

Sensor and Module Design

Tim Nelson

SLAC

3/2/2006



Goals for 2006

KPiX-T

- Working 2X32 chip delivered and tested
- Submission of full-sized chip

Sensors

- Develop detailed design for sensors
- Obtain prototype sensors from Hamamatsu

Cables

- Develop detailed design for pigtails
- Obtain quotes for pigtails

Module Assembly

- Develop fully designed/engineered sensor supports
- Develop fully designed/engineered module mounting scheme

Sensor Design

Much of design can be derived from existing devices

- Double-metal & bump bonding issues from ECAL sensors
- 50(25) readout(sense) geometry from HPK Layer 00 sensors

What's Left?

- Optimize double-metal layer for strip geometry
 - Minimize capacitance and balance with trace resistance
 - Equalize trace capacitance/resistance over entire sensor
- Details of vias in dense 50/25 geometry?
- AC/DC coupling decision?

Design Requirements

Want $S/N > 20$. Following work at Oregon by David Strom:

❏ Limit capacitance to 40 pf

❏ Limit total trace resistance to 500 ohms

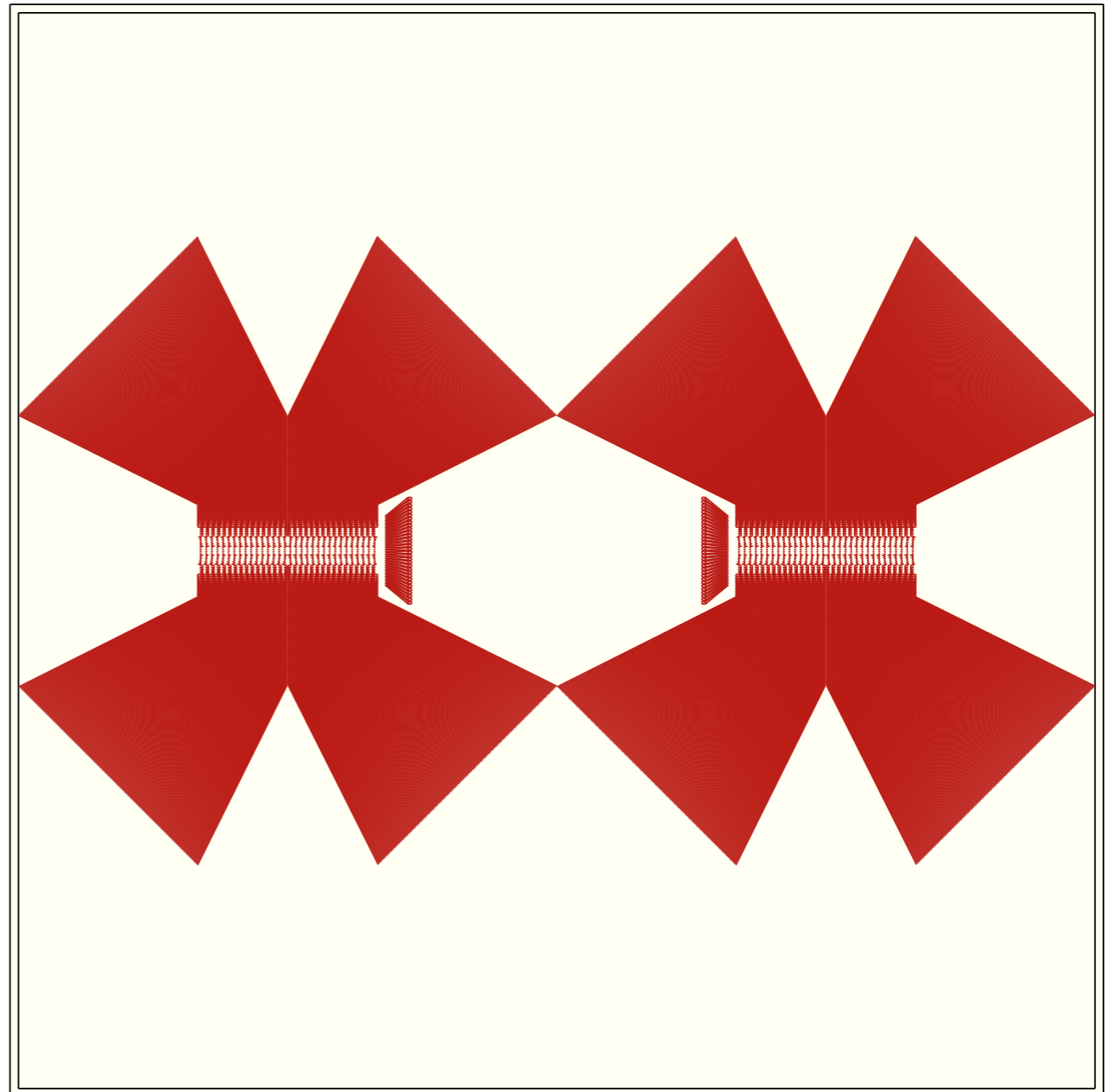
➔ **These result in $S/N = 25$: depends on still-unknown transconductance of input FET (assumed here to be 2mS)**

Want resistance of power supply/return < 1 ohm (including cable!)

➔ **Detector must minimize the resistance of these double-metal traces.**

Preliminary Sensor Design

- 🍯 9.75cm square
- 🍯 0.75 mm bias/guard area
- 🍯 1920 channels (64X30)
- 🍯 Two readout chips!



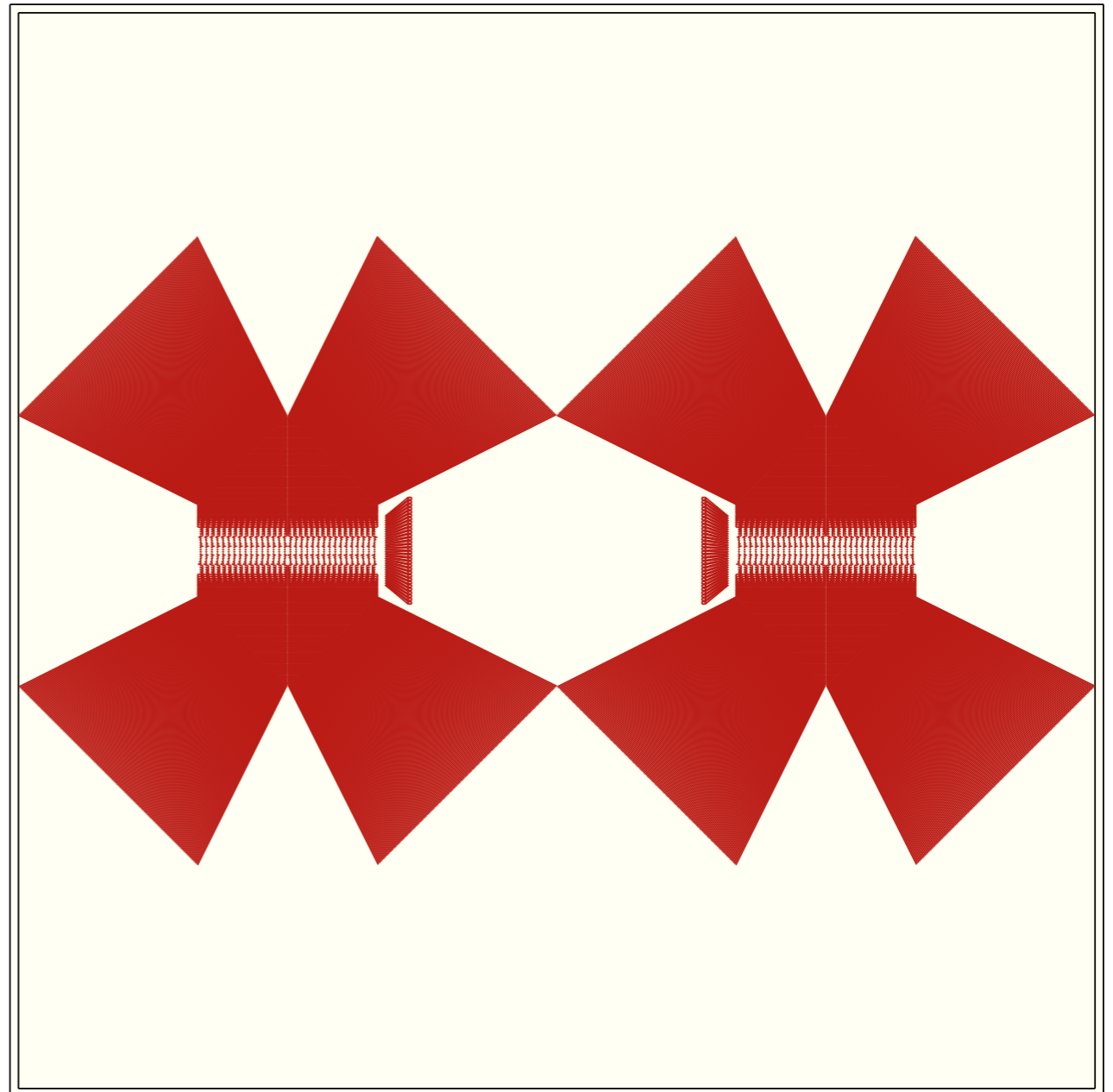
Two Chips vs. One?

Advantages

- ❖ Same die size as ECAL
Dieter: "1024 already quite large."
- ❖ Average double-metal trace reduced in length by factor of 2
➔ Reduces both capacitance and trace resistance
- ❖ Range of double-metal trace lengths reduced by factor of 2
➔ Equalizes both capacitance and trace resistance

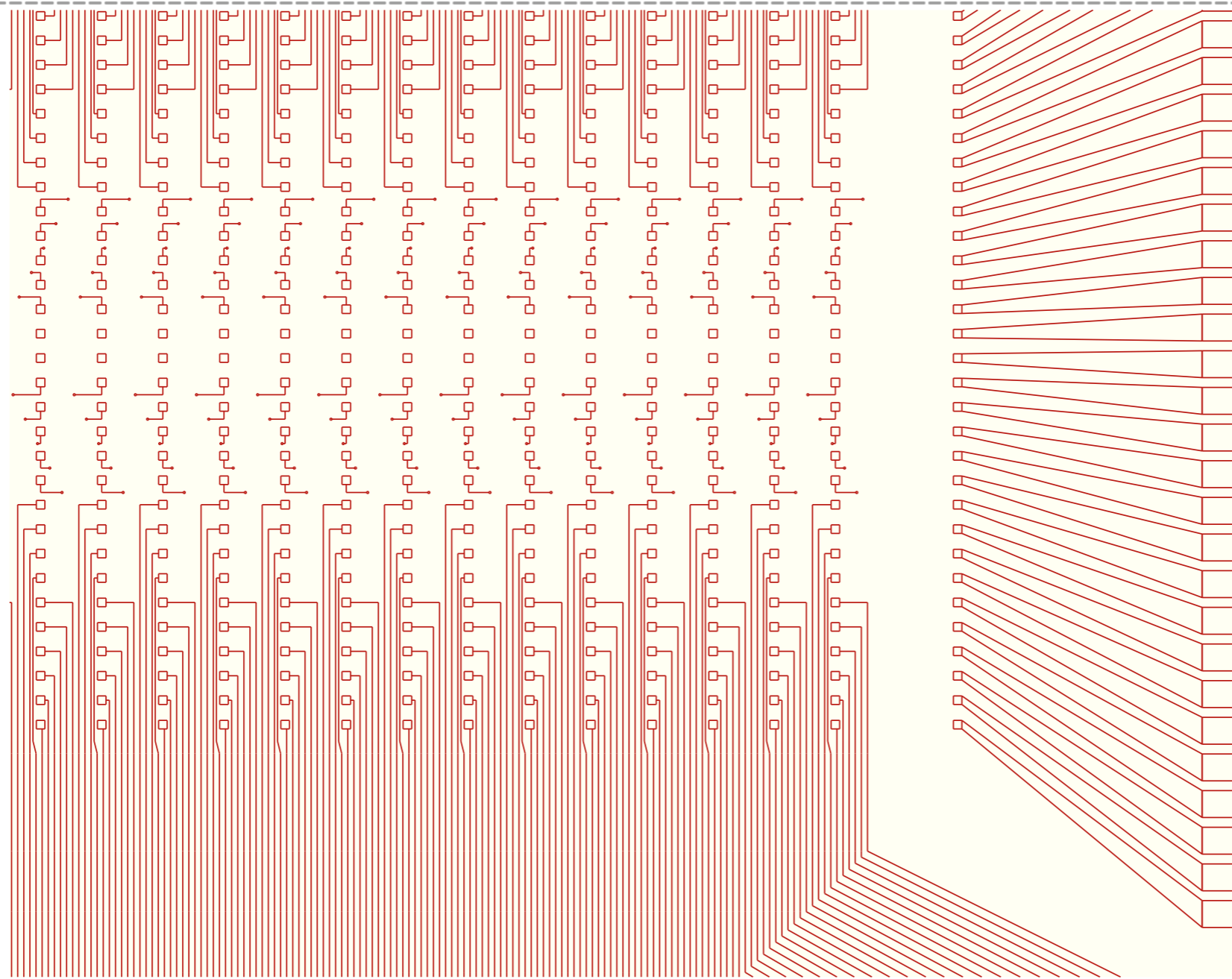
Disadvantages

- ❖ Two chips to connect





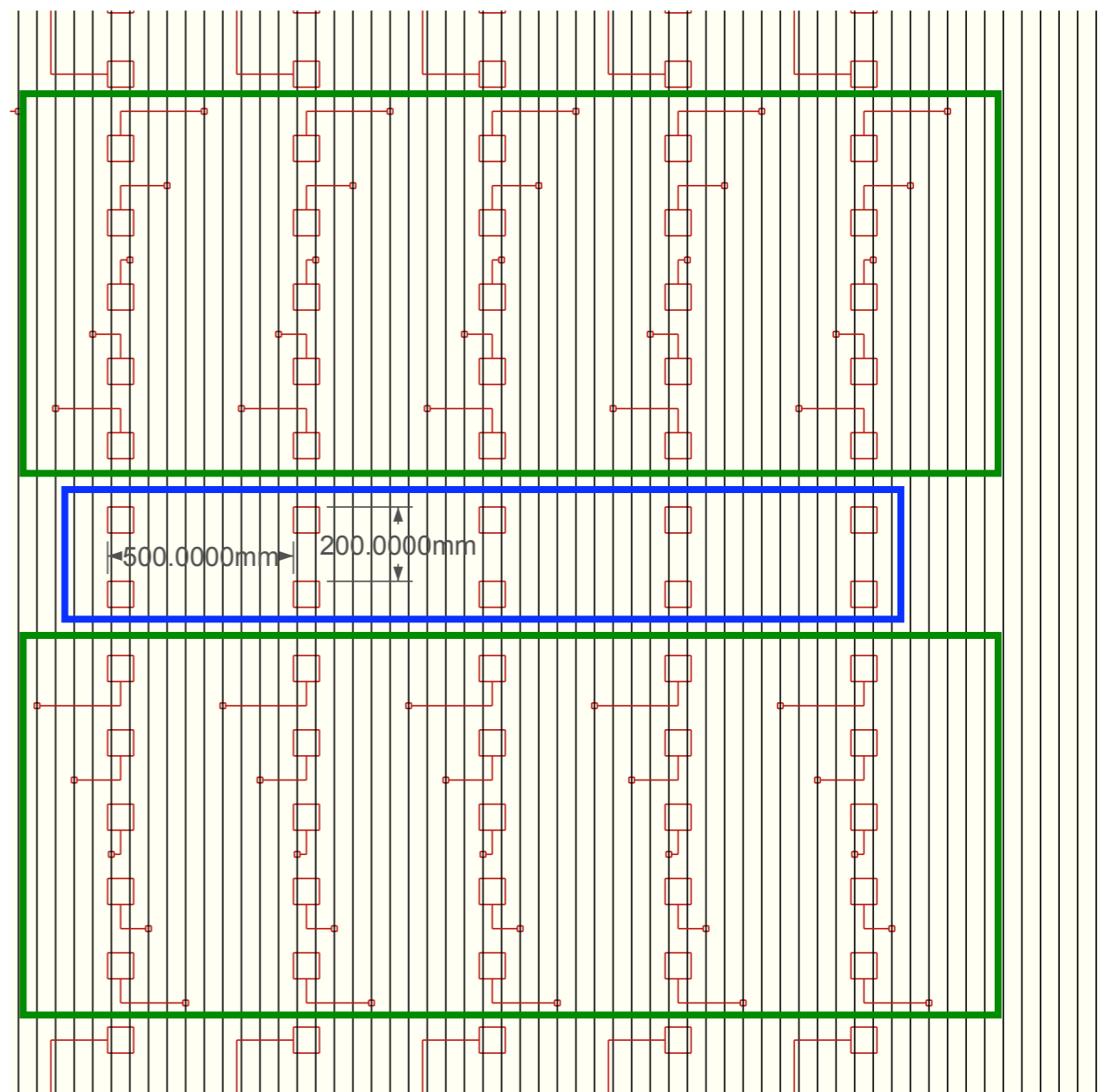
Double-Metal Layout



Double-Metal Layout

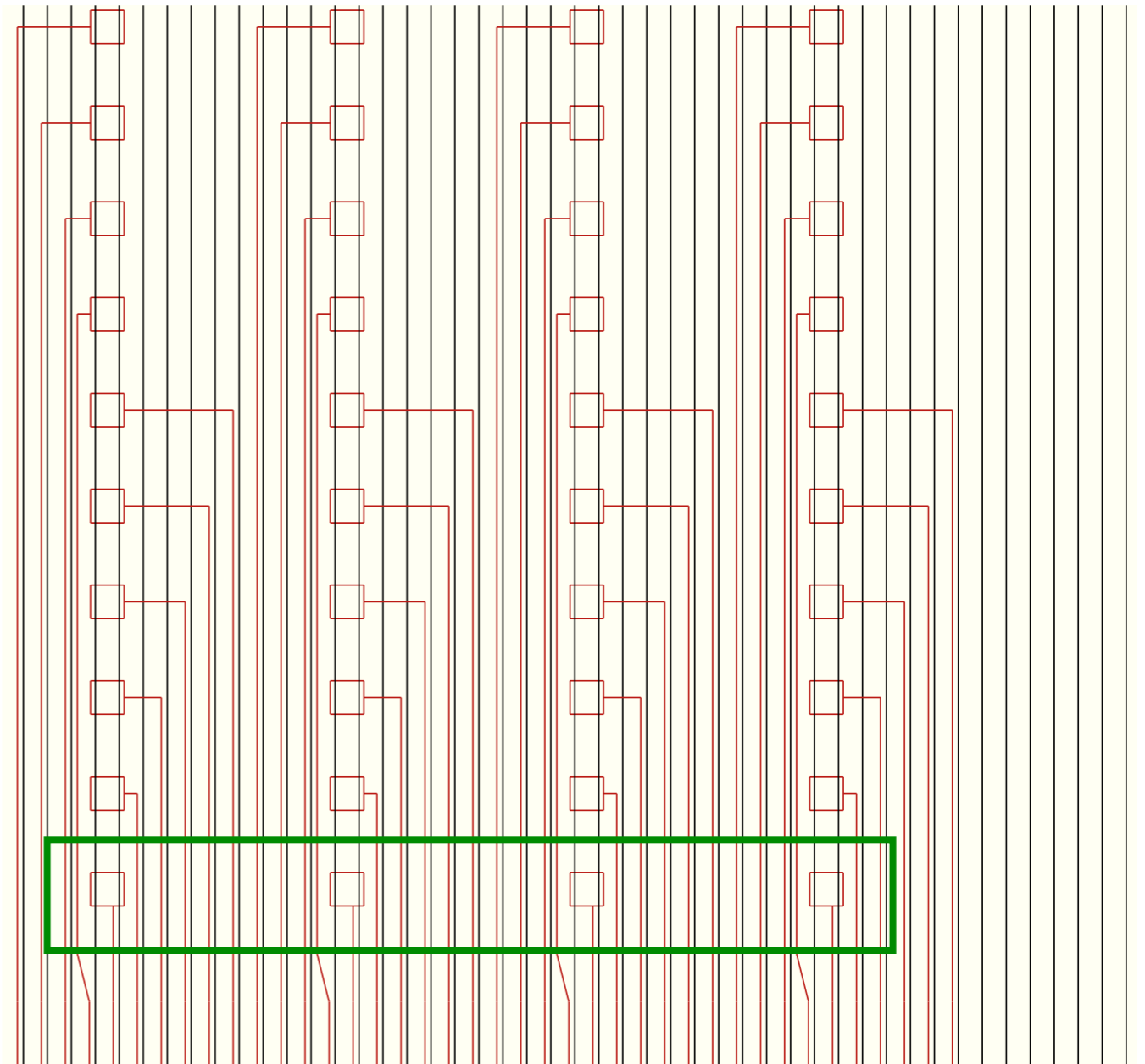
Easier than ECAL

- 🔸 Only use 30/32 KPiX-T rows
- 🔸 10/30 rows can connect directly underneath the chip
- 🔸 20 traces left to route from each column: 10 on each side
- 🔸 With 500 micron column spacing, ten readout strips to route out between each column:
 - ➡ leaves 9 spaces between strips



Double-Metal Layout

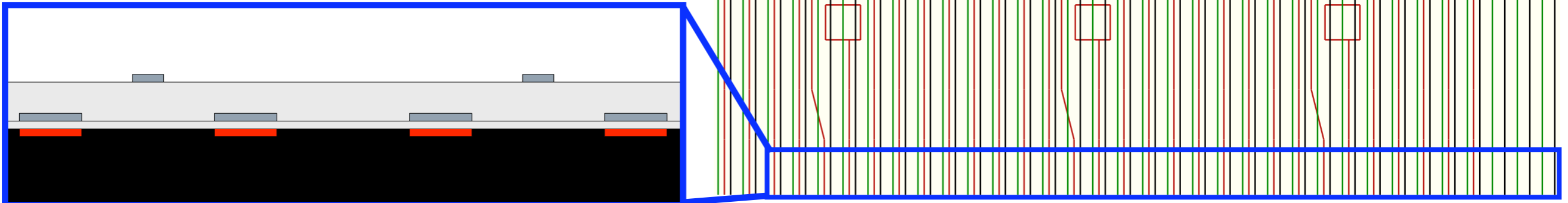
- ❏ **One trace comes for free: directly from edge of array!**
- ❏ **Leaves a trace for each gap between readout strips.**



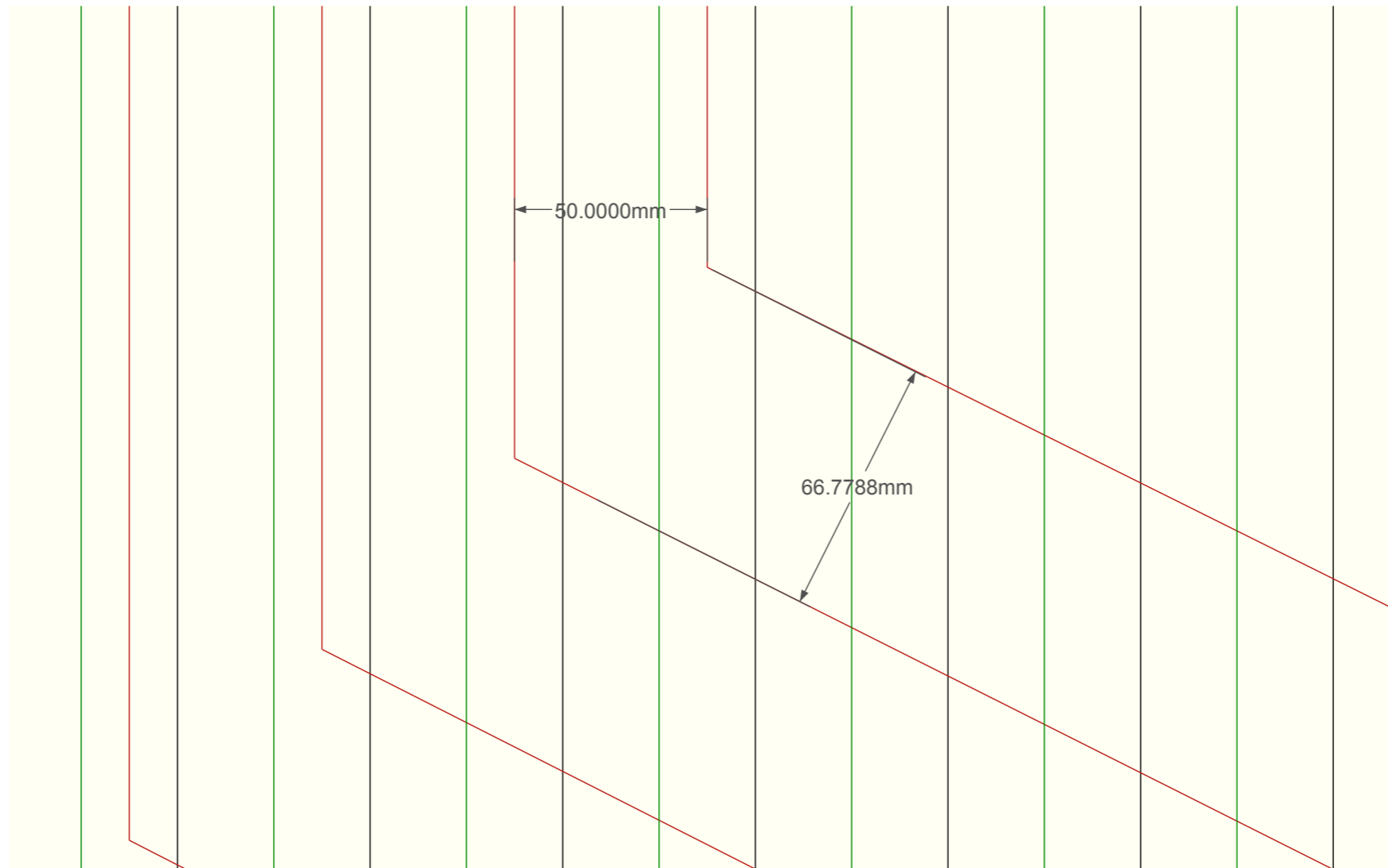
Double-Metal Layout

Don't forget the floating strips!

- ❏ 8 micron strip width
- ❏ 4 micron trace width
(ECAL uses 6, may change to 3-4. HPK says 2 OK.)
- ❏ 5 micron passivation beneath double-metal



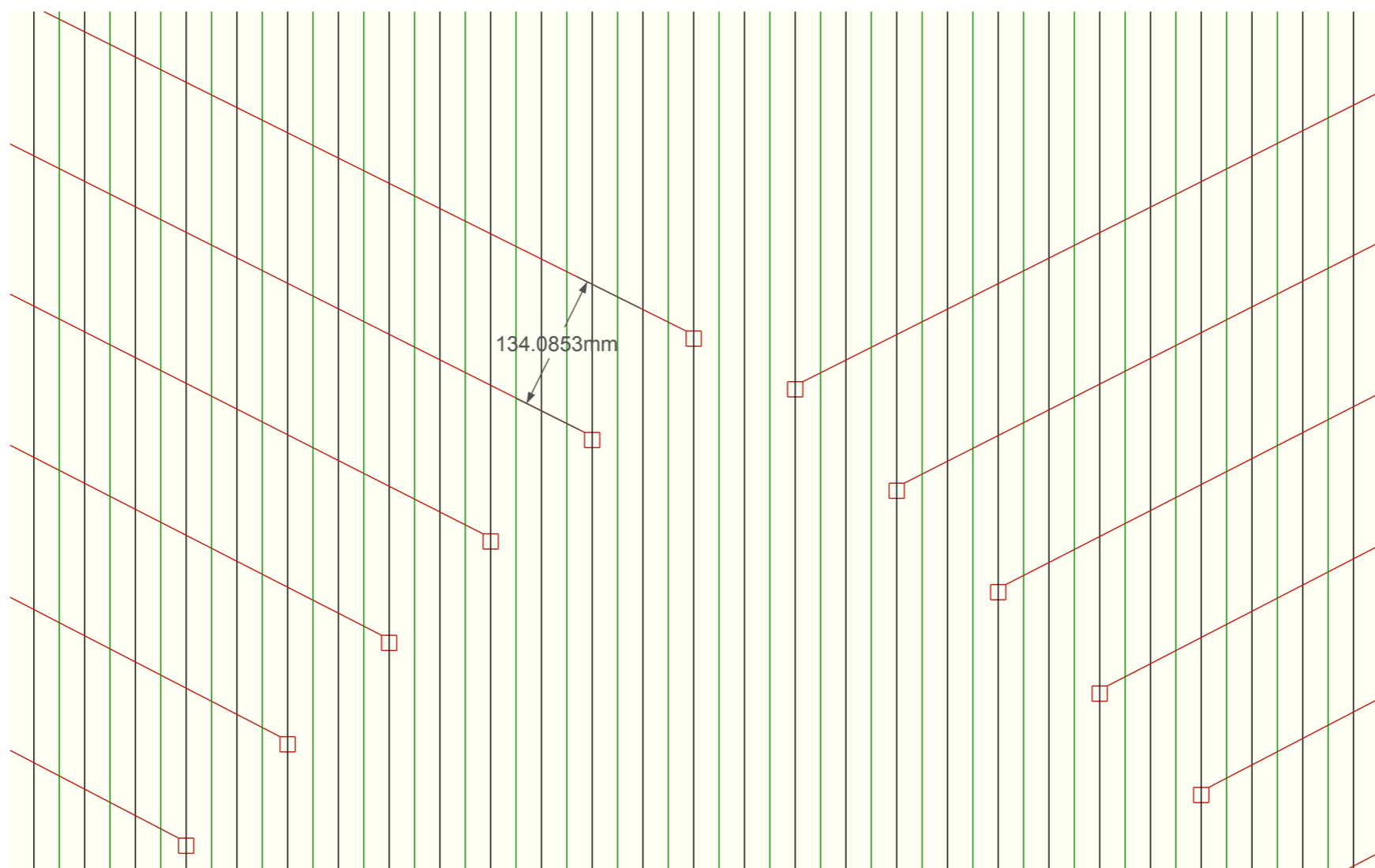
Double-metal Details



Change from 4 to 6 micron trace width at fanout.



Double-metal Details



Crossing capacitance will dominate in fanout: ~6-8 fF / crossing.



Performance Guesstimates

Shortest Trace

15 pF

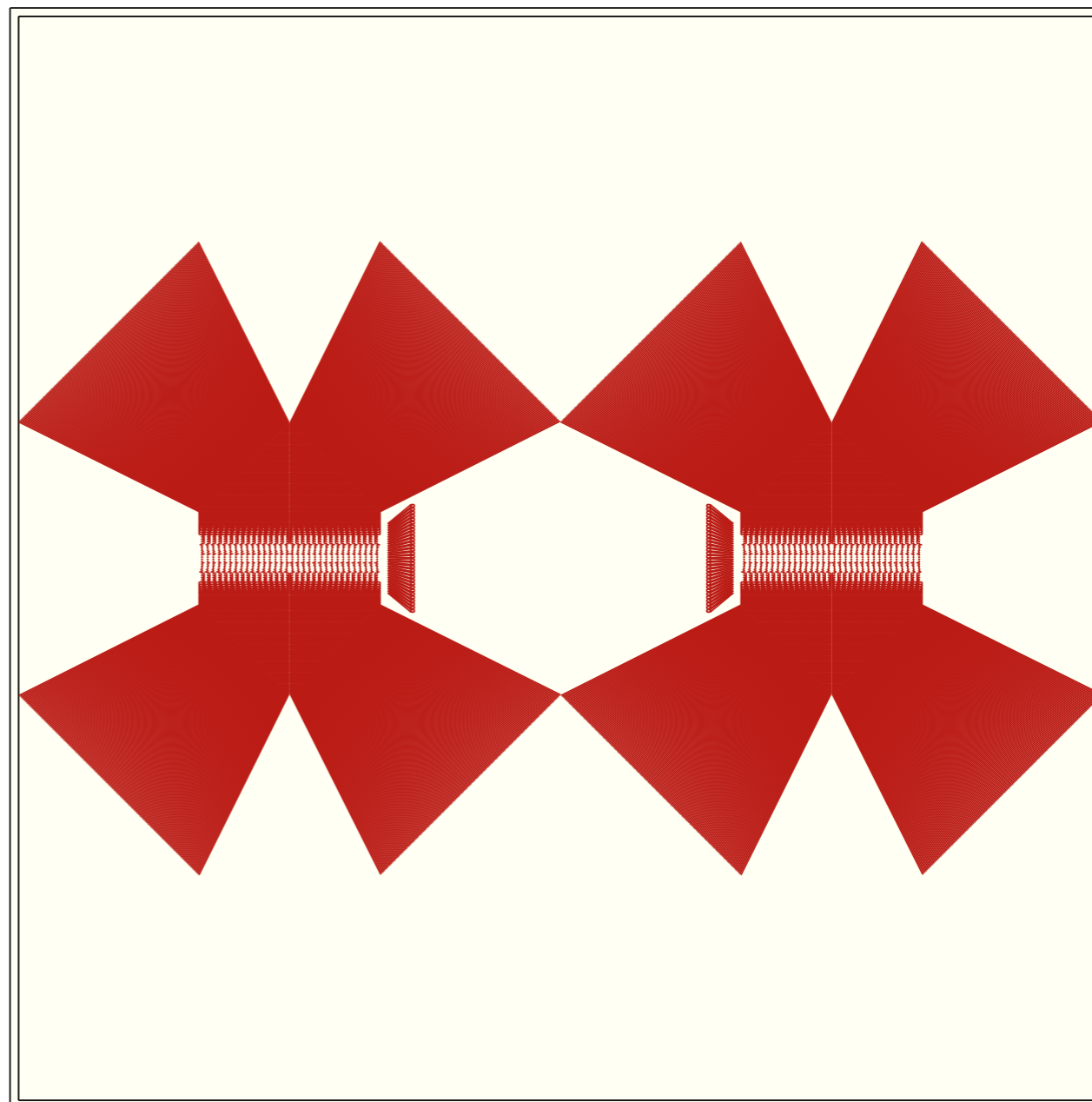
225 ohms

Longest Trace

21 pF

490 ohms

Should easily achieve S/N = 25



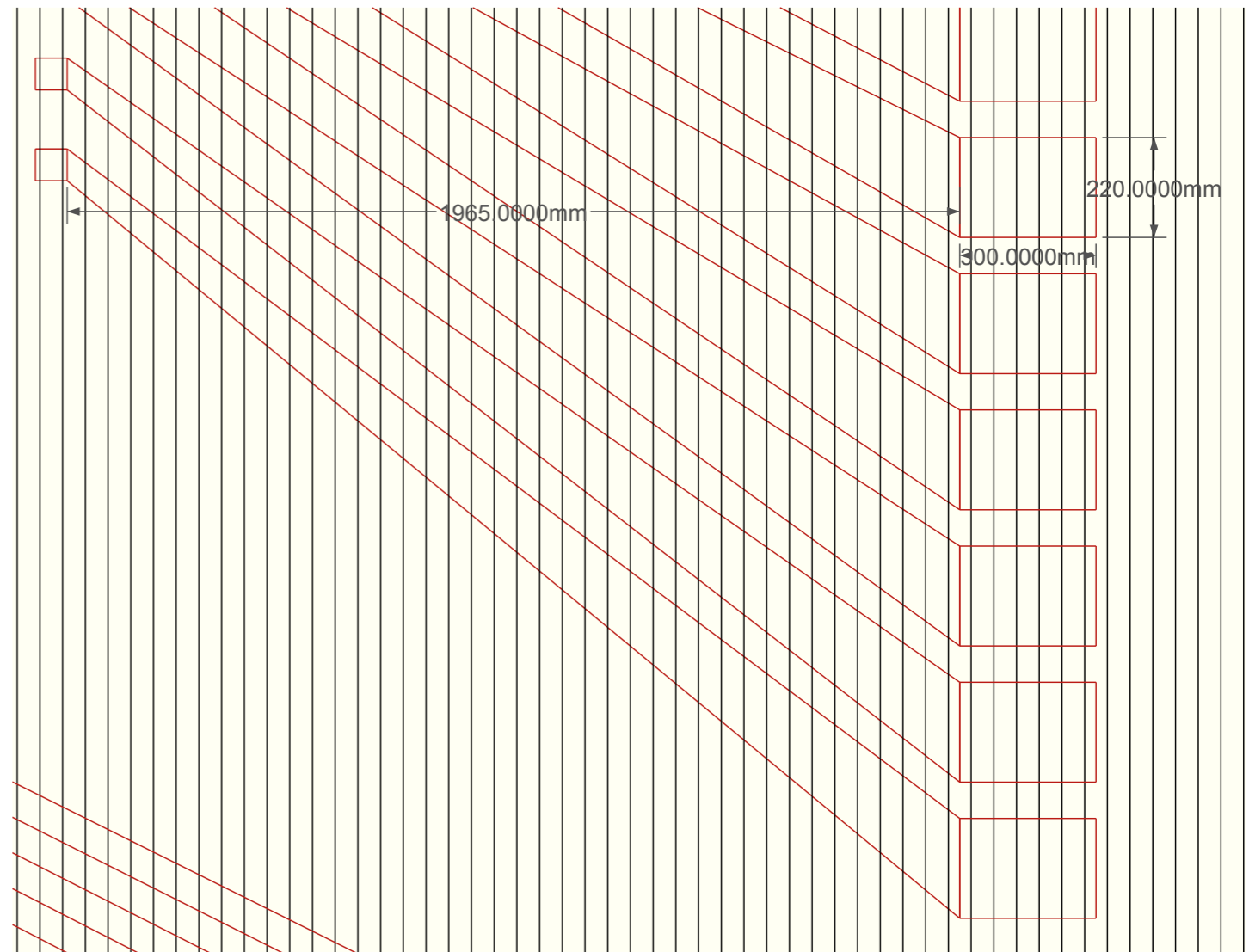
Power Connections

Chip layout has a full column of connections (32) at edge

Current generation uses many of these for test signals: most will ultimately serve power

- ❖ Each double-metal power trace is ~0.5 ohms
- ❖ Several ganged together can achieve required power+return resistance

Strips underneath these traces pick up about 3 pF additional capacitance.



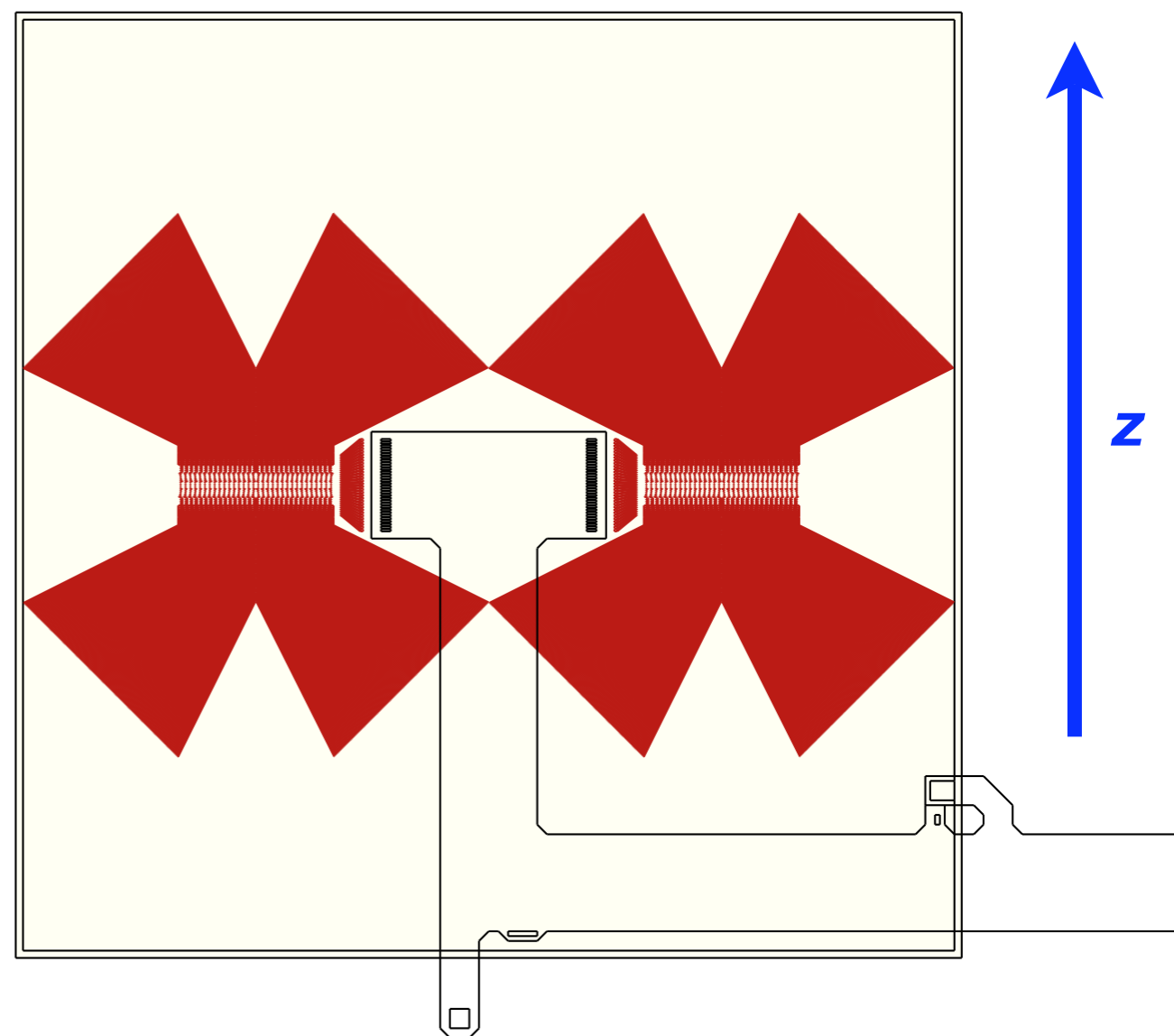
Cable Connection

Proven solution: glue & wirebond cable to face of sensor

- 1mm gap from edge of cable to bond pads on sensor
- 2-2.5mm bond length

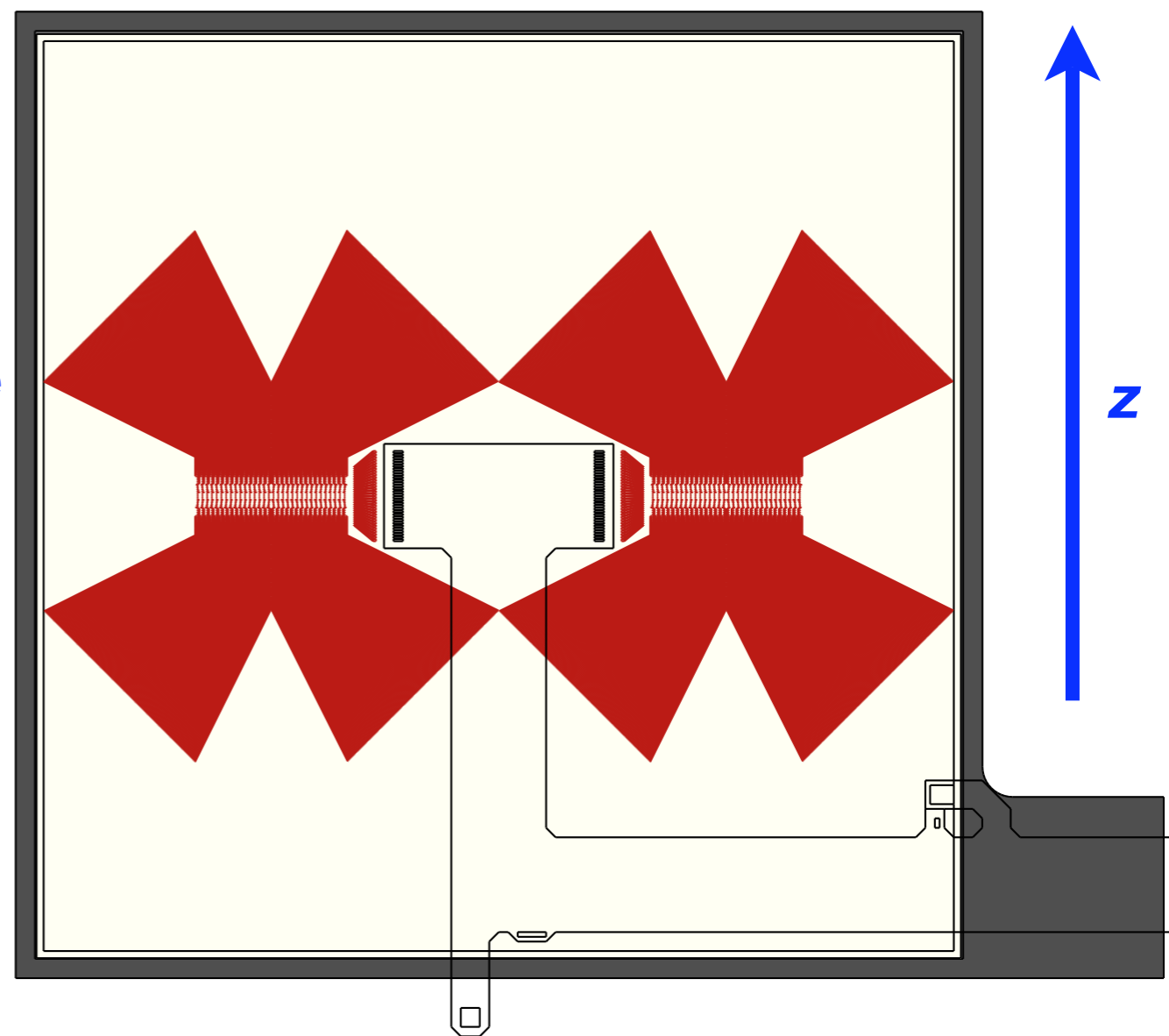
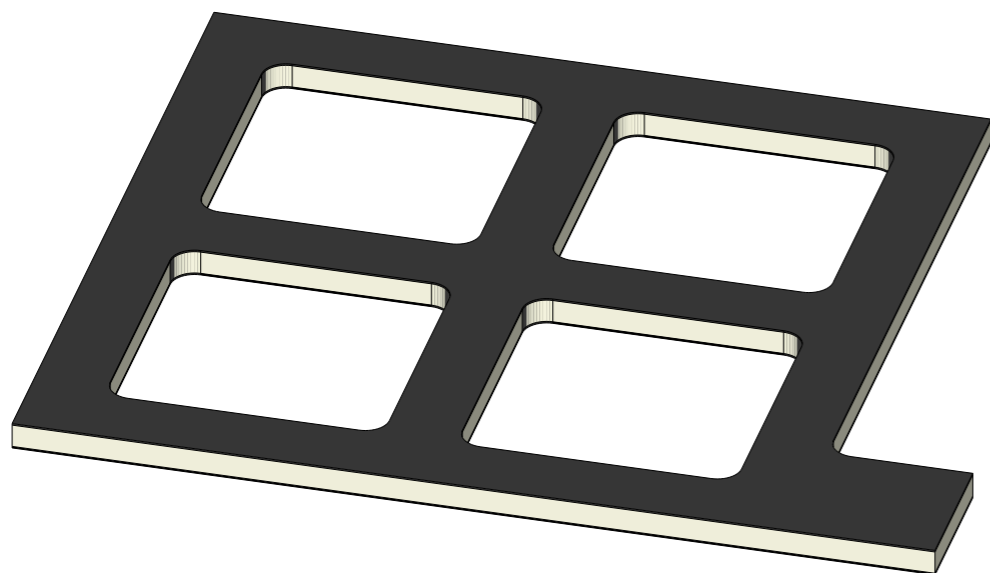
Two biasing schemes shown: arrangement at right preferred.

- Left tab glued to top of sensor and wirebonded to bias ring
- Right tab glued to bottom of sensor with conductive epoxy
- Nearby space on cable can host bias-filtering components



Sensor Support - V0.2

- ❖ Completely different structure
- ❖ “Handle” at right to strain relieve cable and provide support for bias filtering circuit
- ❖ CF directly underneath chips for thermal conductivity in any possible axial or stereo sensor orientation



Sensor Support - V0.2

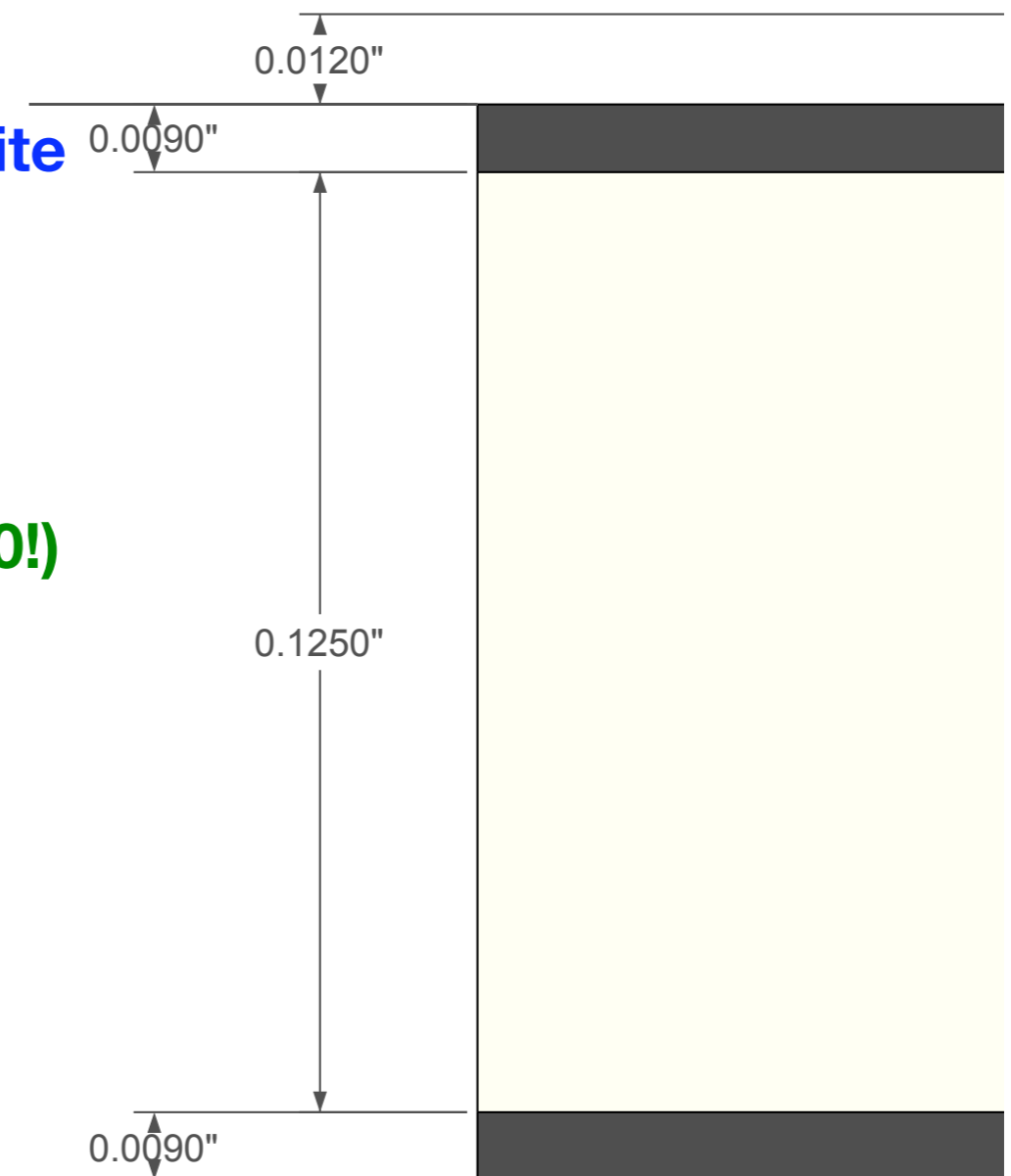
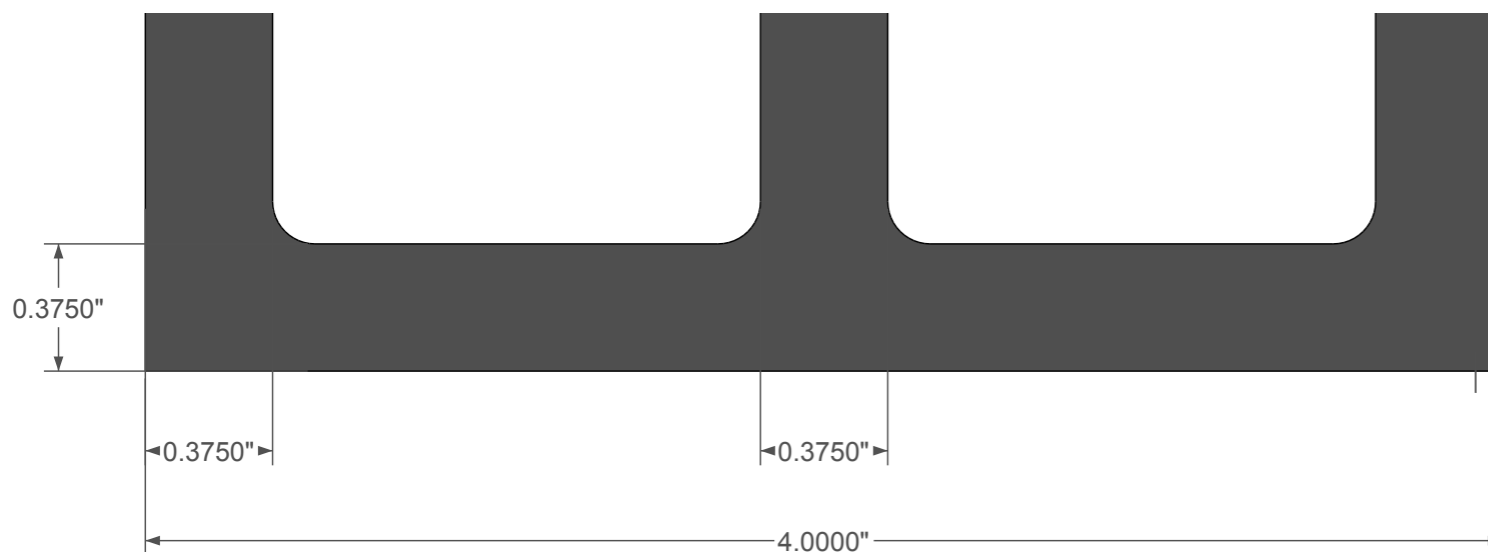
0.125" rohacell between two 0.009",
60-60-60 sheets of high-modulus CF composite

➔ Overall thickness < 4mm

>50% void

➔ Less material than previous design

As mass producible as CF can be (need ~5000!)



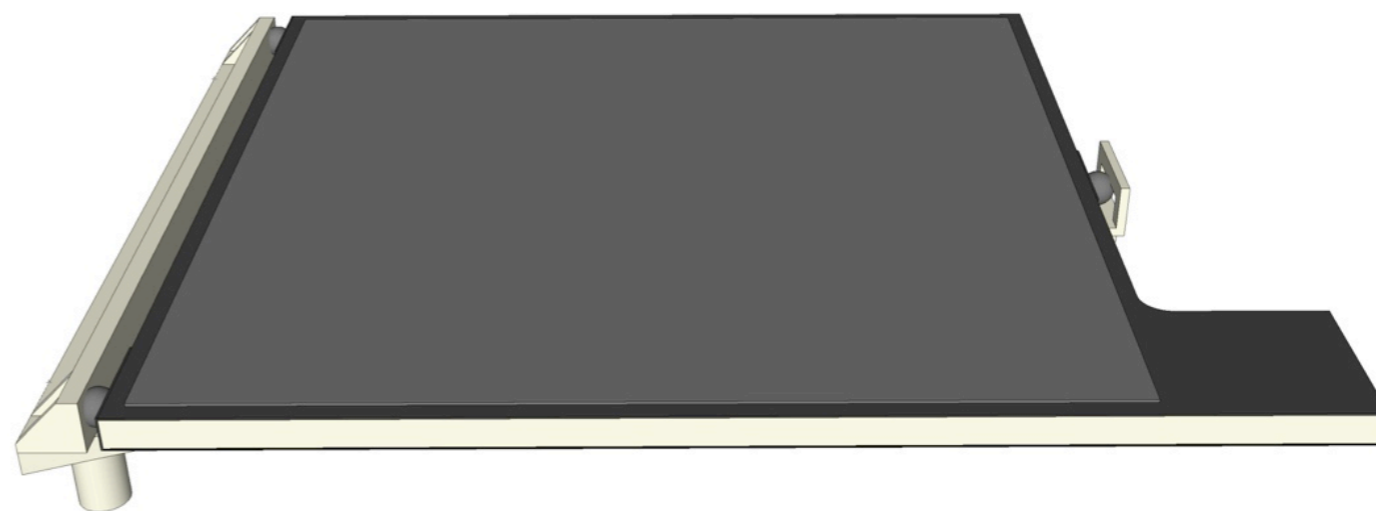
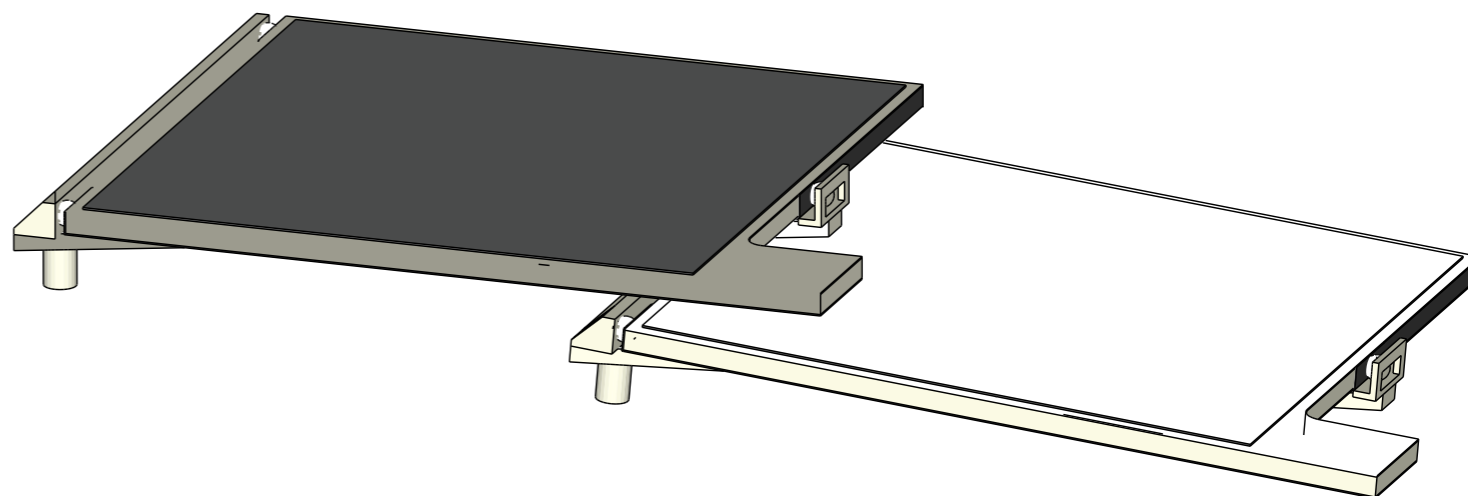
Module Mounting

Developing a serious design for module mounting

- ❏ First concept could not provide required z overlaps
- ❏ Precision questionable for standalone momentum measurement in an axial-only design

Working on three-point ball-and-cup design

- ➔ Can design be such that repeatability of tooling limits precision?



Material for Mating Surfaces

❏ Plastic

- ❏ Light

- ❏ Even for high-performance plastics: not precisely or repeatably machinable (CTE issue)

- ❏ Subject to wear

❏ Metal

- ❏ Precisely & repeatably machinable

- ❏ good wear properties

- ❏ Massive

❏ Silicon nitride (Si_3N_4)

- ❏ Precision meets or exceeds similar metal parts

- ❏ Harder than bearing steel, extremely resistant to wear & fracture

- ❏ Dry coefficient of friction <0.1 (similar to ice-on-ice) ideal for repeatable mating surfaces

- ❏ Relatively inexpensive in standard shapes (balls, sheets, etc.): 0.125" grade-10 ball = \$0.18

- ❏ Radiation length nearly identical to that of silicon (expect parts to total $<0.05\%$ X_0 avg.)

- ❏ May be possible to injection mold directly into PEEK (extraordinary adhesion to PEEK)

Feedback from Ceradyne to understand processing and optimize design



Material for Mounting Clip

❏ Carbon Fiber

- ❏ Ideal CTE match for modules
- ❏ Light and rigid (10-40 msi)
- ❏ Difficult to fabricate part with necessary complications - making 5000 could be problematic

❏ High-performance, semi-crystalline plastic (PEEK)

- ❏ Easily fabricated and mass producible
- ❏ Good injection molding tolerances (500 ppm \Rightarrow 50 microns for 10 cm span)
- ❏ Light and reasonably rigid (0.5 - 1 msi)
- ❏ Poor match for CTE of modules: $3.6 \times 10^{-5} / ^\circ\text{C} \Rightarrow 3.6 \text{ microns}/^\circ\text{C}$ for 10 cm part

❏ Carbon Fiber Filled PEEK





- ❏ Molding requirements only slightly more restrictive than unfilled PEEK
- ❏ Same molding tolerances as for unfilled PEEK
- ❏ Light and rigid (3-5 msi)
- ❏ Reasonable CTE match for modules: 1.5 microns/ $^\circ\text{C}$ for 10 cm part (30% filled, 50% available): effects can be minimized with careful design

Feedback from Victrex to understand processing and optimize design



Next Steps





Sensors

-  Resolve remaining issues (bias scheme, AC vs. DC coupled)
-  Generate complete set of formal drawings for HPK - FNAL
-  Perform more detailed analysis of trace capacitance and resistance - SLAC, FNAL, Tokyo?
-  Take to HPK for quote





Cables

-  Create detailed pigtail design - SLAC? Davis?
-  Quotes and costing for prototypes and production

Sensor Support

-  Create FEA model of support and test under mechanical and thermal loads - FNAL
-  **Finish detailing design (modifications for biasing scheme, mounting details) - SLAC**
-  Generate complete set of formal drawings - FNAL
-  Quotes and costing for prototypes and production

Module Mounting

-  **Finish conceptual design / engineering of mounting clip - SLAC**
-  Create FEA model of mounting clip and examine thermal effects - FNAL
-  Generate complete set of formal drawings - FNAL
-  Quotes and costing for prototypes and production

Another talk in next few weeks on sensor support and module mounting

