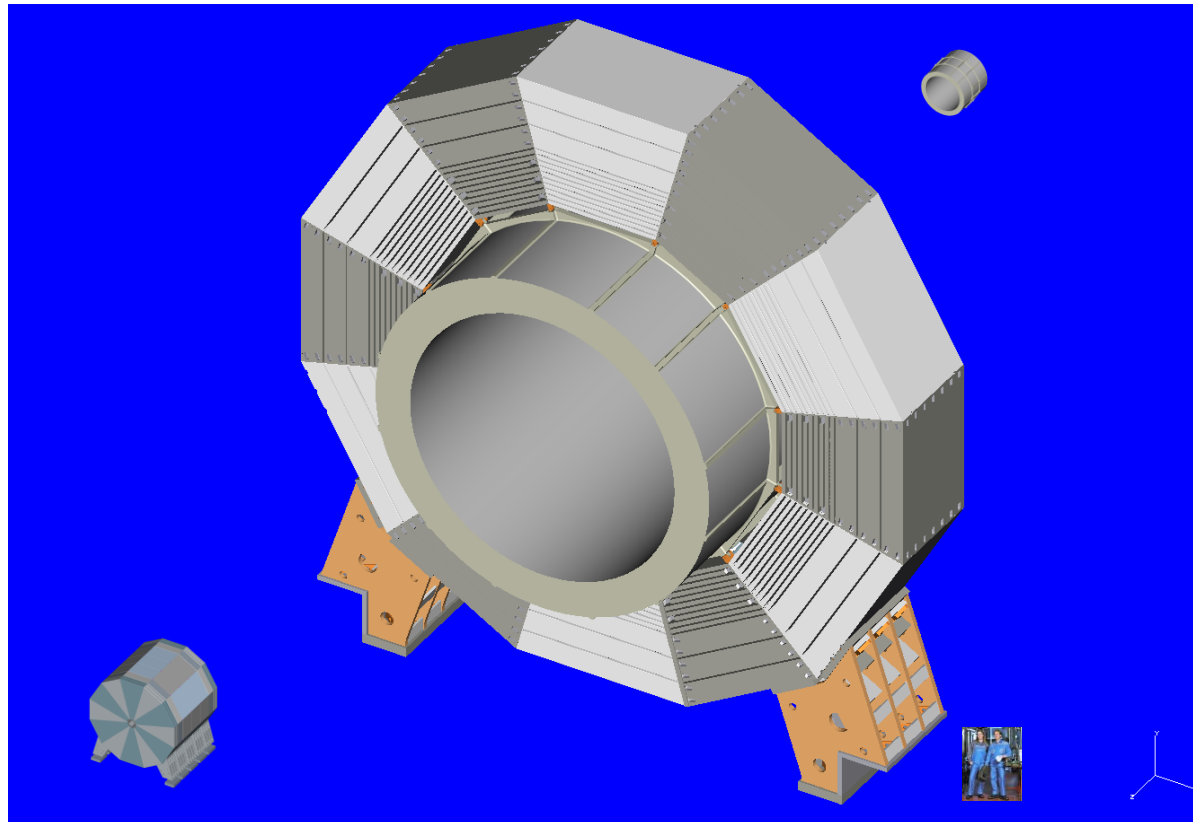
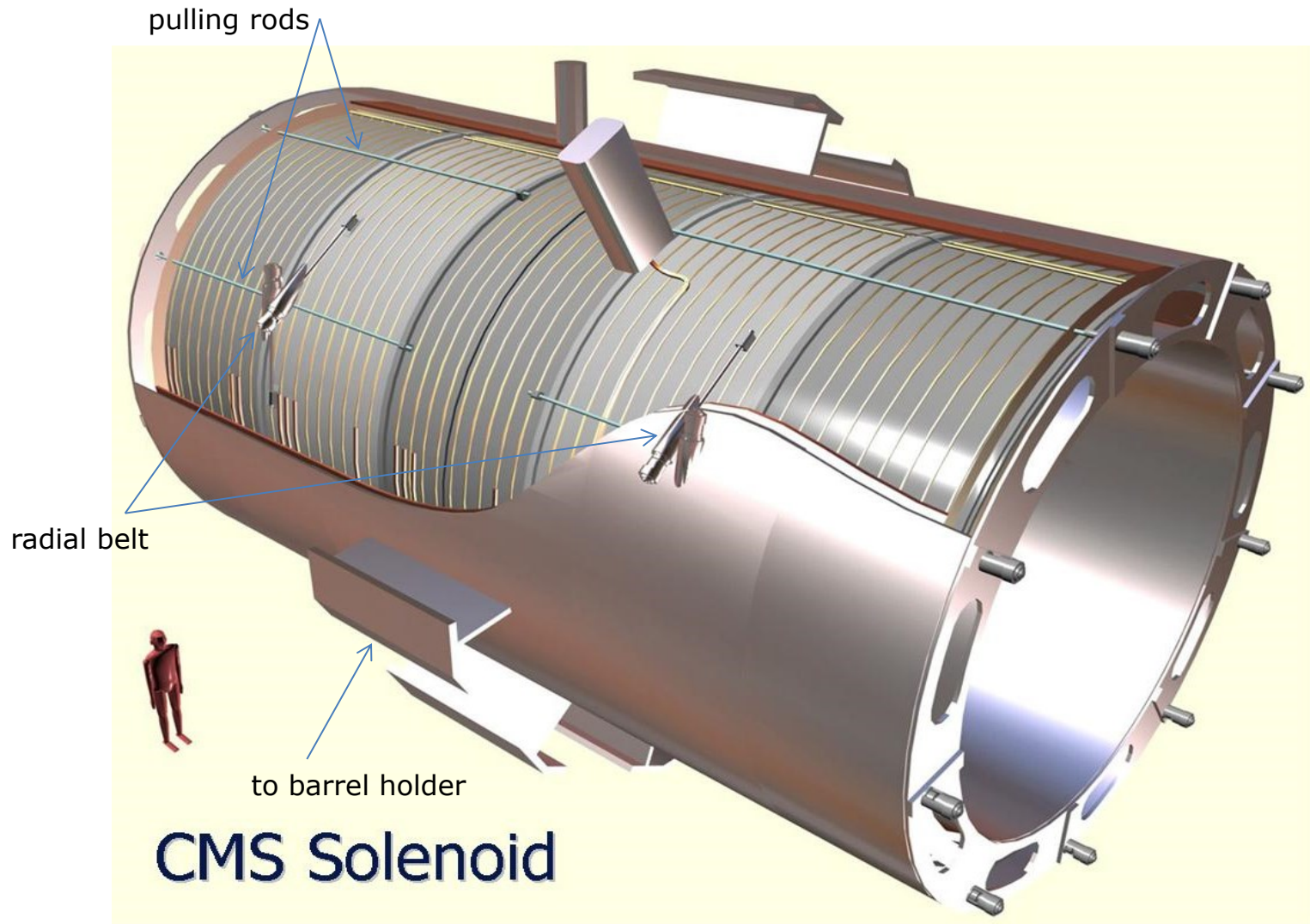


Cryostat Integration / Structural Analysis / Transfer Forces

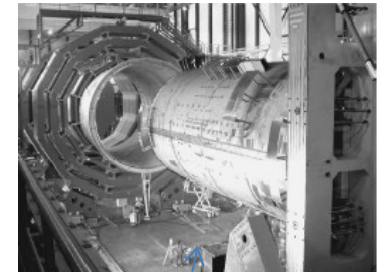


CERN CMS Solenoid schematic



Insertion of outer vac-tank / CMS

5 segment, 2600 lg. sheet thickness: 30 ~2600lg, 40 and 60 mm



to need jig and scaffolding for on-site installation

CMS Cryostat with inner-, outer vacuum vessel and end flange



Cryostat structure proposal / all-welded Radial positions system of the solenoid

effective section modul over ledge



$J_{x-x} = 1,82 \times 10^{12}$

- weight ~ 136 t

eye for radial suspension

Push / rotary hanging
24 x 600kN point

to be done
solenoid vents
suspension points
for radial tier

outer vacuum vessel

- weight ~ 70 t
- stainless sheet thickness = 30 mm

Z support rods: 24 x 45mm,
Titanium alloy
pree stress horizontal
per tie ~ 20 N/mm²

to be done

inner rails for HCAL

inner vacuum vessel

- weight ~ 56 t
- stainless sheet thickness = 40 mm

end flange

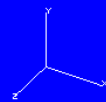
- weight ~ 5t
- end flange thickness = 50 mm

reinforcement

spacer

unbalanced force of the
solenoid ~ 840 kN

900 kN



Reactions of the cold mass supporting system / Force (on left Fig.)

min. comparison material stress:
 Titanium Alloying > 300 N/mm²
 tensile strength stainless steel > 500 N/mm²

Support rods

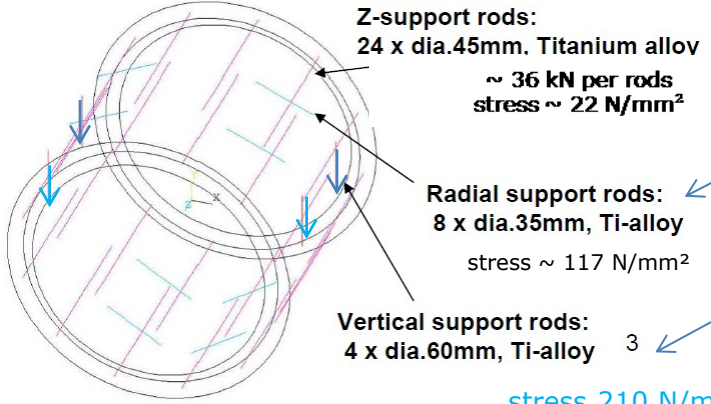
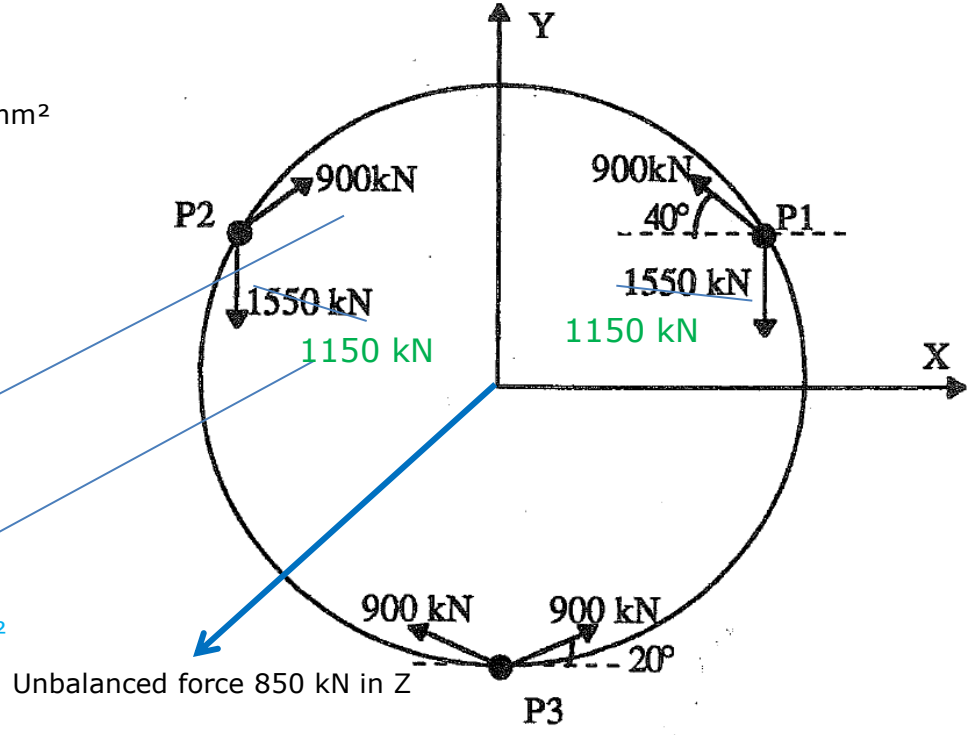


Fig. KEK Hiroshi Yamaoka

stress 210 N/mm²

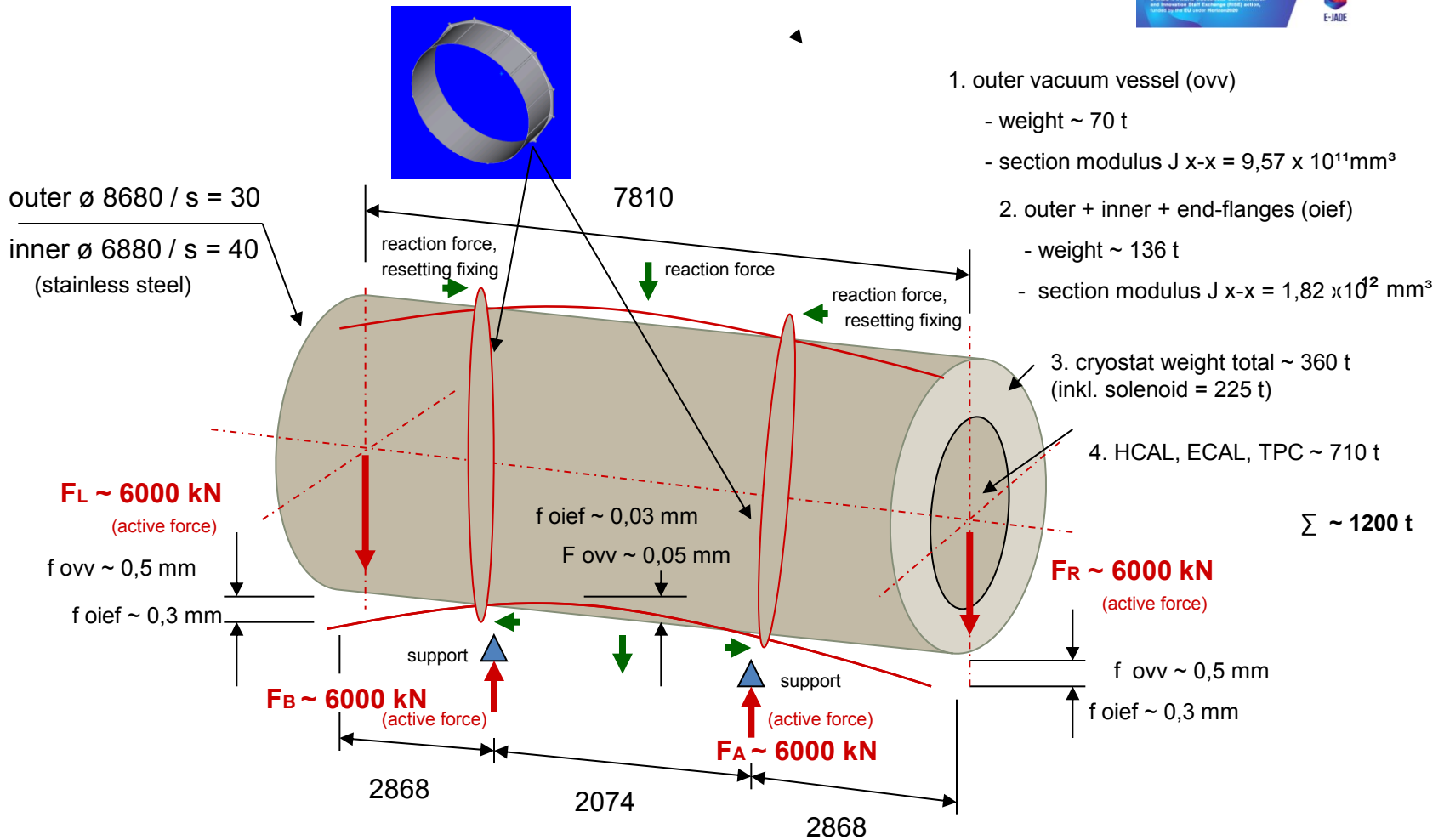


CMS TDR 1 / Page71

Fig. 9.2: Reactions of the cold mass supporting system.

min. safety factor all rods > 2,

Cryostat: applied and resulting forces, deflection line



Loading case Cryostat / Vacuum / elastic deformation

External Pressure 2 bar = Safety factor 2

Belastungsart:

Innendruckbelastung

Außendruckbelastung

Eingabewerte:

Radius Außenwand - r_a (mm)

Radius Innenwand - r_i (mm)

Radius an Stelle x - r_x (mm)

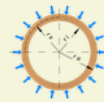
Elastizitätsmodul - E (N/mm²)

Querdehnungszahl - ν (-)

Belastungsdruck - p (N/mm²) / 1 bar = 0,1 N/mm²

Überdruck = positiven Wert eingeben.

Unterdruck = negativen Wert eingeben.



Belastungsart:

Innendruckbelastung

Außendruckbelastung

Eingabewerte:

Radius Außenwand - r_a (mm)

Radius Innenwand - r_i (mm)

Radius an Stelle x - r_x (mm)

Elastizitätsmodul - E (N/mm²)

Querdehnungszahl - ν (-)

Belastungsdruck - p (N/mm²) / 1 bar = 0,1 N/mm²

Überdruck = positiven Wert eingeben.

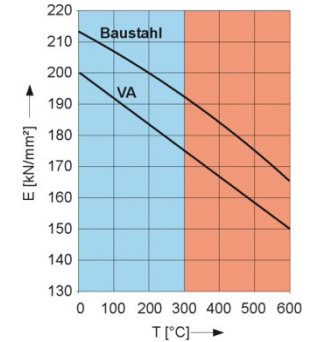
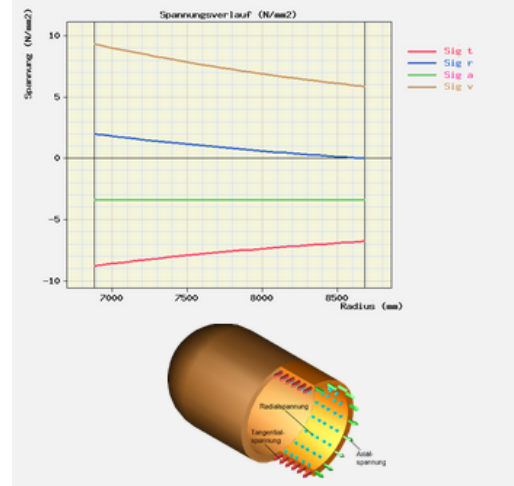
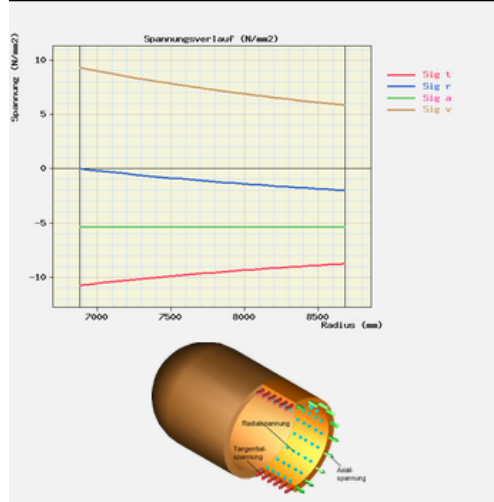
Unterdruck = negativen Wert eingeben.



Radius	6880,0 mm Innenwand	7780,0 mm Radius x	6880,0 mm Außenwand
Elastizitätsmodul - E (N/mm ²)	220000,0		
Querdehnungszahl - ν (-)	0,300		
Außendruckbelastung - p a (N/mm ²)		2,00	
Tangentialspannung - σ_t (N/mm ²)	-10,8	-9,59	-8,76
Radialspannung - σ_r (N/mm ²)	-0	-1,17	-2,00
Axialspannung - σ_a (N/mm ²)		-5,38	
Vergleichspannung GEH σ_v (N/mm ²)	9,32	7,29	5,85
Radialverformung - Δr (mm)	-0,336	-0,327	-0,322
Beuldruck - p br (N/mm ²) - Sicherheit = 3		227,0	

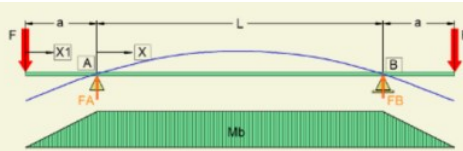
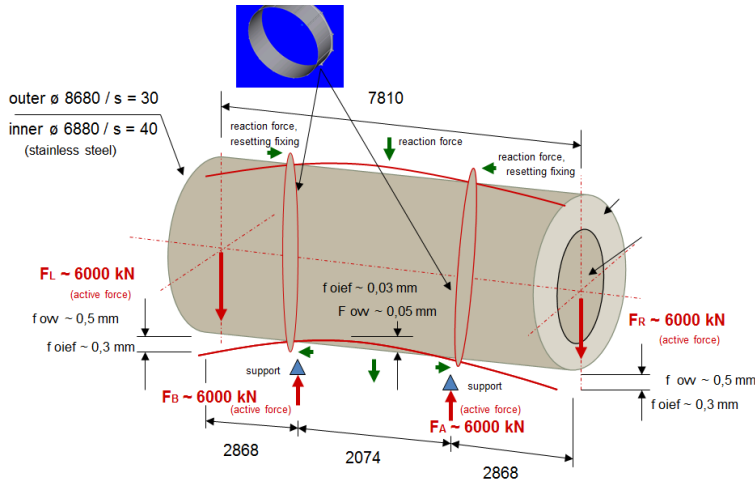
Radius	6880,0 mm Innenwand	7780,0 mm Radius x	6880,0 mm Außenwand
Elastizitätsmodul - E (N/mm ²)		220000,0	
Querdehnungszahl - ν (-)		0,300	
Innendruckbelastung - p i (N/mm ²)		-2,00	
Tangentialspannung - σ_t (N/mm ²)	-8,76	-7,59	-6,76
Radialspannung - σ_r (N/mm ²)	2,00	0,827	-0
Axialspannung - σ_a (N/mm ²)		-3,38	
Vergleichspannung GEH σ_v (N/mm ²)	9,32	7,29	5,85
Radialverformung - Δr (mm)	-0,293	-0,277	-0,267

tangential stress
radial stress
axial stress
Deformation
distortion



Ref. Stress ~ 6 N/mm²
Deformation ~ 0,3 mm

Cryostat: applied and resulting forces, deflection line cal. with pc



Eingabewerte:

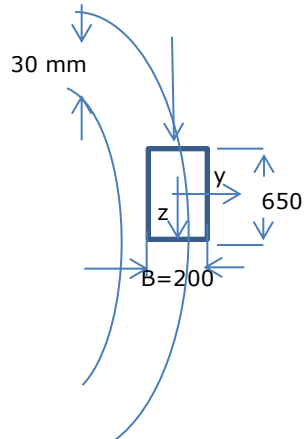
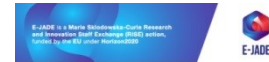
Belastung - F (N)	6000000
Länge - L - (mm)	7810
Kraftabstand - a - (mm)	2864
E-Modul - E - (N/mm ²)	220000
Trägheitsmoment - I - (mm ⁴)	3668239688000
Widerstandsmoment - W (mm ³)	947865552
Berechnungspunkt X - (mm)	3905
Berechnungspunkt X1 - (mm)	0

Ergebnisse:

Auflagerkraft - F (N)	
Koordinate x = 0 mm [FA]	6000000.0
Koordinate x = 7810 mm [FB]	6000000.0
Biegemoment - M (Nmm)	
Koordinate x1 = 0 mm	0
Koordinate x = 0.0 mm [A]	-17184000000.0
Koordinate x = 3905 mm	-17184000000.0
Koordinate x = 7810 mm [B]	-17184000000.0
Max. Biegemoment bei x = 0 mm	-17184000000.0
Biegespannung - σ_b (N/mm²)	
Koordinate x1 = 0 mm	0
Koordinate x = 0.0 mm [A]	18.1
Koordinate x = 3905 mm	18.1
Koordinate x = 7810 mm [B]	18.1
Max. Biegespannung bei x = 0 mm	18.1
Durchbiegung - f (mm)	
Koordinate x1 = 0 mm	0.296
Koordinate x = 0.0 mm [A]	0
Koordinate x = 3905 mm	-0.162
Koordinate x = 7810 mm [B]	0
Max. Durchbiegung bei x1 = 0 mm	0.296
Max. Durchbiegung bei x = 3905.0 mm	-0.162
Neigung - tan α	
Koordinate x1 = 0.0 mm	-0.000114
Koordinate x = 0.0 mm [A]	-0.0000832

Max. defl. 0,3 mm

Hanger Solenoid / 225 T / 4 lifting strut, per 562 kN, rating material



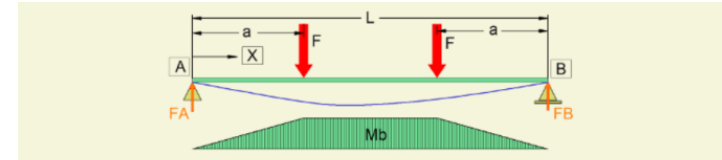
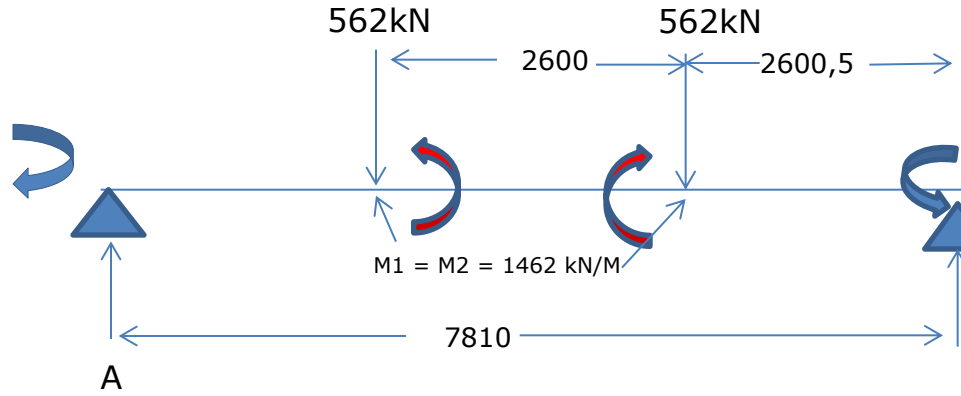
$$\sum M \uparrow = 0$$

$$M_{max} = 562 \text{ kN} \times 2,6005 = 1462 \text{ kN/m}$$

$$562 \text{ kN} \times 7810 - 562 \text{ kN} \times 2600,5 - 562 \text{ kN} \times 5210 = 0$$

$$\delta = M_{max} / W_y \quad W_y = B \times H^2 / 6$$

$$I_y = B \times H^3 / 12$$



Eingabewerte:

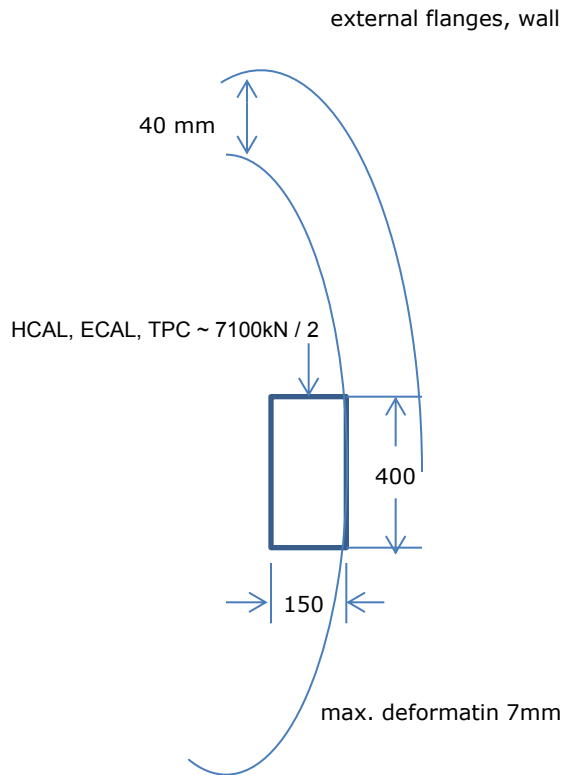
Belastung - F (N)	562000
Länge - L - (mm)	7810
Kraftabstand - a - (mm)	2600
E-Modul - E - (N/mm ²)	220000
Trägheitsmoment - I - (mm ⁴)	457708333
Widerstandsmoment - W (mm ³)	1408333
Berechnungspunkt X - (mm)	2600

Ergebnisse:

Auflagerkraft - F (N)	
Koordinate x = 0 mm [FA]	562000.0
Koordinate x = 7810 mm [FB]	562000.0
Biegemoment - M (Nmm)	
Koordinate x = 0.0 mm [A]	0
Koordinate x = 2600 mm	1461200000.0
Koordinate x = 7810 mm [B]	0
Max. Biegemoment bei x = 2600.0 mm	1461200000.0
Biegespannung - σ_b (N/mm²)	
Koordinate x = 0.0 mm [A]	0
Koordinate x = 2600 mm	103.8
Koordinate x = 7810 mm [B]	0
Max. Biegespannung bei x = 2600.0 mm	103.8
Durchbiegung - f (mm)	
Koordinate x = 0.0 mm [A]	0
Koordinate x = 2600 mm	8.19
Koordinate x = 7810 mm [B]	0
Max. Durchbiegung bei x = 3905.0 mm	9.43

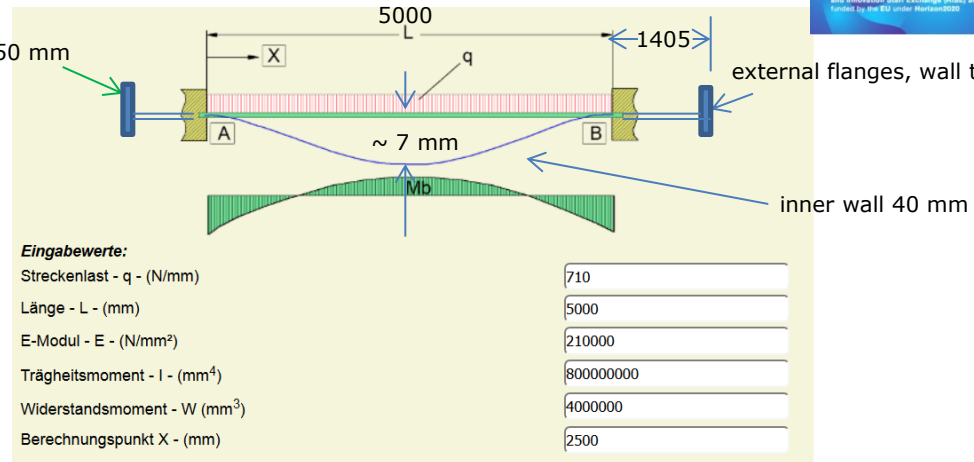
Max. defl. ~ 10 mm

Hanger HCAL, ECAL, TPC, / 710 t constant load, rating material



Rough sketch

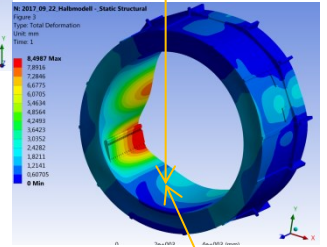
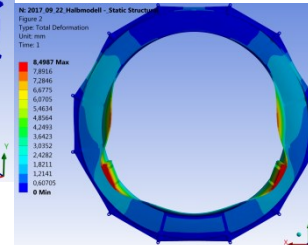
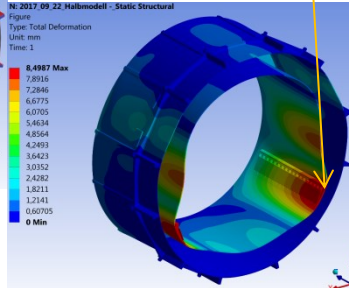
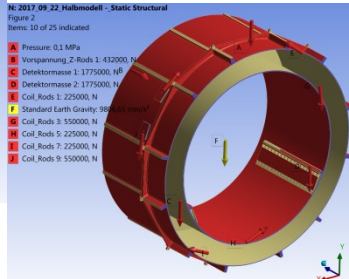
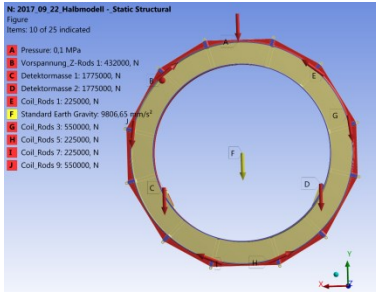
external flanges, wall thickness 50 mm



Auflagerkraft - F (N)	
Koordinate x = 0 mm [FA]	1775000.0
Koordinate x = 5000 mm [FB]	1775000.0
Biegemoment - M (Nmm)	
Koordinate x = 0.0 mm [A]	-1479166666.7
Koordinate x = 2500 mm	739583333.3
Koordinate x = 5000 mm [B]	-1479166666.7
max. Biegemoment bei x = 0 und 5000 mm	-1479166666.7
Biegespannung - σ_b (N/mm²)	
Koordinate x = 0.0 mm [A]	369.8
Koordinate x = 2500 mm	184.9
Koordinate x = 5000 mm [B]	369.8
max. Biegespannung bei x = 0 und 5000 mm	369.8
Durchbiegung - f (mm)	
Koordinate x = 0.0 mm [A]	0
Koordinate x = 2500 mm	6.88
Koordinate x = 5000 mm [B]	0
Max. Durchbiegung bei x = 2500.0 mm	6.88
Neigung - tan α	
Koordinate x = 0.0 mm [A]	0
Koordinate x = 5000 mm [B]	0

Defl. ~ 7 mm

Max. deflection including all loads (vacuum, preloads, temperature), thickness outer 30 / inner 40 mm



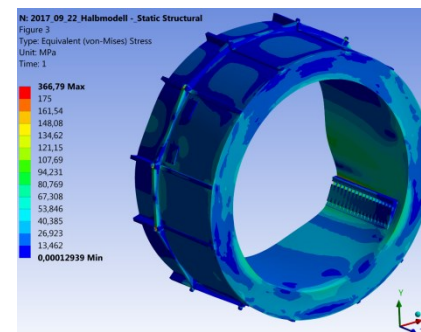
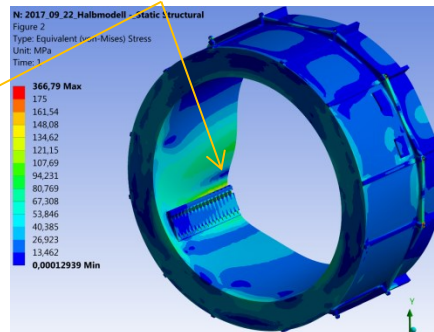
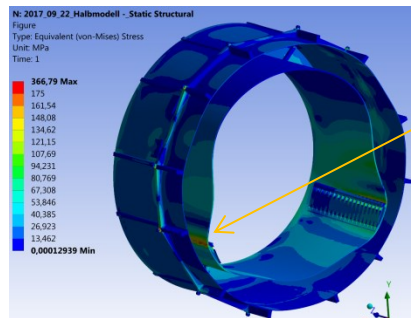
in fact, the deformation due to structural elements could be small.

~ 9 mm

Martin Lemke

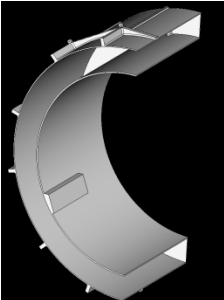
Max. stress including all loads (vacuum, preloads, temperature), thickness outer 30 / inner 40 mm

$\delta \sim 180 \text{ N/mm}^2$

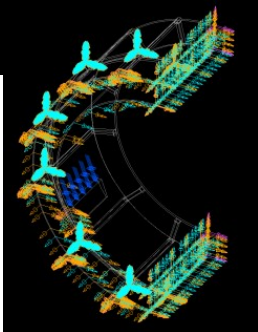


In fact, the stress caused by constructive elements could be small.

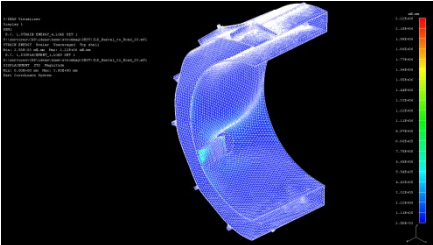
Deformation: 40 mm thickness constructions suggestion force load ledge (with CAD IDEAS)



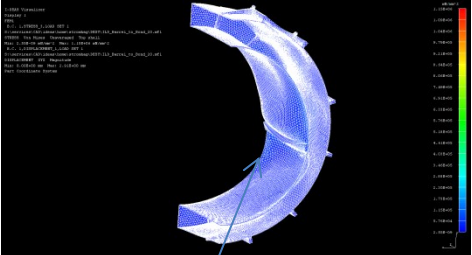
Boundary condition set



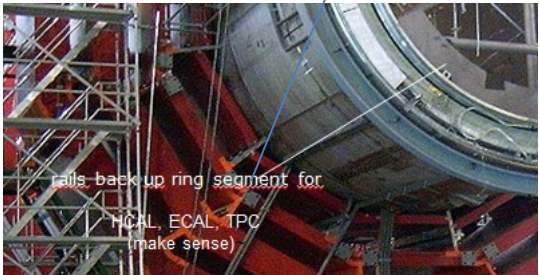
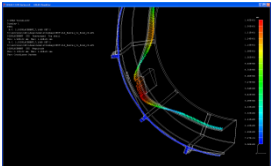
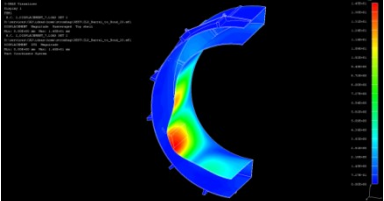
Deformation ~ 6 mm



Deformation 3 mm



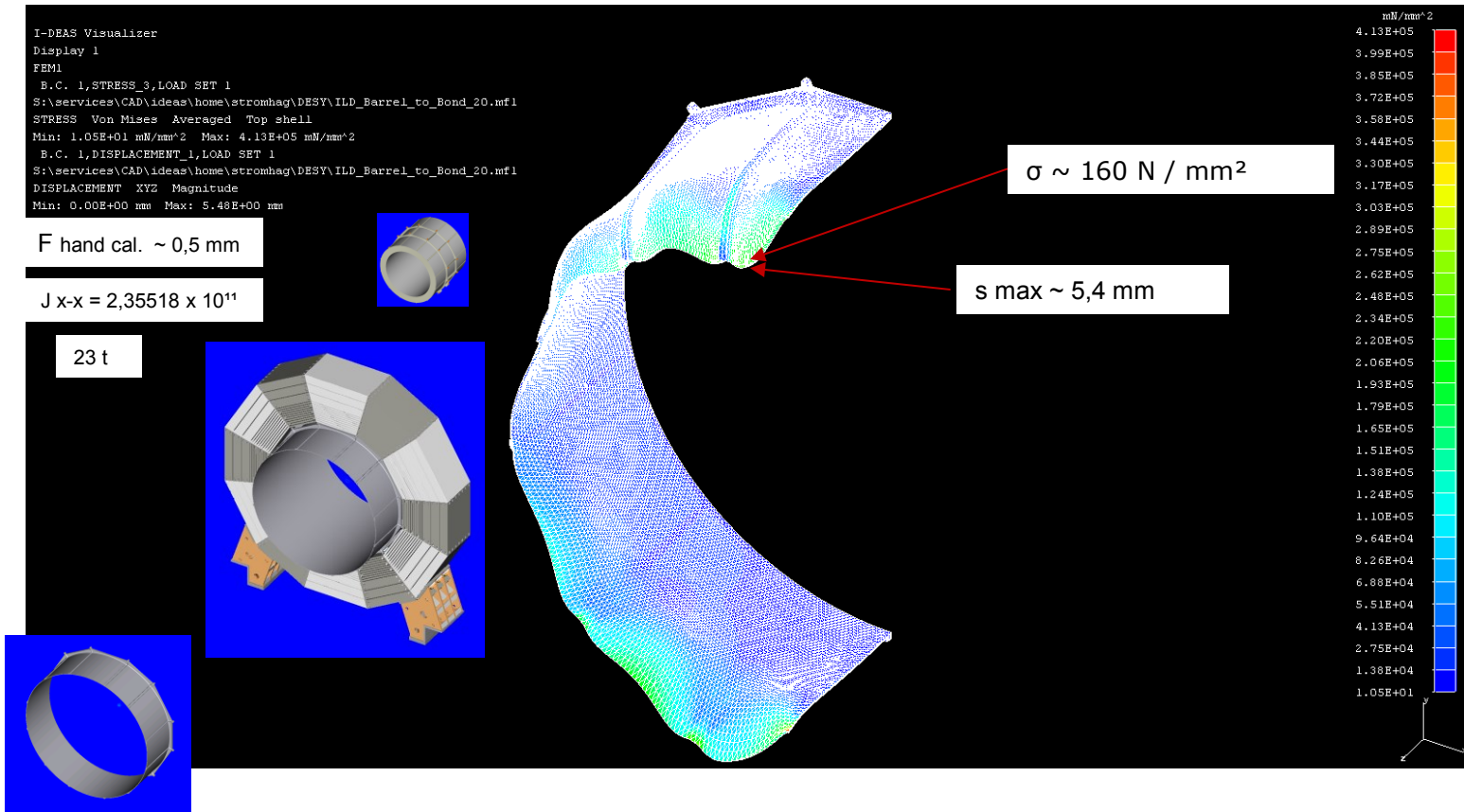
Deformation in Z ~ 2mm



ILD cryostat FEM simulation

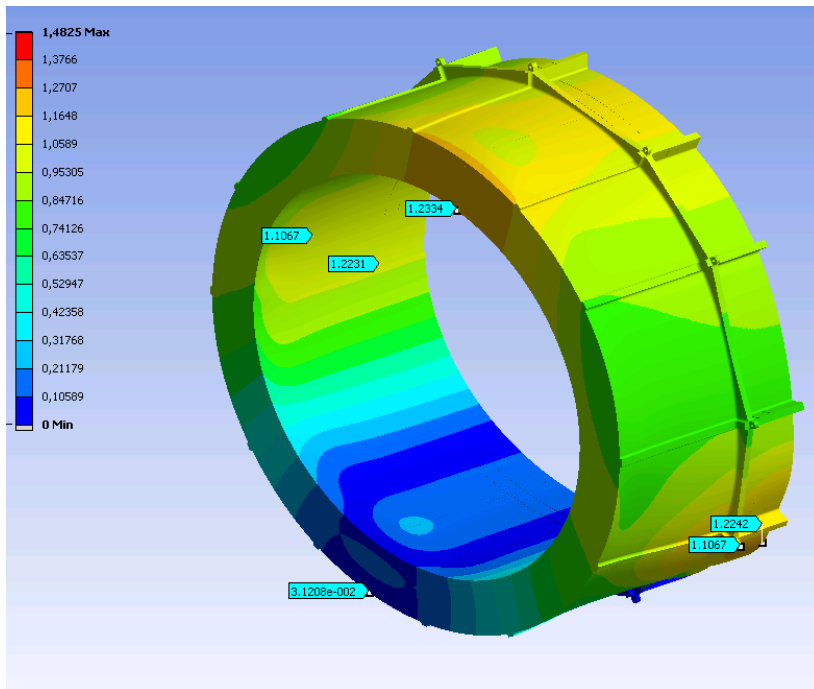
only end half part 2868 mm lg. / F = 3000 kN constant off-circumference

CAD IDEAS

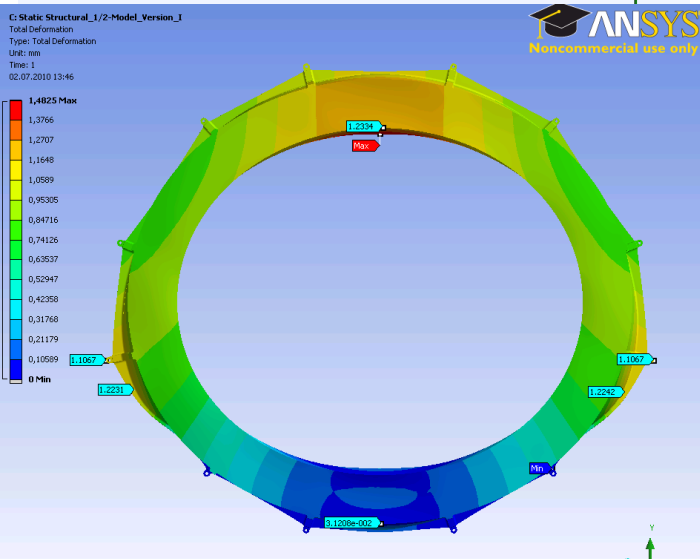
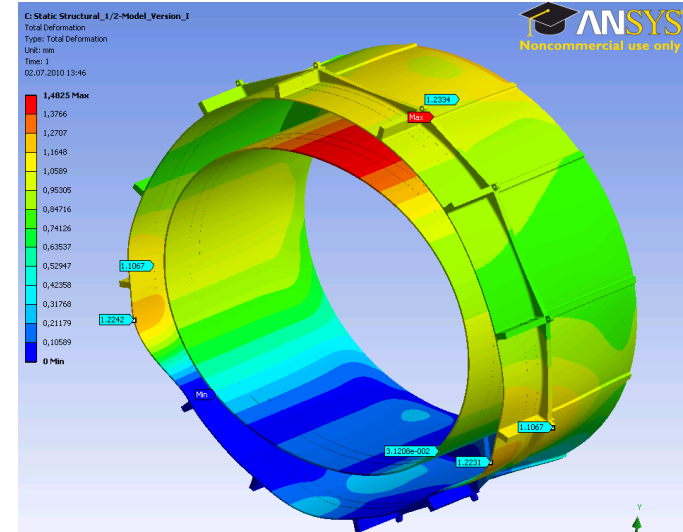


ILD Cryostat total deformation

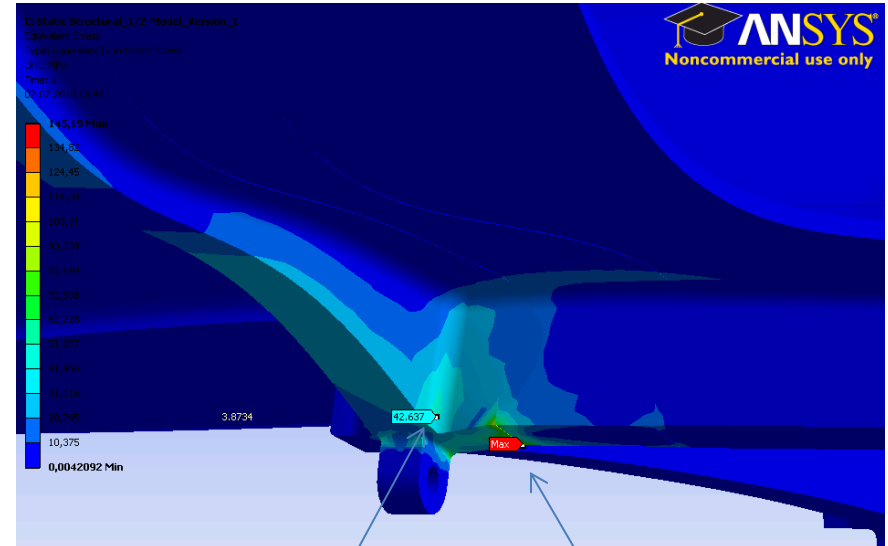
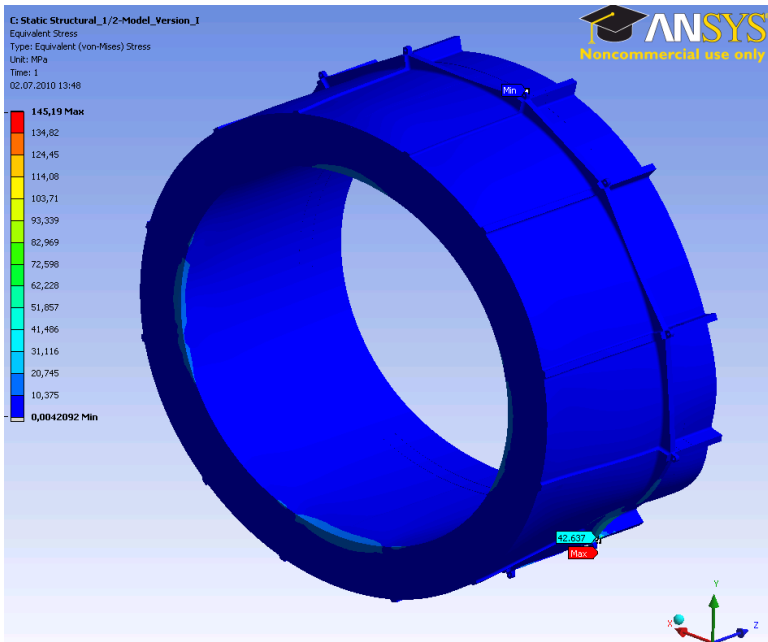
max. $\sim 2\text{mm}$



M. Lemke



ILD Cryostat total stress



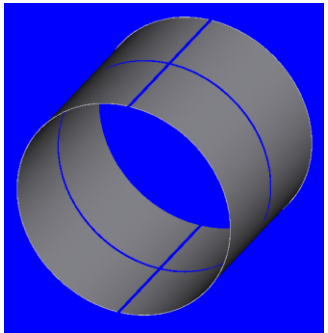
normal max. 43N/mm²

max. ~ 110 N/mm²
(as an exception)

M. Lemke

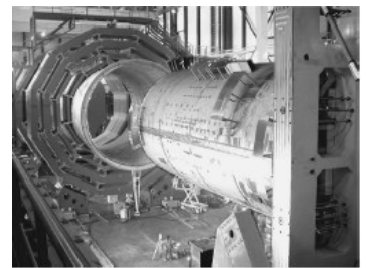


ILD cryostat production flow suggestion / assembly cryostat



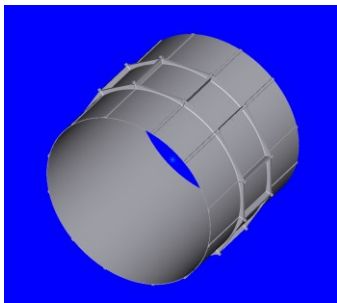
**Outer-, s=30mm; and inner-, s = 40 mm
- vacuum vessel**

-sheet 4 or 8 (max. 13610 mm x 3905 mm,) segment rolled and welded



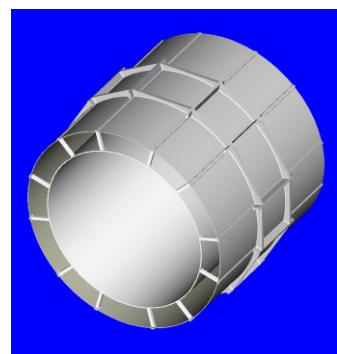
outer vacuum vessel

- prepared edge lined up and welded
- rotation symmetrical pilot hole diameter (\varnothing 40 mm)
- outer reinforcements clamped to barrel and held in place by outer support
- aligned axis of ovv and barrel
- fixed ovv and welded brackets to the central barrel



inner vacuum vessel

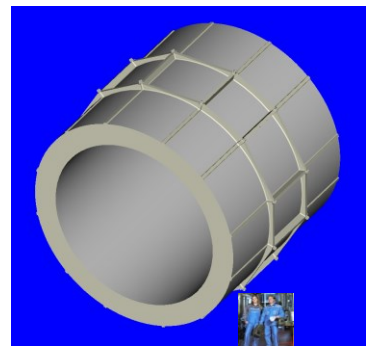
- sheet 4 or 8 rolled and outside scaffold
- aligned and welded
- lodge inner in outer vv, align rims and weld
- welding of end plate



to be done

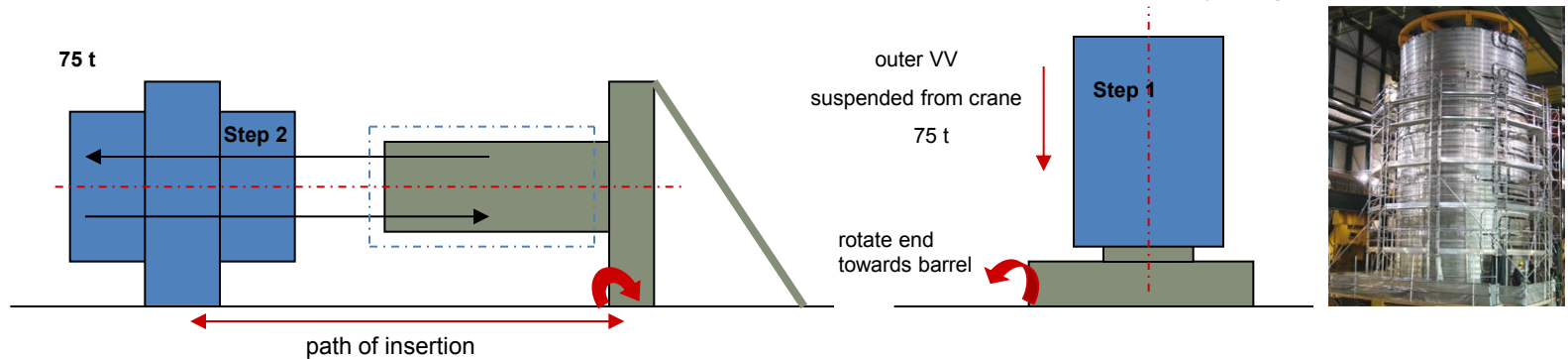
assembly cryostat to ovv

- solenoid completion and fixture



Assembly completion of solenoid and vacuum vessel (CMS)

1. outer vacuum vessel (75 tons) with barrel after installation on turn table, primary alignment



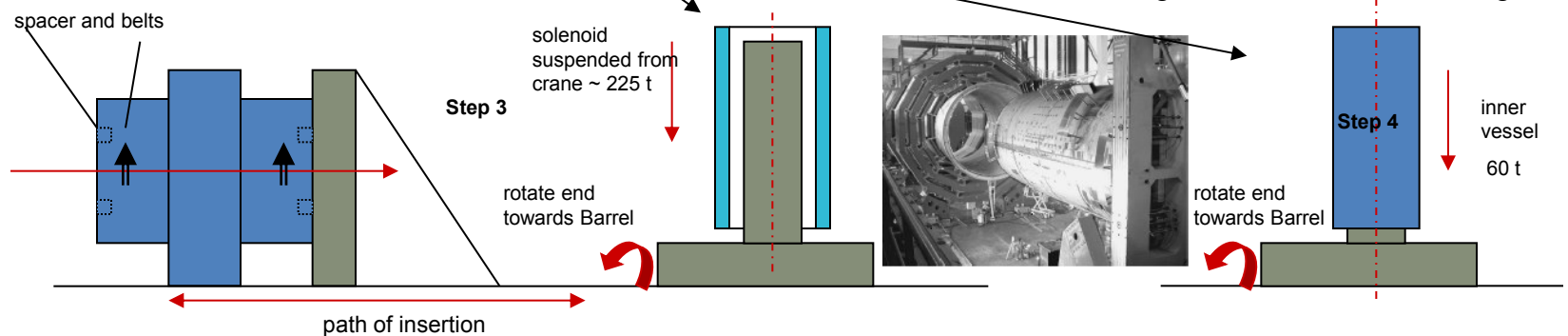
2. assembly and completion of the solenoid (~ 225 t)

- rotate inner vacuum vessel into horizontal position => weld radial tiers and end flange

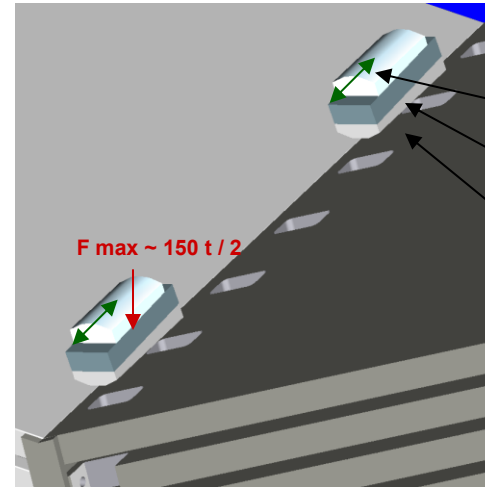
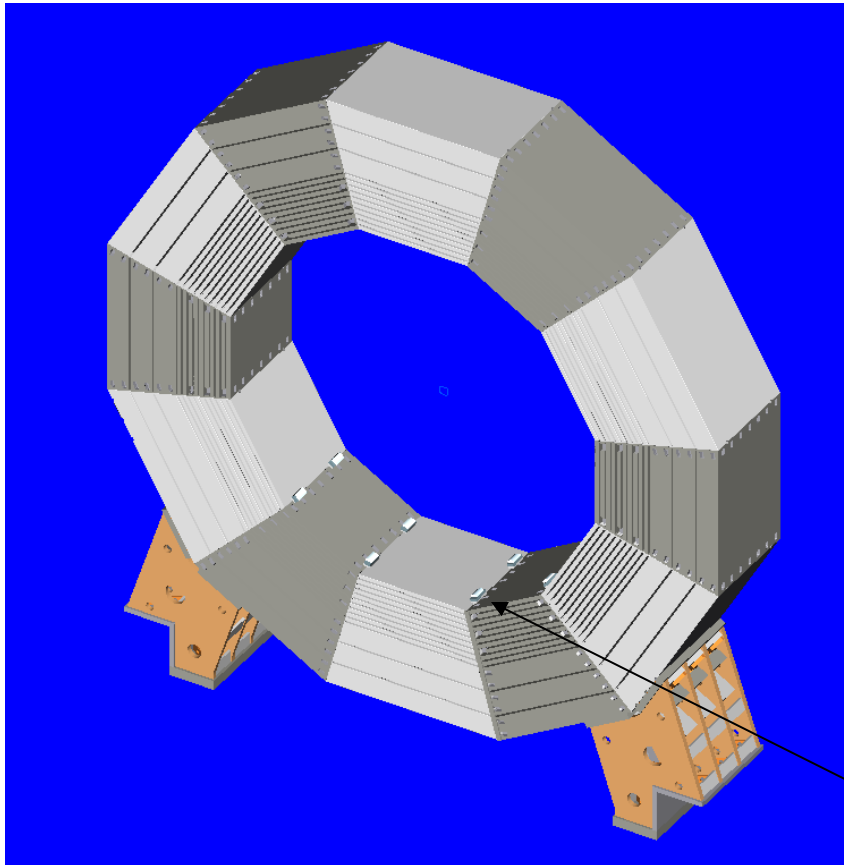
- vertical assembly of the inner vacuum vessel

- rotation of the Inner vacuum vessel in horizontal position

- welding radial tiers and end flange



Cryostat integration in central barrel ILD first step



adjustment distance

integral key, slope 3deg

hardened plate

allowable pressure

S235JR (St37) $R_{mN} \sim 360 \text{ N/mm}^2$

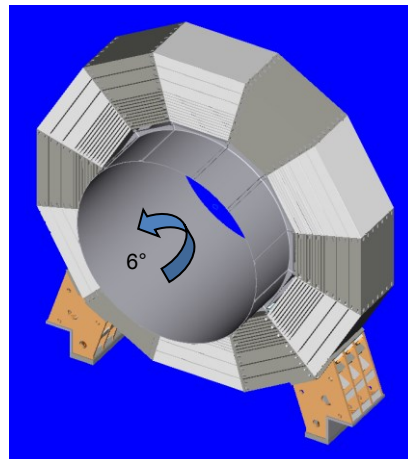
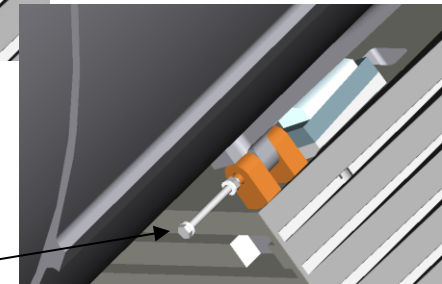
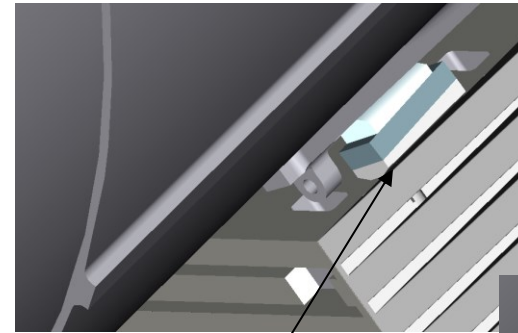
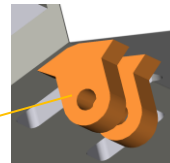
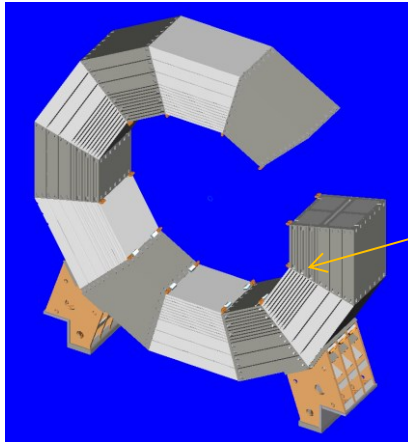
yield point $R_{p0,2N} \sim 235 \text{ N/mm}^2$

$\sigma_{dB} \sim F / A \sim 75\,000 \text{ N} / 8 \times 500 \text{ (mm)} \sim 188 \text{ N/mm}^2$

without preparatory work, full yield settling $\sim 0,8 \text{ mm}$

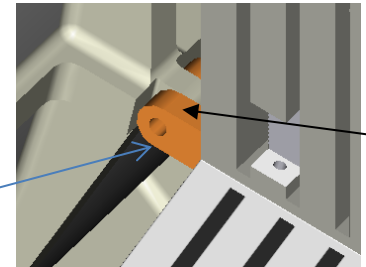
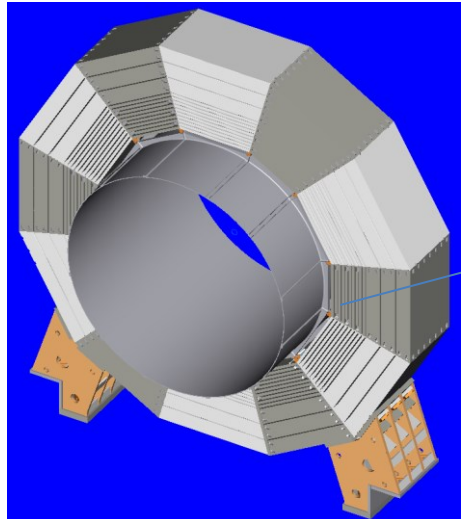
Installation of “jacking up to line” keys with hardened plate to primary alignment (integral key $\sim 3\text{deg}$), shown in position (8 units)

Second step: Push outer vacuum vessel to central barrel



- after primary alignment
- tack weld each bracket to barrel individually,
- from point to point to fit and tack
- fit screw between barrel and ovv
- all bracket to barrel tack welding
- remove circular 6° ovv from barrel
- all bracket end welding
(alternative: welding without removal of ovv)

Drilling of Dowels Holes / 24 Suspension Bolds



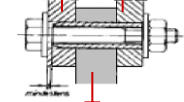
Assembly boring of $\varnothing 50H^{12}$ mm
Bearing case in combination with
Cryostat ear



friction bolt DIN 1481

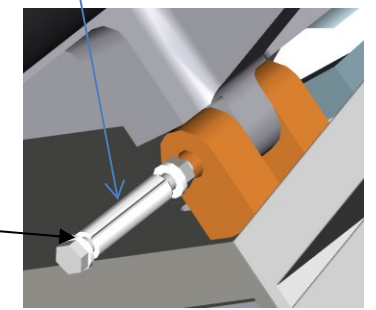
fix with friction bolt DIN 1481 - $\varnothing 50 \times 240$ lg.
hexagon head bolts with large head (HV)
DIN 6914 - M30 x 300 comply with washers
and nuts

Fa ~ 300 kN Fb ~ 300 kN

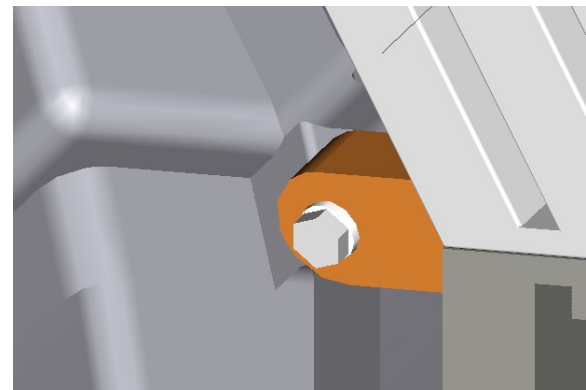


Fr theory ~ 600 kN
Fr applied under 600 kN!
Surface pressure 65 N/mm²

friction bolt DIN 1481
shearing force max ~ 1685 kN
Account: 20 friction bolt to lift 1200 t



shear stress factor ~ 2,5 (1,2 is ok)
surface pressure 125 N / mm²
S235JR ~ 235 N/mm² > 125 N/mm²
pressure factor ~ 1,8 (1,2 is ok)



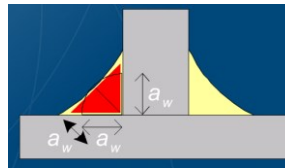
tightening screw condition:
hydraulically operated in
sequence for 24 bolt
DIN 6914 - M30 x 300
M ~ 1650 Nm, Fv ~ 350 kN

Cryostat integration in central barrel welding bearing case

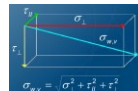
account to data sheet DVS 0705 / DIN 18800

weld seam: $a_w \sim 35 \text{ mm}$,
 $l = 80 \text{ mm}$, $A_w = 2800 \text{ mm}^2$

steel: S235JRG2
 $R_m \sim 360 \text{ N/mm}^2$
 $R_e \sim 215 \text{ N/mm}^2$



$\sigma_{II} \sim 18 \text{ N/mm}^2$
 $\sigma_{\perp} \sim 32 \text{ N/mm}^2$
 $\tau_{II} \sim 32 \text{ N/mm}^2$
 $\tau_{\perp} \sim 32 \text{ N/mm}^2$
 $\sigma_{\text{exist}} \sim 48 \text{ N/mm}^2 < \sigma_w \sim 207 \text{ N/mm}^2 \text{ (St37)}$
 (factor ~ 4)



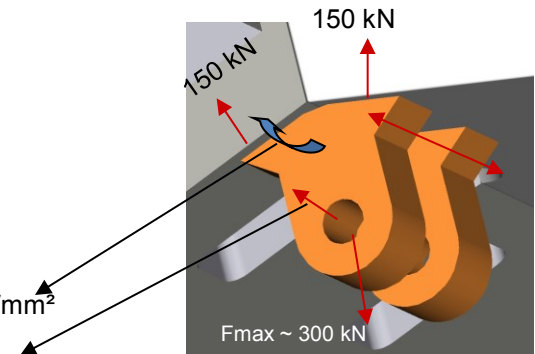
stress reference value

M bending moment $\sim 19 \text{ kNm}$

F axial $\sim 150 \text{ kN}$

σ normal stress $\sim 152 \text{ N/mm}^2 < \sigma_{\text{tol.}} \sim 195 \text{ N/mm}^2$

DVS 0705



Conclusion



- Performed detailed study
 - plant dimensioning load and variable geometric
 - stability of Cryostat / force
 - plant discussion optimal material strengths
 - safety factor
 - Instruktion report

A lot of studies need to be performed:

- design of cryostat supporting system,
- all geometrical parameters,
- finish cryostat constructions concept
- cryostat quench scenarios
- cabling concept
- power supply connection design
- cryostat safety instruction sheet
- scaffolding
- gas-, cables-, water-, power-connection
- escape routes
- safety periphery and risk assessment analyse
- collaboration with other interacting group

