

Discussion Contribution to the design of the cathode-HV

Power supply

Connector

Cable

Power Supply (I)



Estimate of power necessary: assuming $U = 100 \text{ kV}$

and $R = 1 \text{ G}\Omega$ for resistor chain $\rightarrow I = 100 \text{ }\mu\text{A} \rightarrow P = 10 \text{ W}$

(more realistic for triple GEM readout $280 \text{ V/cm} \cdot 225 \text{ cm} + 2500 \text{ V} = 65\,500 \text{ V}$)

This should not be a problem because the power is very low.

Only question I could think of is the residual ripple.

If we aim for a field homogeneity of 10^{-5} , probably also the HV should have a ripple as low as 10^{-5} ?

Short internet research turned out some candidates:



FuG – HCP series:

Setting resolution $\pm 1 \cdot 10^{-4}$

Residual ripple (0-10MHz)

$< 1 \cdot 10^{-4} \text{ pp} + 50 \text{ mVpp}$,

typ. $5 \cdot 10^{-5} \text{ pp}$

Option lower ripple

On several series a lower ripple can be achieved by better smoothing.

Series	Vmax	Amax	Pmax	Width	Height	Depth	Weight
HCP 140-65000	65 kV	2 mA	140 W	443 mm	133 mm	450 mm	21 kg
HCP 350-65000	65 kV	5 mA	350 W	443 mm	266 mm	450 mm	45 kg
HCP 700-65000	65 kV	10 mA	700 W	443 mm	355 mm	550 mm	55 kg
HCP 1400-65000	65 kV	20 mA	1,4 kW	443 mm	399 mm	550 mm	70 kg
HCP 2800-65000	65 kV	40 mA	2,8 kW	443 mm	399 mm	550 mm	80 kg
HCP 140-100000	100 kV	1 mA	140 W	443 mm	221 mm	550 mm	50 kg
HCP 350-100000	100 kV	3 mA	350 W	443 mm	221 mm	550 mm	55 kg
HCP 700-100000	100 kV	6 mA	700 W	443 mm	355 mm	550 mm	73 kg
HCP 1400-100000	100 kV	12 mA	1,4 kW	443 mm	399 mm	550 mm	90 kg



CURRENT (mA)	SERIES	STYLE	MORE INFO	PDF
6	WJ	Rack		
20	KT	Rack		
30	KB	Rack		
50	LH	Rack		
80/160	SH	Rack		
250/500	GX	Rack		

Power Supply (II)

Glassmann High Voltage Incorporated → KT series
 Static Voltage Regulation: Better than $\pm 0.005\%$ for specified line variations and 0.01% for no load to full load variations.
 Ripple: Better than 0.025% of rated voltage at full load
 (0.1% RMS for $> 100\text{kV}$).

CPS High Voltage → Model 2600

Output voltage: 0 to 30 or 0 to 60 kVDC (full scale programmable)
 Ripple at full output and load: $< 100\text{ mV}$ peak-to-peak for $100\ \mu\text{A}$
 $< 200\text{ mV}$ peak-to-peak for up to $500\ \mu\text{A}$
 $< 1\text{ V}$ peak-to-peak for over $500\ \mu\text{A}$



CAEN or ISEG did not seem to have more than $\sim 30\text{ kV}$

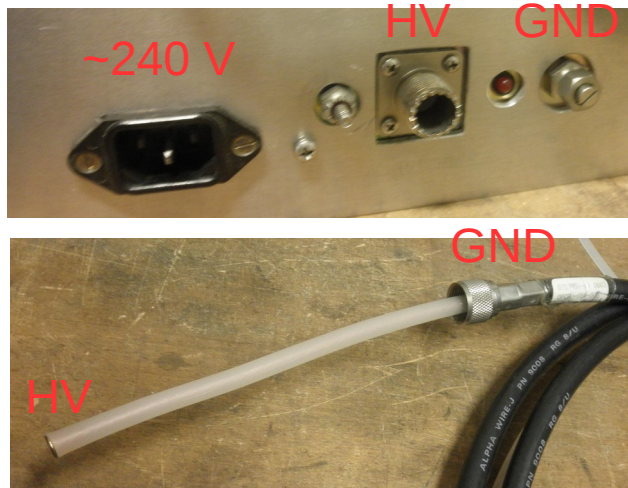
Connector



There are two sides:

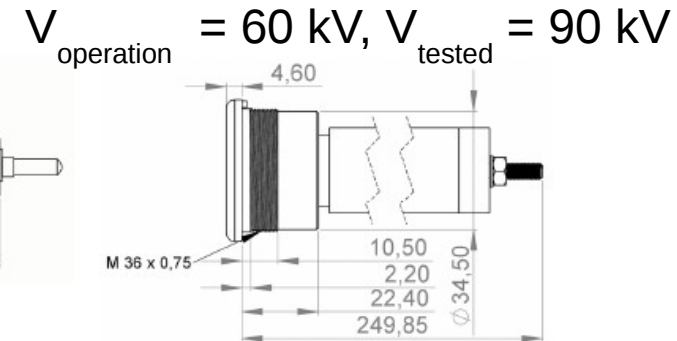
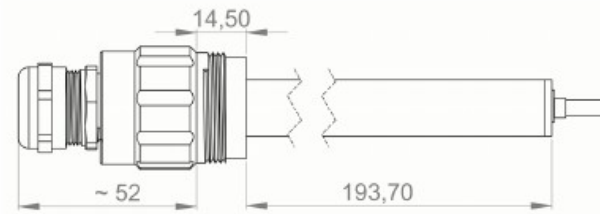
1.) power supply: Usually given by power supply producer

Examples are

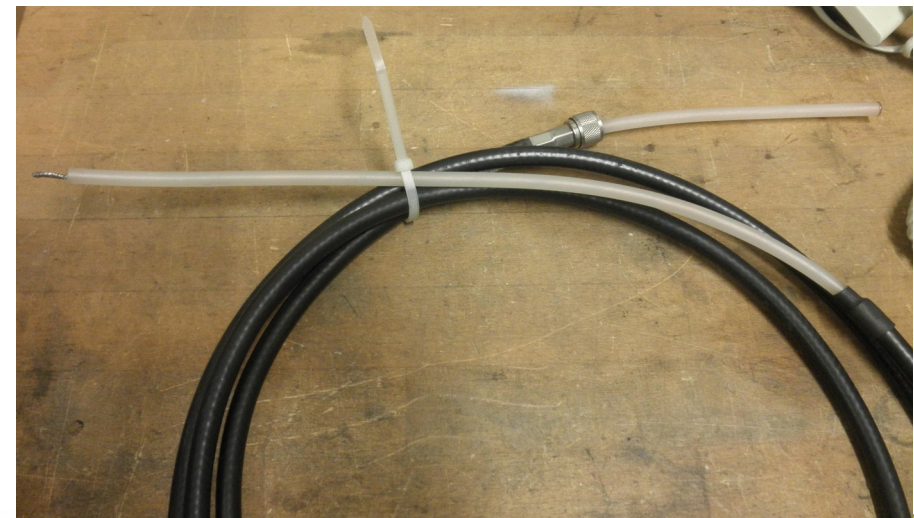


Hivolt (www.hivolts.de)

▪ DIMENSIONS S165 / B165



2.) cathode: → HV expert at Bonn (ELSA accelerator) suggested: Remove sufficient length of GND shielding and solder/clamp the HV line to the cathode. If there is a connector, you still have to get from the connector to the membrane and fix it there, the problems stays the same or even increases.



Assuming same pitch as the LP for the ring electrodes of field cage: 2.8 mm
Length of detector: 225 cm (-1 cm for gating GEM)

→ 803 resistors

Assuming 1.25 M Ω between two strips

→ 1 G Ω total resistance

BUT it depends on the insulation resistance of the HV cable!

We would need only very low currents ($I = 100 \mu\text{A}$). So the cable core can be thin (diameter 0.75 mm $\rightarrow I = 15 \text{ A}$)

Example: LEMO cable 201 340, price 7.54 €/m,

$R_{\text{conductor}} = 56.1 \Omega/\text{km}$, $R_{\text{insulator}} = 1 \text{ G}\Omega/\text{km}$, conductor diameter 0.75 mm

$V_{\text{operating}} = 50 \text{ kV}$, $V_{\text{tested}} = 75 \text{ kV}$, outer diameter 7.25 mm

Cable (II)



HVP (<http://www.hvproducts.de>)

VOLTAGE		PART NUMBER	CONDUCTOR SIZE				SEMICON DIA (mm)	DIELECTRIC		SHIELD			SEMICON MATERIAL	JACKET MATERIAL	OUTSIDE DIAMETER (mm)	IMPEDANCE (ohms)	CAPACITANCE (pF/Mtr)	MIN BEND RADIUS (mm)	MIN AMBIENT TEMP C	MAX CONDUCTOR TEMP C	WEIGHT KG/MTR
DC (kV)	AC (kV)		AWG	STRANDS	mm ²	DIA (mm)		MATERIAL	DIA (mm)	CONSTRUCTION	AWG (equiv)	Coverage (%)									
60	20	2024S J	12	19/25SPC	3.31	2.30	3.40	SILICONE	9.10	34 TC BRAID	15	82	ink & tape		13.34	39	187	25	-65	200	0.232
60	20	2149SVJ	18	19/30TC	0.83	1.30	2.00	LDHMW PE	5.80	34 TC BRAID	17	86	N/A	PVC	8.51	50	121	64	-51	60	0.075
60	20	2240-R2	12	19/25SPC	3.35	2.40	3.60	EPR	10.20	34 TC BRAID	14	95	extruded	polyurethane	17.02	45	157	152	-51	130	0.373
75	25	2110SUJ	2	133/23TC	33.62	6.60	8.10	EPR	14.50	30 TC BRAID	4	95	N/A	polyurethane	20.07	19	387	102	-51	71	0.730
100	30	2062S J	8	133/29SPC	8.37	4.20	5.60	SILICONE	16.50	34 TC BRAID	16	82	ink & tape		20.57	41	164	140	-65	200	0.596
100		2124	16	19/29TC	1.31	1.50	2.50	LDHMW PE	9.40	34 TC BRAID	13	90	N/A	PVC	11.18	61	98	152	-51	60	0.149
100		2125	12	19/25TC	3.31	2.30	3.30	LDHMW PE	9.40	34 TC BRAID	13	90	N/A	PVC	11.18	48	121	152	-51	60	0.149
100	30	2242	10	19/23TC	4.92	2.90	4.80	EPR	15.70	34 TC BRAID	14	90	extruded	polyurethane	21.59	48	141	127	-51	130	0.596

Conductor: $A = 1.31 \text{ mm}^2$, 1.5 mm diameter

Dielectric: 9.4 mm diameter, material LDHMW PE

Outside diameter: 11.18 mm, min. bending radius 152 mm, weight 149 g/m

Capacitance: 96 pF/m

No information on $R_{\text{insulator}}$

HIVOLT (<http://www.hivolt.de>)

Conductor: $A = 1.2 \text{ mm}^2$

1.5 mm diameter

Impedance 61 Ω

Dielectric: material LDHMW PE

Outside diameter: 11.2 mm

Capacitance: 98 pF/m

RATED VOLTAGE		TYPE	CONDUCTOR SIZE		DIELECTRIC MATERIAL	JACKET MATERIAL	OUTER DIA [mm]	NOTES	STATUS
[kV _{DC}]	[kV _{AC}]		[AWG]	[mm ²]					
60	20	2024SVJ	12	3.1	SILICONE	PVC	12.7		P
60		2149SVJ	18	0.96	LDHMW PE	PVC	8.6		P
60	20	HSC-60-1PSUA-2	18	0.96	LDHMW PE	TPE-U	7.7		P
60		HXC-60-1EA-8	14	2	EPR (black)	PVC	11.1		P
100	30	2062SVJ	8	8.5	SILICONE	PVC	20.8		P
100		2124	16	1.2	LDHMW PE	PVC	11.2		P
100		2125	12	3.1	LDHMW PE	PVC	11.2		S
100	30	HSC-100-1PSUA-2	16	1.2	LDHMW PE	TPE-U	13.2		E