text{ mm}^2$ at dump needs to be increased a factor of 10.
- The proposed solution is to allow the beam size grow naturally in a field-free region by moving the dump from $s = 200 \text{ m}$ to 340 m with respect to IP. Also, the quad doublet after the polarimeter chicane is removed to cancel focusing at the dump.
- To fit the divergent disrupted electron and beamstrahlung photon beams for the dump window, two round collimators with $r = 8.8 \text{ cm}$ and 13.2 cm are placed at $s \sim 200 \text{ m}$ and 300 m , respectively, to reduce maximum beam size at dump to $15 \times 15 \text{ cm}$.



Charged and Beamstrahlung Losses in the 20 mrad Extraction Line

| E_{CM} | y-offset (nm) | e-loss in collimators (kW) | | γ -loss in collimators (kW) | | Max. e-loss density in magnets (W/m) | | |
|----------------------|------------------|----------------------------|---------|------------------------------------|---------|--------------------------------------|------------|-------|
| | | Coll. 1 | Coll. 2 | Coll. 1 | Coll. 2 | SC quads | Warm quads | Bends |
| 0.5 TeV nominal | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 200 | 0 | 0 | 0.15 | 0.05 | 0 | 0 | 0.13 |
| 0.5 TeV high lumi | 0 | 47.4 | 74.5 | 2.8 | 0.7 | 15 (2.1*) | 60 | 37 |
| | 120 | 47.2 | 95.3 | 151 | 10.3 | 3.8 (0*) | 95 | 372 |
| 1 TeV nominal | 0 | 0.85 | 0 | 0 | 0 | 0 | 1.8 | 4.8 |
| | 100 | 4.8 | 0.11 | 0 | 0 | 0 | 7.1 | 77 |
| 1 TeV high lumi | 0 | 64.1 | 43.6 | 1.5 | 0.2 | 1106 | 4379 | 2032 |
| | 80 | 129 | 15.4 | 69 | 9.5 | 1071 | 5391 | 7362 |

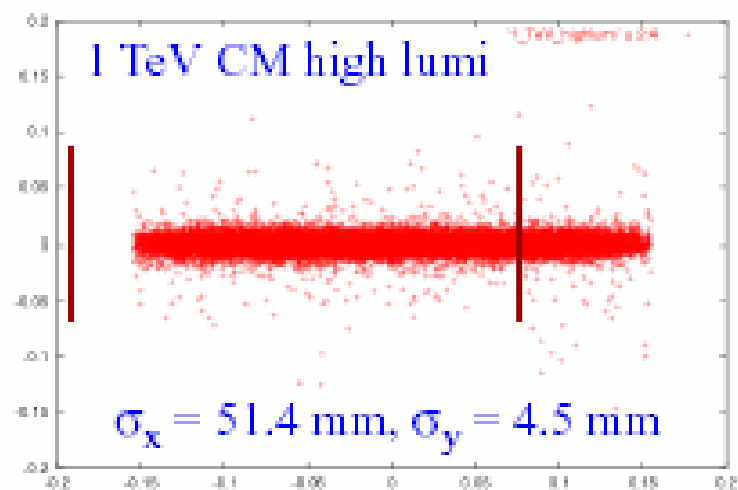
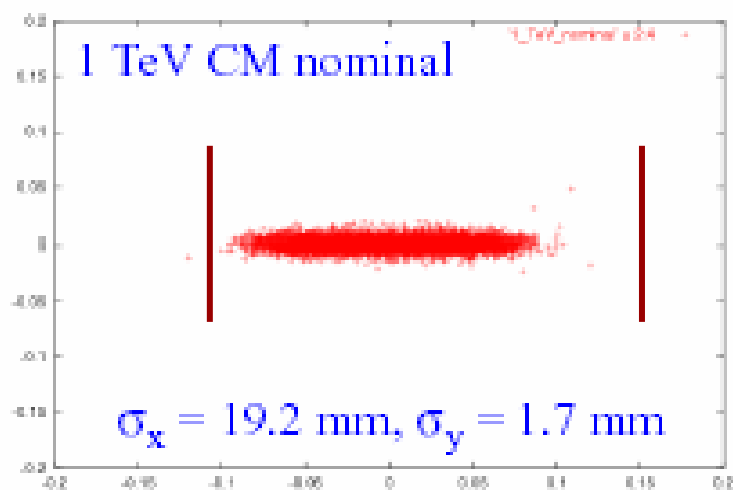
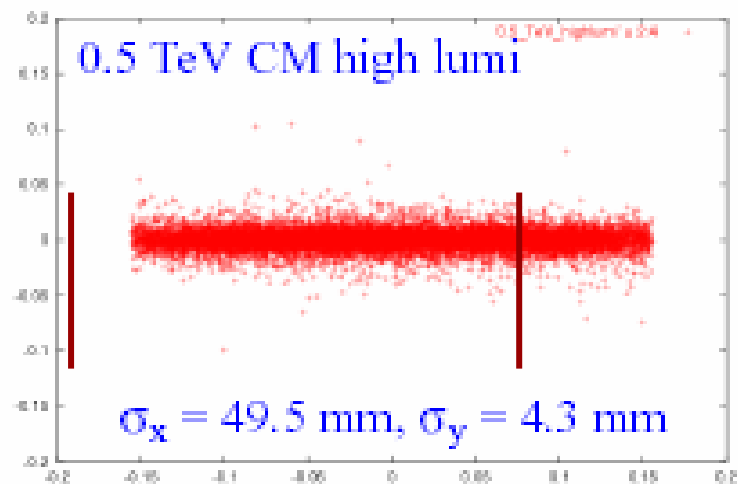
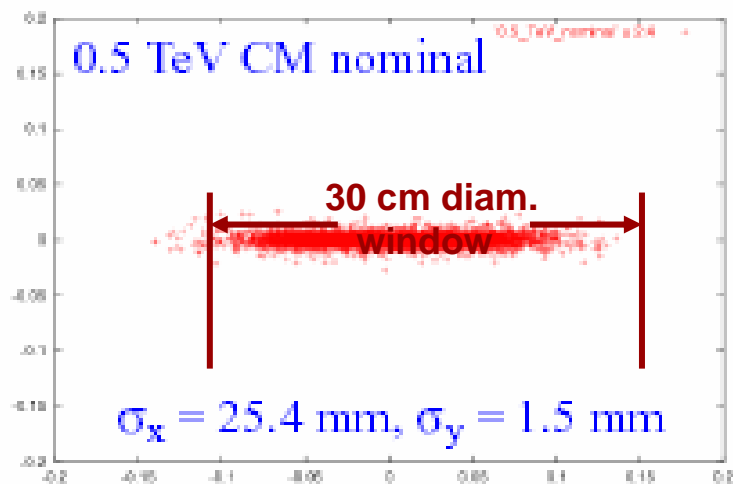
* After increasing aperture in QDEX1C and QFEX2A to $r = 25$ and 36 mm, respectively.

* Coll. 1 at 200 m, coll. 2 at 300 m, beam dump at 340 m

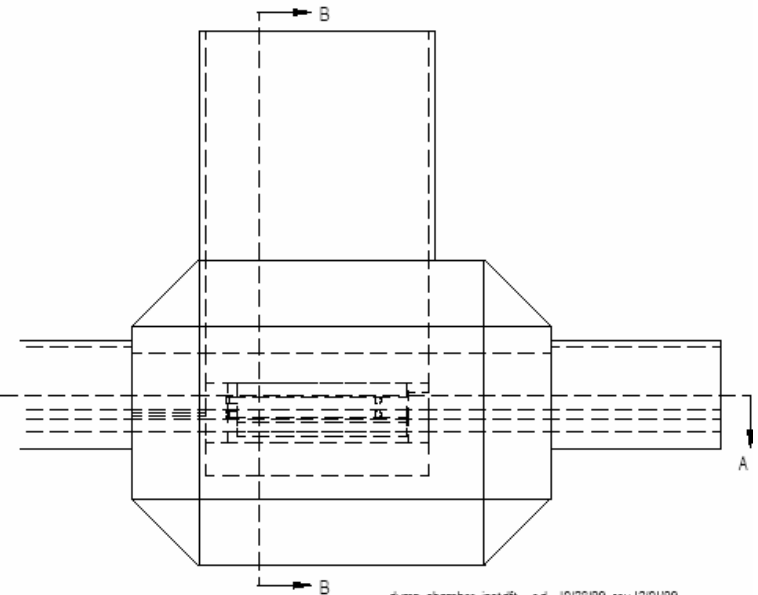
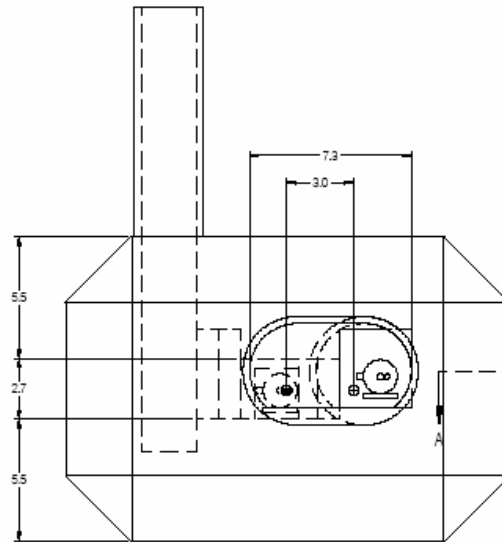
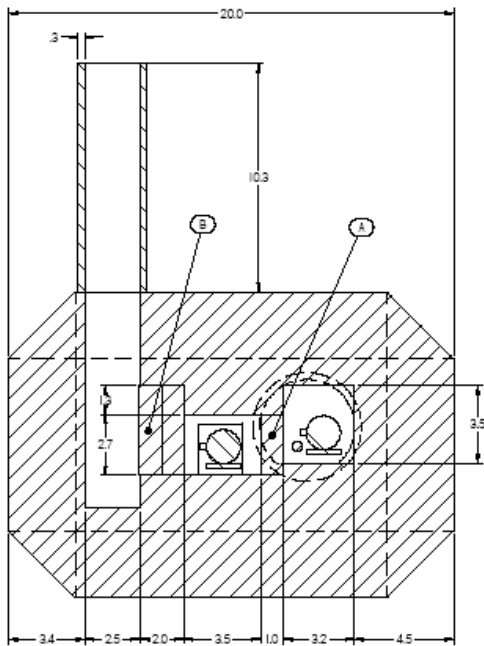
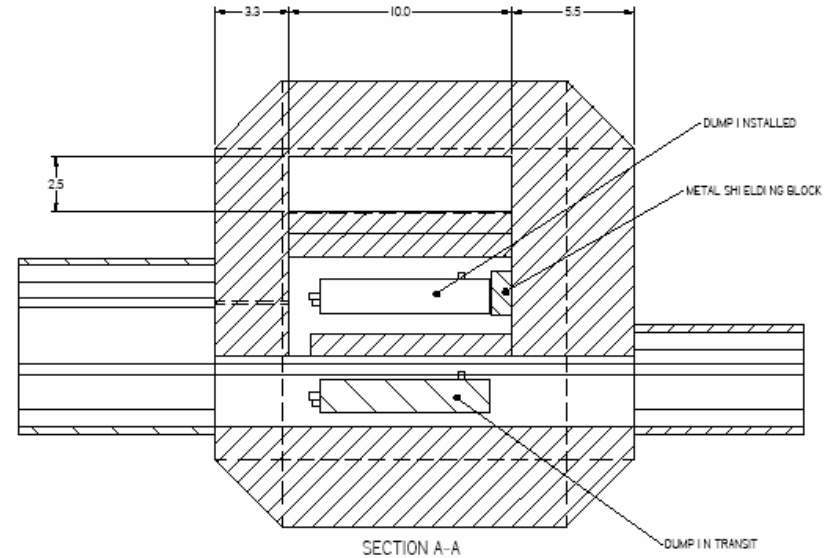
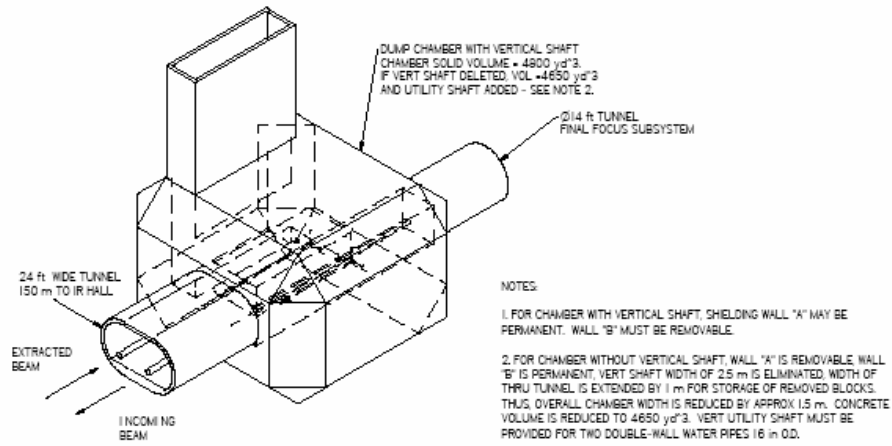
* Maximum beam size (charged and beamstrahlung) limited to ± 15 cm

X-Y disrupted distribution at dump (no IP offset)

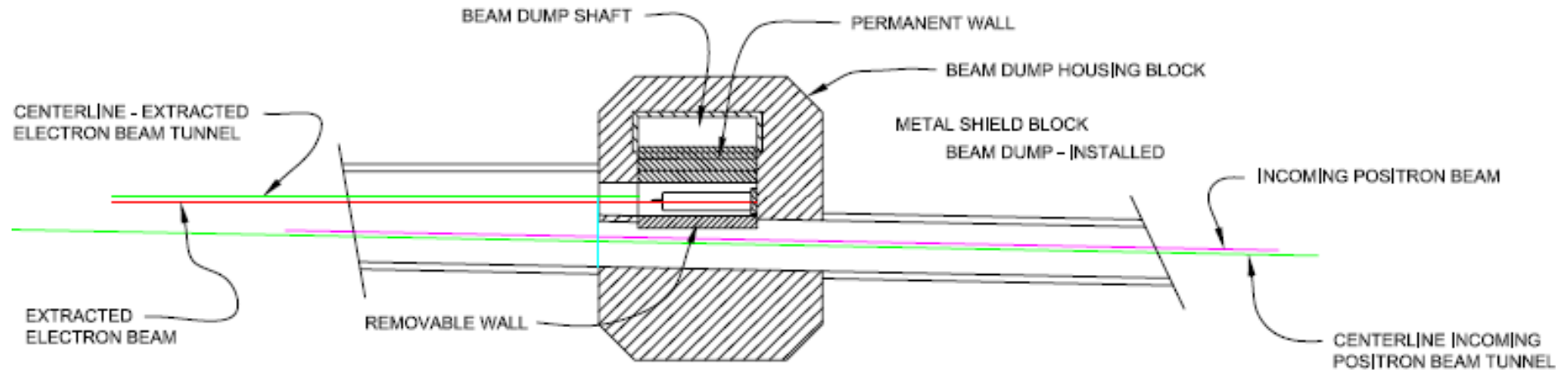
(scale in meters)



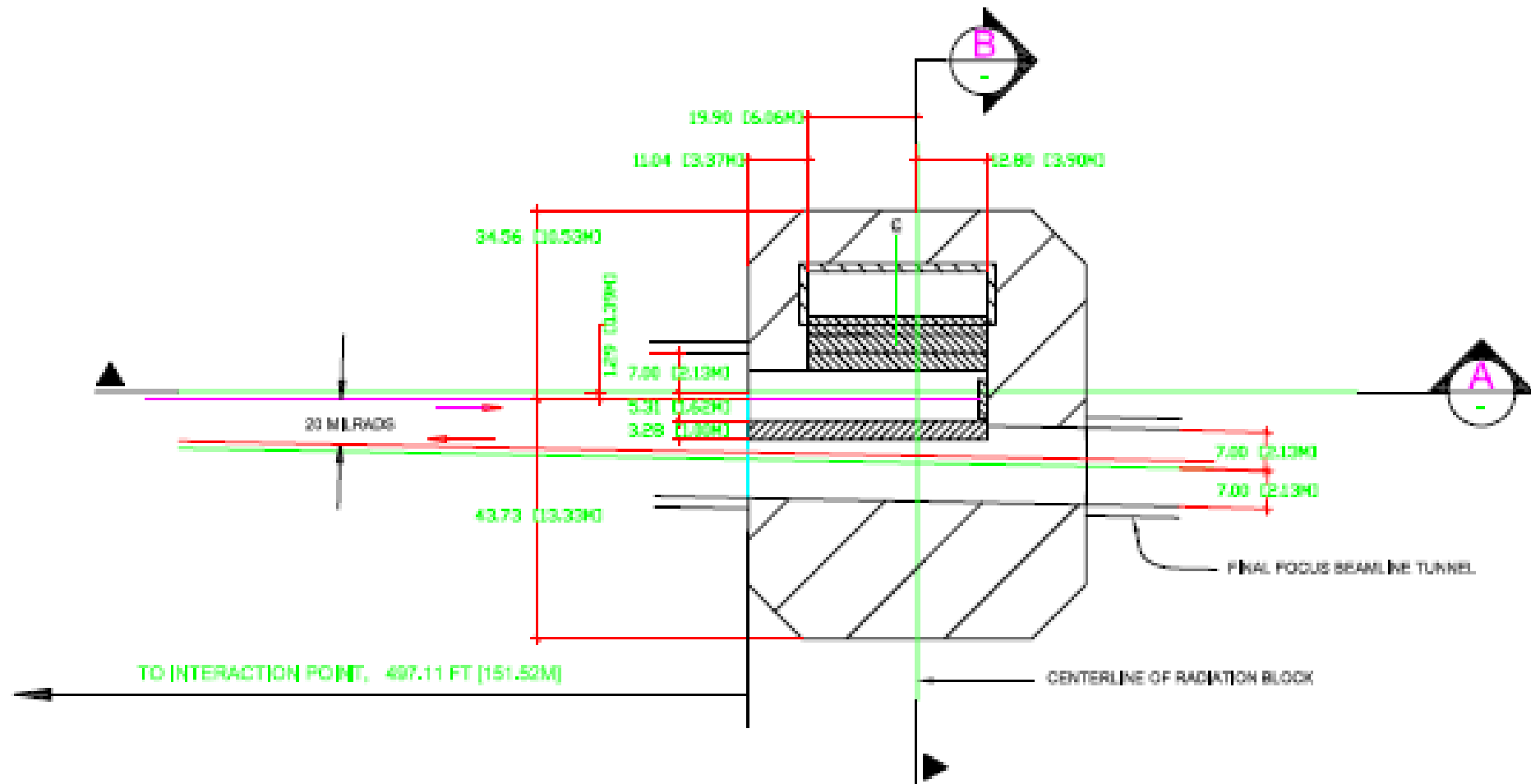
Beam Dump – Overview



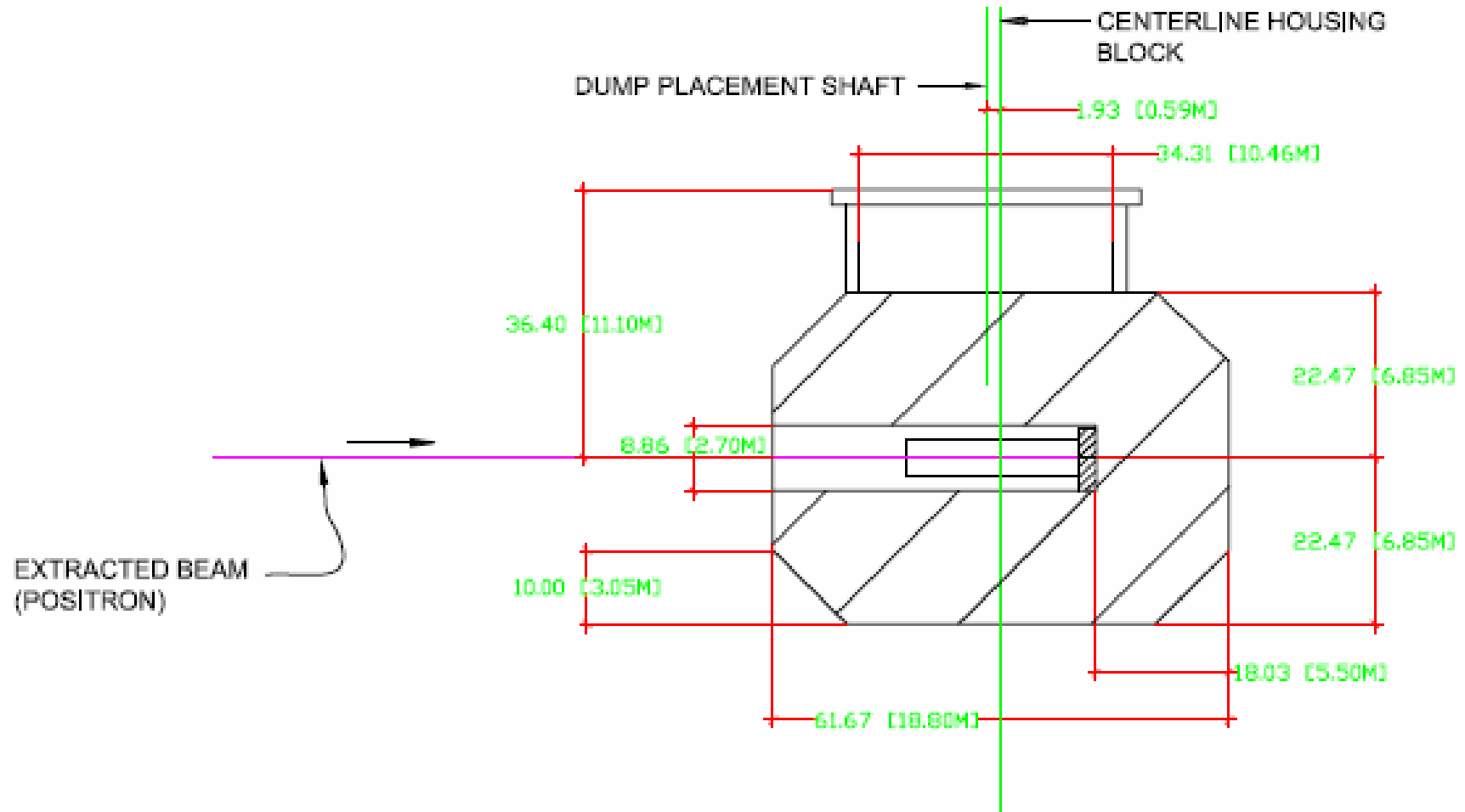
Beam Dump – General Arrangement Plan View



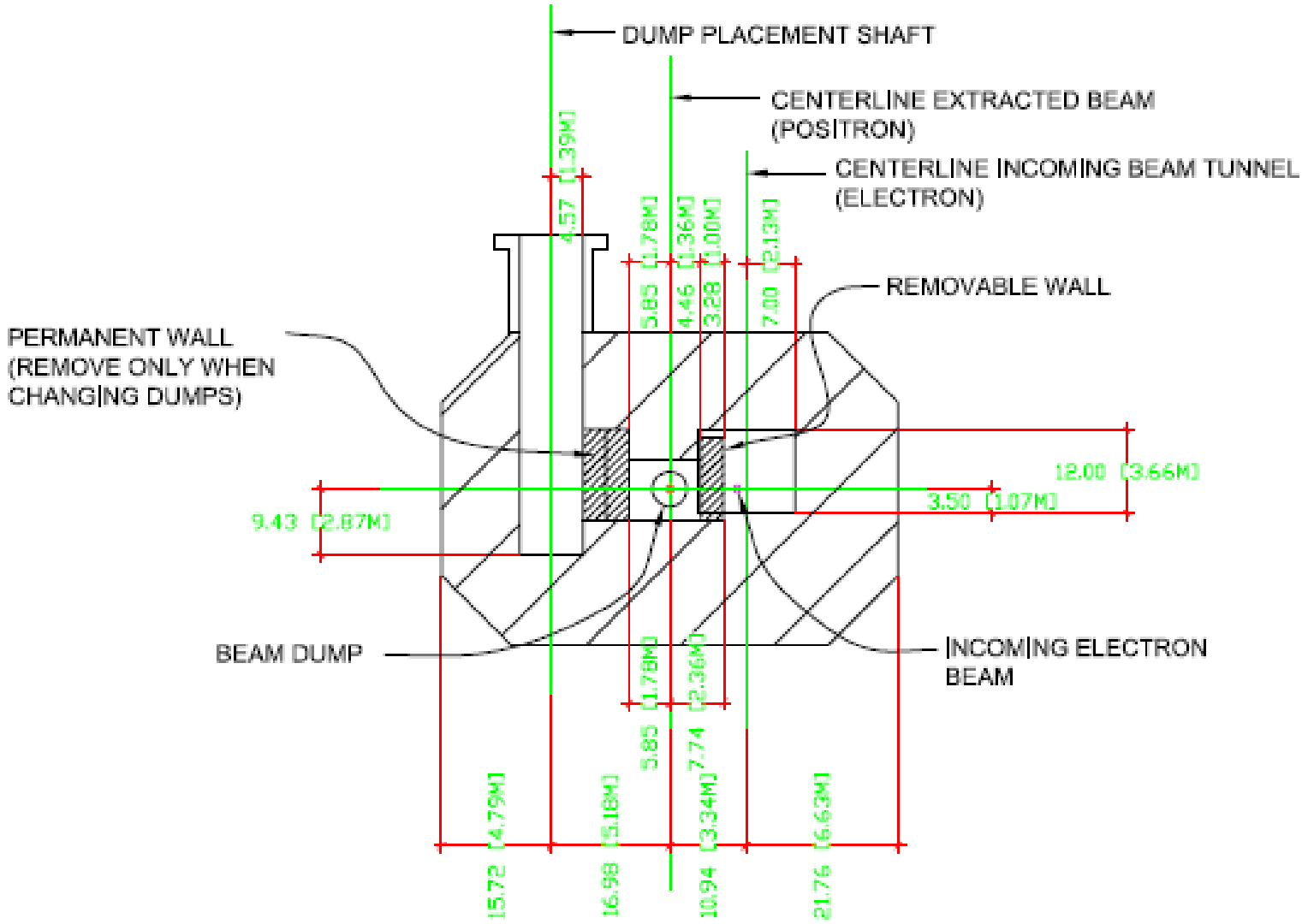
Beam Dump Housing Block Plan View



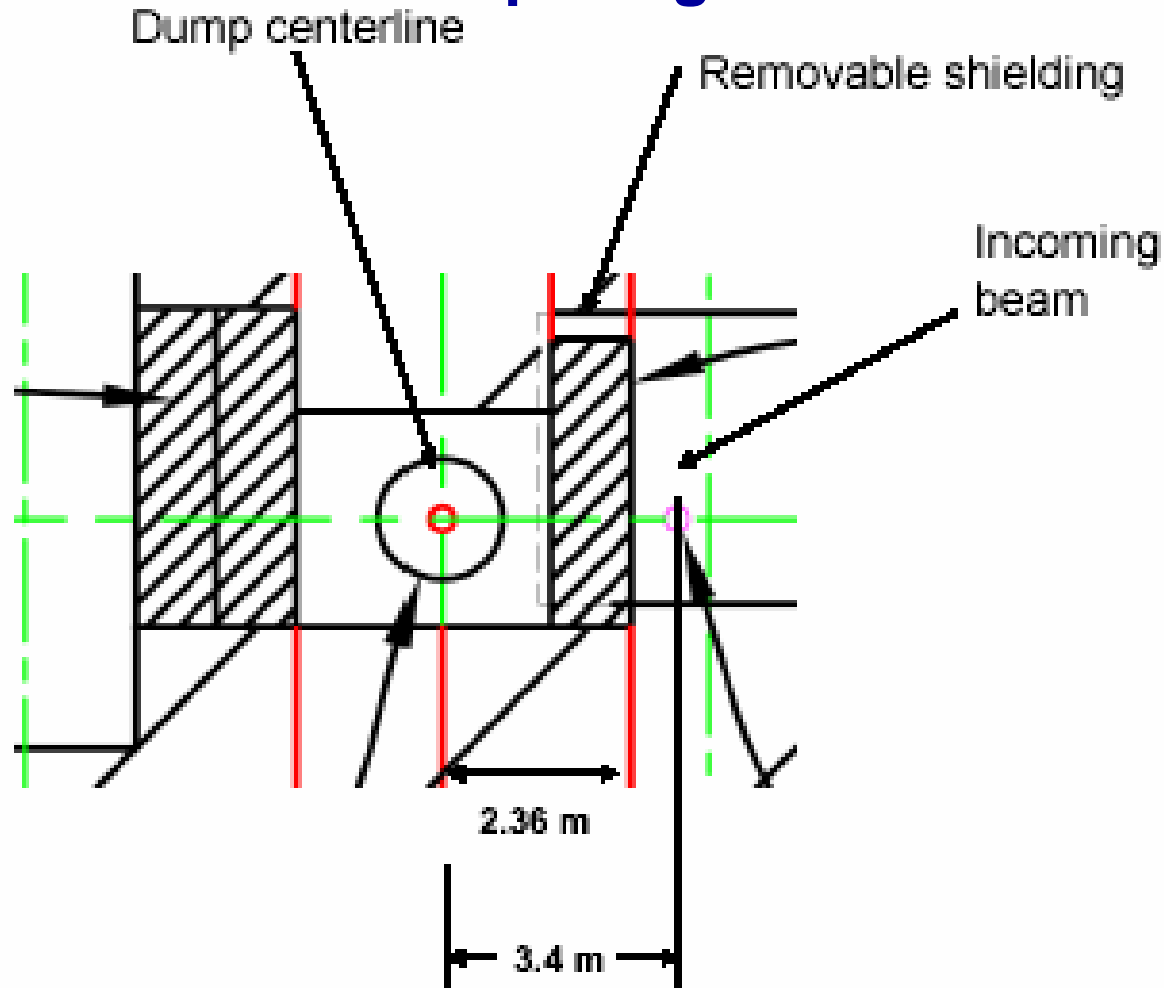
Beam Dump Housing Block Section A-A



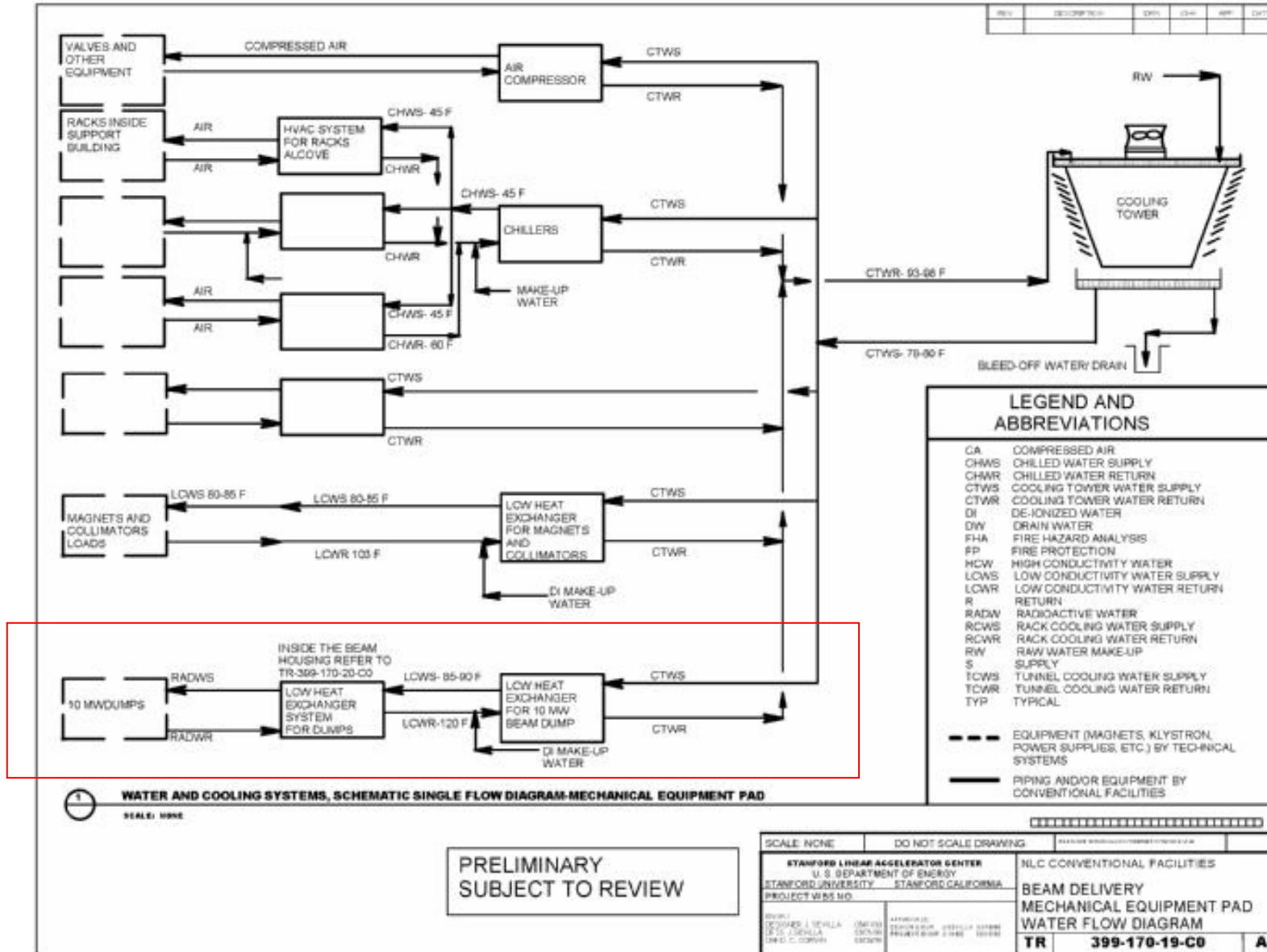
Beam Dump Housing Block Section B-B



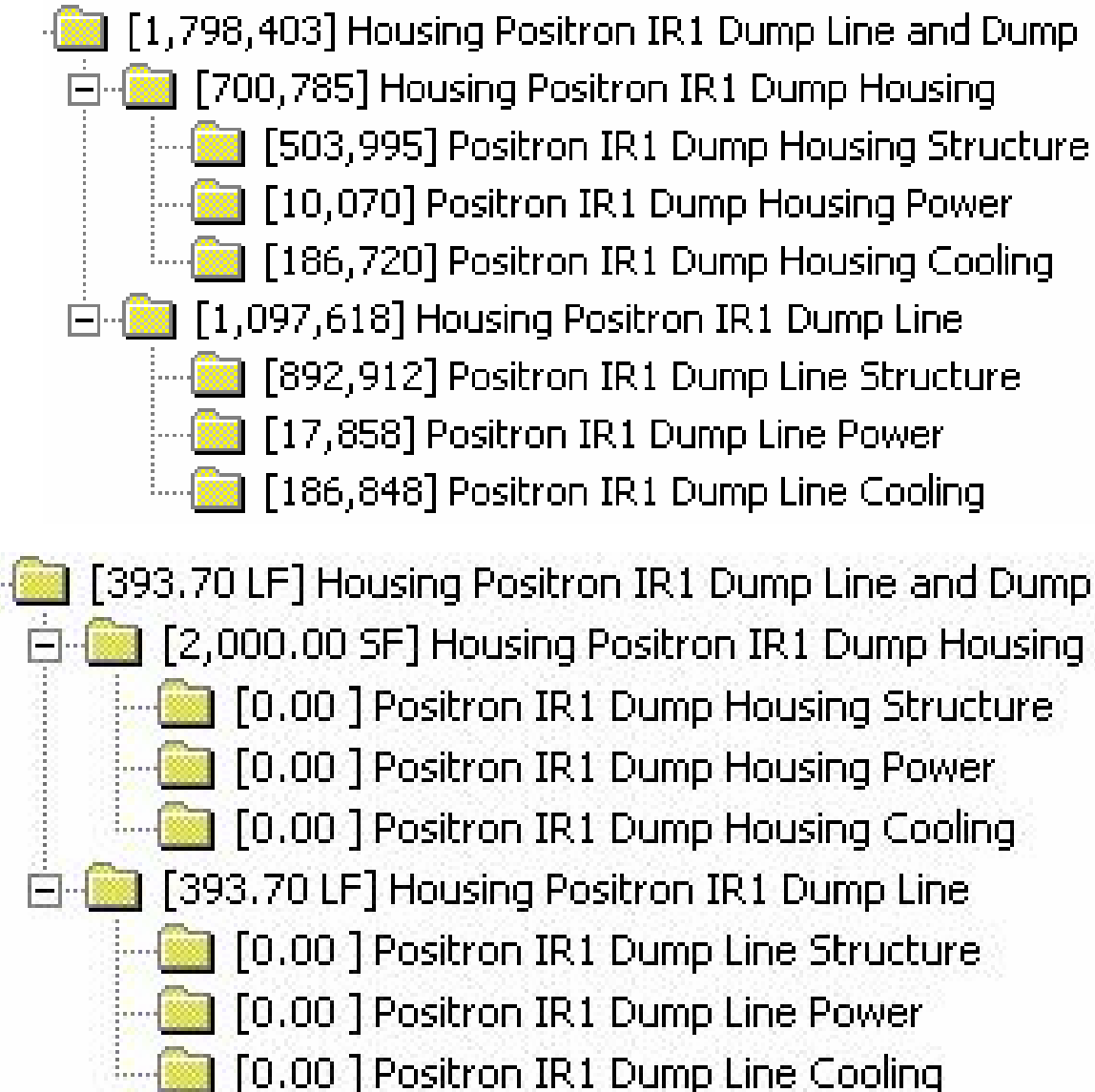
Detail Showing Required Transverse Spacing



1999 NLC Mechanical Requirements



1999 Dump Cost Estimate Civil & Mechanicals (Corvin & Sevilla)



~1999 Cost Model & Caveats Dump Vessel

Welded low-carbon stainless (316L) plate with robotic/semi-robotic window replacement

- While few US facilities could handle the size, not really a technical challenge
- Welds X-rayed
- 1965 costs scaled by Walz to produce 1996 estimate, which in turn scaled by Eriksson/Doyle to produce 1999 and 2001 estimate of \$165k
 - At the time materials estimated to cost \$50k
- Recent discussions with Walz/Doyle lead to \$1.5M upper limit for industrial production of a 20MW sized dump

~1999 Cost Model & Caveats Civil

Three features dominate cost discussion:

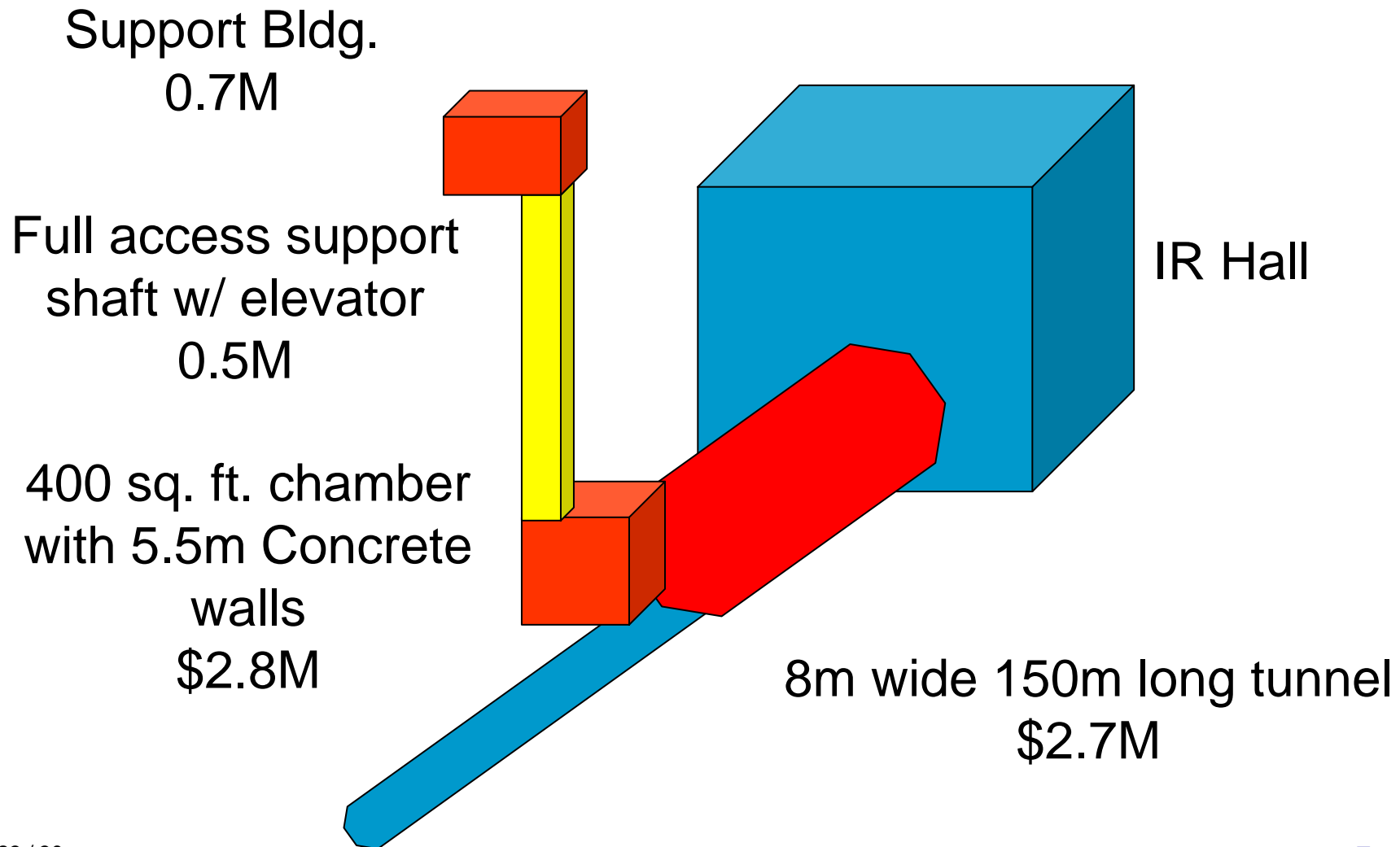
- Depth
- Geology (how wet)
- Length of tunnel requiring “road-header” for excavation as opposed to tunnel boring machine

2001 Model

- Dry cavern with 145m of beamline @ 15m
 - Surface pit construction techniques for both beamlines & vault
 - 3x more expensive if deep
 - 2x more expensive if wet
 - 3x more expensive per unit L x Area to road-head tunnel

ILC sites all wet &/or deep with beamlines 400-800m long

~1999 Civil Costs



1999 Mechanical Costs

| | |
|---|---------------|
| 10MW cooling system (1st level) | \$165k |
| Piping up support shaft | \$80k |
| Intermediate cooling system | \$225k |
| Cooling Tower | \$137k |
| Total | \$607k |

Total Costs

| Item | NLC-1999 | Deep, Long, Wet ILC | ILC |
|-------------------------|------------------------|---------------------|------------|
| Dump Vessel | \$0.2M | x10 | \$1.5M |
| Mechanicals | \$0.6M | Shaftx10 | \$1.4M |
| Civil-Dump Installation | \$4.0M | x3x2 | \$24M |
| Civil-Extraction Lines | \$2.7M | X3-6 | \$8-16M |
| Radioactive Waste | \$0M | | \$0M |
| Total | \$8.5M | | \$35-43M |
| | 1999-2006 @ 3%/yr=1.23 | | \$43-\$53M |

Beam Dump Cooling Schematic from SLAC-TN-67-29

Technical Considerations

- **Water**
 - Prevent mass boiling of water ($\Delta T=30^{\circ}\text{C}$): Flow=1800 gpm
 - Prevent localized boiling (1 train): $v=1.5$ m/sec
- **Window**
 - Prevent burn through
 - Use Cu for transverse conduction
 - Local velocity and coolant temp. prevent film boiling
 - Prevent window fatigue
 - Semi-hard or full-hard materials
- **Vessel Installation/Removal**
 - Elevator or double wide tunnels or downstream burial pit

Technical Considerations Cooling System

- **H₂ generation**
 - Catalytic H₂/O₂ recombiner
- **Radio-Isotope Production**
 - ¹⁵O – delay access 20 minutes
 - ¹¹C – delay access 3 hours
 - ⁷Be – dual filters
 - ³H₂ – periodic disposal of radiated water
- **Isolation of RAD water from cooling tower**
 - Intermediate heat exchanger system
 - Insure favorable Δp

Summary

- **Still our belief that dump should not be an issues except for the window**
- **More work needed before we can say that there is or is not a problem**