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## CLIC 380 GeV BDS design and tuning

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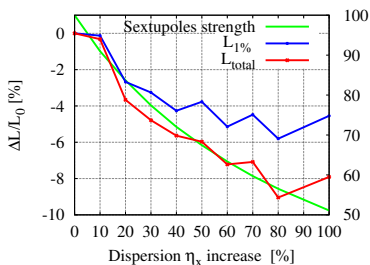
# Introduction

- The nominal 380 GeV BDS design with  $L^* = 4.3$  m was optimized based on the previous 500 GeV BDS design
- A long  $L^*$  design has been design as well, allowing QD0 to be located outside of the Detector (see motivations for longer  $L^*$  in the talk "*Status of the CLIC 3 TeV BDS with  $L^* = 6$  m*")
- For both  $L^*$  design options, the dispersion level along the FFS was optimized according to the maximum luminosity achievable as well as their tuning efficiency (Tuning-based design optimization)
- The final performance of both designs and their tuning efficiency under transverse misalignment of the optics and under more realistic error conditions will be presented

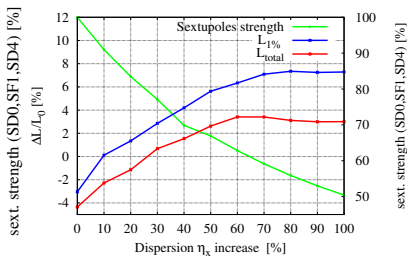
# BDS design optimization with $L^* = 4.3$ m and $L^* = 6$ m

- For  $L^* = 4.3$  m, the FFS is based on the previous 500 GeV lattice and the optics strengths were rematched for 380 GeV
- For  $L^* = 6$  m, the length of the FFS has been scaled according to the increase of  $L^*$  (length increased from 550 m to 770 m)
- For both  $L^*$  designs, the dispersion level along the FFS was optimized in order to maximize the luminosity :

$L^* = 4.3$  m



$L^* = 6$  m



## BDS design optimization with $L^* = 4.3$ m and $L^* = 6$ m

- It was found for both  $L^*$  designs **uncorrected residual 2nd order chromaticity** which strongly impact the beam size (mainly  $\sigma_x^*$ )
- The chromaticity correction along the FFS was not optimal was the residual **aberrations were fully corrected by optimizing the distance between QF1 and QD0**

$L^* = 4.3$  m

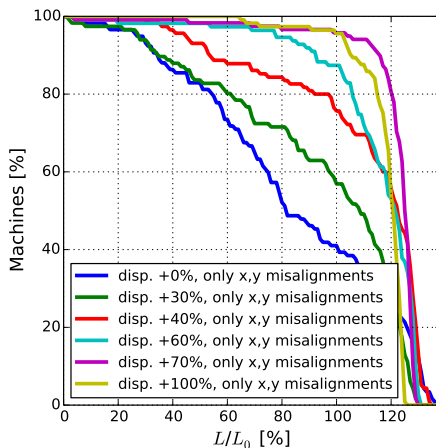
$\eta_x$ increase (%)	$\sigma_x^* / (\sigma_y^*)$ (nm) (before $L_{FD}$ optim.)	$\sigma_x^* / (\sigma_y^*)$ (nm) (after $L_{FD}$ optim.)
0	149.7 / 2.75	<b>144.8 / 2.55</b>
10	150.5 / 2.72	<b>145.0 / 2.58</b>
20	151.4 / 2.81	<b>145.2 / 2.43</b>
30	152.1 / 2.80	<b>146 / 2.41</b>
40	153.2 / 2.8	<b>145.5 / 2.40</b>
50	153.7 / 2.8	<b>146 / 2.45</b>
60	154.6 / 2.77	<b>147.3 / 2.42</b>
70	155.2 / 2.76	<b>148 / 2.38</b>
80	157.1 / 2.83	<b>149 / 2.38</b>
90	157.4 / 2.85	<b>150.4 / 2.39</b>
100	160.1 / 2.87	<b>152.6 / 2.40</b>

$L^* = 6$  m

$\eta_x$ increase (%)	$\sigma_x^* / (\sigma_y^*)$ (nm) (before $L_{FD}$ optim.)	$\sigma_x^* / (\sigma_y^*)$ (nm) (after $L_{FD}$ optim.)
0	153.8 / 4.74	145.4 / 3.8
10	155.2 / 4.3	145.5 / 3.9
20	156.6 / 4.0	145.4 / 3.45
30	157.7 / 3.75	145.7 / 3.13
40	157.6 / 3.66	145.8 / 3.4
50	160 / 3.44	146.6 / 2.94
60	160.6 / 3.3	147 / 2.88
70	162 / 3.3	148 / 2.7
80	163 / 3.2	149.2 / 2.75
90	164 / 3.17	150 / 2.7
100	167 / 3.14	152 / 2.72

# Tuning the $L^* = 4.3$ m lattice under transverse misalignments

- **Tuning-based optimization goal** : find the optimal dispersion level along the FFS by taking as figure of merit the **tuning performance**

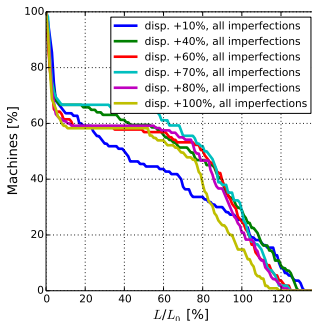


- The optimal dispersion level for  $L^* = 4.3$  m according to the tuning performance under transverse misalignment imperfections was found by **increasing  $\eta_x$  by +70%**

# Tuning the $L^* = 4.3$ m lattice under realistic errors



Errors	Value
Transverse misalignment (RMS)	$10\ \mu\text{m}$
roll	$300\ \mu\text{rad}$
strength	0.1%

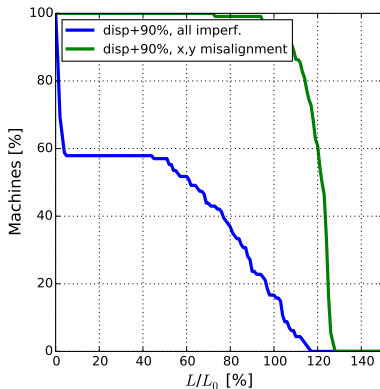


$\eta_x$ increase (%)	$L_{\text{tot, average}} (10^{34} \text{ cm}^{-2} \text{ s}^{-1})$ (x,y mis. only)	$L_{\text{tot, average}}$ (all imperfections)
10	1.28	0.845
40	1.62	0.997
60	1.7	0.942
<b>70</b>	<b>1.8</b>	<b>1.03</b>
80	1.71	0.93
100	1.7	0.85

$L^*$ (m)	<b>4.3</b>
$L_{\text{total}} / L_{1\%} (10^{34} \text{ cm}^{-2} \text{ s}^{-1})$	1.99 / 1.15
$\sigma_x^* / \sigma_y^*$ (nm)	148 / 2.38

# Tuning-based optimization of the $L^* = 6$ m

- Tuning-based optimization for  $L^* = 6$  m found optimal dispersion by **increasing  $\eta_x$  by +90%**

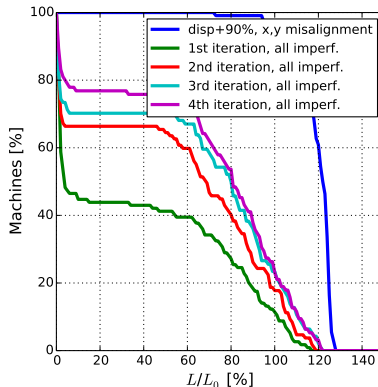


$L^*$ (m)	6
$L_{total} / L_{1\%}$ ( $10^{34} \text{ cm}^{-2} \text{ s}^{-1}$ )	1.75 / 1.05
$\sigma_x^* / \sigma_y^*$ (nm)	150 / 2.7



## Tuning-based optimization of the $L^* = 6$ m

- Tuning-based optimization for  $L^* = 6$  m found optimal dispersion by **increasing  $\eta_x$  by +90%**



- Iterations of tuning using only Linear Knobs under realistic error condition shows that the correction of linear aberrations is not enough to fully tune the beam
- Non-linear knobs has to be constructed and implemented in the tuning procedure** (on-going work)

# Conclusions

- Both  $L^*$  option designs have been optimized, according to their maximum luminosity achievable and tuning efficiency, and **fulfill the design luminosity requirements as well as the luminosity budget** for static and dynamic imperfections
- The tuning simulations have shown that under only transverse misalignments, only 1 iteration of BBA and linear knobs are needed to reach the tuning goals
- Under more realistic error conditions, **non-linear knobs will be needed for both designs in order to correct the 2nd order aberrations generated by the strength and roll errors** (ongoing work)