



LINEAR COLLIDER COLLABORATION

Designing the world's next great particle accelerator

# Status radiation cooled target for the undulator-based $e^+$ source

AWLC 2018, Fukuoka, Japan

May 29, 2018

Sabine Riemann, Felix Dietrich, DESY,  
Gudrid Moortgat-Pick, Andriy Ushakov (Hamburg U)  
Peter Sievers (CERN)

# outline

- What is new since LCWS 2017?  
Simulation studies for the ILC250 target wheel:
  - Temperature distribution for 7mm thick Ti6Al4V target
  - Stress distribution in 7mm thick Ti6Al4V target
  - Discussion whether the load is acceptable
- Next steps & plan

## All results

- are included in the WG report
- Should be cross-checked

# Source parameters – 1312 bunches/pulse

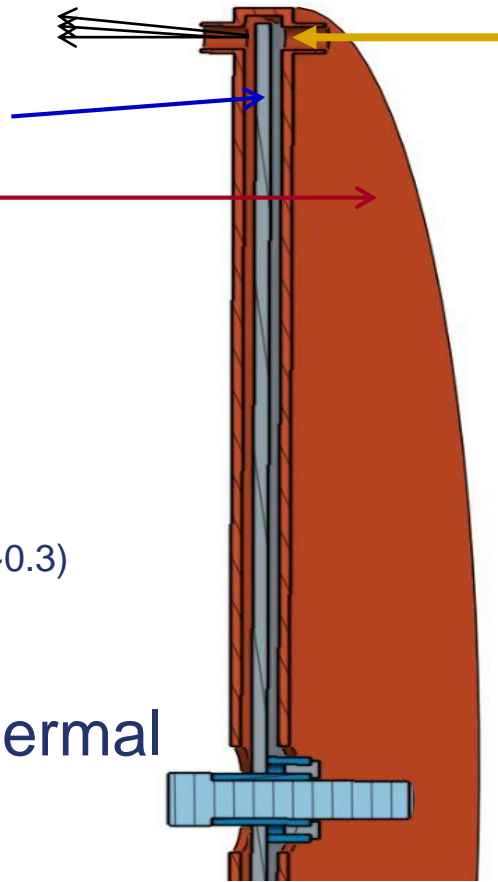
Electron beam energy	GeV	126,5	125	150	175	250
Active undulator length	m	231		147		
Undulator K		0.85		0.8	0.66	0.45
Photon yield	$\gamma$ /e-	393		224	157	76.1
Photon energy (1 <sup>st</sup> harmonic)	MeV	7.7	7.5	11.3	17.6	42.9
Average photon beam power	kW	62.6	60.2	48.8	45.2	42.9
Distance target – middle undulator	m	401	570	500		
Target (Ti6Al4V)thickness	mm	7	14.8			
Average power deposition in target	kW	1.94	5.4	3.9	3.3	2.3
Photon beam spot size on target ( $\sigma$ )	mm	1.2	1.72	1.21	0.89	0.5
Peak Energy Deposition Density (PEDD) in spinning target per pulse	J/g	61.0	43.7	41.0	42.4	45.8
Polarization of captured positrons	%	29.5	30.7	29.4	30.8	24.9



Used for current target simulations

# Cooling by thermal radiation

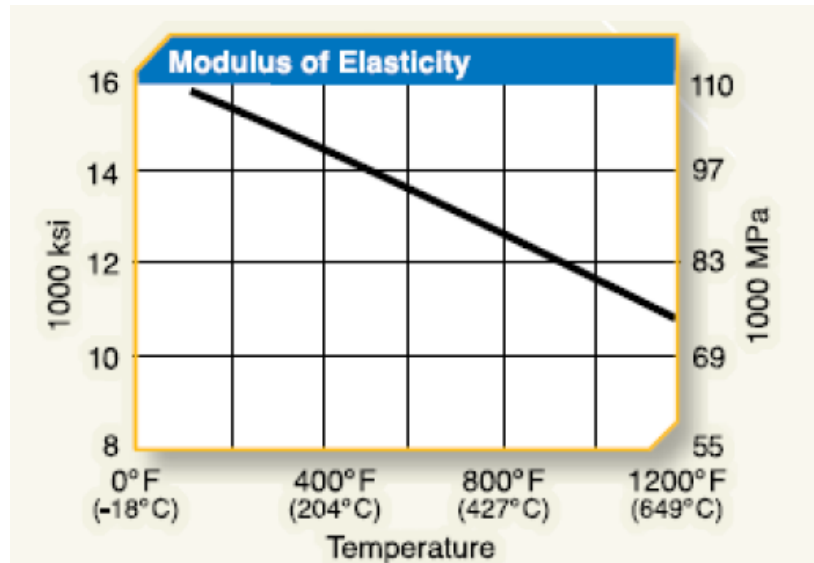
- heat is radiated from spinning target wheel to stationary water-cooled cooler
  - Rough estimate: for 2kW power deposition about 0.6 m<sup>2</sup> are needed to keep material at 400C average temperature (effective surface emissivity ~0.3)
- But: high-temperature Ti alloys have low thermal conductivity ( $\lambda = 0.06 - 0.15 \text{ K/cm/s}$ )
  - heat dissipation ~ 0.5cm in 7sec
  - heat accumulates in the rim near to beam path



# Temperature dependence of Ti6Al4V parameters

Important for the simulation of target load: all parameters depend strongly on temperature

- So far, we took into account temperature dependence of specific heat, thermal conductivity and thermal expansion (see arXive 1801.10565) .
- Values given in data sheets depend slightly on vendor
- New: also modulus of elasticity  $E(T)$  used
  - $E$  is important for stress evaluation:  
 $\text{Stress} \sim E \propto \Delta T$
  - At  $\sim 500^\circ\text{C}$   $E \approx 83\text{GPa}$  about 75% of  $E(\text{RT})$
  - Material response at higher  $T$  is more relaxed



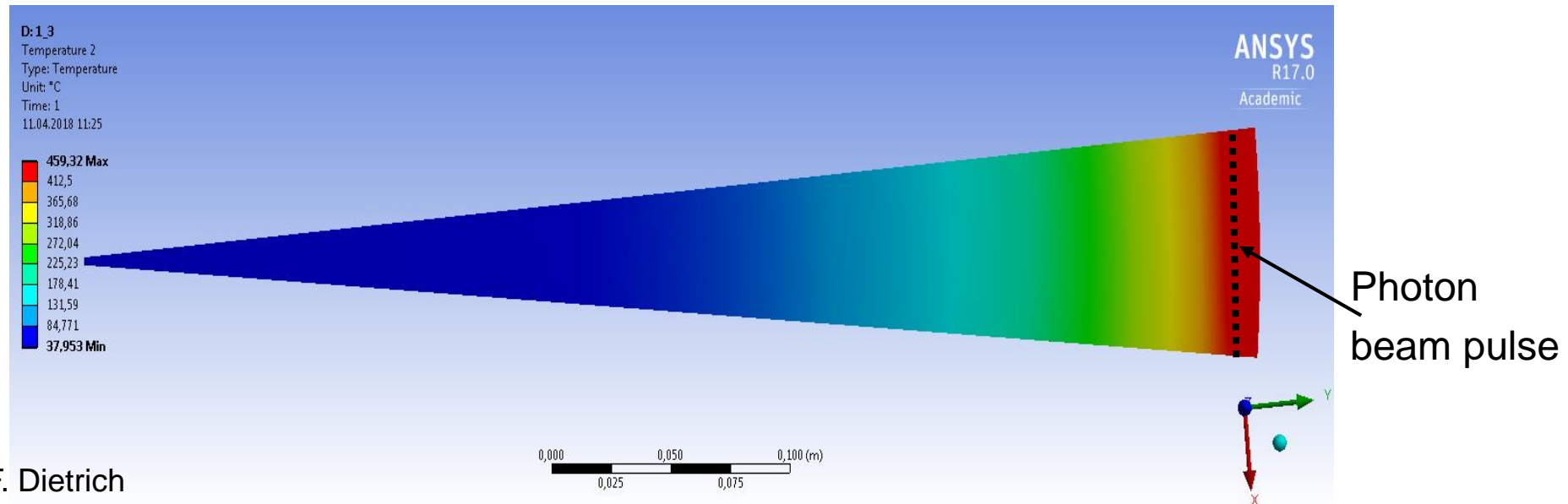
Taken from  
ATI data sheet  
Ti Grade 5

# Temperature distribution in target wheel

- Average energy deposition in target ~2kW (ILC250, ILC500)
- ANSYS simulations for radiative cooling of target wheel
  - Efficiency of cooling depends on emissivity of surfaces of wheel and cooler ( $\epsilon_{Ti}$  and  $\epsilon_{Cu}$ )

Temperature distribution in target piece corresponding to 1 pulse length; ILC250

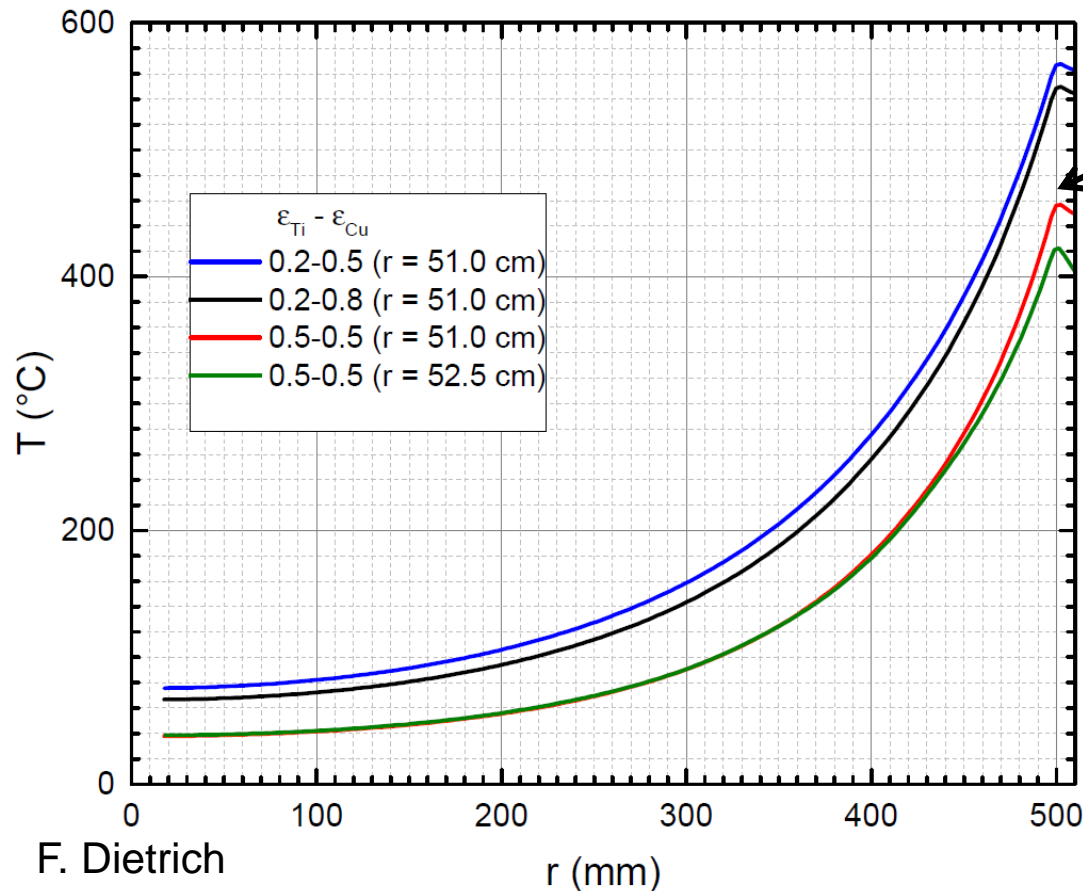
( $\epsilon_{eff} = 0.33$ ;  $\epsilon_{Ti} = \epsilon_{Cu} = 0.5$ )



F. Dietrich

# Temperature on target, ILC250

Average temperature in wheel as function of radius  $r$  for different surface emissivities of target and cooler (Cu)



Photon beam impact always at  $r=50$ cm

$\epsilon_{\text{eff}} = 0.33$  for  $\epsilon_{Ti} = \epsilon_{Cu} = 0.5$

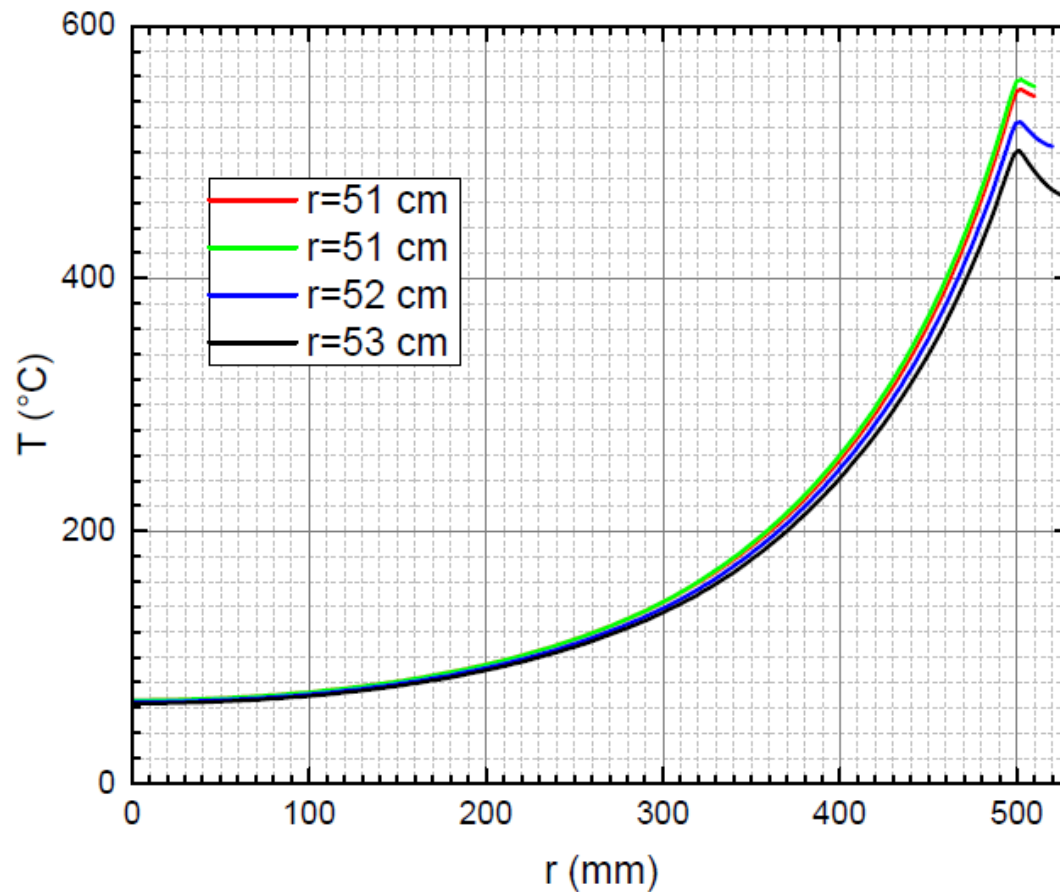
Deposited  $E = 2$  kW

$T_{\text{ave}} \leq 460^\circ\text{C}$

We checked different wheel radii,  
 $r = 51 \dots 52.5$  cm

→ max temperatures can be  
slightly decreased for larger  
wheel radius

F. Dietrich



Radial temperature distribution in target wheel

Red: no expansion slots

Green, blue, black: with 20cm long expansion slots



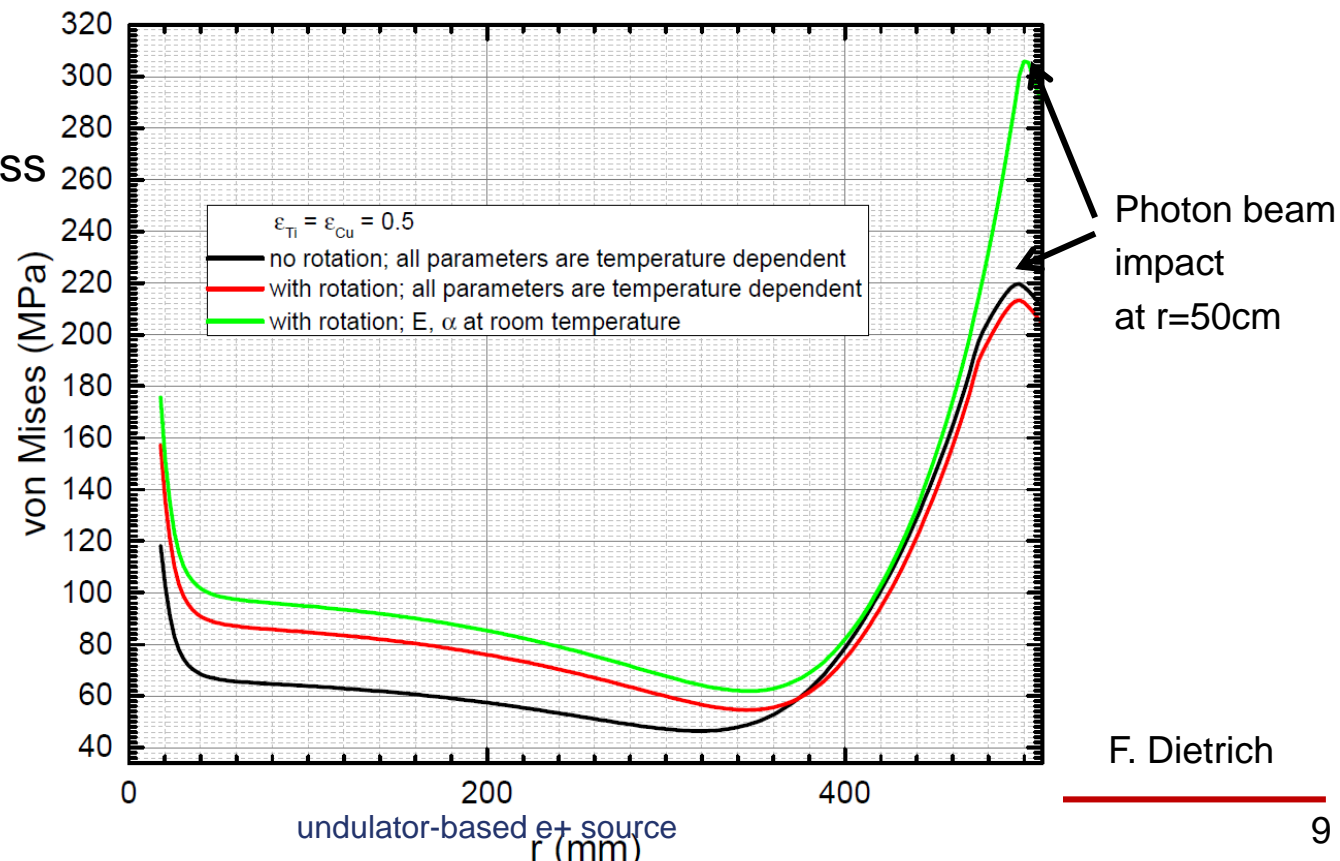
# Stress in target (ILC250)

Consider target disc, thickness 7mm,  $r_{\text{out}} = 51\text{cm}$  (...53cm), beam hits target at  $r=50\text{cm}$

- Material expansion  $\Leftrightarrow$  high thermal stress in beam impact region
- Stress due to rotation (hoop and radial) is  $<50\text{MPa}$ , in the rim region  $<10\text{MPa}$

Average von Mises stress  
along wheel radius  $r$

$\sigma_{\text{vM}} < 220\text{MPa}$



- Dynamic stress at radius  $r$

$$\sigma_H = \frac{3 + \nu}{8} \rho \omega^2 \left( 1 - \frac{r^2}{r_o^2} \right) \left( 1 - \frac{r_i^2}{r^2} \right)$$
$$\sigma_r = \frac{3 + \nu}{8} \rho \omega^2 \left( 1 + \frac{r_i^2}{r_o^2} + \frac{r_i^2}{r^2} - \frac{1 + 3\nu}{3 + \nu} \frac{r^2}{r_o^2} \right)$$

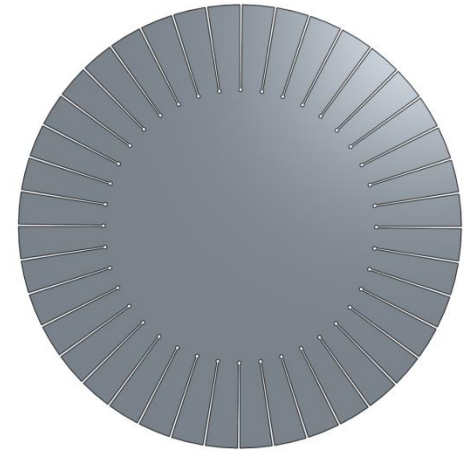
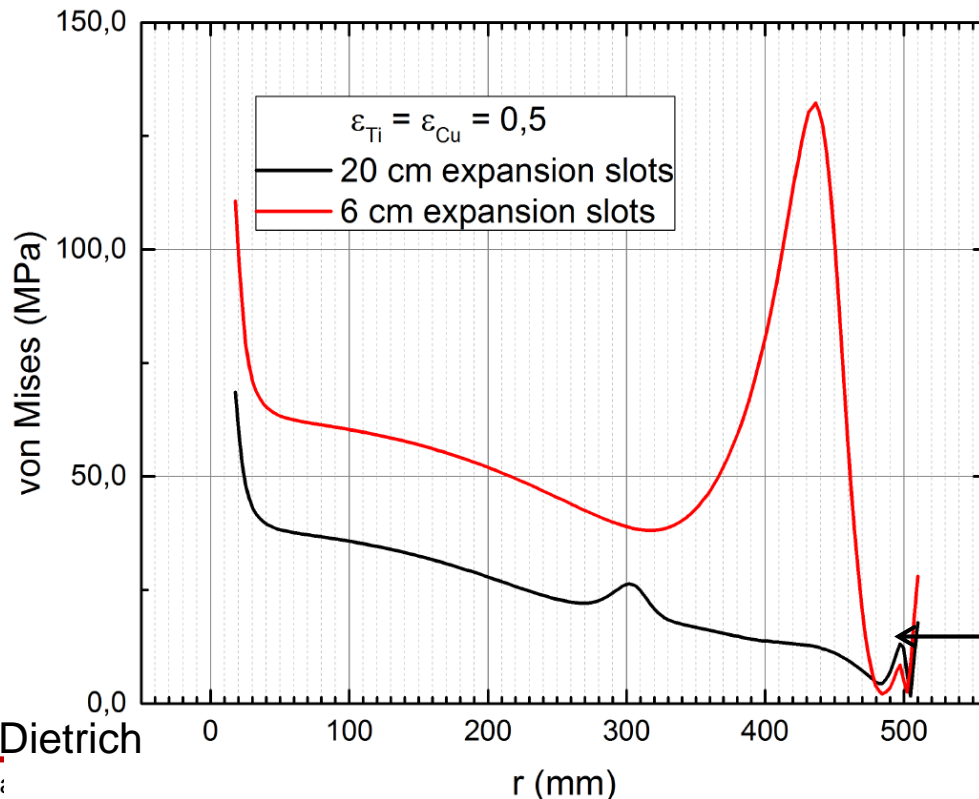
$r_o$  = outer wheel radius,  $r_i$  = inner radius at shaft

- Max radial stress is located at  $\sqrt{r_o r_i}$ , i.e. more in the inner region where the T is low (assuming full disc)
- Hoop stress from rotation at the beam path (highest T) is low,  $\sim 9\text{MPa}$
- ANSYS calculations for detailed stress evaluation

# Stress in target (ILC250)

Consider target disc, thickness 7mm,  $r_{\text{out}} = 51\text{cm}$  (...53cm), beam hits target at  $r=50\text{cm}$

- Expansion slots (6cm and 20cm long)  
static stress substantially reduced,  $\sigma_{\text{VM}} \leq 20\text{MPa}$  in rim region

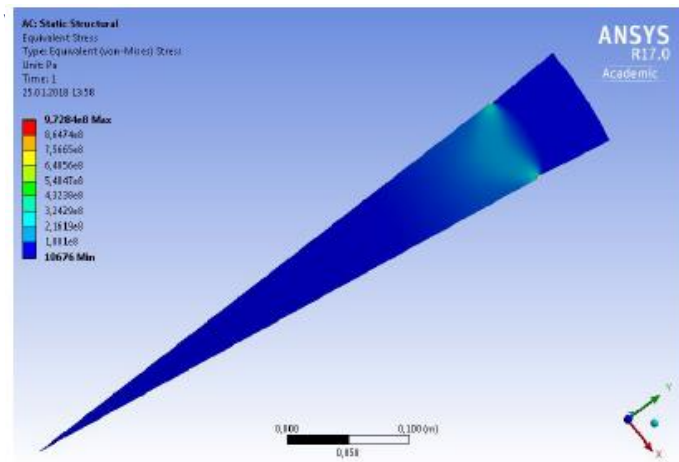


Expansion slots require synchronization with beam pulses!!

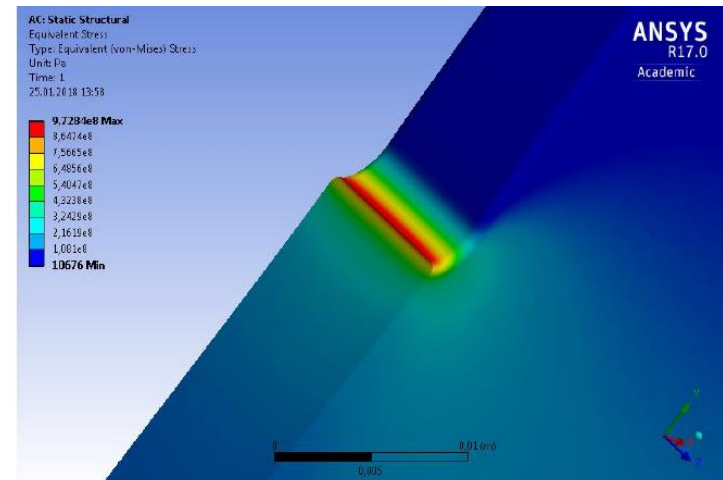
Photon beam impact at  $r=50\text{cm}$

# Expansion slots

- stress around the bore of the expansion slots;
  - Stress can be reduced with optimized bore shape
- Results on this page are still with E(RT), see 1801.10565



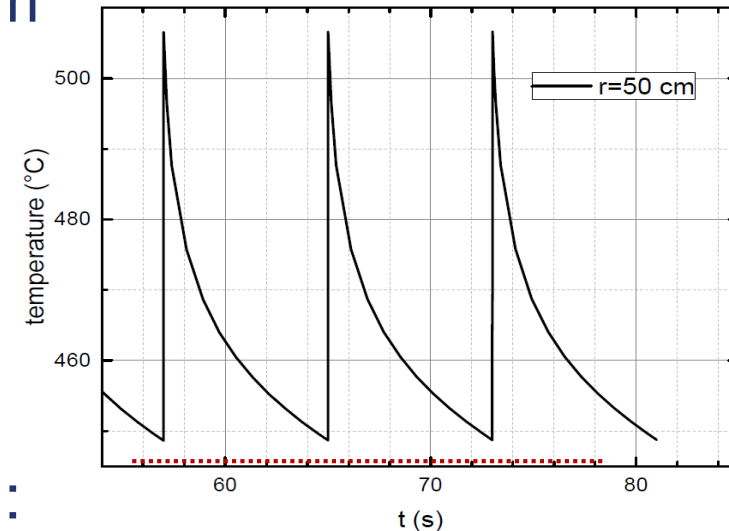
1cm long



		full disc	expansion slots	
			20 cm	6 cm
von Mises	[MPa]			
	r = 50 cm	348	7.39	2.71
	r = 45 cm	192	4.43	125
	r = 30 cm	67.66	47.4	44.5

# Cyclic load at the target - peak temperature

- Max temperature evolution along rim
  - if wheel has equilibrium temperature distribution reached, pulse increases temperature up to  $\sim 510^\circ\text{C}$   
( $2\text{kW}$ ,  $\epsilon_{\text{eff}} = 0.33$  for  $\epsilon_{\text{Ti}} = \epsilon_{\text{Cu}} = 0.5$ )
- Resulting peak stress at beam path:
  - detailed ANSYS simulations are still running
  - Time of energy deposition is too slow, intensity too small to create shock waves
  - Estimate:  $\sigma_{\text{peak}} \sim E \propto \Delta T$   
 $\sigma_{\text{peak}} < 150 \text{ MPa}$
  - In total:  $\sigma_{\text{peak}} < 220\text{MPa} + 150\text{MPa} = 370\text{MPa}$  in case of no expansion slots
  - The stress is compressive

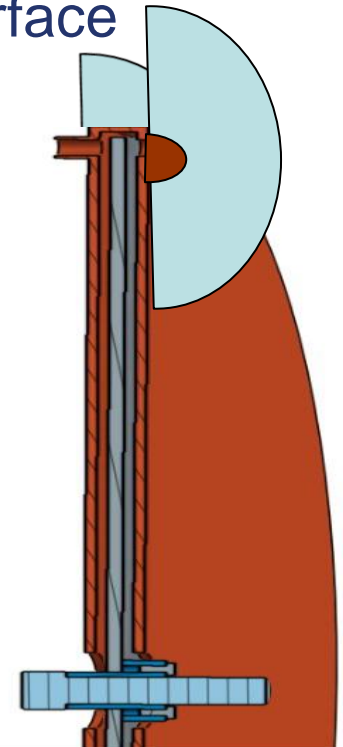


# Cyclic load – what does the target material stand?

- Material limits depend on
  - temperature
  - type of load (compressive or tensile)
  - Duration of load and cyclic load, ...
- References for Ti6Al4V give no clear answer; we concluded to be safe if cyclic stress amplitudes are below 300 MPa for temperatures up to ~500C.
- We performed tests with the e- beam at the Microtron in Mainz: We simulated cyclic load similar as expected at ILC e+ target.
  - Ti6A4V samples were radiated with pulses that create stress amplitudes similar as expected at ILC e+ target
  - Number of load cycles corresponded to 1-2 years ILC operation,
  - The material Ti6A4V was heated up to ~900C
  - Material survived well (see IPAC2017, TUPAB002)
    - Structure in beam area was changed to larger grains
    - Max dimensional change was below  $\leq 3\%$  in the centre of the beam spot

# Target + optical matching device (OMD)

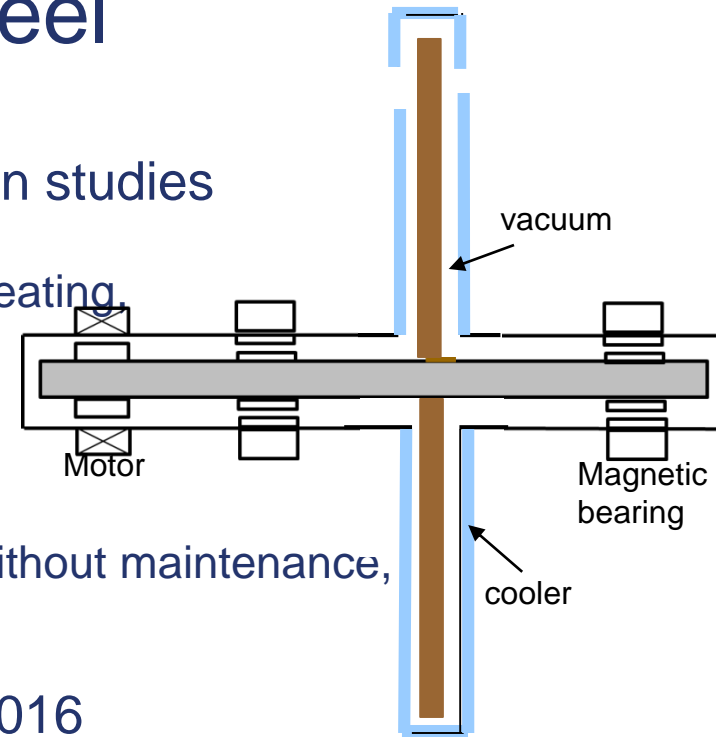
- The OMD occupies part of the radiating target surface  
→ surface for effective cooling is reduced up to ~25% for the QWT (~13% for the Flux concentrator)
- Assuming no cooling → max average  $T[K]$  rises by factor ~1.075 (460C → 515C)
- In reality, the OMD acts a 'cooler'
  - 500W would radiate to QWT surfaces (~250W at front and 250W at back)
  - About 250W would radiate to the FC front
- This additional heat load for the OMD has to be taken into account for its engineering design



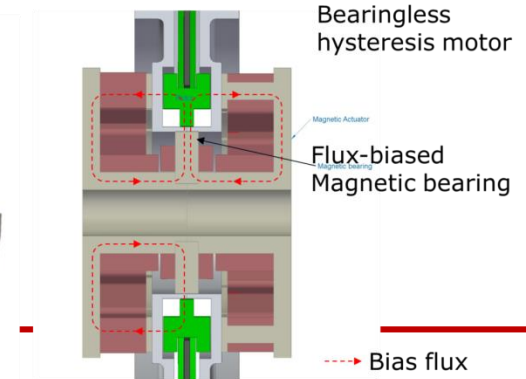
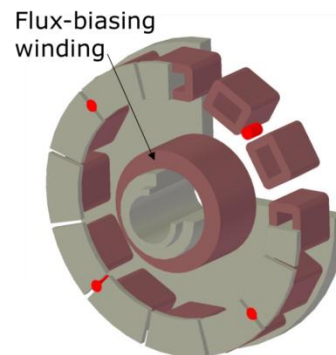
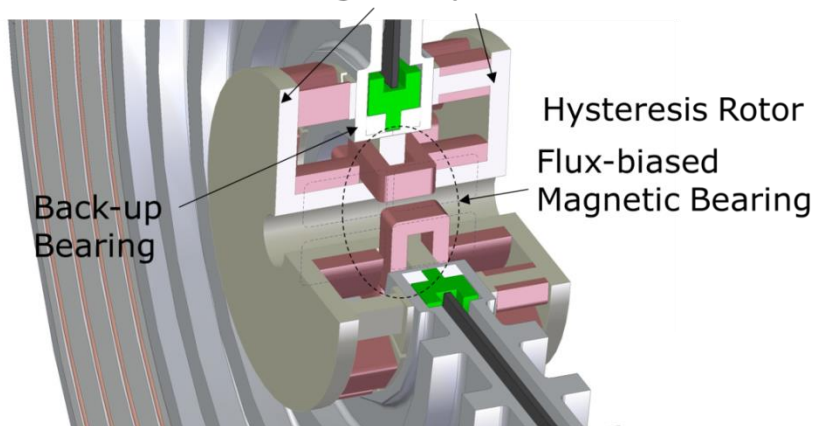


# Drive and bearing for the wheel

- Nothing new – status unchanged
- Specification to be done based on simulation studies for the target wheel
  - response of rotating wheel to the beam load, heating, stress, cooling, imbalances, etc
  - Weight of the Ti alloy disc for ILC250: ~25kg
  - Eddy currents
- Magnetic bearings, drive motor etc:
  - are widely used and operated over long time without maintenance,
  - Companies: Rigaku, Juelich, SKF ...
- Proposal by M. Breidenbach et al, ICHEP 2016



Bearingless Hysteresis Motors





# Upgrade to high luminosity (2625 bunches/pulse)

- Doubled energy deposition in target increases average  $T$  [K] by  $\sim 2^{1/4}$ 
  - **460 C  $\rightarrow$   $\sim$  600 C**
- Peak temperature rises by factor  $\sim 1.5 \Leftrightarrow \Delta T < 100\text{K}$
- Possible options to handle the higher temperatures
  - Design with increased radiation area near the beam path (fins) is required. First studies exist (see former workshops)
  - Expansion slots are recommended
  - connection of the Ti alloy target with a cooler material of high heat conductivity to increase cooling efficiency.  
The design of the contact target-cooler has to be optimized and tested

# Upgrade to higher energies

- For nominal luminosity the energy deposition and max temperatures are no problem:
  - 500GeV  $\rightarrow E_{\text{dep}}$  in target  $\sim 2\text{kW}$
  - Optimize target thickness for the CM energy
- Luminosity upgrade at higher energies:
  - change the wheel geometry with fins for more efficient radiation (larger radiating area)
  - Connect the rim of the wheel with material of higher heat conductivity  $\rightarrow$  wheel consisting of target rim + radiator  $\rightarrow$  increased cooling efficiency

## General remark:

- Think about materials/Ti alloys which are designed for high load at working temperatures up to 700-800C
- M. Breidenbach, LCWS 2015, ICHEP 2016: use Ti-SF 61

# Summary target disc

- Target wheel could be designed as disc; following the simulation studies the load is below the limits even in a disc wheel without expansion slots
- With expansion slots the stress due to average heating and cyclic load is safely below the material limits but the wheel rotation must be synchronized with the beam pulses
- target heating and cooling efficiency should be tested with a module consisting of a target piece corresponding to the sector which belongs to one pulse.
  - Such sector is located in vacuum, heated on one side → check temperature distribution in the target piece and radiation to a test cooler
  - Check cooling efficiency for different surface parameters, geometry etc.

# R&D work for the next years

- Finalize the specifications for a target wheel (250 GeV collision energy)
- test in the lab the cooling by thermal radiation for a target piece
  - There is no doubt that radiative cooling will work, but details and optimization should be tested.
  - Test also performance beyond the desired operation temperatures of the target. This is essential for the safety margins
  - Design for such cooling-test-module
- Test load limits for target materials
- Study of the response of the spinning target wheel to the beam pulses, stress due to transient and average heating and thermal expansions are under way; (currently performed at DESY Zeuthen and University Hamburg)
- Develop a full-size mock-up for the target to test the target rotation in vacuum
  - it includes the full set-up of the target including motor,
  - bearings
  - full-size wheel

→ Target wheel for e<sup>+</sup> production

# Thank you!