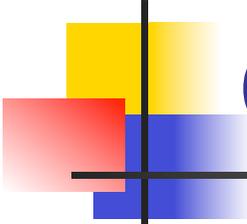


Conceptual Design of ILD Yoke

Uwe Schneekloth
DESY

LCWS 2013, Univ. of Tokyo
12.11.2013

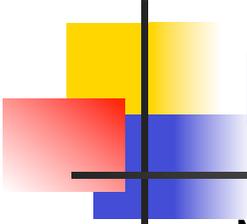


Outline

- Design requirements
- Magnetic Stray Field and Forces
- Present status of design
 - Barrel
 - End-cap
- Yoke Assembly
- Options/Optimization
- Conclusions

Mainly report on progress at DESY

- K.Büsser, M.Lemke, B.Krause, C.Martens, A.Petrov, K.Sinram, U.S., R.Stromhagen (all part time)



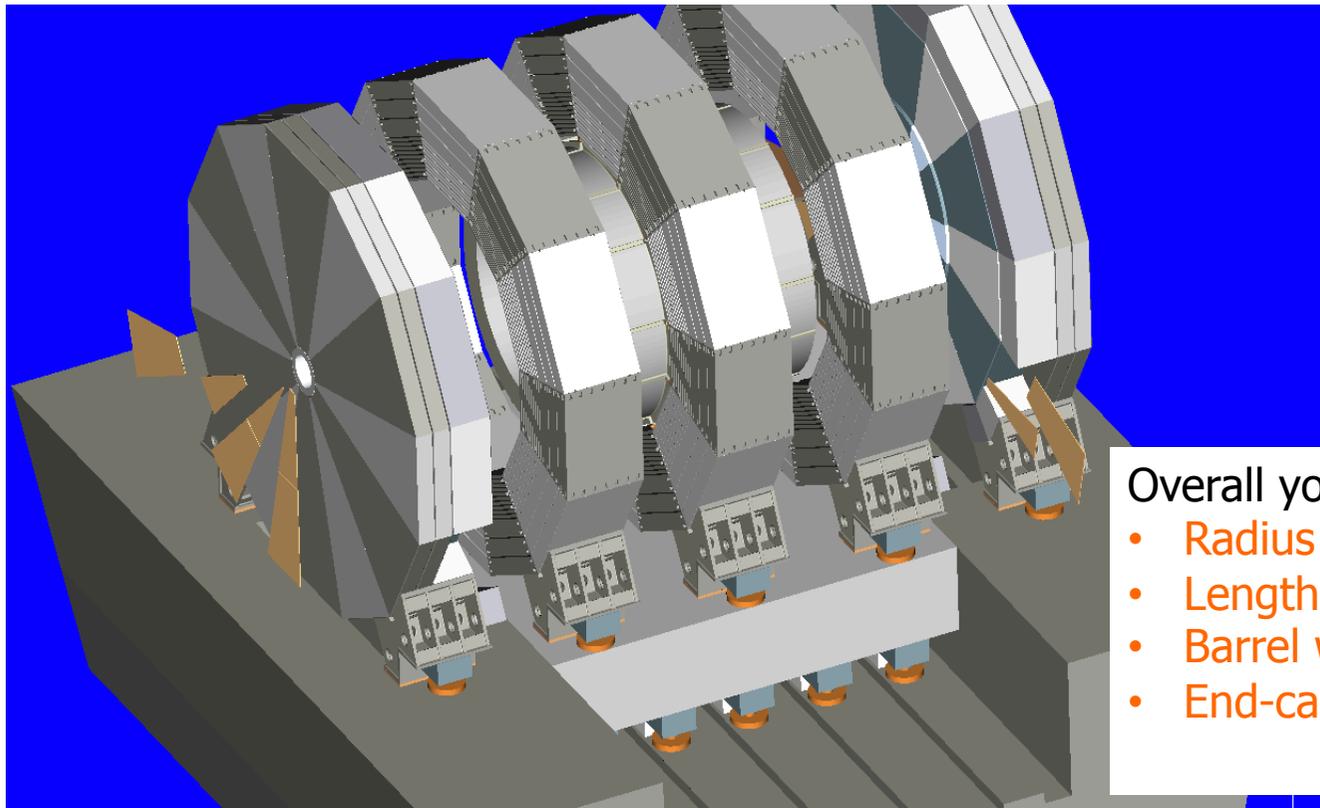
Function and Challenges of Iron Yoke

- Muon identification and hadron rejection
 - Muon momentum measurement done with inner tracking detectors
 - Some muon ID with calorimeter, but need high purity and redundancy
 - Rejection of beam halo-muons
- Tail-catcher/backing calorimeter
- Flux return
 - Field homogeneity in TPC
 - Stray field
 - Large magnetic forces
- Main mechanical structure of detector
- Radiation shielding
 - Detector should be self-shielding, T.Sanami, Warsaw ECFA Workshop
- Main challenges of yoke design
 - Reduce stray field to acceptable level **Determines total thickness and cost of iron**
 - Huge magnetic forces on end-caps
 - Optimize design w.r.t. to performance, site requirements and cost

Yoke Design Overview

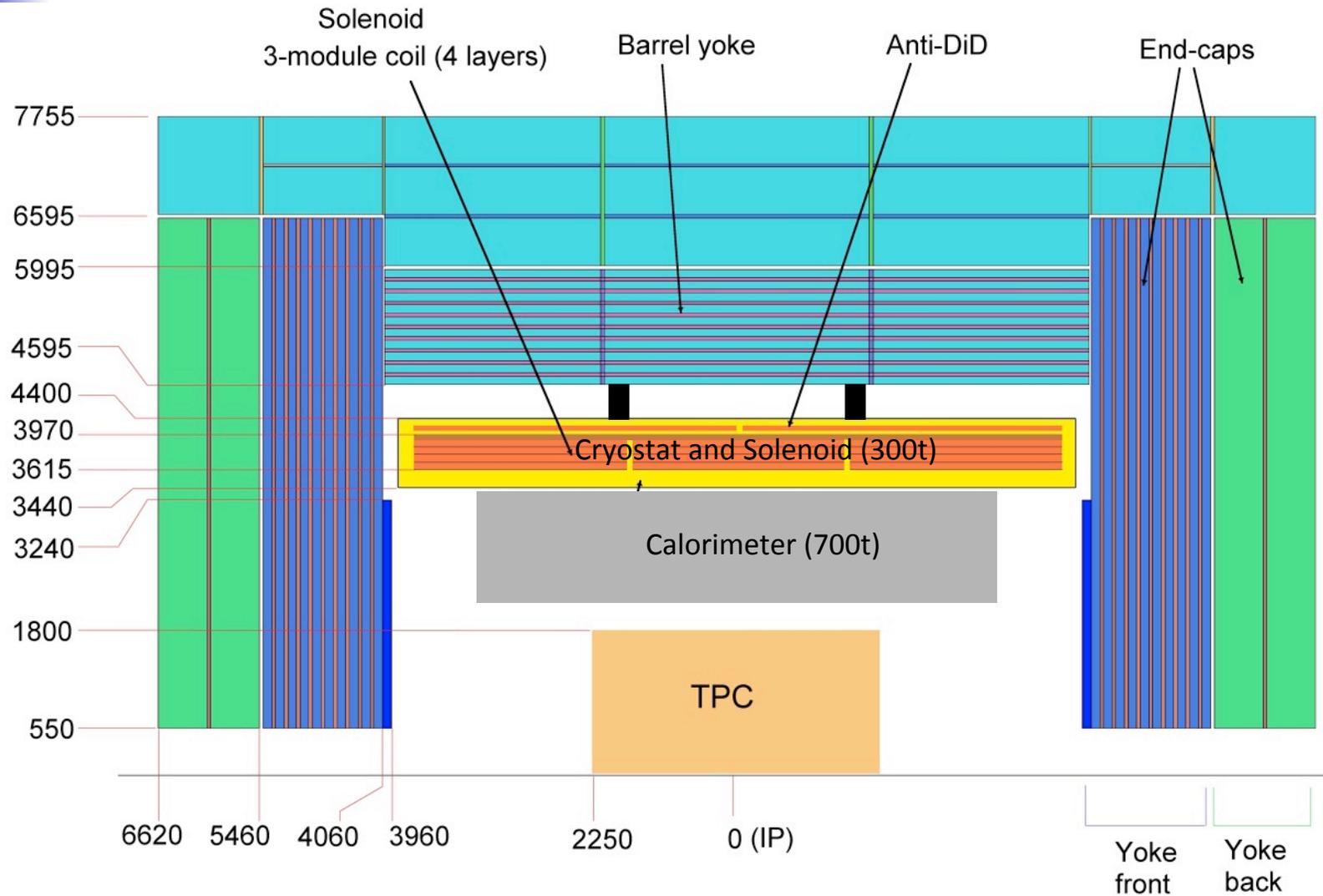
Design based on CMS

- Large volume, 4T magnet
- Assembly in surface hall, moved to IR hall through vertical access shaft
- 3 instead of 5 (CMS) barrel rings
- End-cap option split into inner and outer pieces

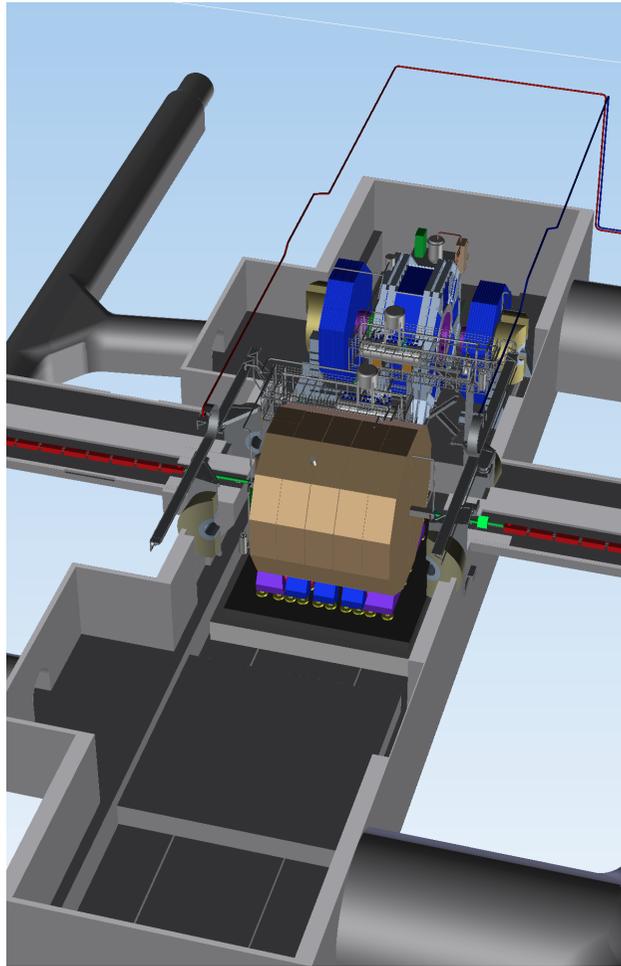


- Overall yoke dimensions
- Radius 15.5m
 - Length 13.2m
 - Barrel weight 6900t
 - End-cap weight 6500t
total 13400t

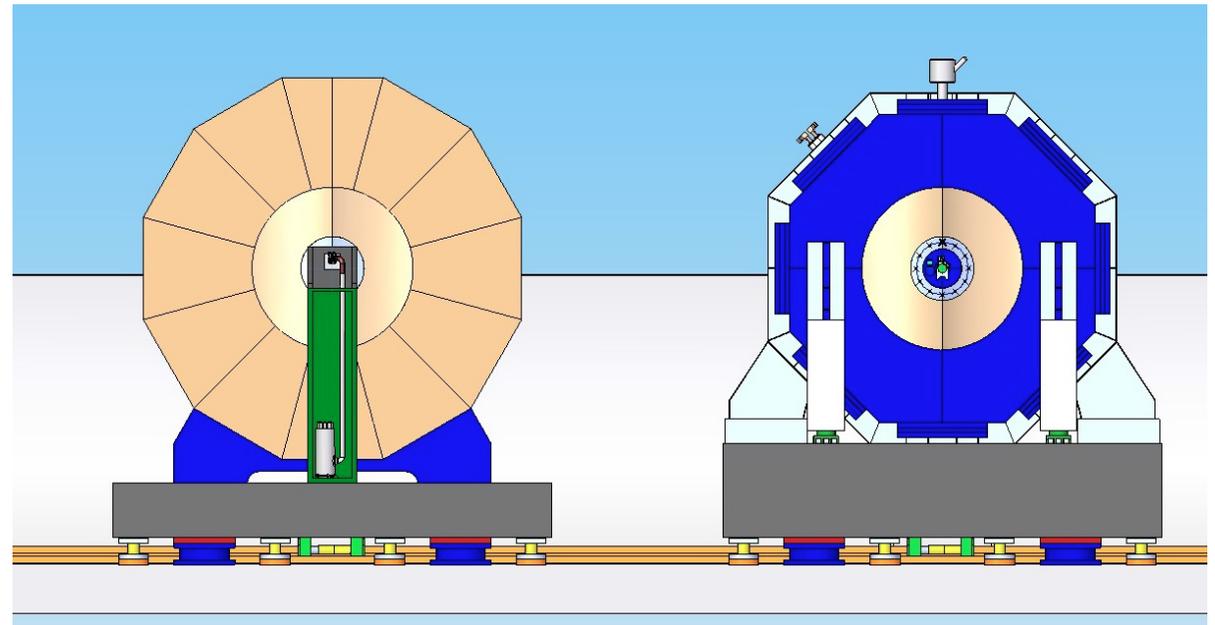
Yoke Cross-Section Overview

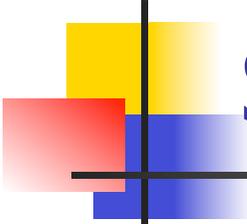


ILC Experimental Hall



- Two detectors in hall, in beam and in park position
- On platform for fast movement in/out of beam position
- Requirements on stray field
 - 50G in 15m radial distance from detector center based on CMS experience





Segmentation of Iron Yoke

Barrel

- 10 100mm thick steel plates with 40mm gaps for chambers
- 3 560mm thick steel plates with 40mm gaps for chambers

End-cap

- 100mm field shaping plate
- 10 100mm thick steel plates with 40mm gaps for chambers
- 2 560mm thick steel plates with 40mm gaps for chambers

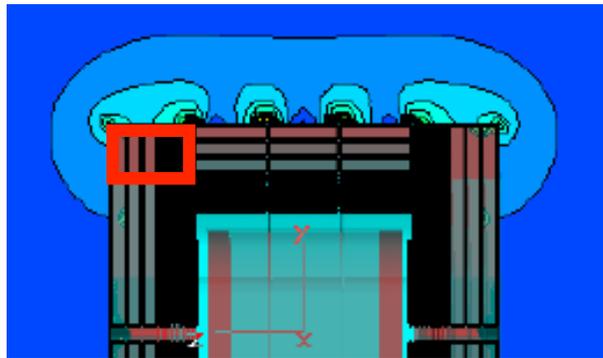
- Thickness of inner 10 plates determined by physics requirements: energy measurement of hadronic showers (tail catcher) and muon identification
- Total amount of outer plates determined by requirements on stray field
 - Limit of 50G may be relaxed (100G?)
=> could reduce amount of iron and hence cost
 - Quite some uncertainty in field calculation, FEM simulations at limit
=> may keep present iron thickness

Stray Field Calculations

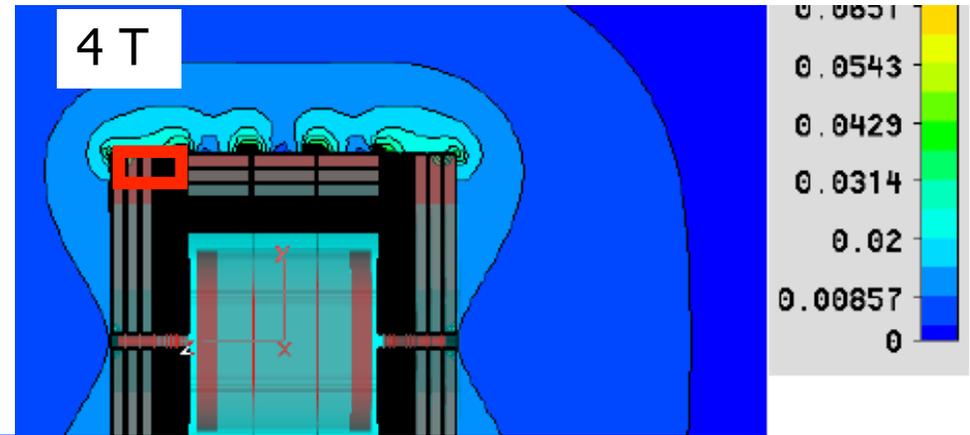
A. Petrov, 2008

3.5 T

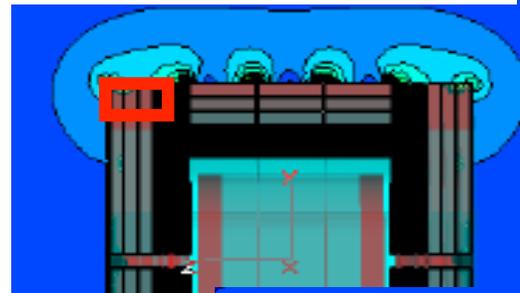
gaps filled



4 T



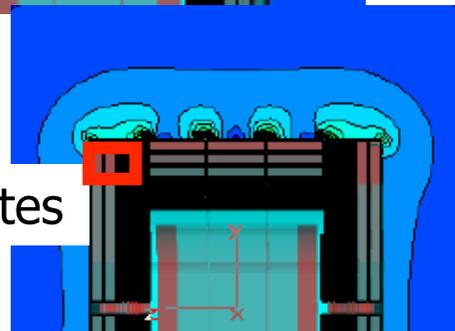
gaps partly filled



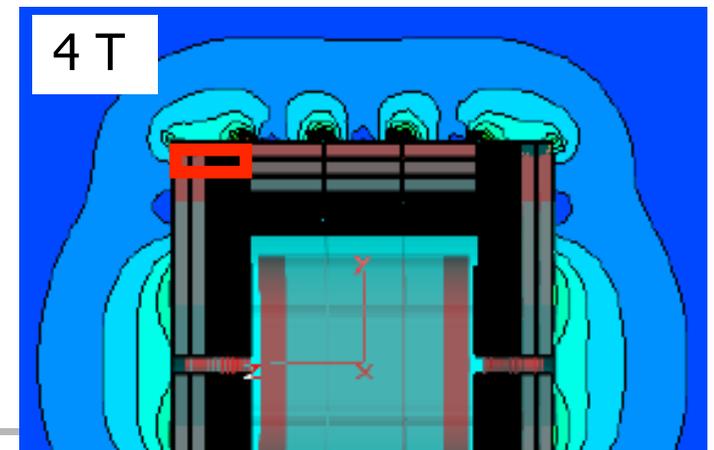
Seoul mtg

iron thickness 2.68/2.12m
total thickness 3.16/2.56m
 $r_{out} = 7.655m, z = 6.605m$

gaps partly filled, EC 2 plates

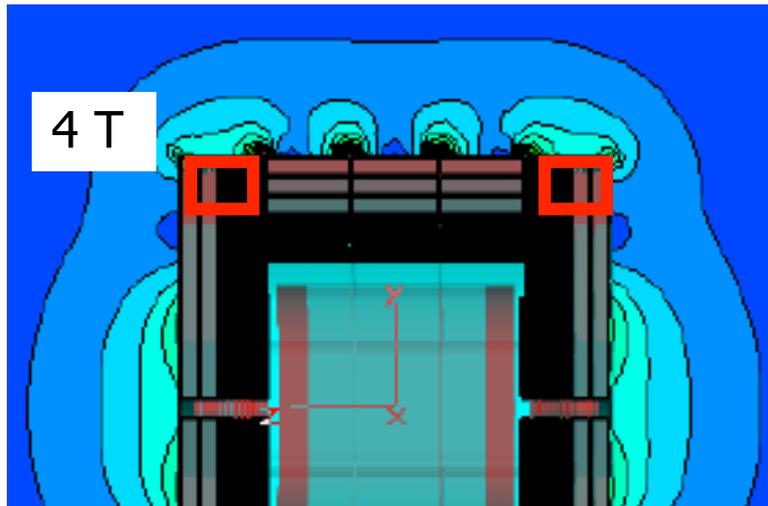


4 T



Magnetic Stray Field

Did extensive field calculation for several geometries

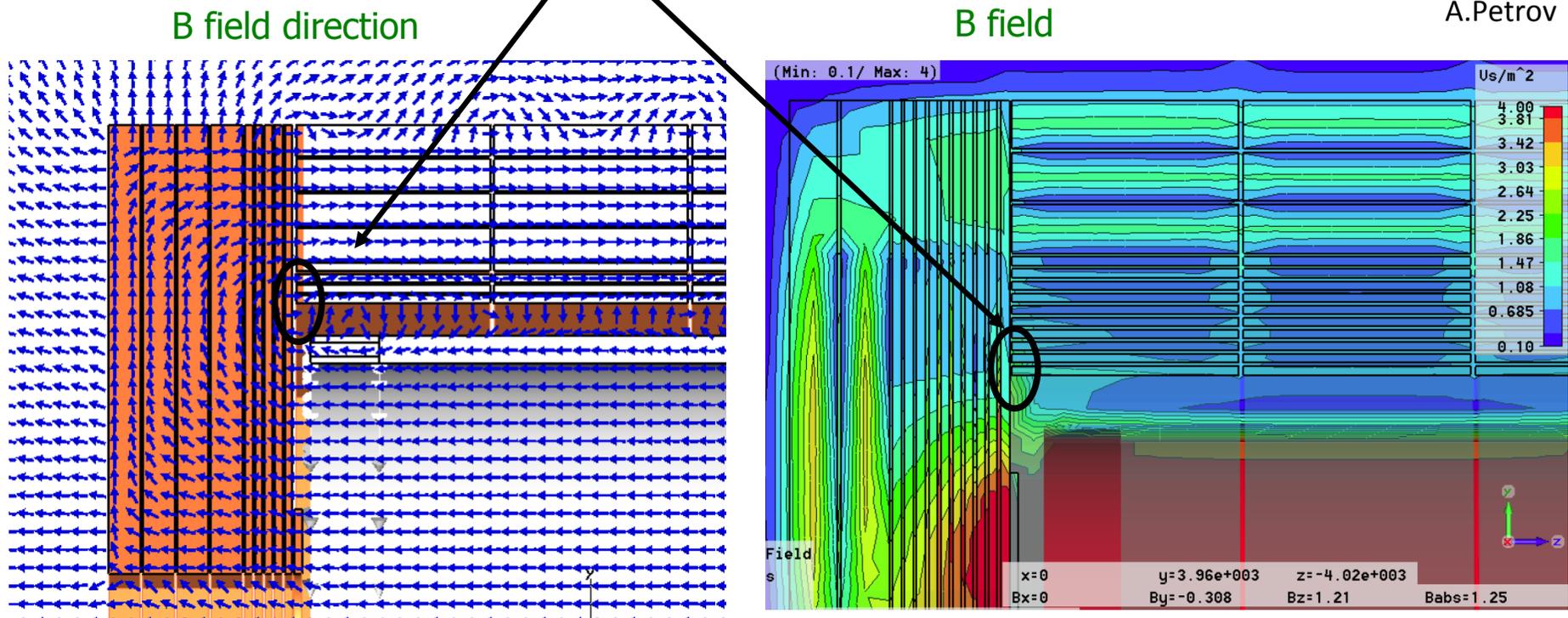


B EC
iron thickness 2.68/2.12m
total thickness 3.16/2.56m
 $r_{\text{out}} = 7.655\text{m}$, $z = 6.605\text{m}$

- Achieved goal of $< 50\text{G}$ at 15m from beam line for 4 T
- Thickness of iron and size of detector is determined by stray field requirements
- Important to close gaps as much as possible
- Stray field requirements may be relaxed (100G?)
 - > Yoke could be slightly smaller
- New FEM calculations give larger stray field. In addition, at limit of FEM.
 - > Will probably keep present iron thickness
- Need better understanding of FEM calculations

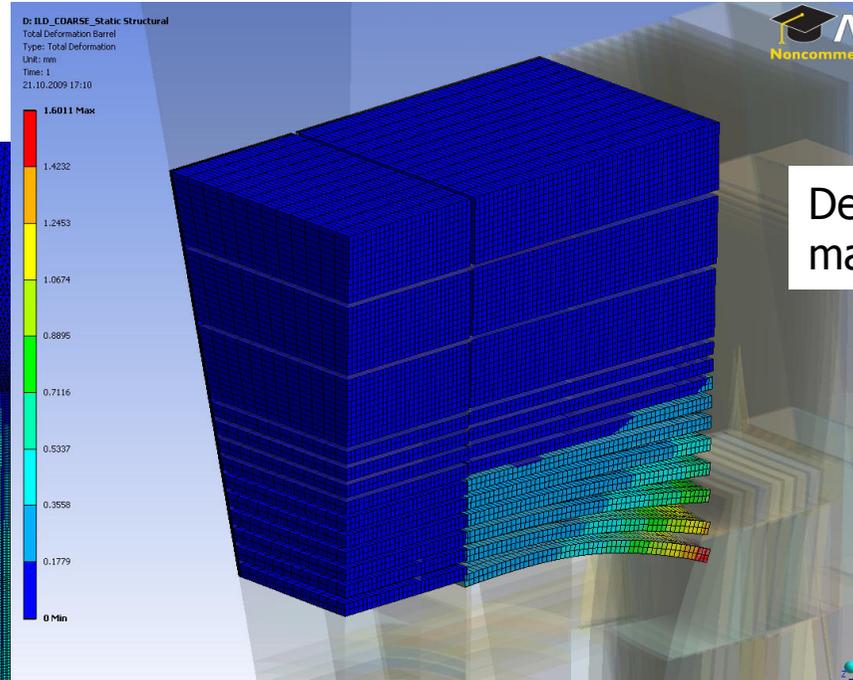
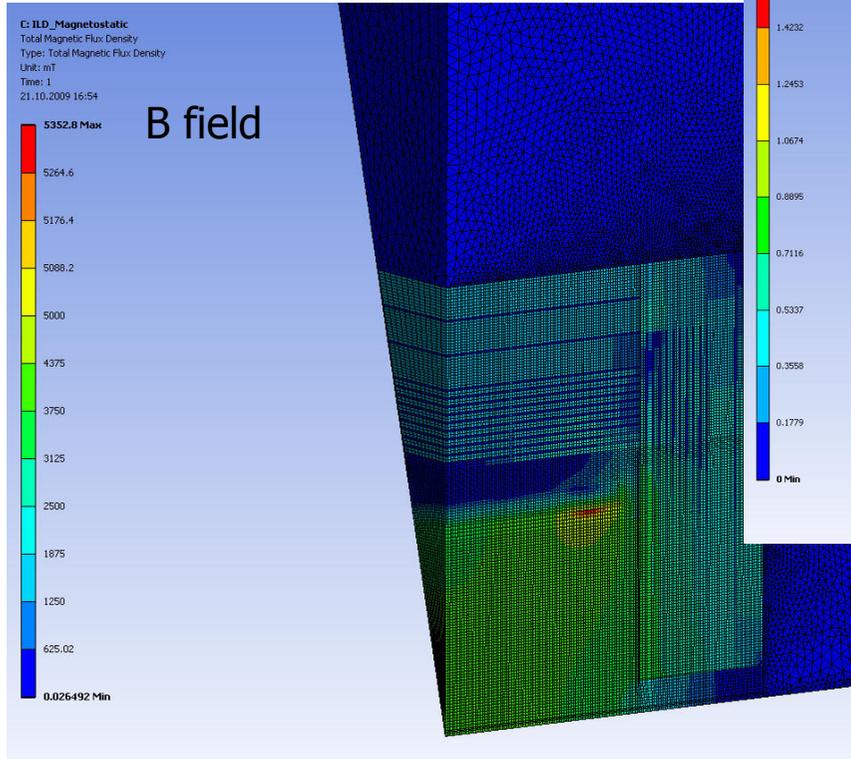
Forces on Barrel

- Magnetic forces acts in z-direction. Barrel is compressed. No problem.
- Exception: magnetic force on innermost plate of outer wheels
- Unlike end-cap, radial forces on barrel are mainly to due gravity



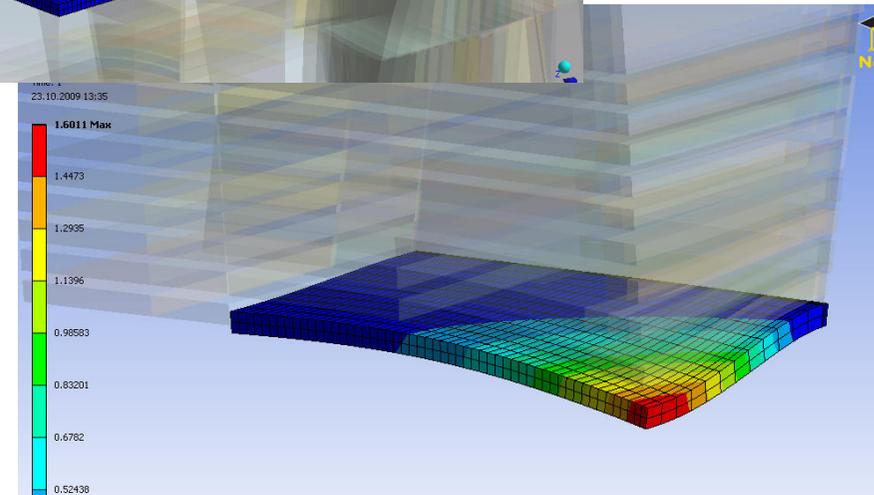
Magnetic Forces on Barrel

Forces much weaker
than for end-cap

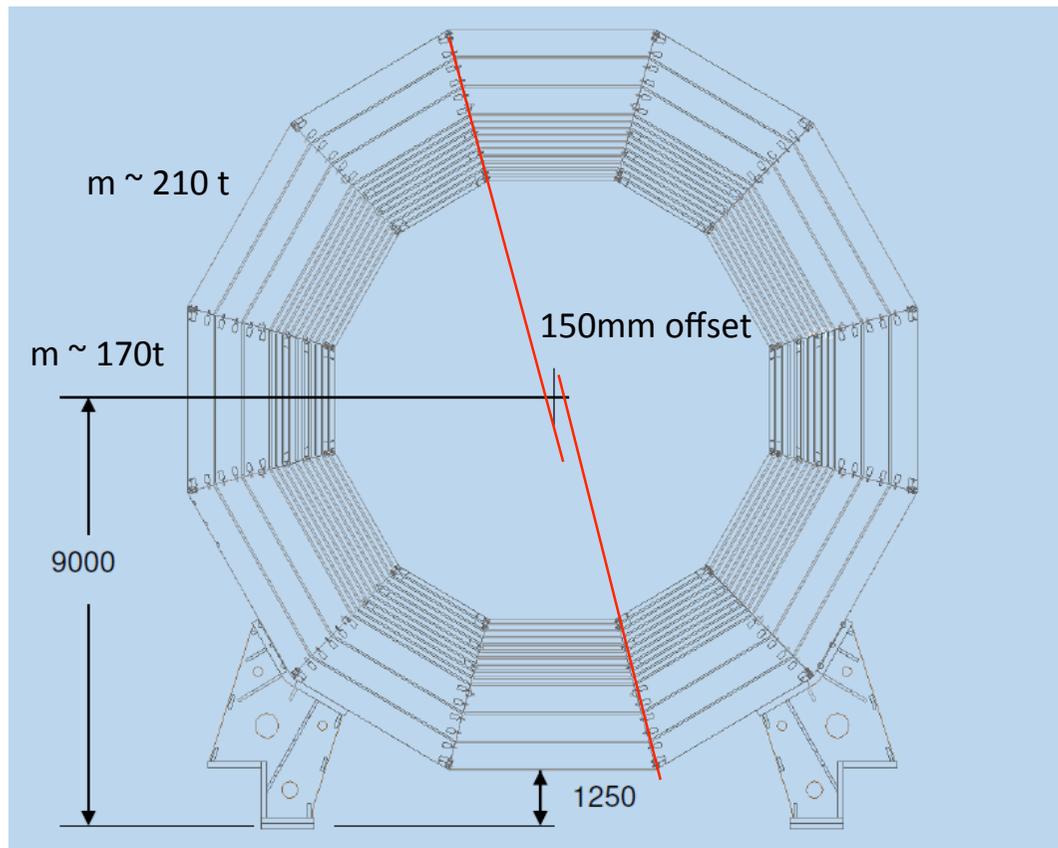


Deformation due to
magnetic forces

Deformation of inner plate
of outer wheel 1.5mm
No problem



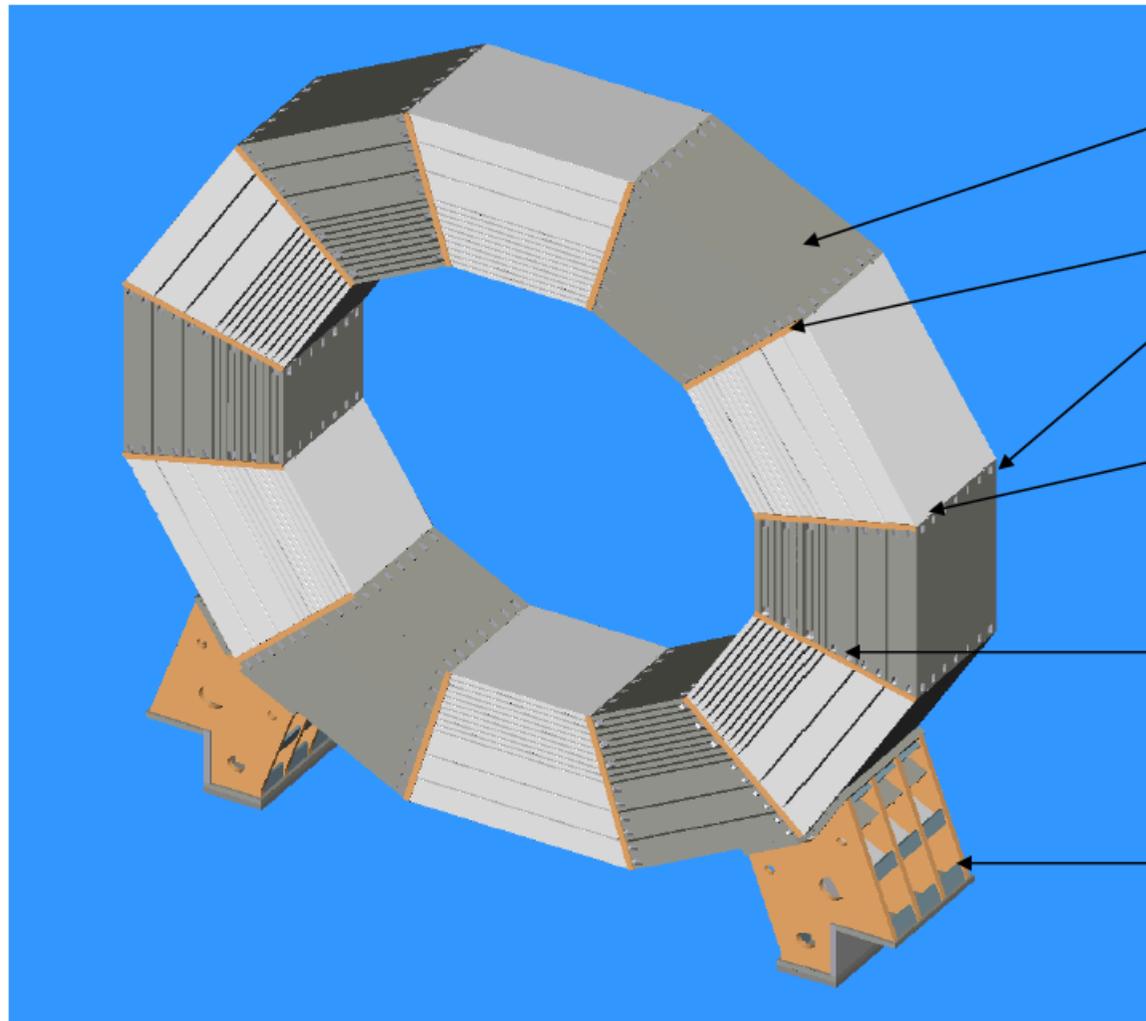
Design of Barrel



- Three barrel wheels, each consisting of 12 segments
 - Segments with welded plates
 - Segments bolted together
- Iron Segmentation
 - Inner part: 10 plates 100mm, 4mm gaps for detectors
 - Inner part: 10 plates 100mm, 4mm gaps for detectors
- Thickness of iron given by stray field requirements
- Radial iron thickness 2.68 m

Barrel Design

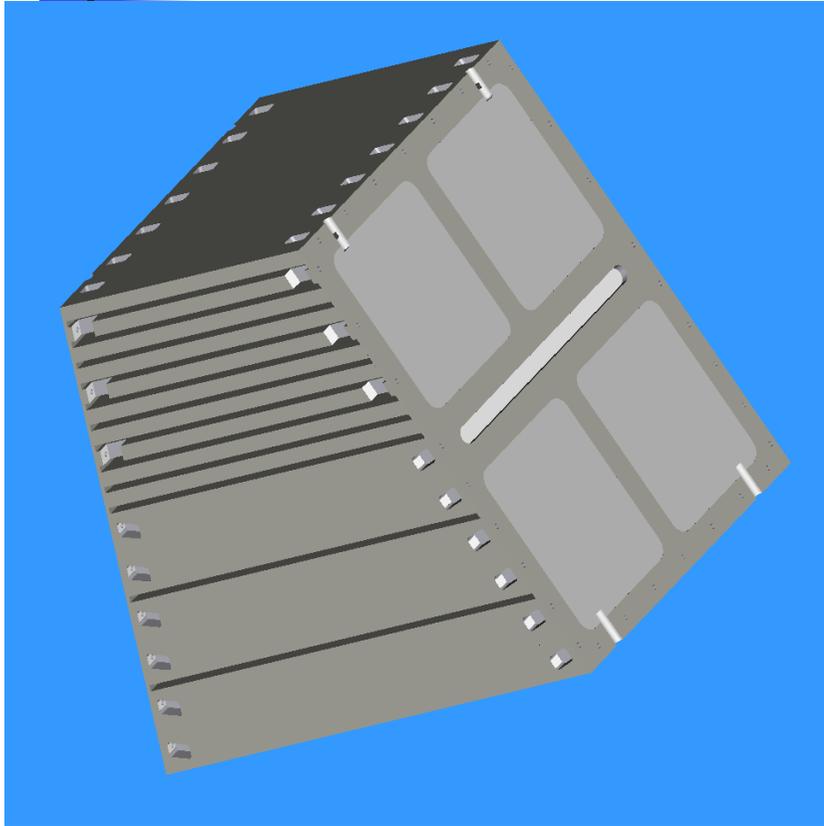
R. Stromhagen



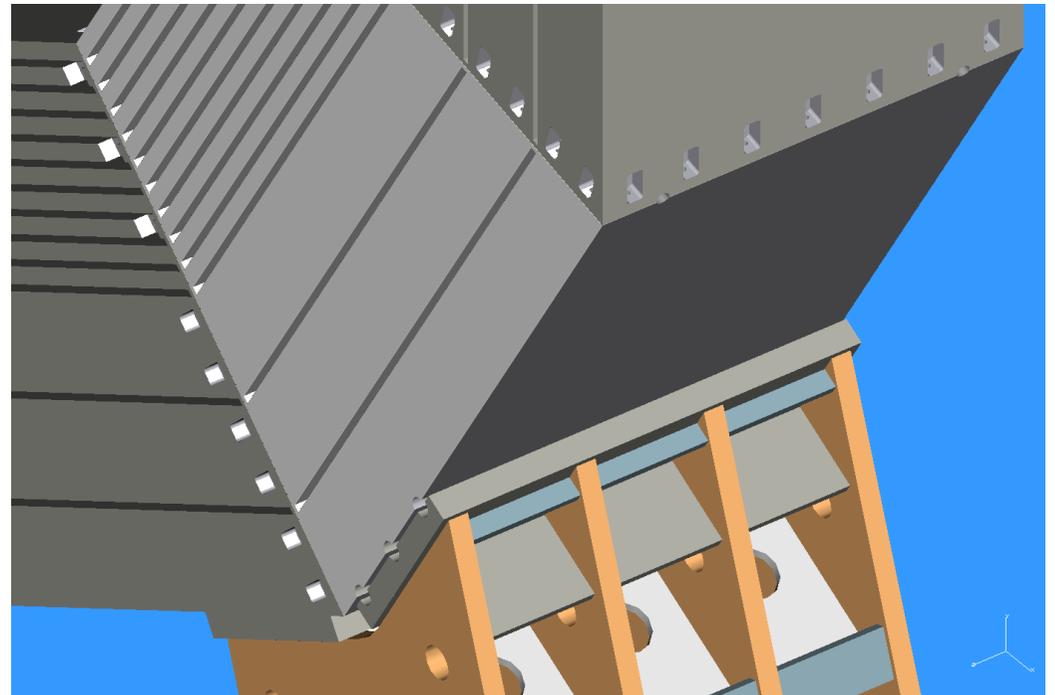
Assembly:

- segments ~ 200 t. welded
- shoulder for end-stop
- screws min. M30 / (min. 32 pieces)
- bolts (4 pieces
d ~ 120, lg. 350
assembling bore)
- key ledge, horizontal
(1 per segment
160x160, 2200 lg.
mm)
- stand (screws min. M30,
d ~ 120, lg. 350,
assembling bore)

Barrel Segment Design



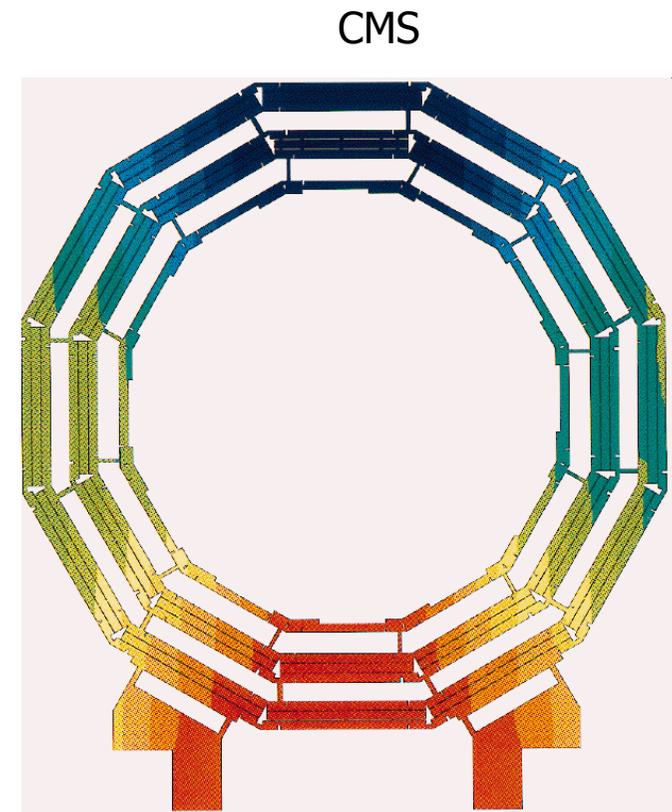
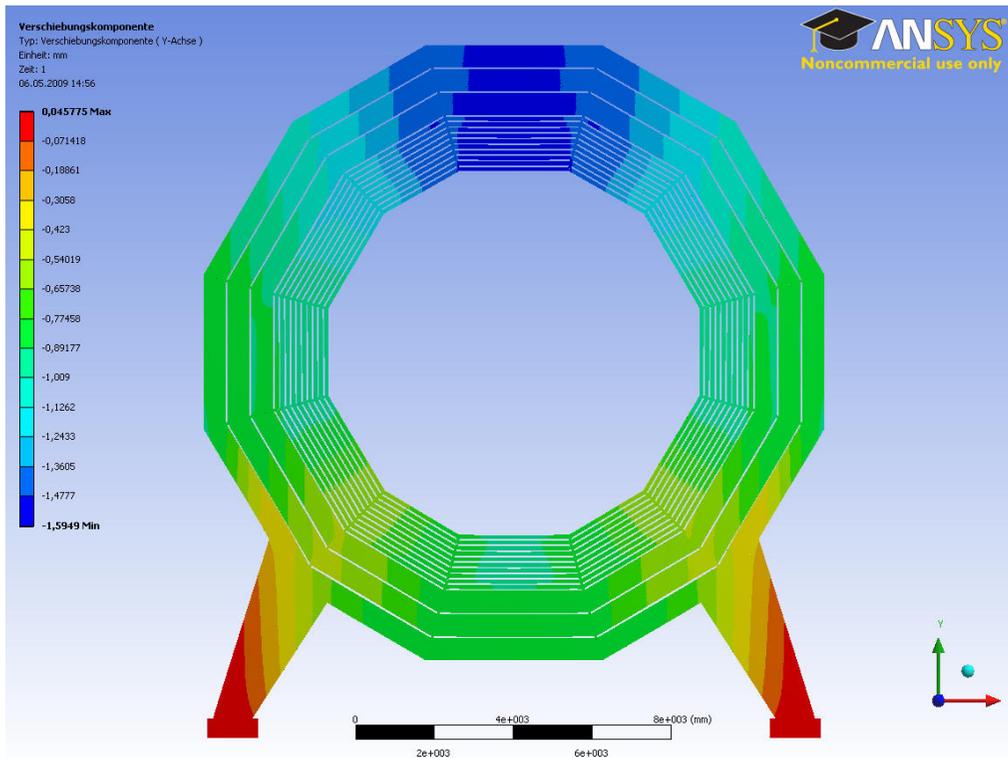
Segment weight ~ 210 t



Deformation due Gravitational Load

Vertical deformation of outer wheel

- Assuming solid connection between segments
- Max. deformation 1.6mm
(Support feet too small, simplified)



Max. vertical deformation 4.1mm

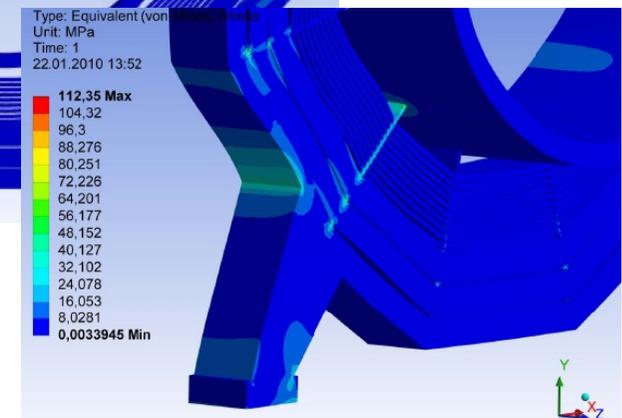
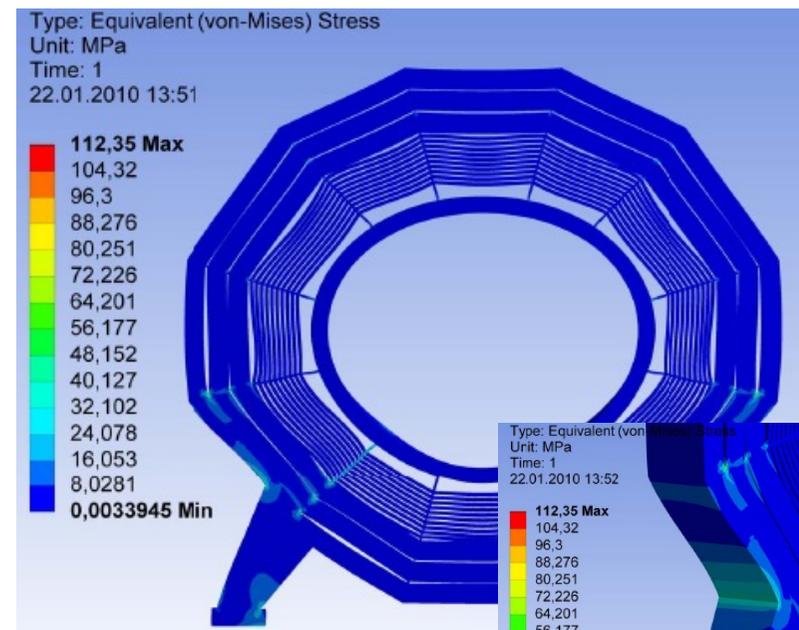
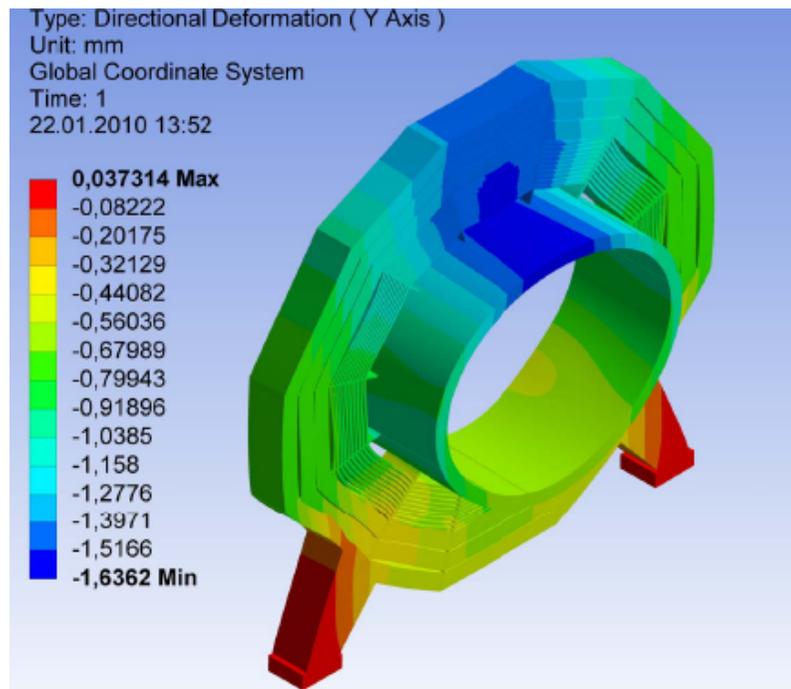
Deformation and Stress

Vertical deformation of central wheel

- Including load of cryostat, coil and calorimeter of 1000t
- Assuming cryostat solid with scaled up density

Caveat: cryostat much too stiff in this model

M.Lemke



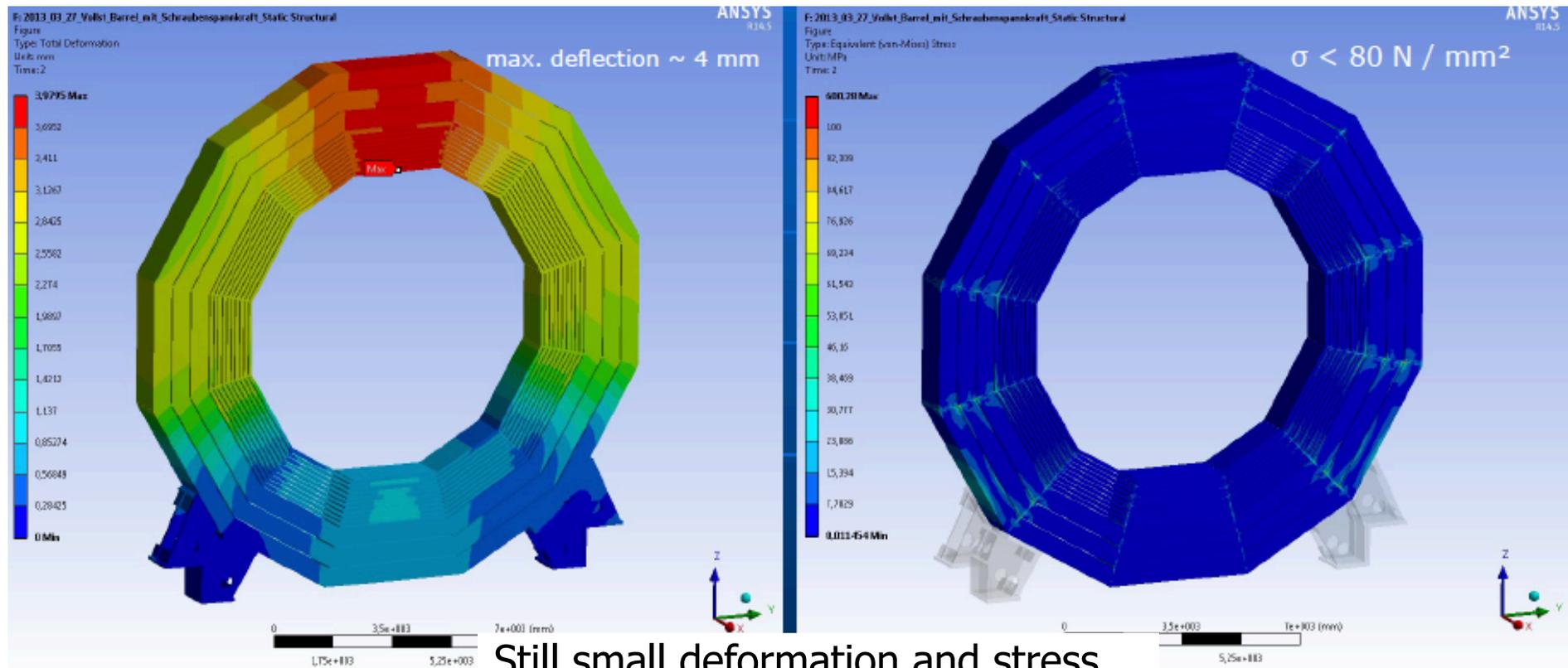
Small deformation and stress

Barrel Deformation and Stress

Total Deformation due to gravitational load and stress

New FEM model

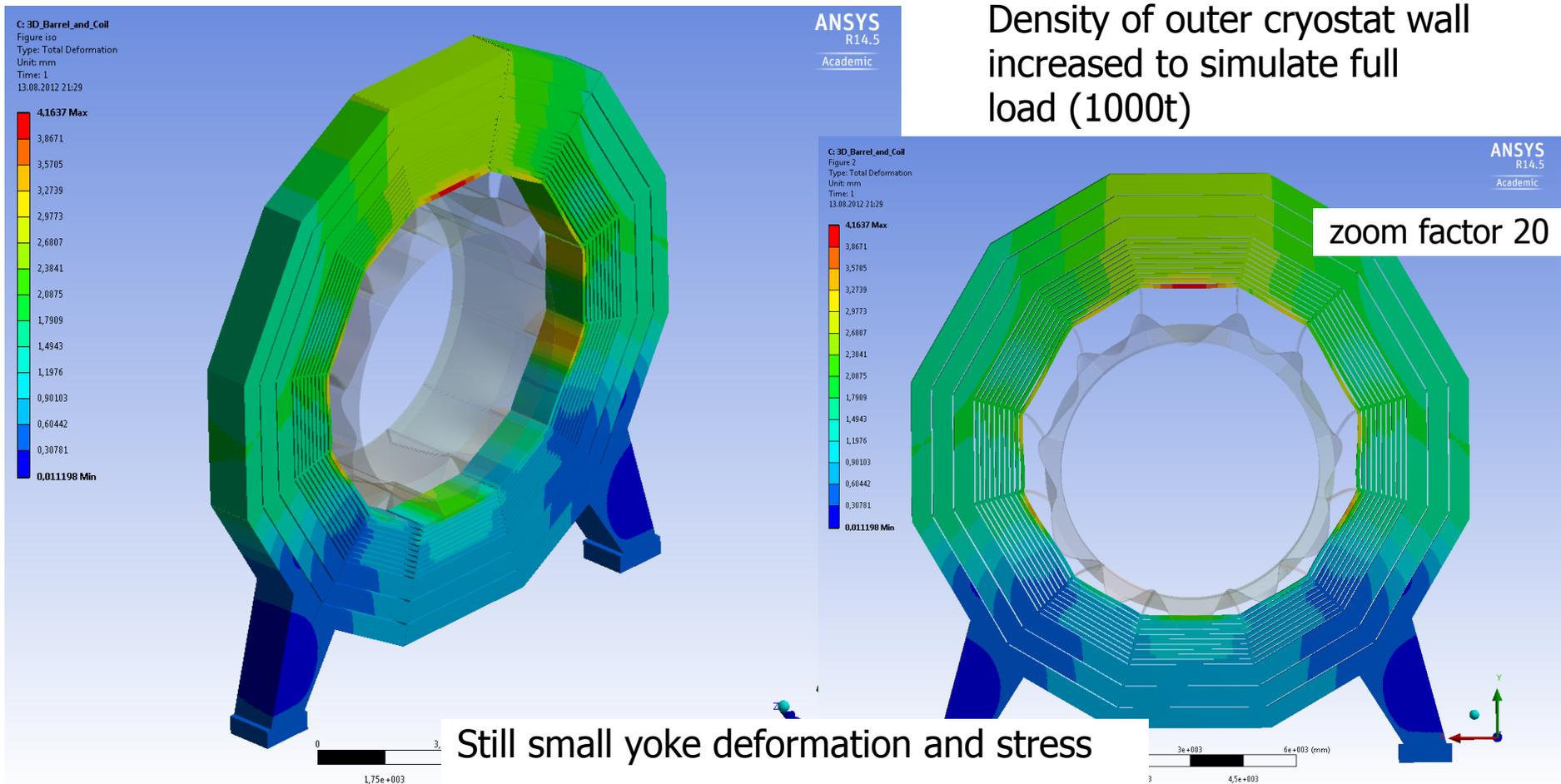
- Including bolts between segments
- Not solid model anymore



Still small deformation and stress

Barrel Deformation – Central Wheel

Total Deformation due to gravitational load including coil and HCAL load
Bolts between segments, not solid model anymore



Magnetic Forces on End-Cap

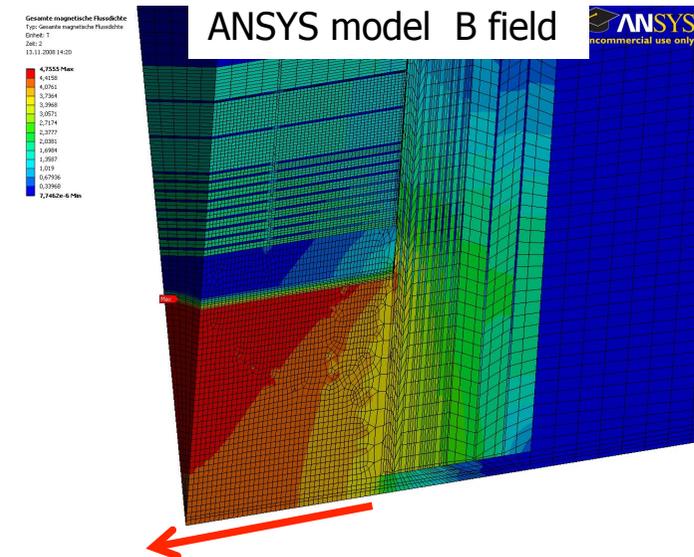
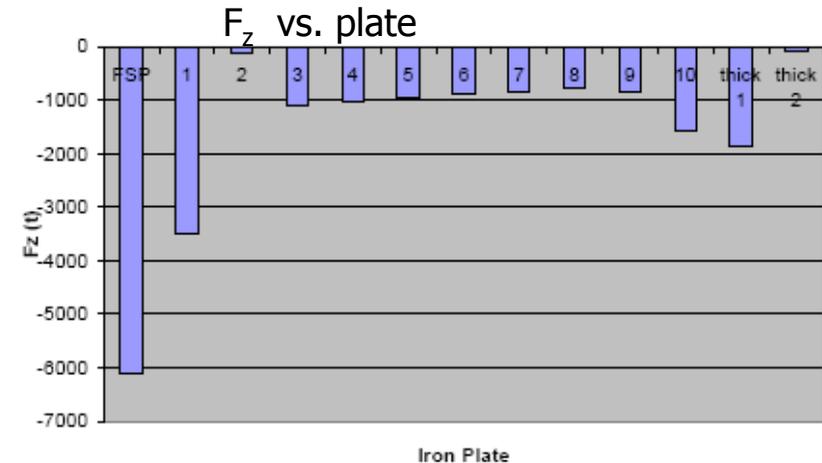
FEM Calculations 4T B field

CST EM Studio

- Force on center of each segment
→ total force $F_z = 20000t$
Model floor with support feet and steel plate in floor

ANSYS

- Force at each segment node
Resulting force on hard stop
→ $F_z = 19000t$ for 3 thick EC plates
 $F_z = 18000t$ for 2 thick EC plates
Model with open gaps



~ 20000t force acting on end-cap

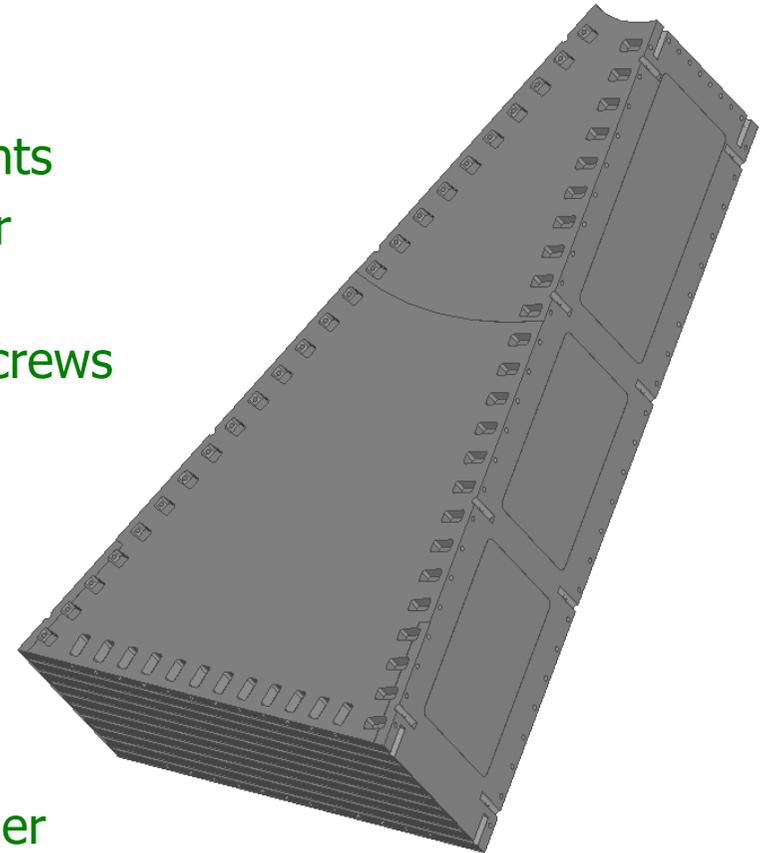
End-cap Design

Inner end-cap

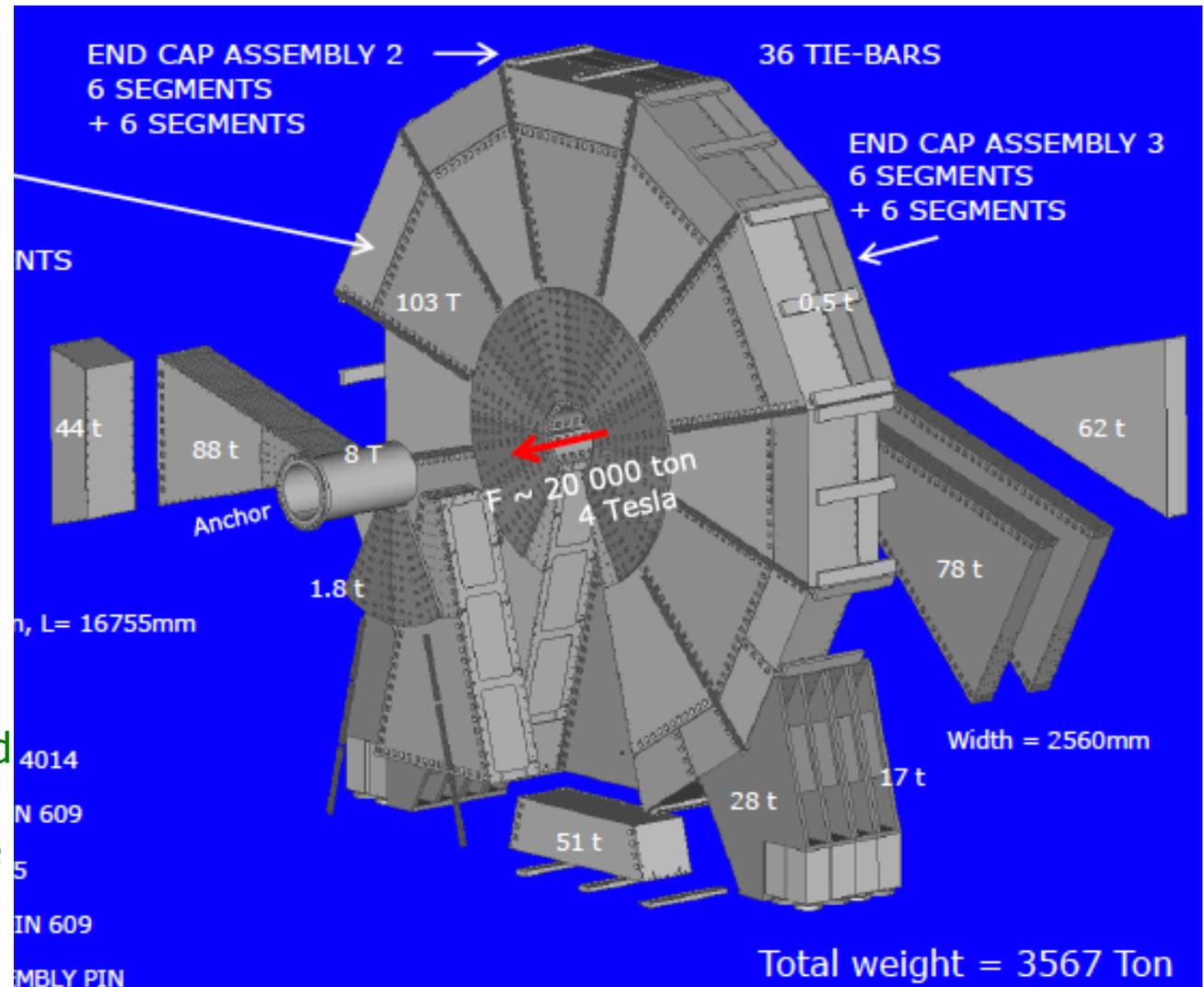
- Consisting of 12 wedge-shaped segments
- 10 100mm thick plates welded together
25x 40mm² spacers
- Segments bolted together using M36 screws
- Field shaping plate 100mm part of or attached to first plate
 - Welded, giving 200mm total thickness or
 - Bolted to plate segments

Outer end-caps

- Two disks, 560mm thick plates
- Wedge-shaped segments bolted together
- In addition on outer radius iron pieces to close gaps of inner end-cap gaps



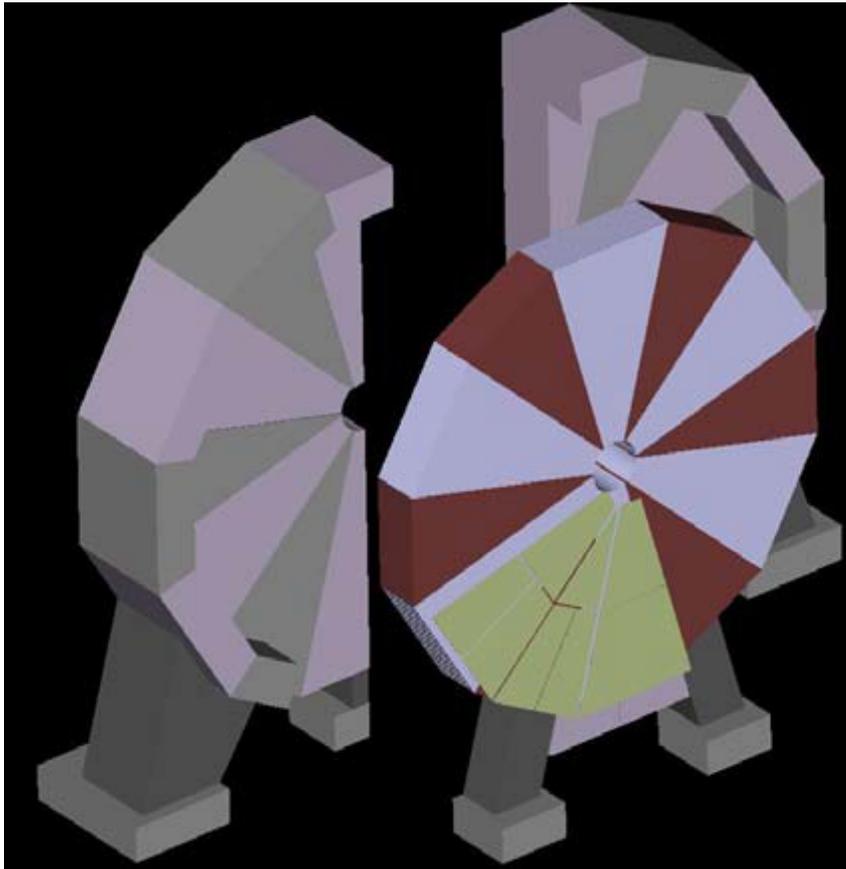
Mechanical Design of End-Cap



Comments

- Quite detailed study (R. Stromhagen)
- Should separate inner and outer EC again
- Unclear whether separate inner plates necessary

Inner and Outer End-caps



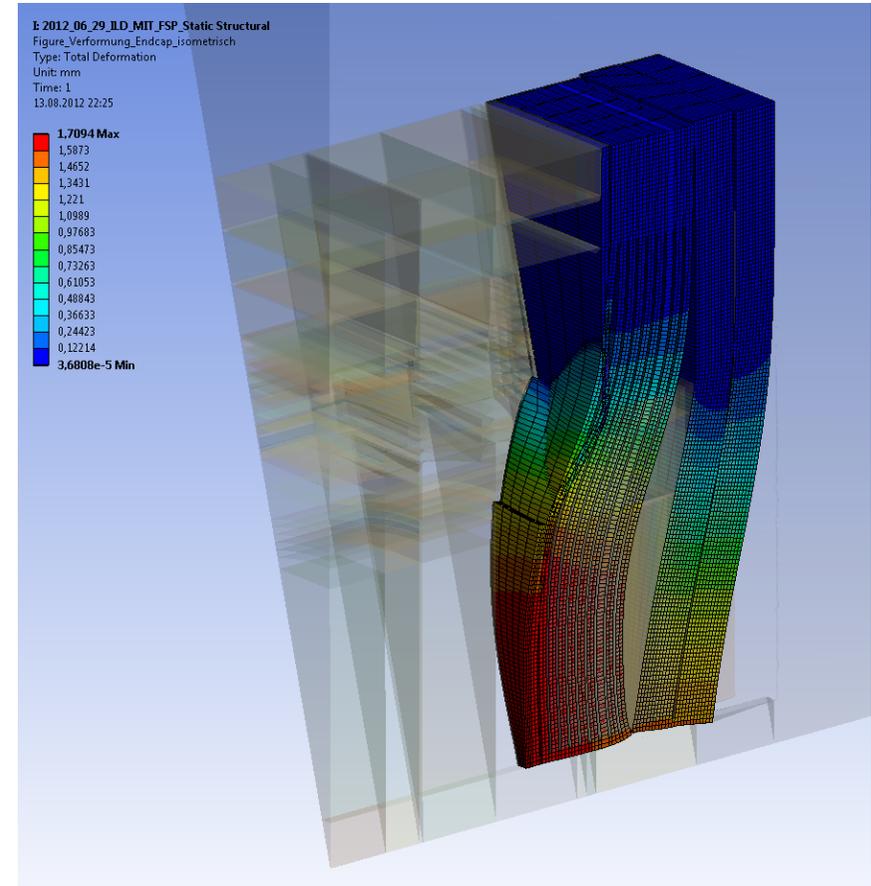
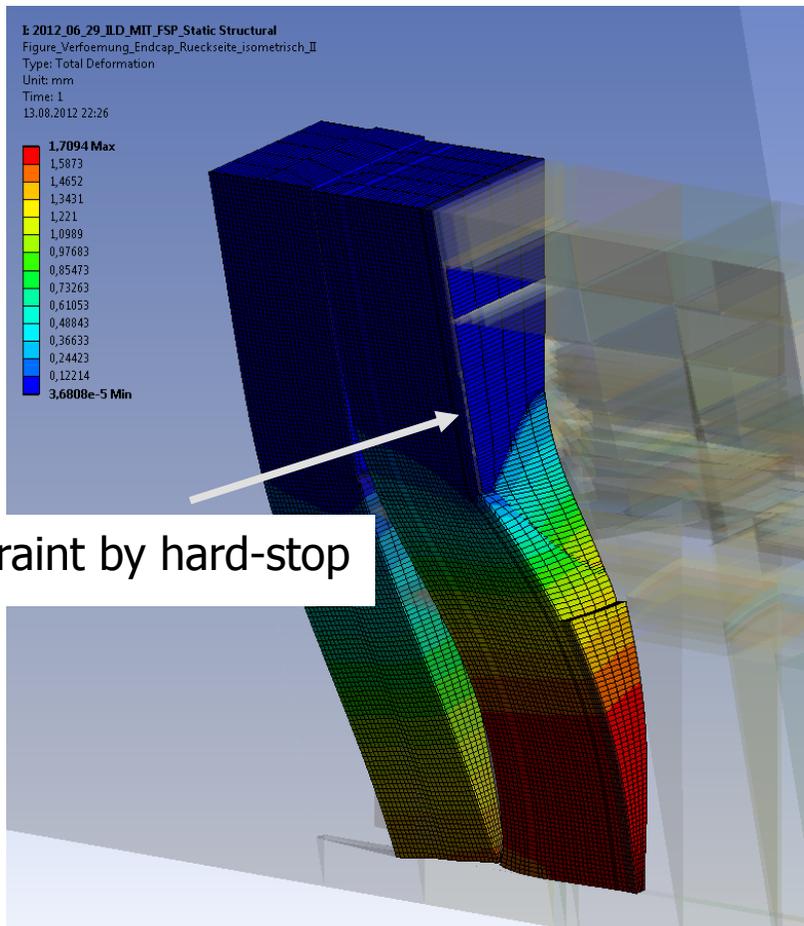
Option: inner and outer end-caps split in z-direction, not vertically

- Fast access to muon chambers in inner EC
- Reduce weight of movable parts

Model not up date. Outer EC not split vertically

End-cap Deformation

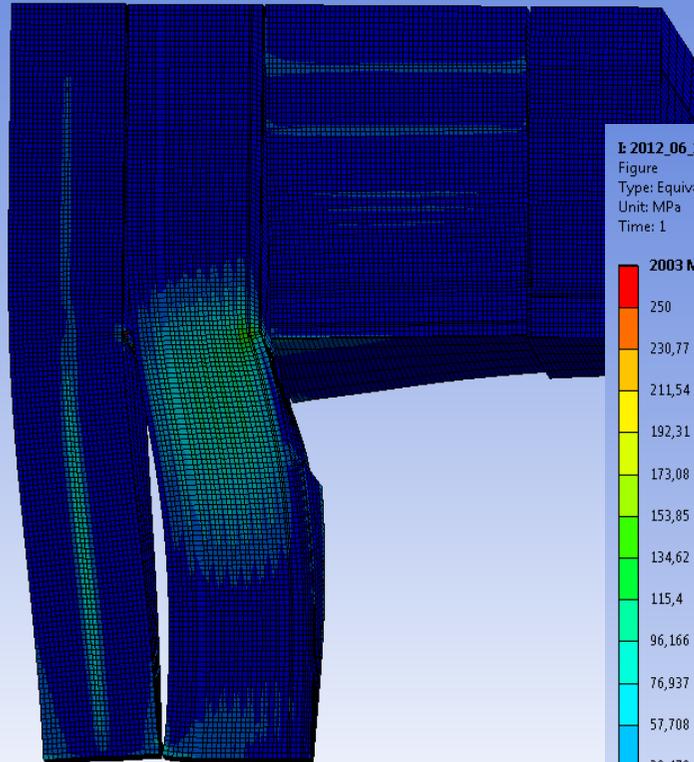
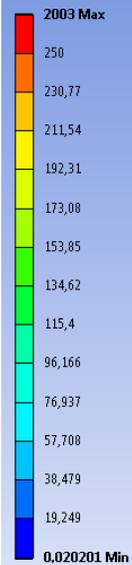
Max. deformation $\sim 2\text{mm}$
due to magnetic force



End-cap Stress

E 2012_06_29_ILD_MIT_FSP_Static Structural
Figure_iso_side
Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1

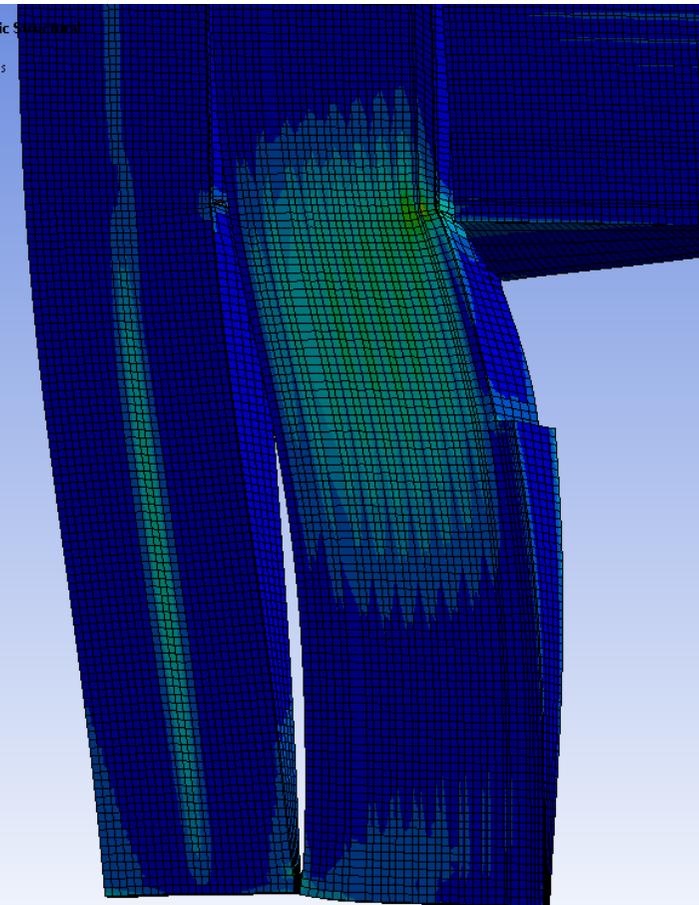
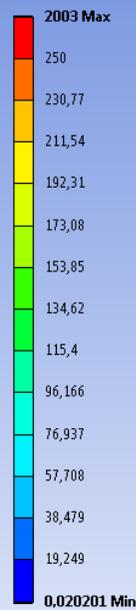
ANSYS
R14.5

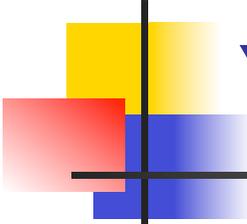


0,00 1500,00 3000,00 (mm)

stress < 200 N/mm²

E 2012_06_29_ILD_MIT_FSP_Static Structural
Figure
Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1





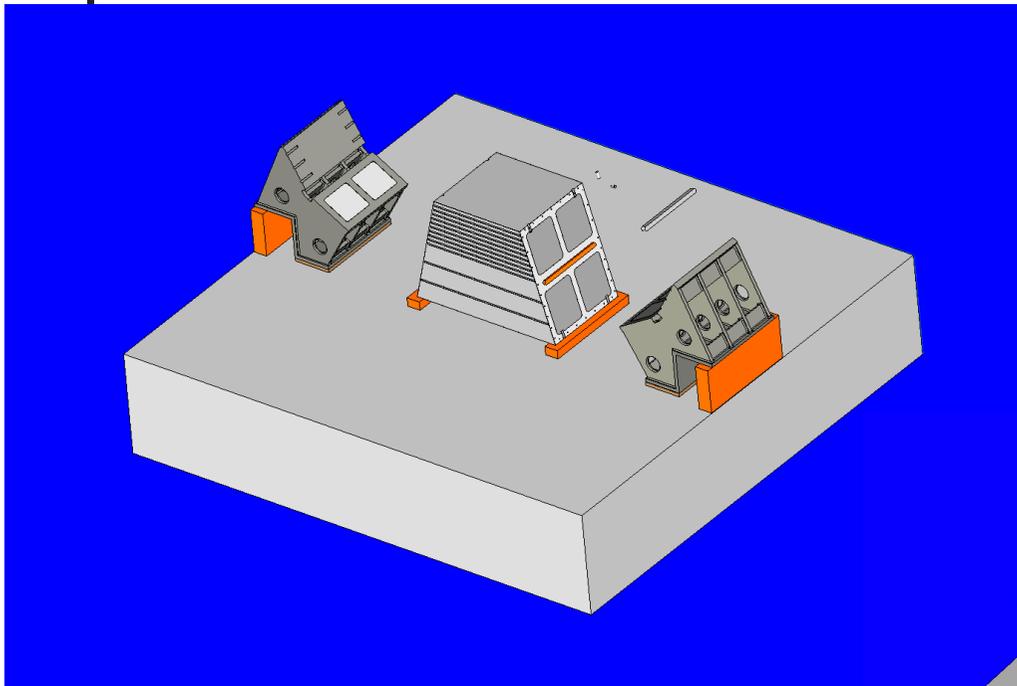
Yoke Assembly

In principle, yoke design and assembly based on CMS assembly

- Barrel consists of 3 large wheels (CMS 5)
 - Barrel segments form a rigid structure
 - No “mandrel” or Ferris wheel needed for assembly
- Each end-cap consists of 1 (or 2) large large disk (CMS 3)
 - Similar shape and assembly
- Original CMS-style assembly (vertical access)
 - All machining and pre-assembly at manufacturer site
 - Assemble wheels and disks in surface building
 - Disassembled again, segments shipped to ILC site
 - Lower wheels/disks into IR hall
- Now, Japanese mountain site IR hall (horizontal access)
 - Yoke design, manufacturing and shipment unchanged
 - Segments (max. weight $\sim 210\text{t}$, gross weight $\sim 250\text{t}$) moved to IR hall
 - Barrel wheels and end-caps assembled in IR hall

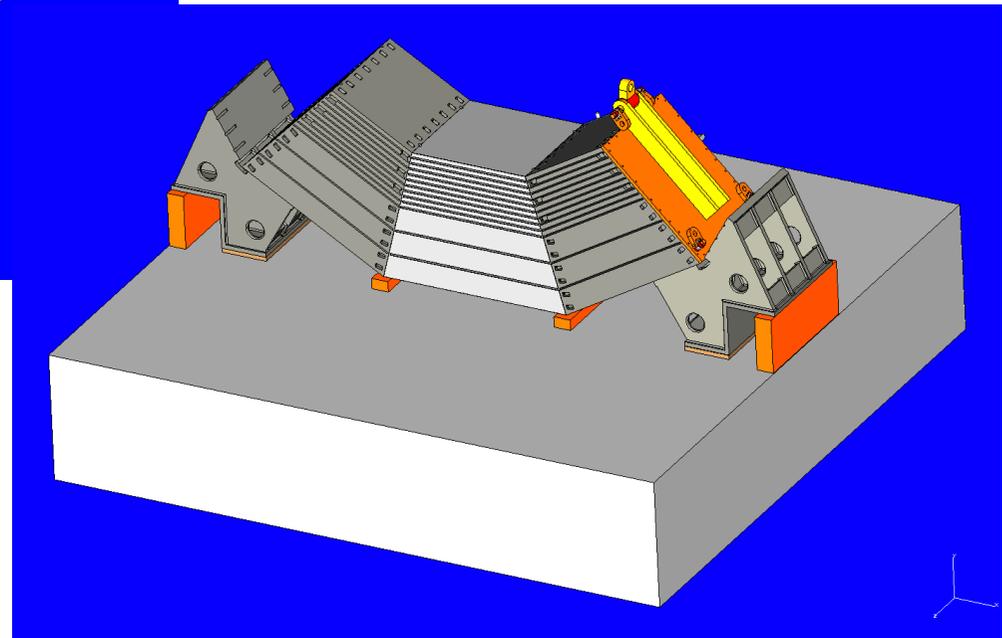
Barrel Assembly

R.Stromhagen

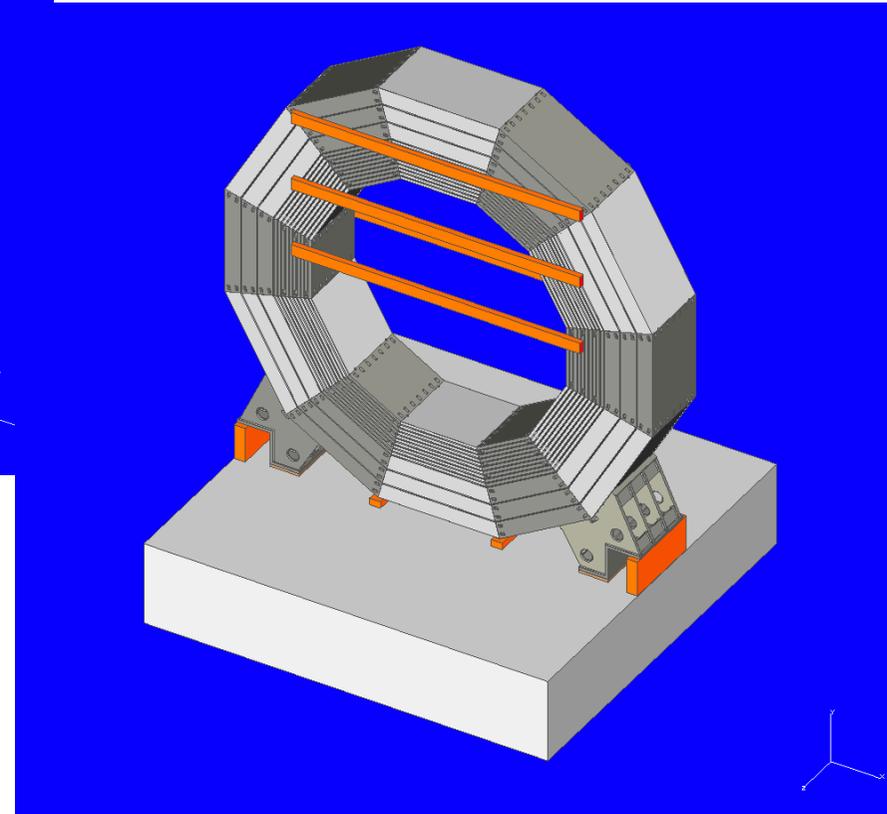
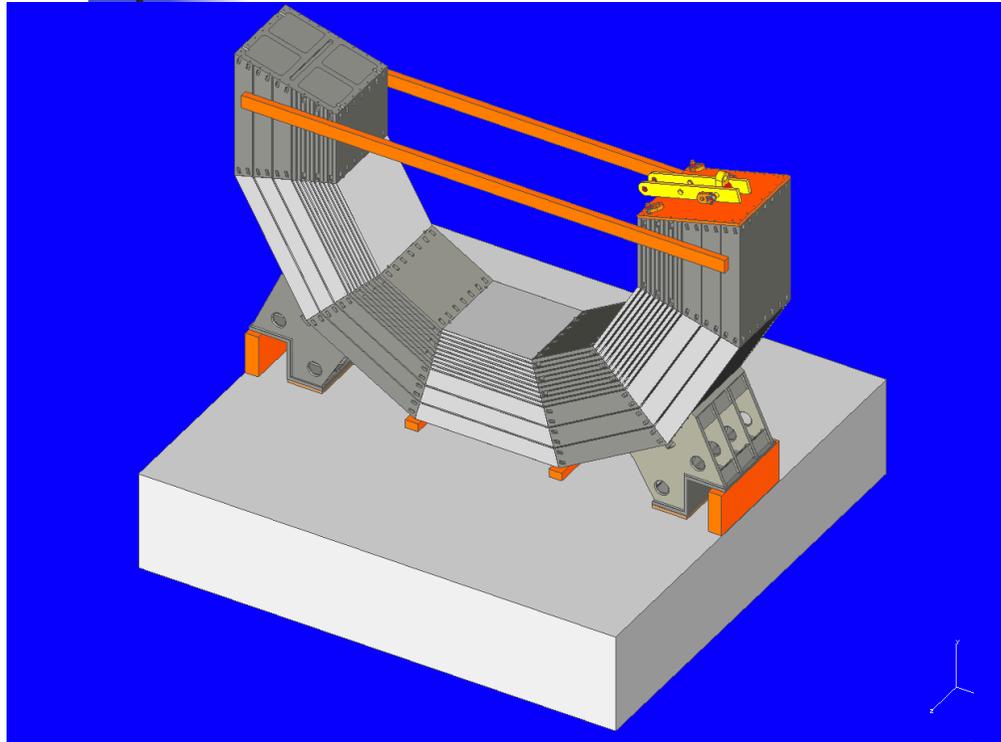


Tools needed:

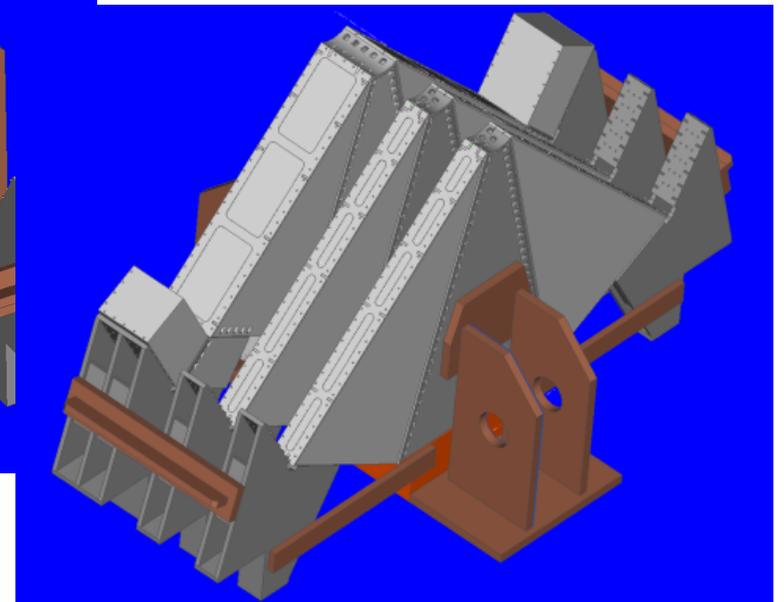
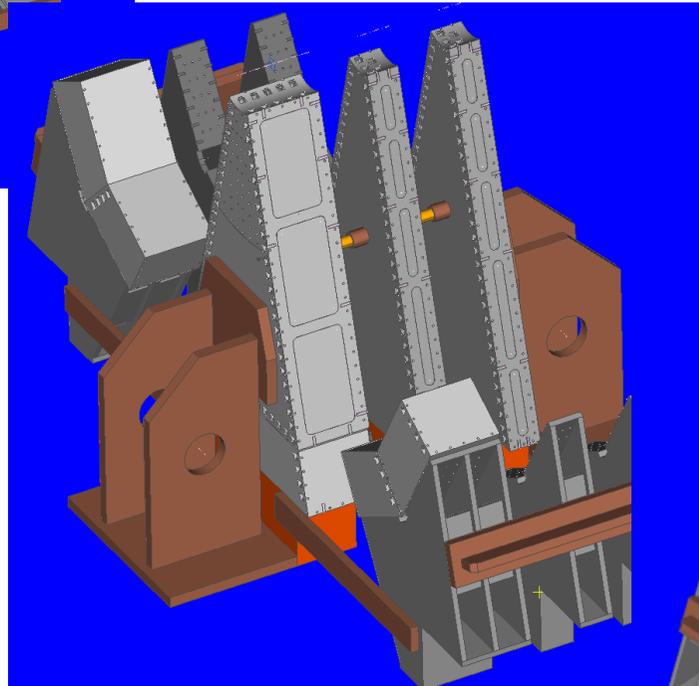
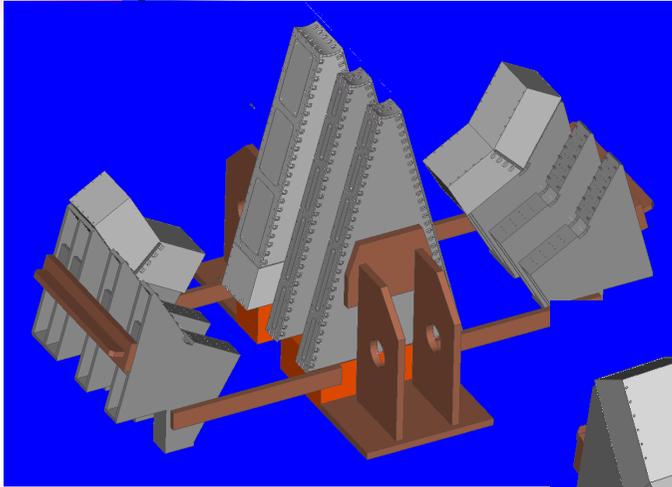
- 250 t crane
- Hoists
- Support structures
- Survey



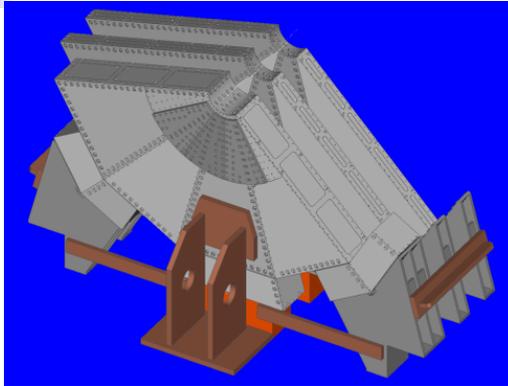
Barrel Assembly



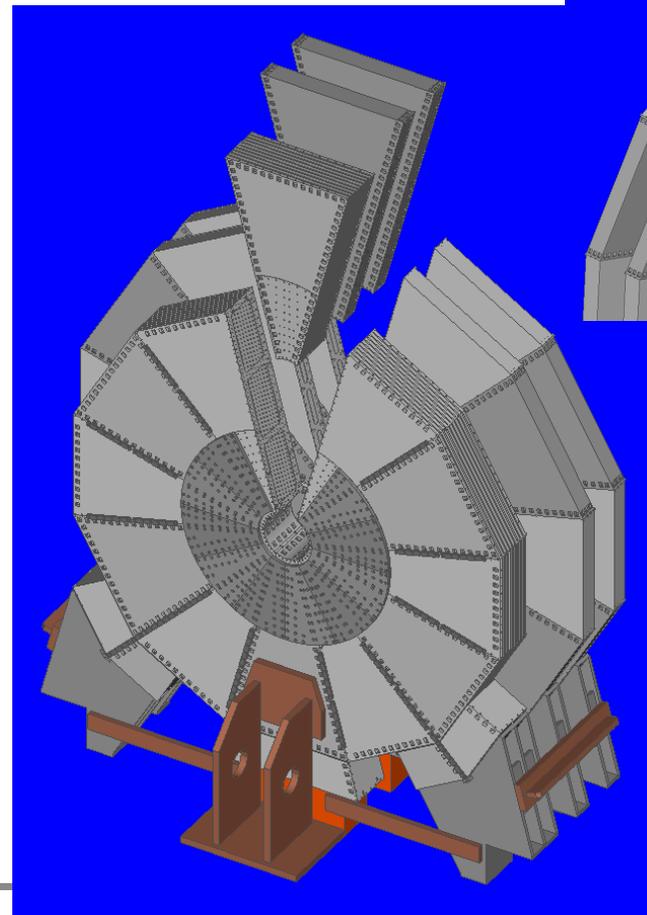
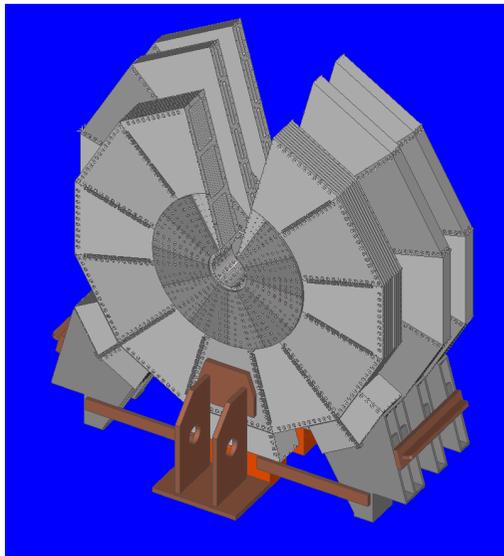
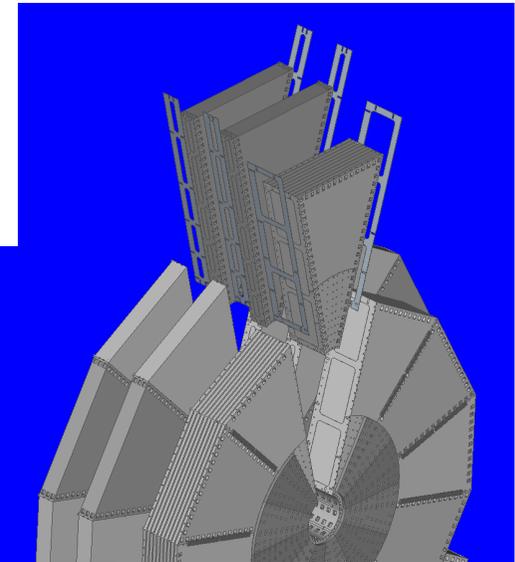
End-cap Assembly



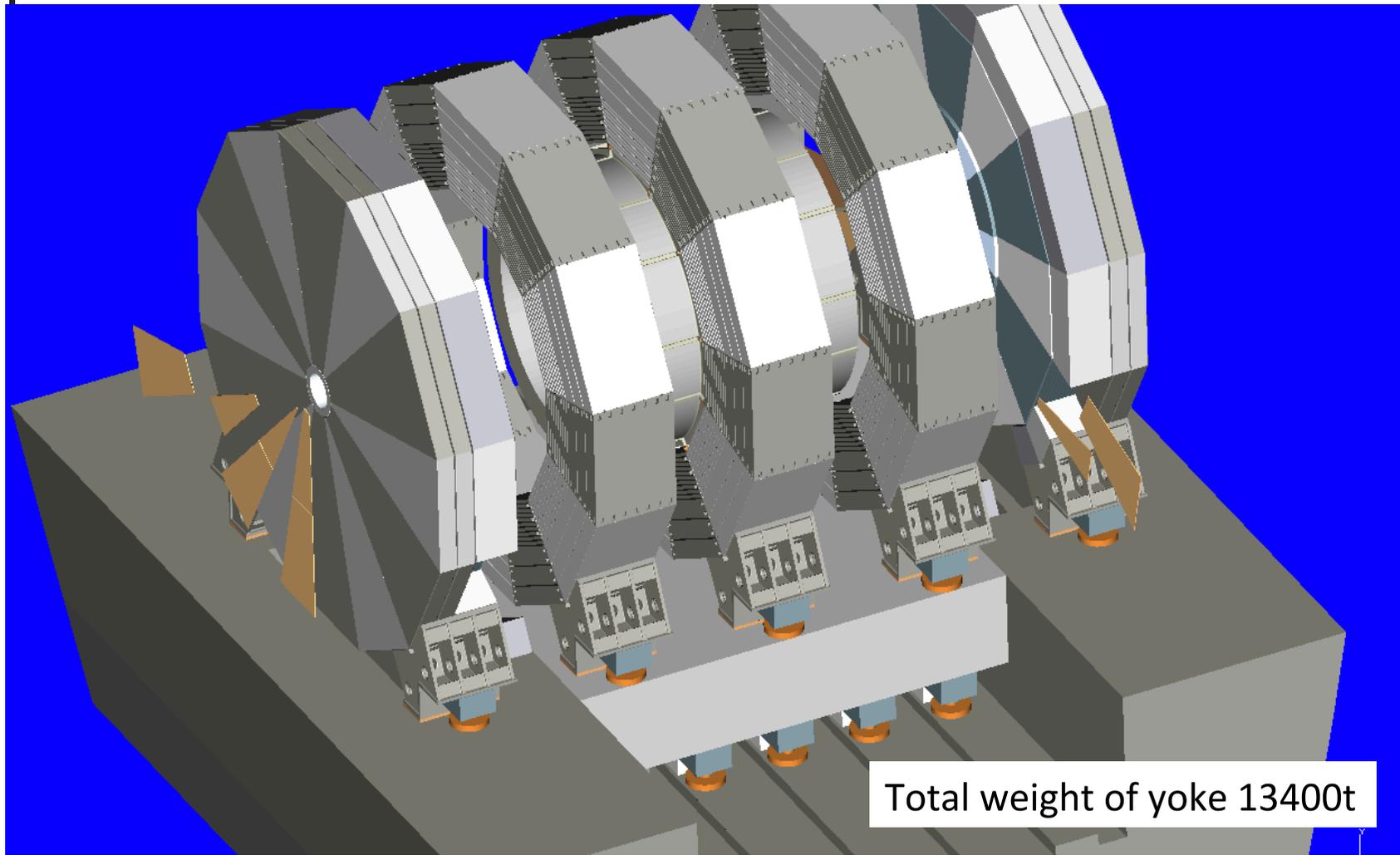
End-cap Assembly

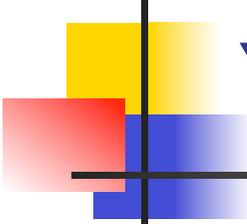


Final segment:
precision machined
or adjusted with shims



Assembled Iron Yoke

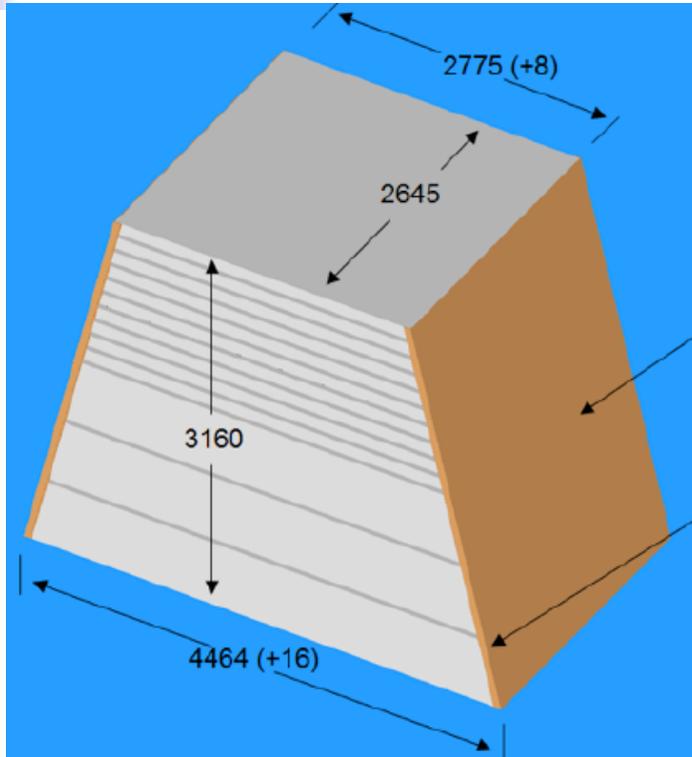




Yoke Transportation

- Have to check transportation limits in Japan
 - Are ~250t transports a problem?
 - Are less heavy transports significantly cheaper?
 - In Europe <100t straight forward. Much more difficult if heavier, need special permit

Segment Dimensions

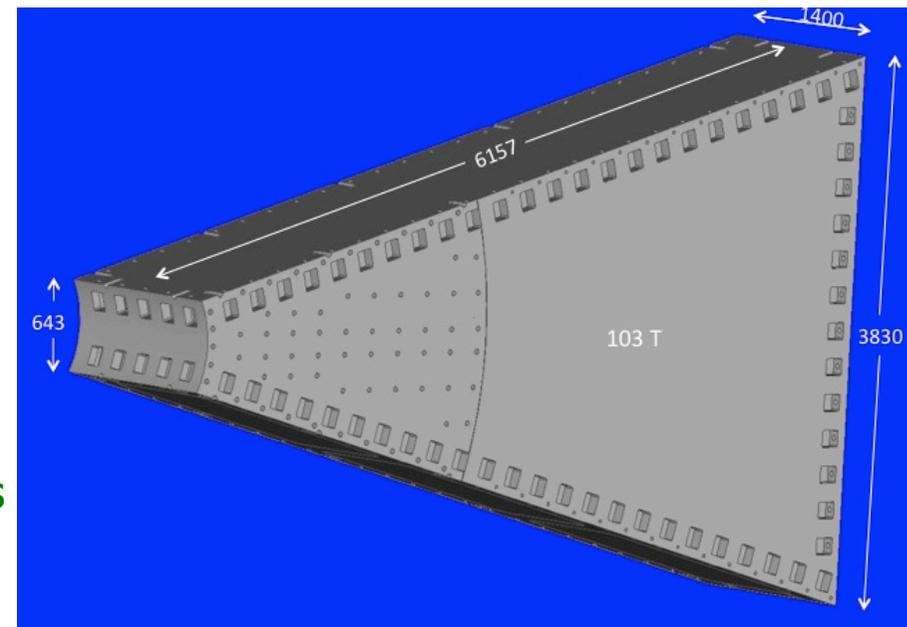


Barrel

- Weight ~210t 18 pieces
- Plus 18 slightly smaller pieces weight ~170t

Inner end-cap

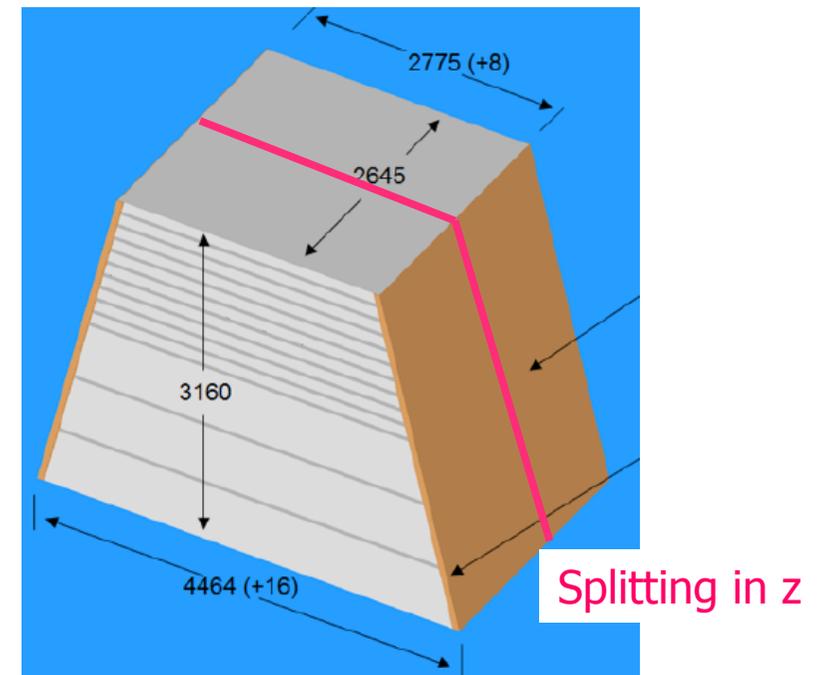
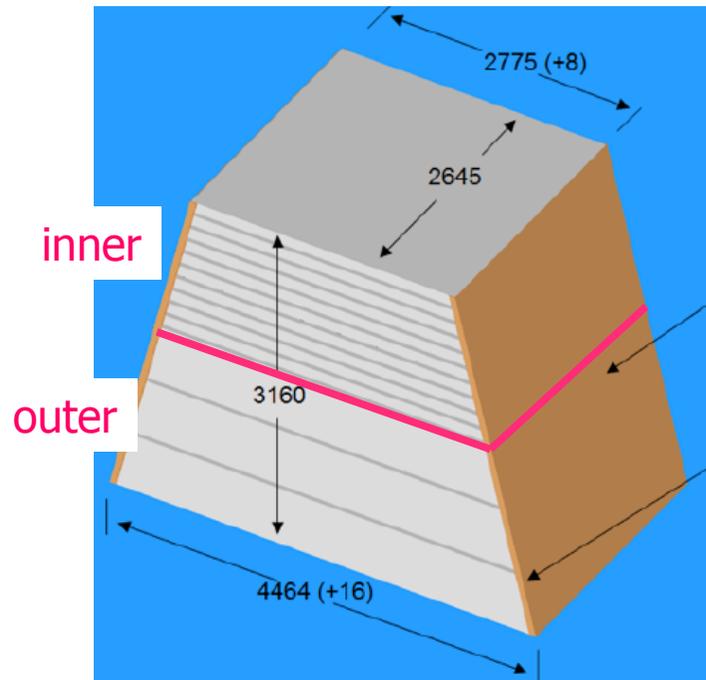
- Weight ~100t 6 pieces
- Plus 6 slightly + outer end-caps

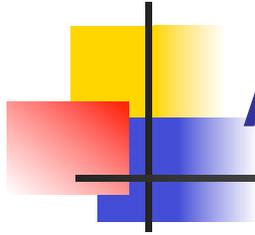


Barrel Segment Dimensions

Could reduce segment size and weight

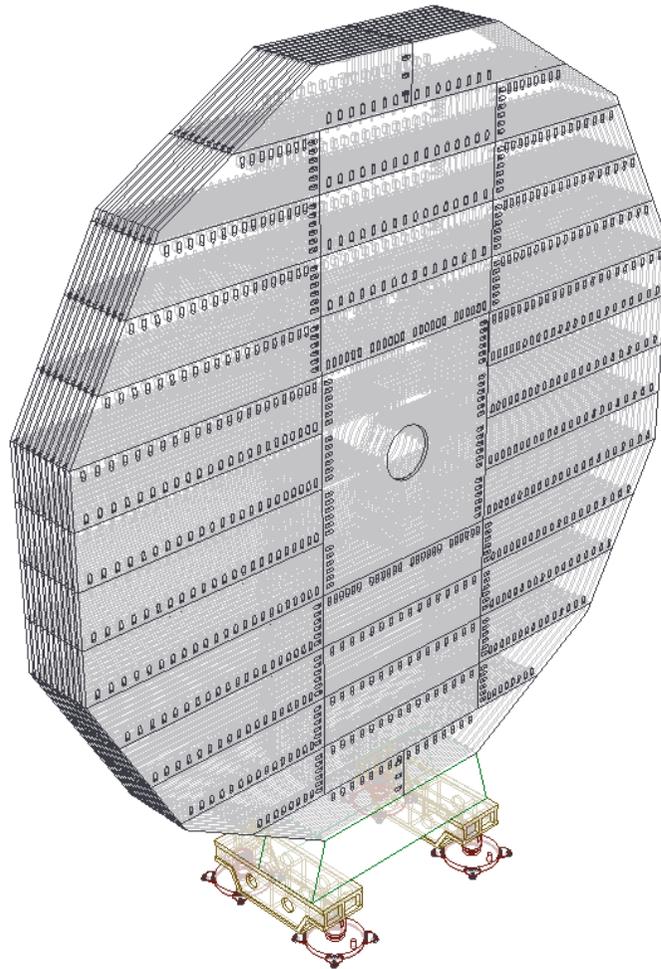
- Splitting into inner and outer segments
 - Need additional mounting/connection plates between inner and outer
 - Achieving tolerance during machining more difficult
- Splitting in z-direction
 - No problem with forces. Magnetic force acting in z-direction. Compressing wheels
 - Achieving tolerances easier



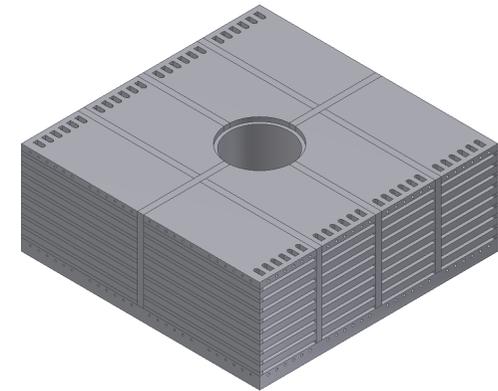
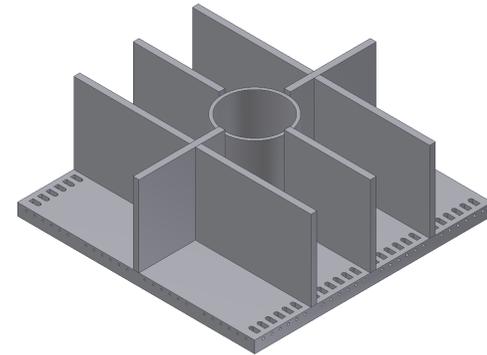


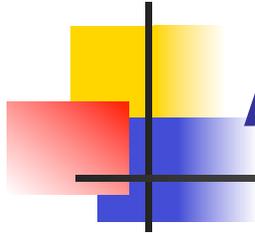
Alternative End-Cap Design

Design by Hubert Gerwig and Nicolas Siegrist, CMS/CERN



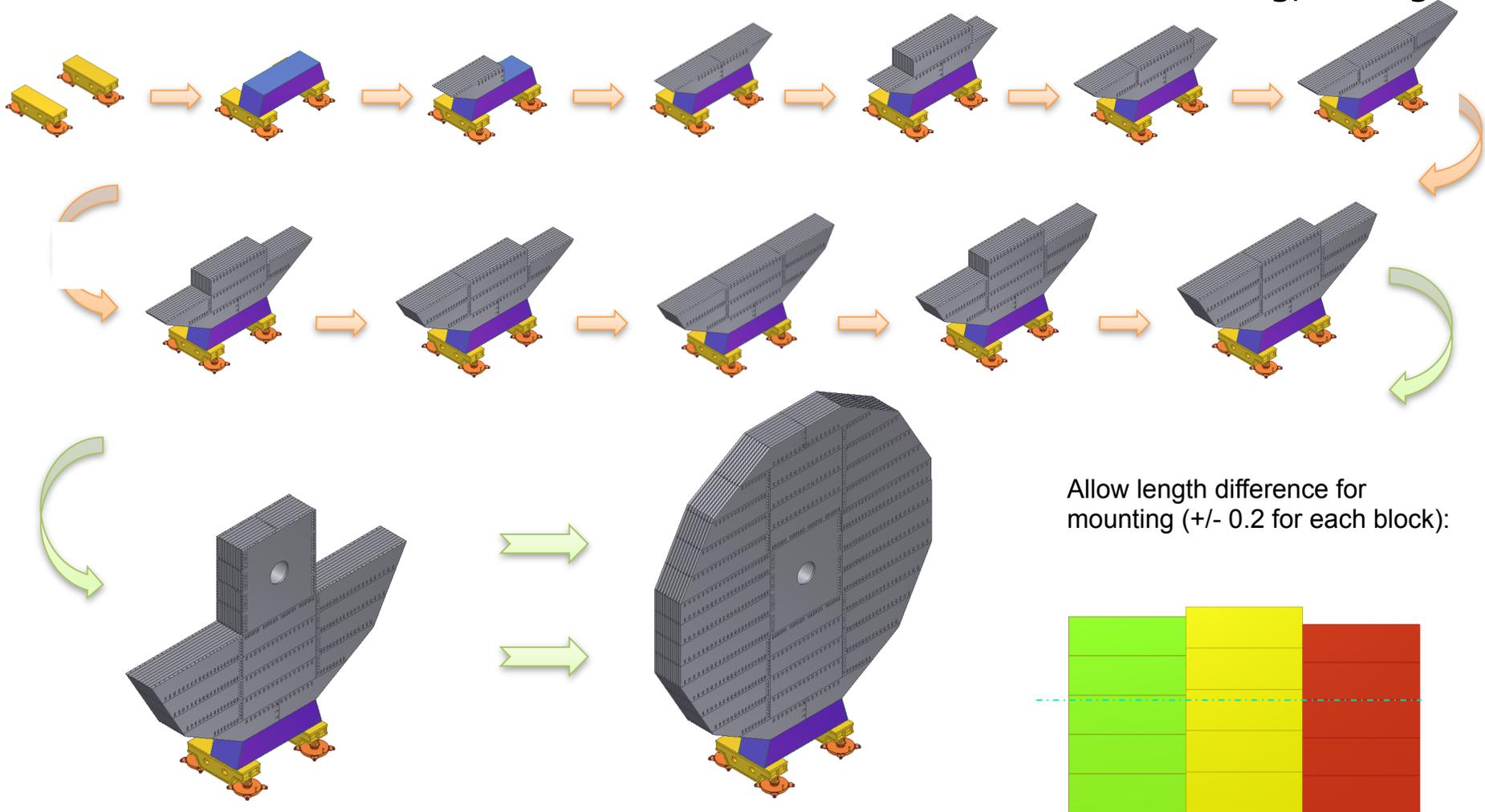
Segments of 40t
Central part 120t





Alternative End-Cap Design

H.Gerwig, N.Siegrist

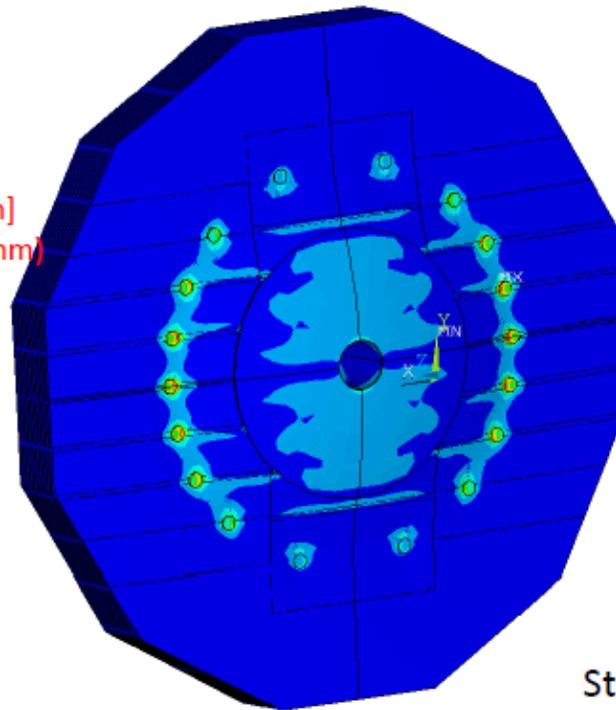


End-Cap Design Horizontal Supports

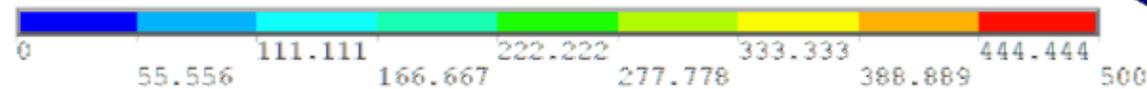
CLIC note 2010-10
Gerwig et al.

```
NODAL SOLUTION  
STEP=1  
SUB =1  
TIME=1  
/EXPANDED  
SEQV (AVG)  
DMX =5.998  
SMN =-1.14825  
SMX =1548
```

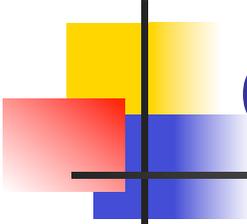
Deformation [mm]
(FYI: in CMS ~16mm)



Stress in the horizontal
spacers below 200 MPa

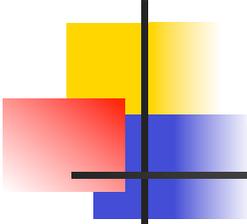


Considering to use better quality steel



Comparison of Inner End-cap Designs

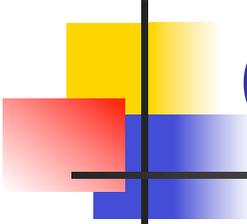
- Radial reinforcement design
 - ϕ symmetric deformation and stress
 - Iron and magnetic field ϕ symmetric
 - Hard stops straight forward
 - Symmetric forces acting on barrel
 - 12 segments plus small inner support tube
 - Fewer surfaces to be machined precisely
 - Half as much reinforcement (and dead space)
 - Present models (2x25mm) radial vs. (2x50mm) horizontal supports
-> dead space 3% vs. 12%.
- Horizontal reinforcement design
 - Deformation and stress somewhat higher
 - 36 segments segments plus big central piece
 - Assembly somewhat easier
 - Installation of muon chambers easier
- Should do cost comparison (manufacturing, transport, assembly)



Material Properties - Tolerances

Preliminary

- Mechanical properties
 - Yield strength > ~250 MPa
 - Ultimate strength > ~350 MPa
 - Good weldability (low carbon content)
- Magnetic
 - Absolute properties not essential since highly saturated
 - Relative permeability should be uniform
- Tolerances
 - Outer dimensions $\sim \pm 5\text{mm}$
 - Inner dimensions tolerances up to manufacturer
 - No gaps, surfaces must fit



Conclusions

Present conceptual design quite advanced

- Not yet cost optimized

Several options/open issues

- Thickness of iron (determines cost)
 - Required stray field limit?
 - Need better understanding of stray field calculations
 - Reliability of FEM calculations. Is 0.1% accuracy realistic?
- Need critical assessment of design and construction method
 - Cost and performance optimization
 - Size and weight of yoke segments
 - Manufacturing, transport and assembly of small vs. large segments
 - Time of construction and assembly
 - Decide of end-cap options
- In contact with Japanese industry. Will visit KHI on Friday