

# Design check of ILC Main Beam Dump

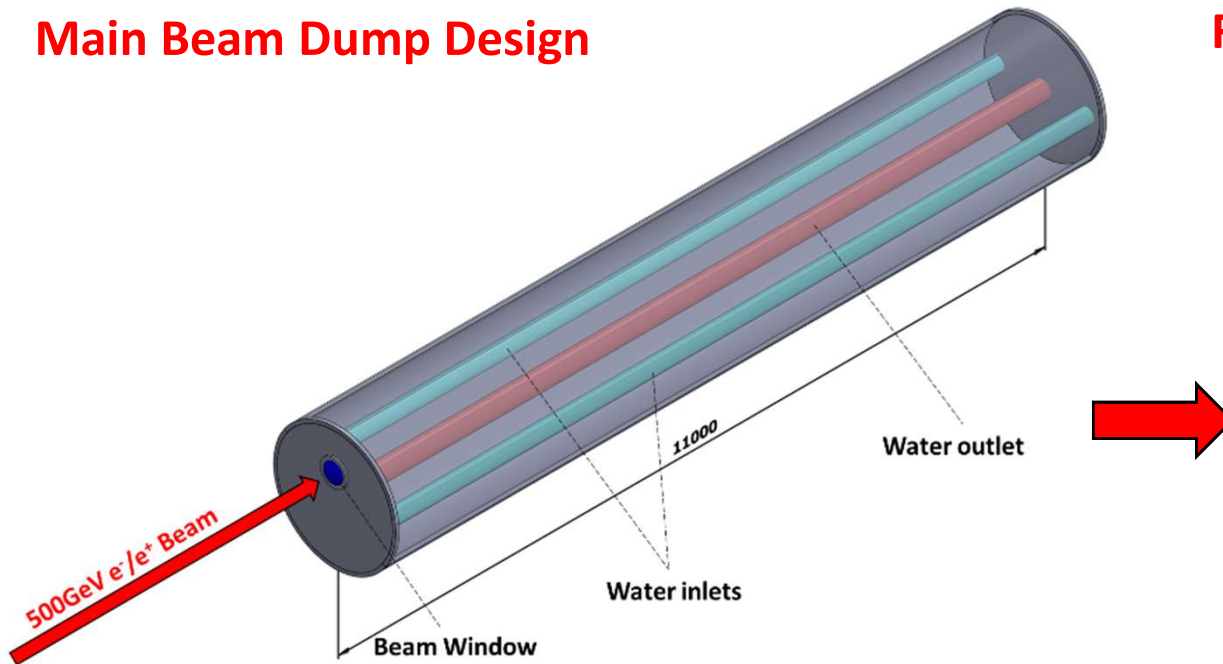


Yu Morikawa

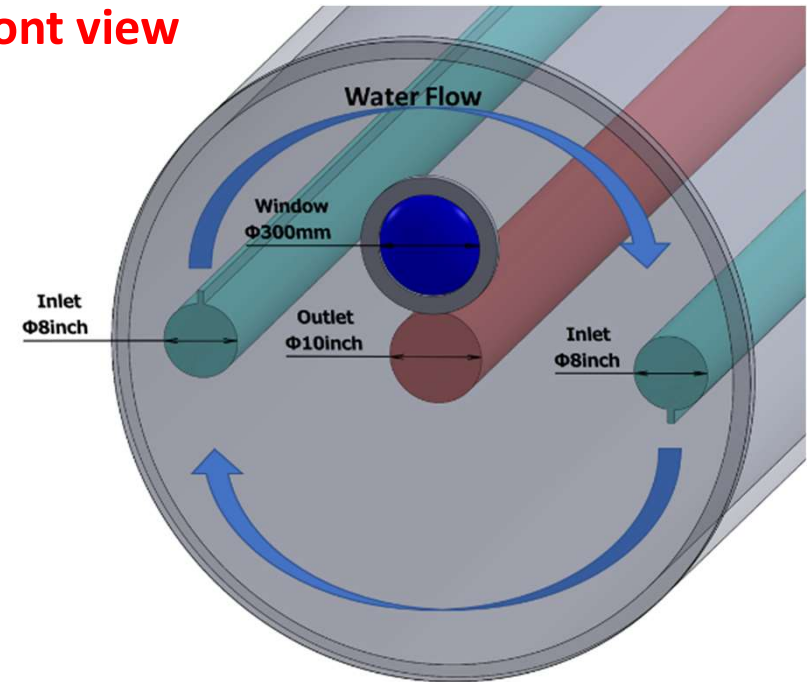


# Base design of ILC Main Beam Dump

## Main Beam Dump Design



## Front view



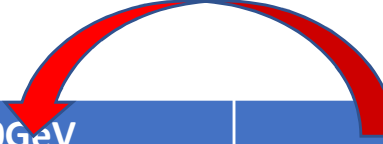
### 【Base Design】

- **Water power absorber** and **forced convection** to extract the heat.
  - \* Water is compressed **1 MPa**  $\Rightarrow$  **boiling temp 180°C**
  - \* Vortex water flow  $\Rightarrow$  Mass flow rate : **104.5kg/s** each inlet, Ave flow velocity **2.17m/s**
- Beam Window made of **Ti-6Al-4V**.
  - Beam sweep : 1kHz sweep, sweep radius : **6cm**



# What are required conditions in 250GeV operation?

ILC Main Beam Dump is designed based on 1TeV Beam Parameters.  
How much thermal load would be relaxed with 250GeV nominal status?



	250GeV nominal	1TeV Energy upgrade
Beam Energy	125GeV	500GeV
Electrons per Bunch	$2 \times 10^{10}$ (3.2nC)	$1.74 \times 10^{10}$ (2.79nC)
Bunches per Pulse	1312	2450
Beam Size	$\sigma_x = 2.42\text{mm}$ , $\sigma_y = 0.27\text{mm}$ @ Beam Dump entrance	
Beam divergence	1 $\mu\text{rad}$ @Beam Dump entrance	
Momentum spread	0.2% Beam Dump entrance	
Pulse length	0.727ms	0.897ms
Pulse Energy	0.52MJ	3.41 MJ
Rep rate	5Hz	4Hz
Average Power	<b>2.6 MW</b>	<b>13.7 MW</b>



# Contents

- ◆ **Thermal Analysis**
  - Energy deposition**
  - Peak temperature in water flow**
  - Pressure wave in water**
  - Beam window durability**
- ◆ **Water Activation**
- ◆ **Required System**
  - Pump system**
  - Recombiner system**
  - Water filtering**
  - Shielding for prevention of activation**

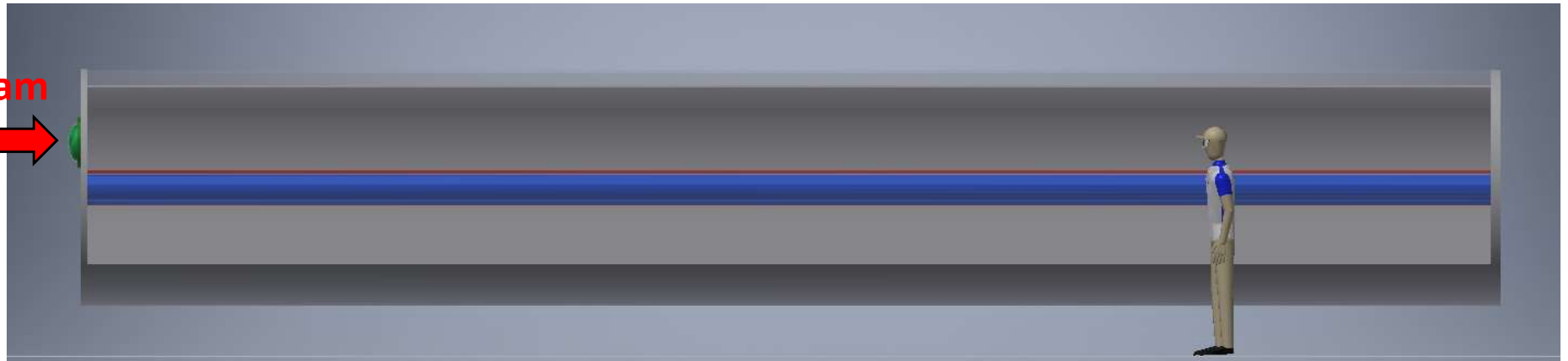
# Thermal Analysis



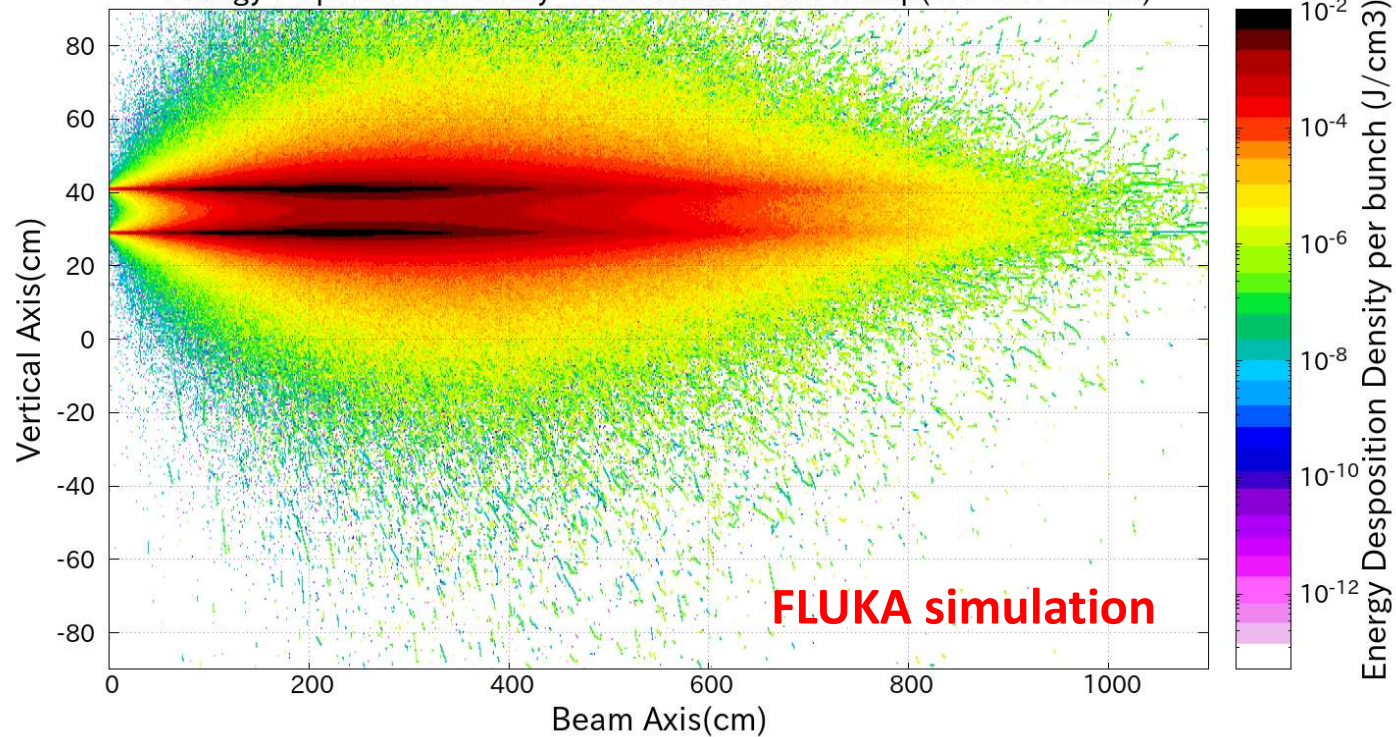
# Energy Deposition in water– Side View

[Energy Deposition in water]

$e^-/e^+$  Beam



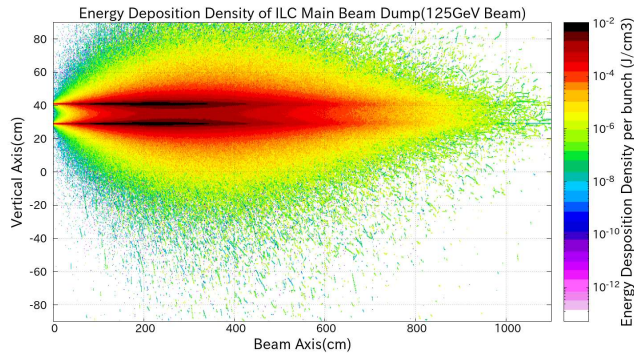
Energy Deposition Density of ILC Main Beam Dump(125GeV Beam)





# Peak Energy Deposition Density

FLUKA simulation



Max value along beam axis



**[250GeV nominal]**

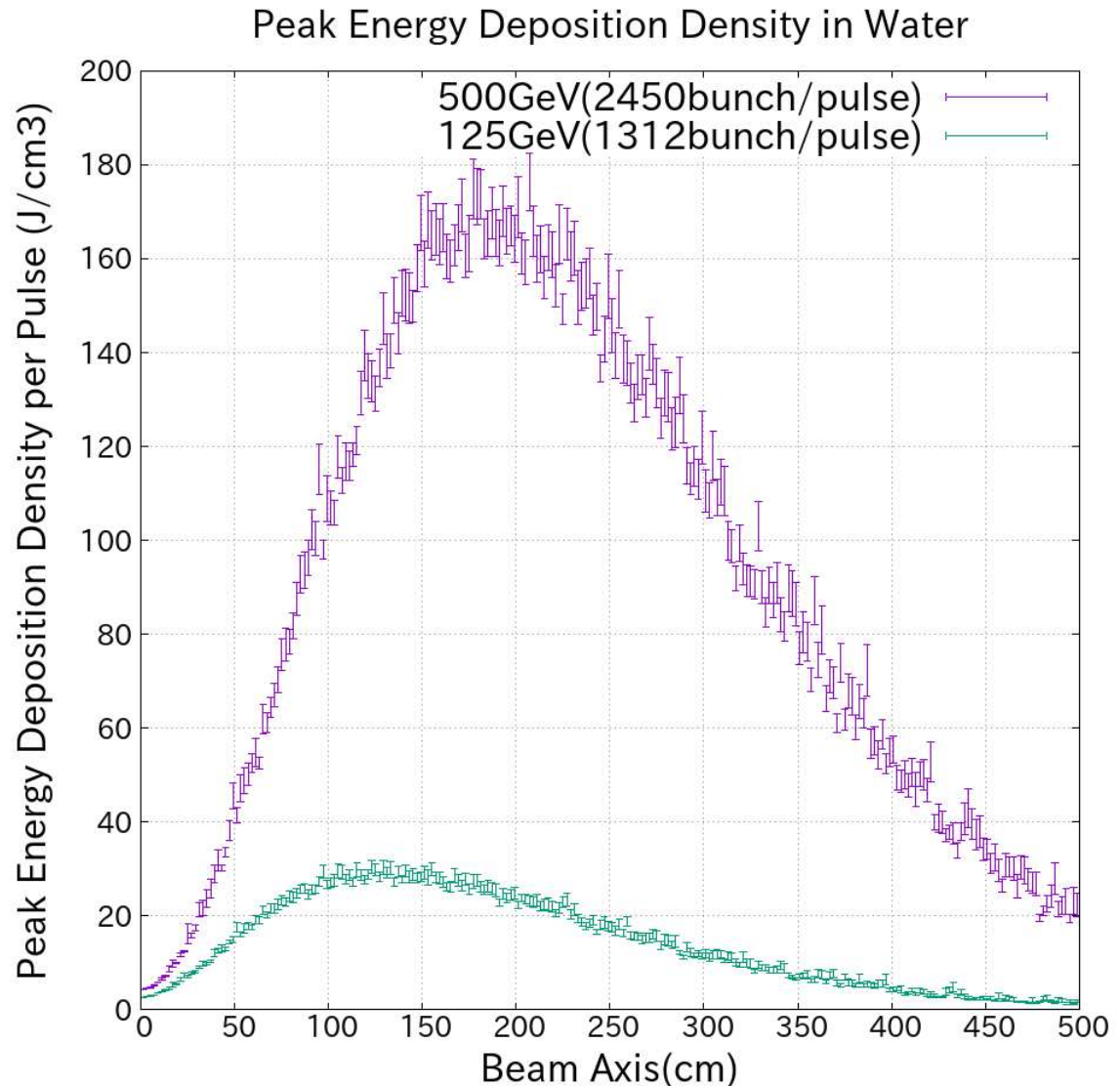
**Max PEDD = 28J/cm<sup>3</sup>**

**@ Z=125cm**

**[1TeV stage]**

**Max PEDD = 170J/cm<sup>3</sup>**

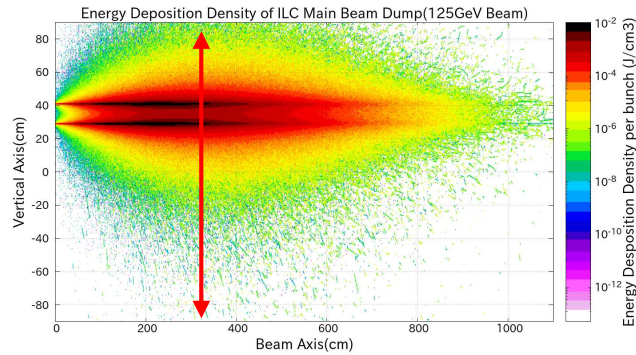
**@ Z=190cm**





# Longitudinal Power

FLUKA simulation



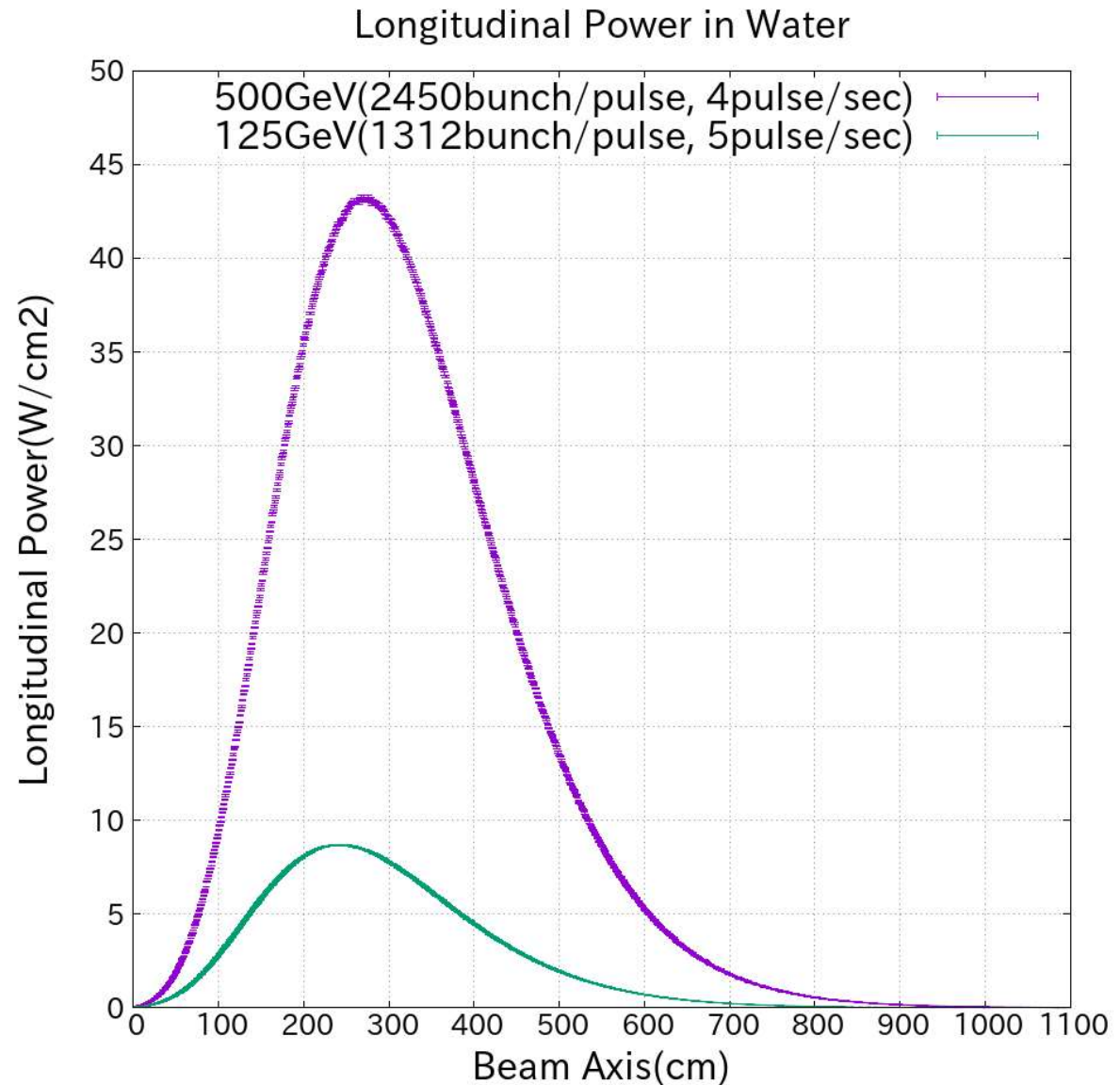
Integrate transverse

**【250GeV nominal】**

**Max Longitudinal Power =  
43kW/cm @ Z=280cm**

**【1TeV stage】**

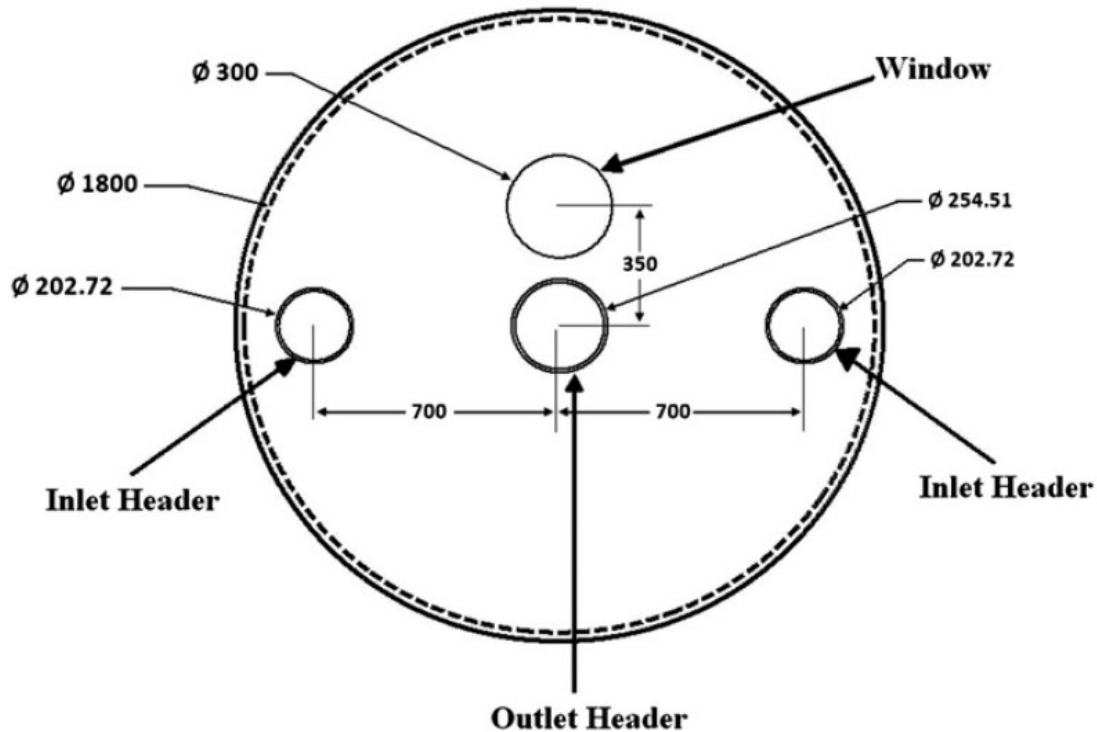
**Max Longitudinal Power =  
8.4kW/cm @ Z=230cm**



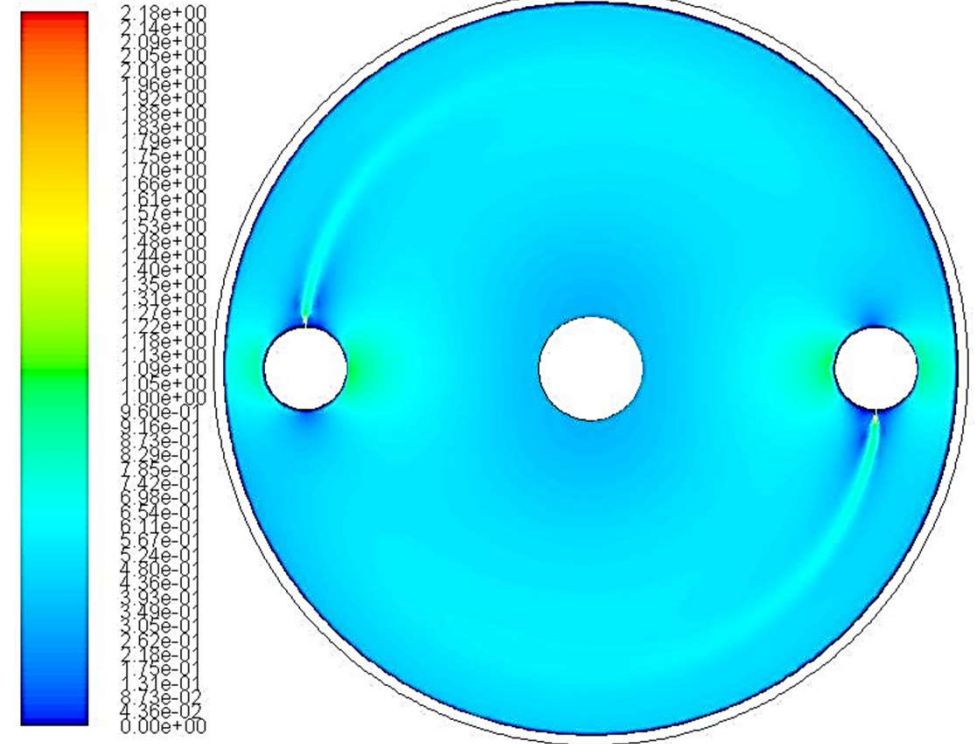


# Temperature Evaluation

Geometry



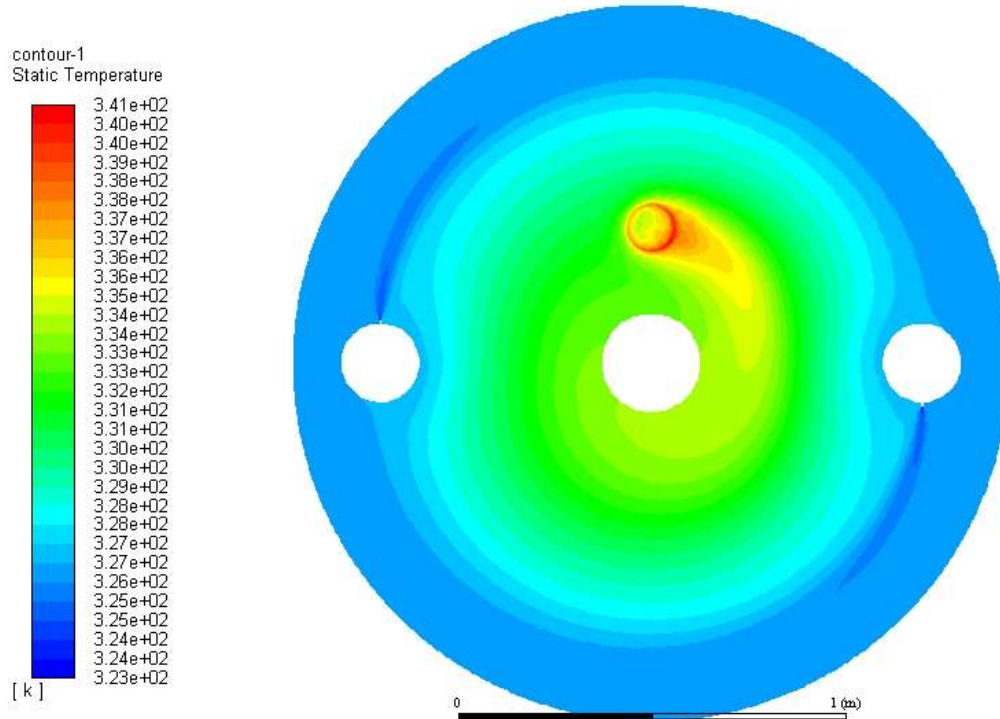
Flow Velocity



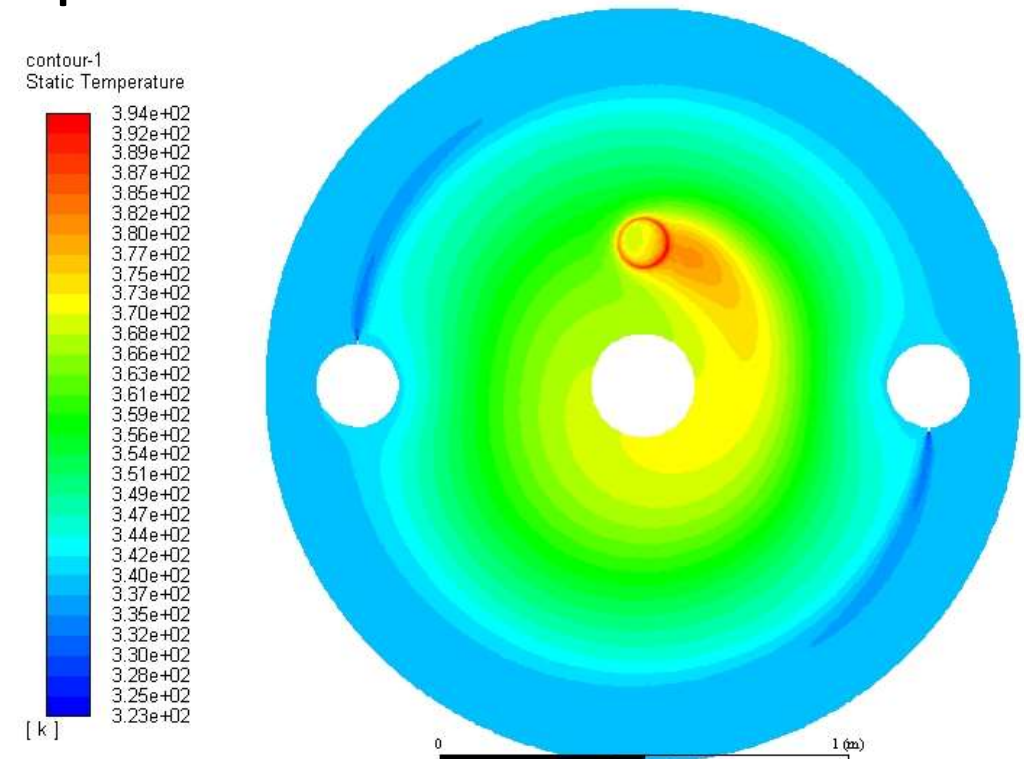
- CFD calculation (ANSYS-FLUENT)
- 2D analysis where peak longitudinal power is observed.  
Z=230cm for 250GeV nominal, Z=280cm for 1TeV status.
- Beam heat is Imported from FLUKA data to each cells.

# Max Temperature

## Temperature Distribution when Beam pulse complete



**250GeV nominal Status**  
(125GeV, 1312bunch/pulse, 5pulse/sec)



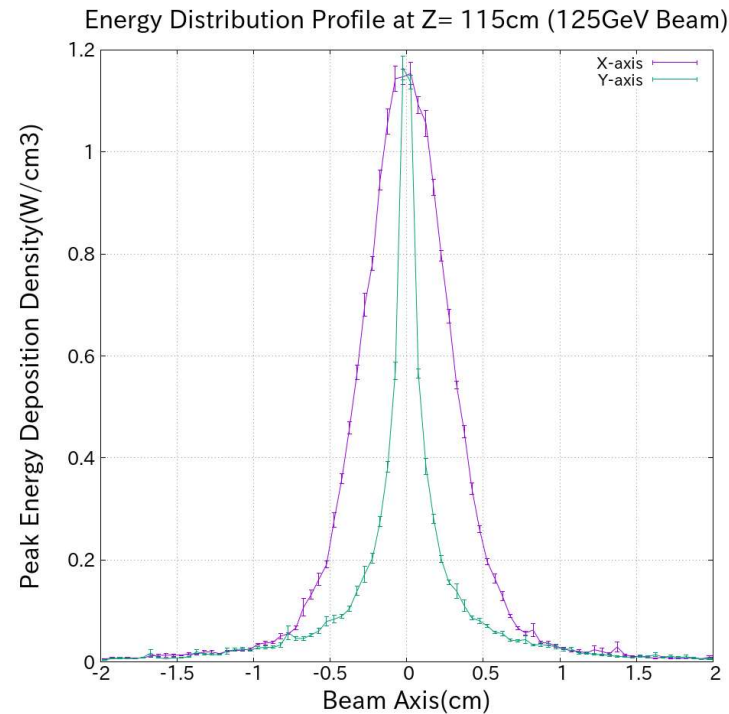
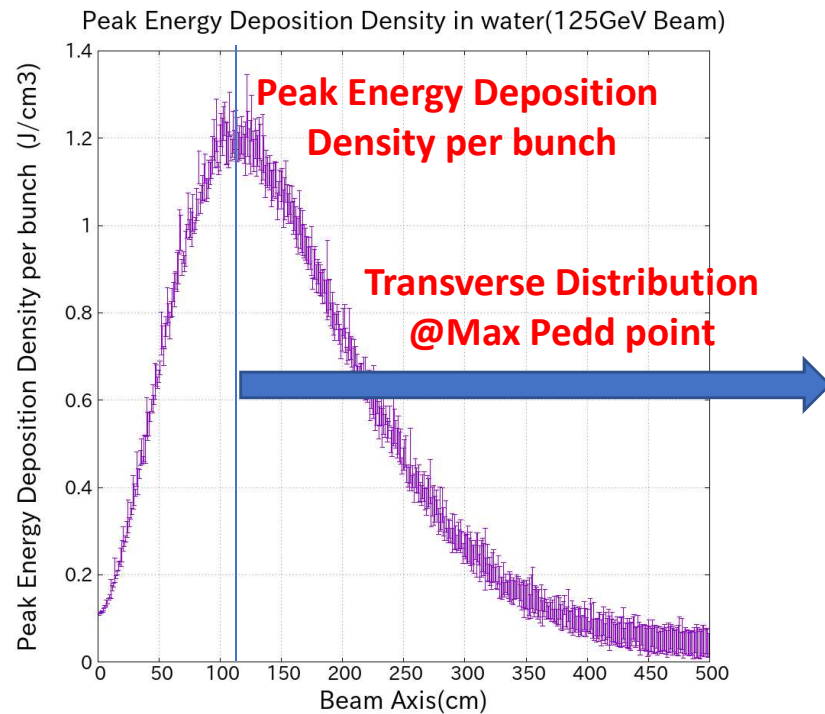
**1TeV Status**  
(500GeV, 2450bunch/pulse, 4pulse/sec)

**【Max Temperature】 250GeV-nominal : 68°C , 1TeV : 121°C**

# Pressure Wave in Water

# 1bunch energy deposition in water

Pressure rise is occurred by thermal expansion and propagate as pressure wave.  
 In water of main beam dump, pressure wave is generated by each bunch.



- Max PEDD : 1.2J/cm<sup>3</sup> @Z=115cm
- Heat Distribution @Z=115cm :  $\sigma_x=2.55\text{mm}$ ,  $\sigma_y=0.53\text{mm}$



# Pressure wave simulation

## ◆ Pressure Wave Evaluation

- Mie Gruneisen Shock Equation  $P = P_H + \Gamma\rho(e - e_H) \Rightarrow \delta P = \Gamma\rho\delta e$

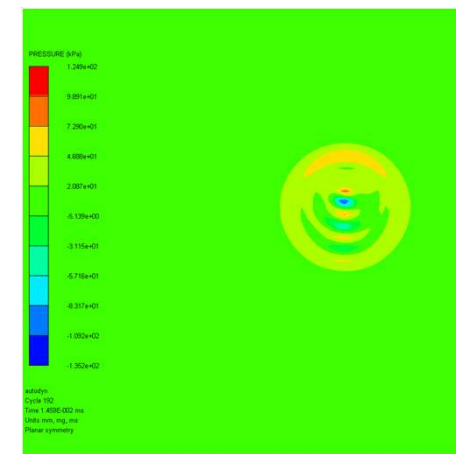
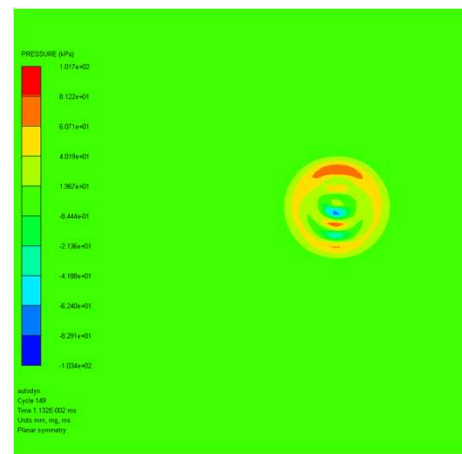
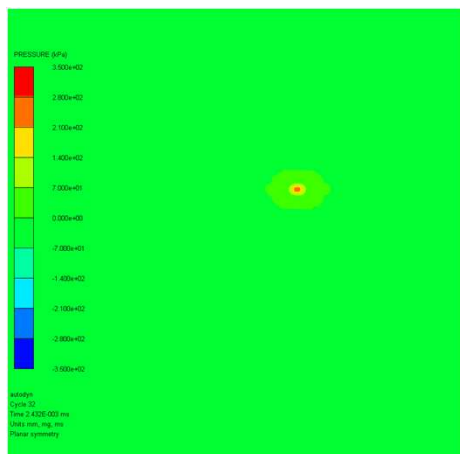
$\Gamma$ :Gruneisen Gamma,  $\rho$  : density,  $e$  : energy deposition density

$\Gamma=0.32$  for 60°C water

$\Rightarrow$  1bunch pressure rise  $dP=0.32 \times 1.2\text{J}/\text{cm}^3 = 3.84\text{bar}$

## ◆ Pressure Wave Simulation

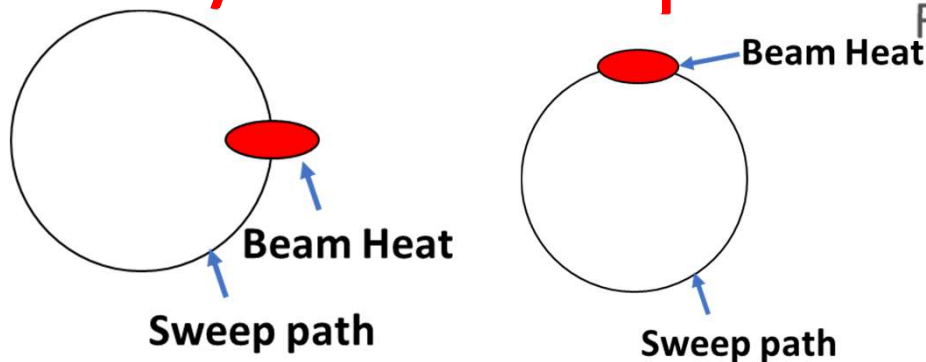
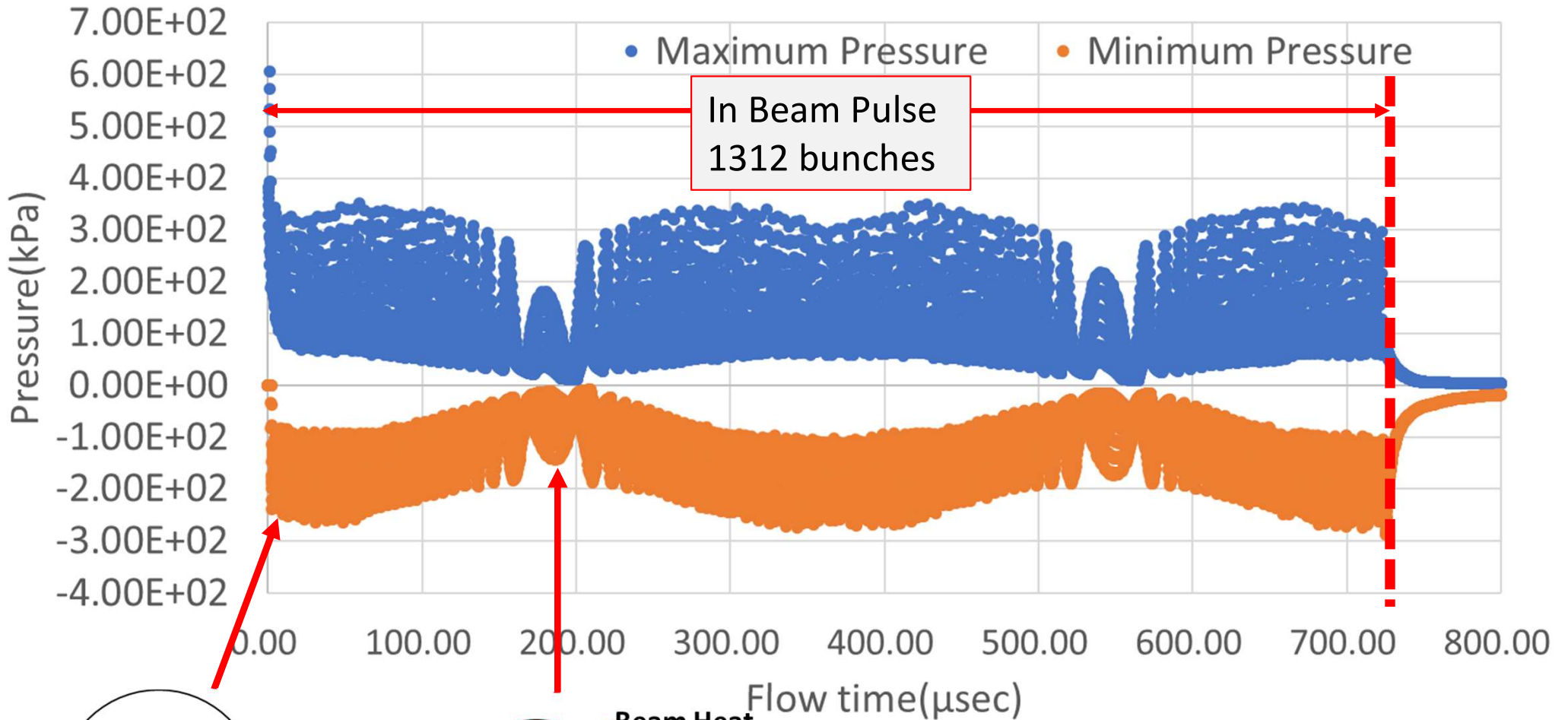
- Thermal shock can be evaluated by Hydrocode(This time, I used Autodyn).
- 2D simulation @Peak Energy Deposition density observed(Z=115cm) to evaluate the negative pressure in water(Cavitation)





# Max and Min Pressure Intensity

Maximum and Minimum Pressure in Water

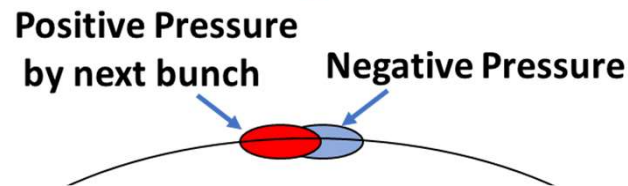
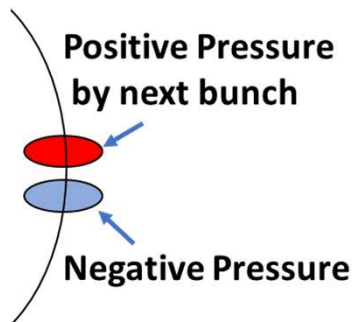
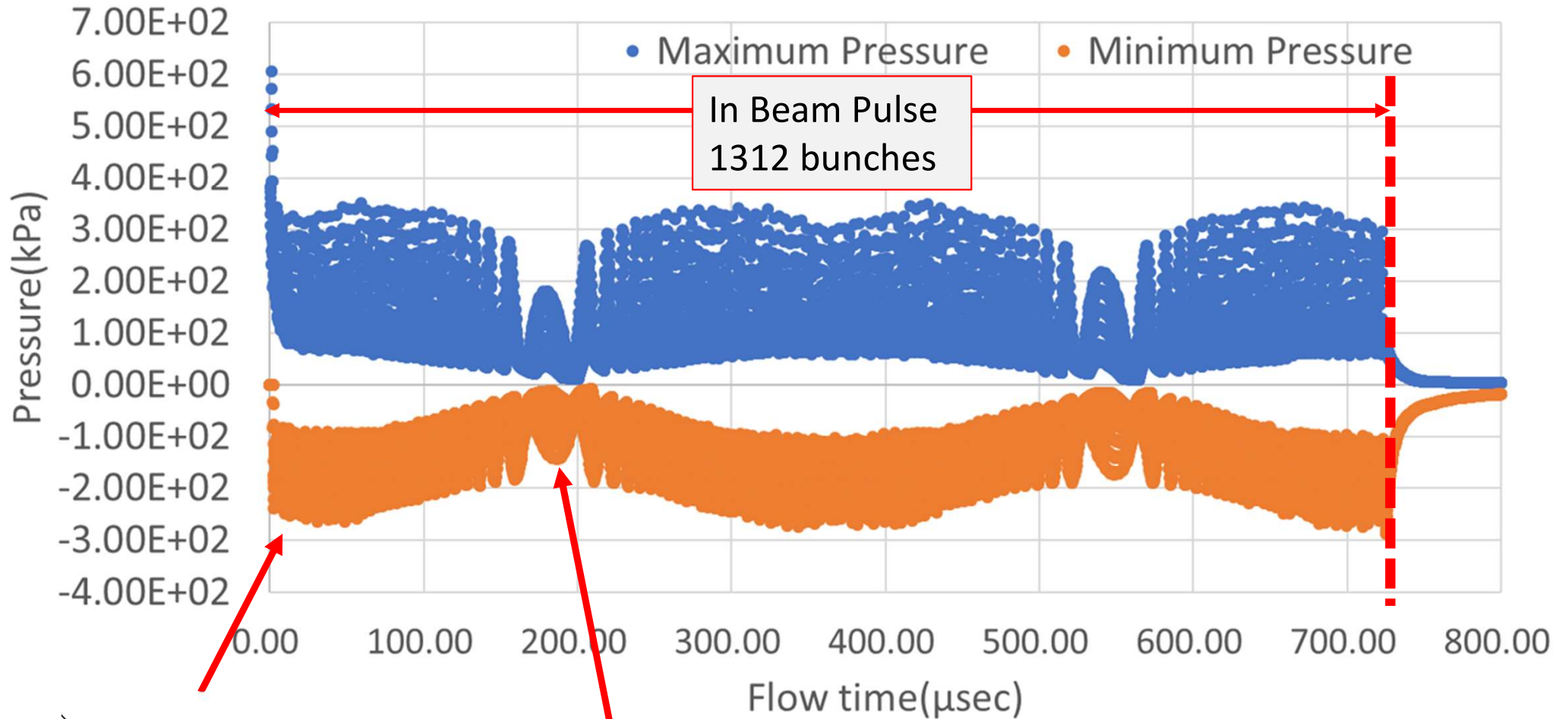


- Bunch space is 556nsec  
 $\Rightarrow$  pressure wave will advance 0.92mm.  
 (wave velocity=1650m/sec)
- Heat distribution is  $\sigma_x=2.55\text{mm}$ ,  $\sigma_y=0.53\text{mm}$ .



# Max and Min Pressure Intensity

Maximum and Minimum Pressure in Water

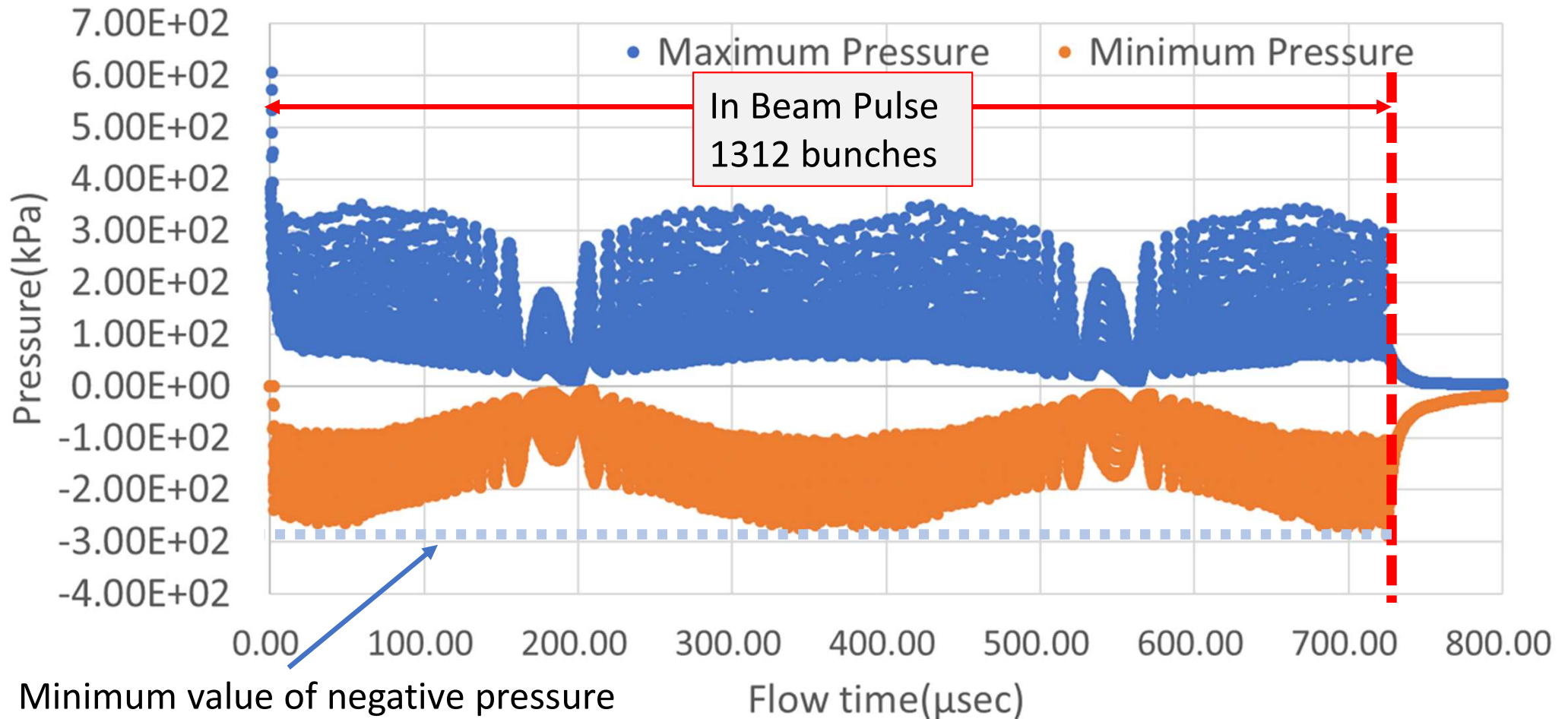


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⇒ pressure wave will advance 0.92mm.  
(wave velocity=1650m/sec)
- Heat distribution is  $\sigma_x=2.55\text{mm}$ ,  $\sigma_y=0.53\text{mm}$ .



# Max and Min Pressure Intensity

Maximum and Minimum Pressure in Water



Highest Pressure : 6.2 bar , Lowest Pressure : -2.8bar



# Beam Window

(Detail : LCWS2017 “Simulation Study of ILC Main Beam Dump Window”)



# Heat Load of Beam Window

Nominal

	250GeV nominal	500GeV TDR baseline	500GeV Lum. Upgrade	1TeV Energy upgrade	1TeV TDR design
Beam Energy	125GeV	250GeV	250GeV	500GeV	500GeV
Electrons per Bunch	$2 \times 10^{10}$ (3.2nC)	$2 \times 10^{10}$ (3.2nC)	$2 \times 10^{10}$ (3.2nC)	$1.74 \times 10^{10}$ (2.79nC)	$2 \times 10^{10}$ (3.2nC)
Bunches per Pulse	1312	1312	2625	2450	2820
Pulse Energy	0.52MJ	1.05 MJ	2.10 MJ	3.41 MJ	4.5MJ
Rep rate	5Hz	5Hz	5Hz	4Hz	4Hz
Average Power	2.6 MW	5.25 MW	10.5 MW	13.7 MW	18MW
Max Energy deposition density per pulse	10J/cm <sup>3</sup> Δ3.9°C	10J/cm <sup>3</sup> Δ3.9°C	20J/cm <sup>3</sup> Δ7.7°C	16.3J/cm <sup>3</sup> Δ6.3°C	22.5J/cm <sup>3</sup> Δ8.3°C
Total deposition power	14.2W	14.2W	28.5W	18.5W	24.5W
Max DPA value Per pulse	$1.1 \times 10^{-9}$	$1.1 \times 10^{-9}$	$2.1 \times 10^{-9}$	$1.7 \times 10^{-9}$	$2.3 \times 10^{-9}$
DPA after 5000hour	0.1	0.1	0.19	0.12	0.17

The most severe condition

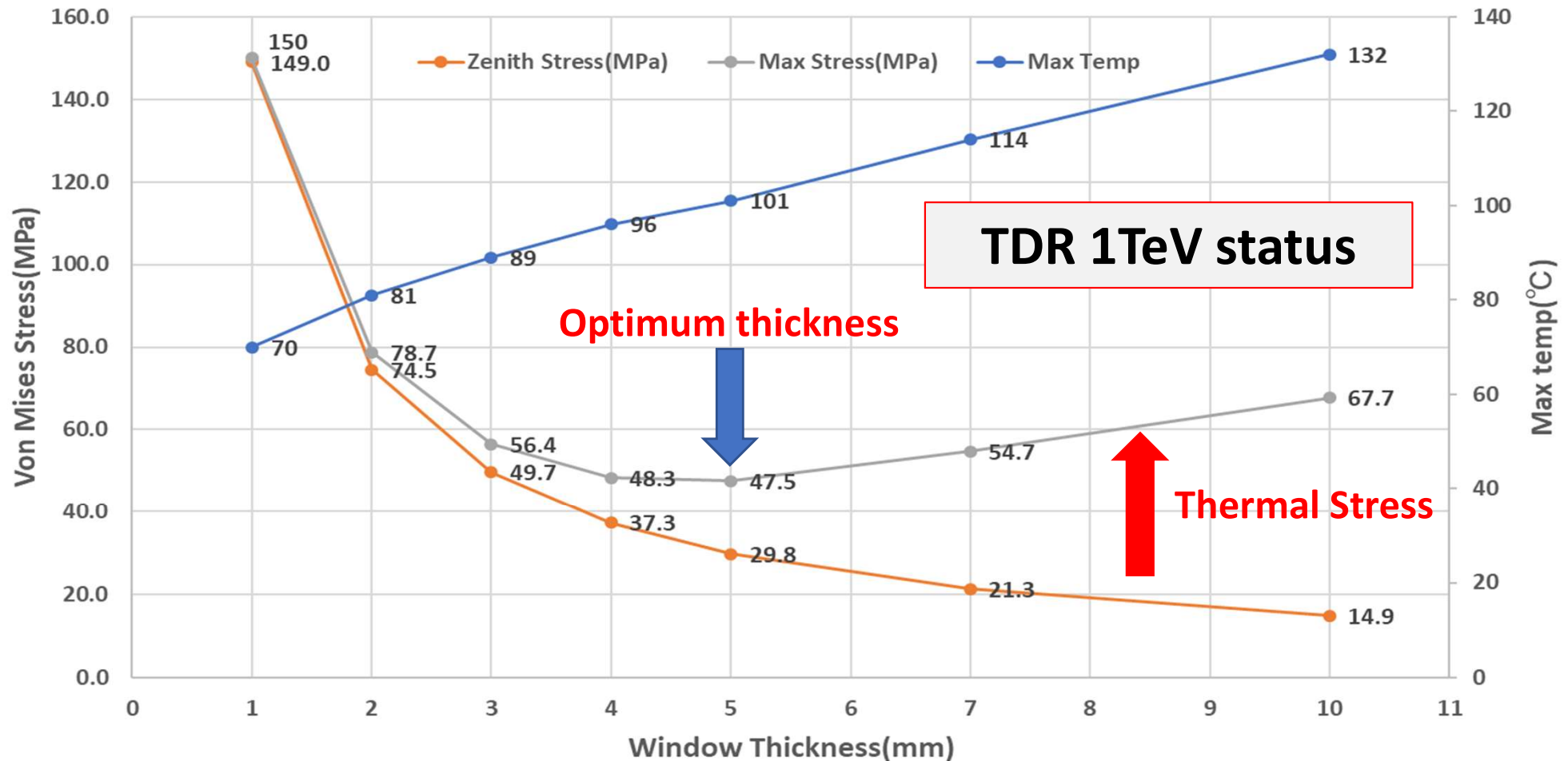
- Compare to TDR 1TeV status, Heat load of 250GeV nominal is **42%↓** decreased.



# Stress vs window thickness

[Simulation Results : **Von Mises Stress**] Heat transfer rate : **500W/m<sup>2</sup>K**

Thickness dependence of window temp and stress

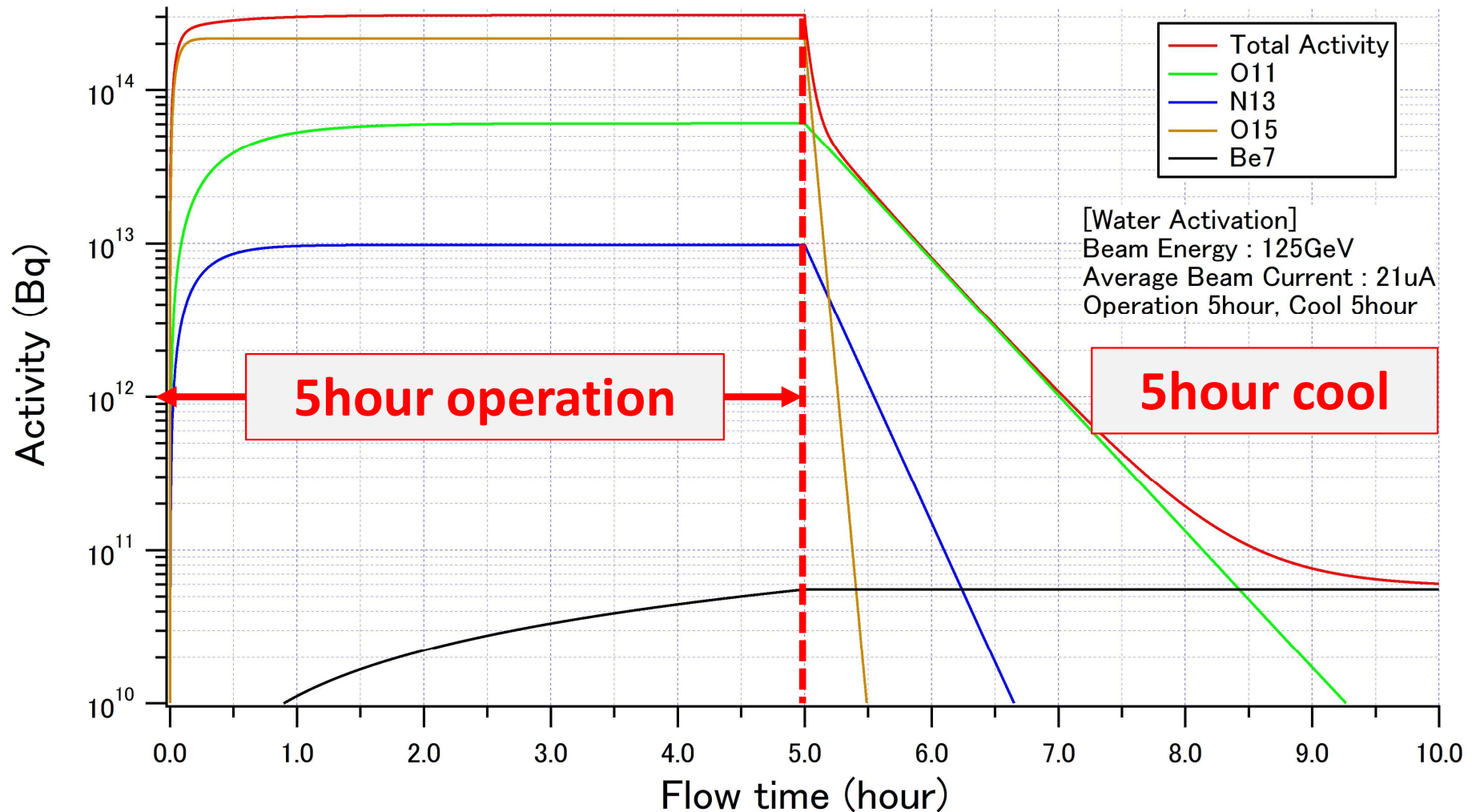


- Window material(Ti6Al4V) can withstand the stress of around **450MPa**. Even if 1TeV status, 5mm thick window has safety factor of ~10.

# Water Activation



# Radioactivity - short time scale

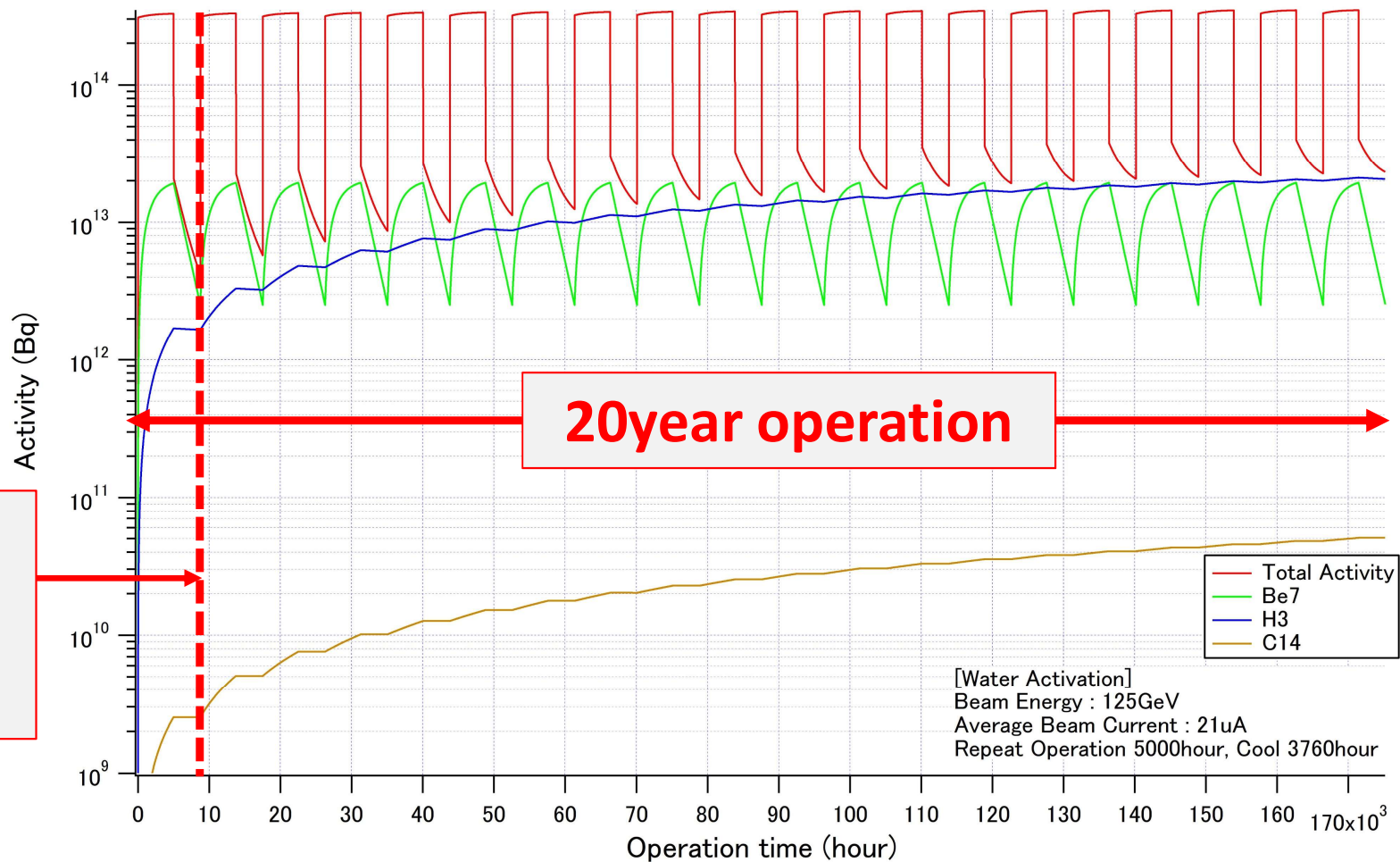


## ◆ Short time scale(hours)

- Major activities are, O11(half life:20min), N13(10min), O15(2min).
- These activities are rapidly decreased. After 4hour cool, major activity will be Be7.



# Radioactivity - long time scale



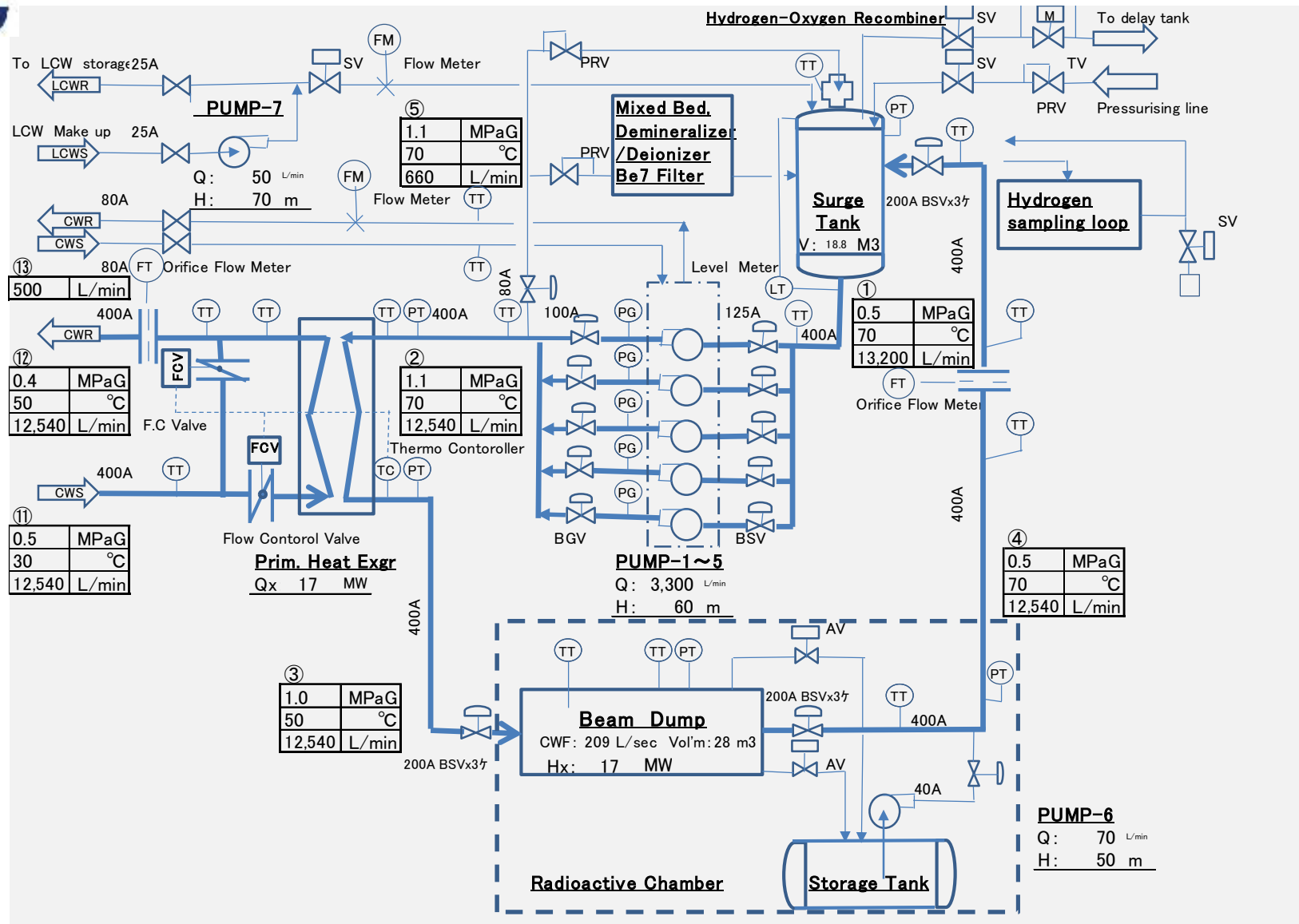
## ◆ Long time scale(years)

- Major activities are, Be7(half life:53day), H3(12.3y), C14(5.7e3y).
- Saturation Activities are, Be7=2e13(Bq), H3=5.4e13, C14=3.7e13
- Be7 is major component of gamma emitter(477keV) and will be saturated in 1year.

# **Required System with 250GeV status**



# Cooling Water System

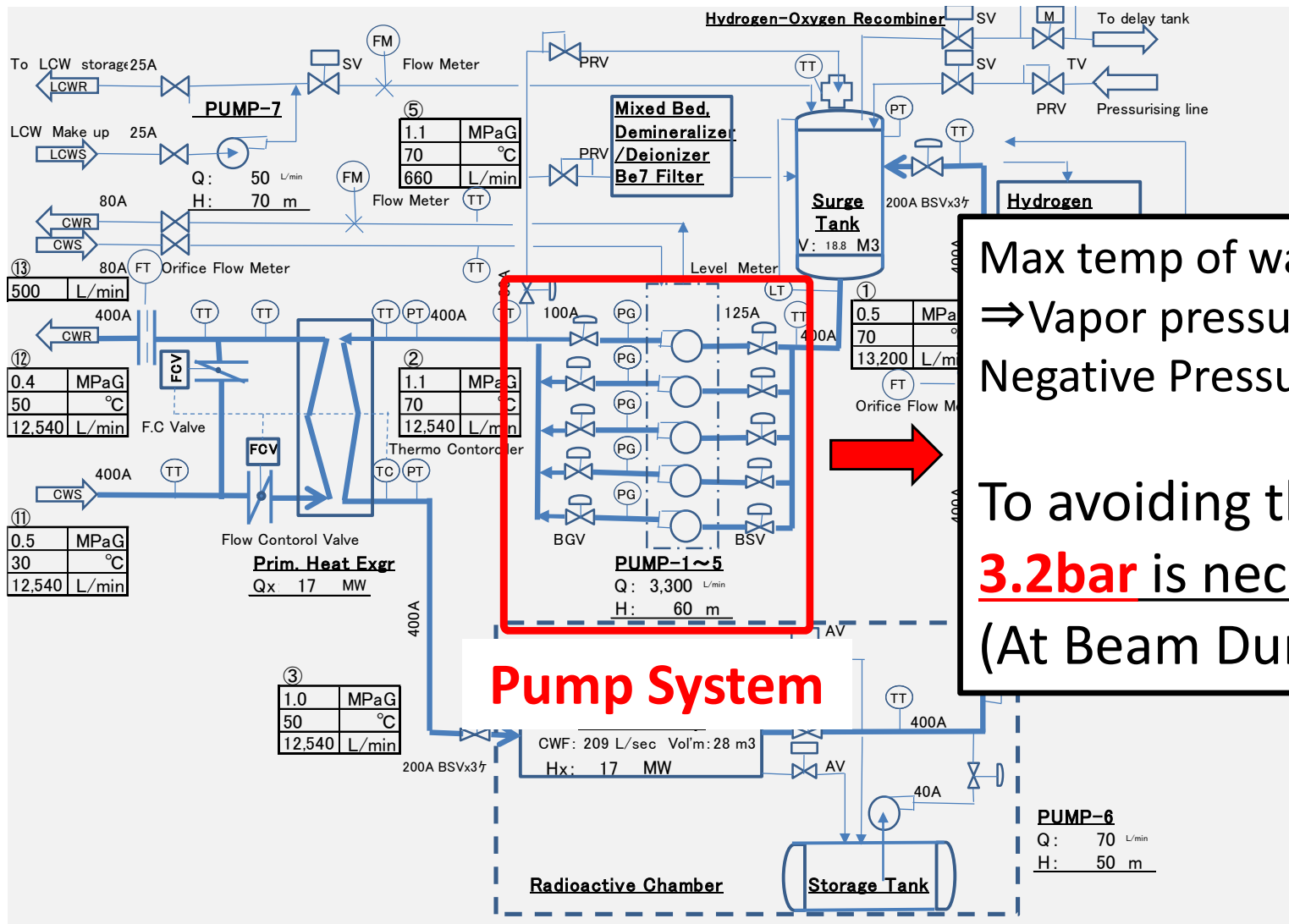


◆ I started the discussion with qualified industry to make detailed design.





# Required Pressure

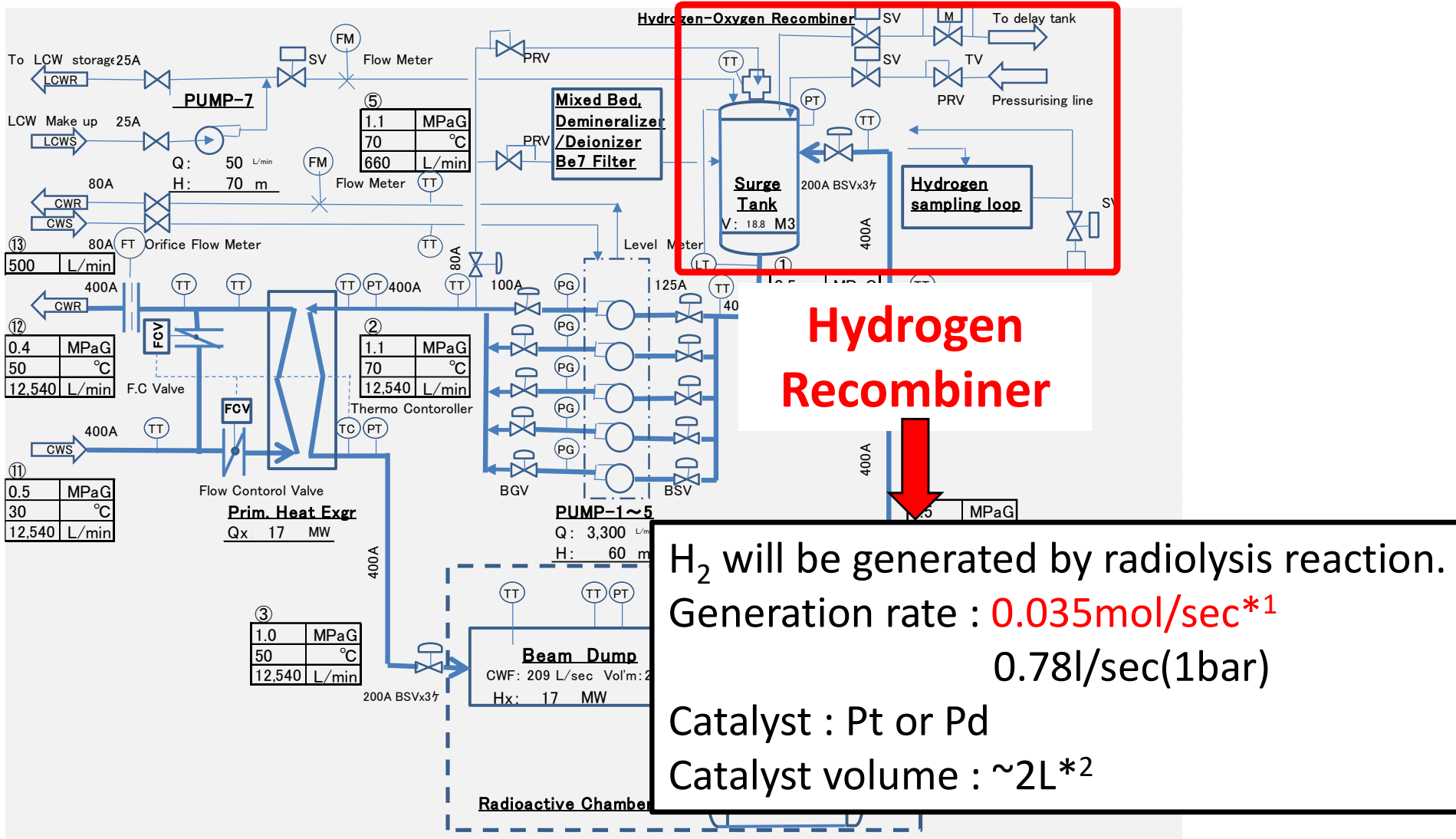


Max temp of water :  $\sim 70^{\circ}\text{C}$   
 $\Rightarrow$  Vapor pressure of  $70^{\circ}\text{C} = 0.32\text{bar}$   
Negative Pressure :  $\sim -2.8\text{bar}$

To avoiding the partial boiling,  
**3.2bar** is necessary at least.  
(At Beam Dump)



# Hydrogen Recombiner

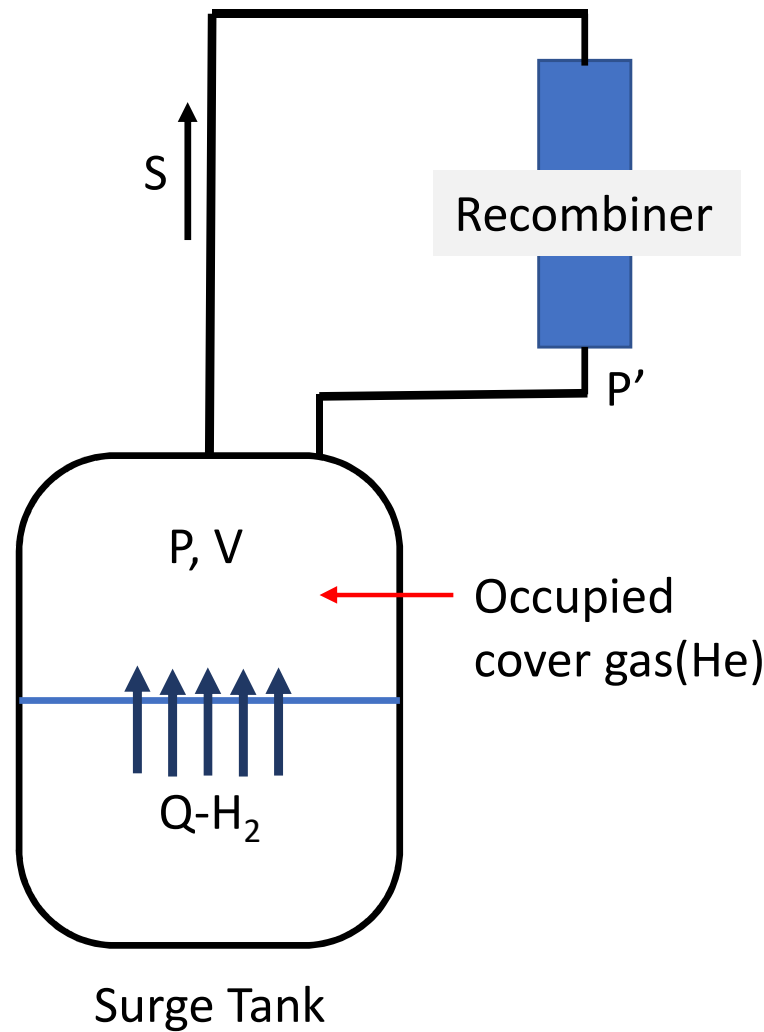


\*1 : scaled from SLAC experience : D.R. Walz and E.J. Seppi, Radiolysis and Hydrogen Evolution in the A-Beam Dump Radioactive Water System, SLAC-TN-67-29, October, 1967.

\*2 : scaled from Base design of ILC Main Beam Dump : P. Satyamurthy, et.al., Design of an 18 MW vortex flow water beam dump for 500 GeV electrons/positrons of an international linear collider, NIM A 679 (2012)



# Hydrogen Recombiner



## ◆ H<sub>2</sub> pressure

$$-V \frac{dP}{dt} = S(P - P') - Q$$

V: gas volume, S: volume flow, Q : gas generation velocity  
 P : pressure before recombiner, P' : pressure after recombiner

$$\Rightarrow \text{steady state } Q=S(P-P')$$

$$Q(\text{H}_2)=0.035*8.314*(50+273.15)=94\text{Pa}\cdot\text{m}^3/\text{sec}$$

When recombine efficiency is 80%,  $P-P'=0.8P$

$$\text{Hydrogen Pressure(steady) } P_{\text{H}_2} = Q/(0.8 \times S)$$

$$\text{If } S = 50\text{L/sec } (0.05\text{m}^3/\text{sec}), \quad P_{\text{H}_2} = 2350\text{Pa}$$

## ◆ Volume fraction of H<sub>2</sub>

If cover gas pressure is 3bar,

Total Pressure : 302,350Pa

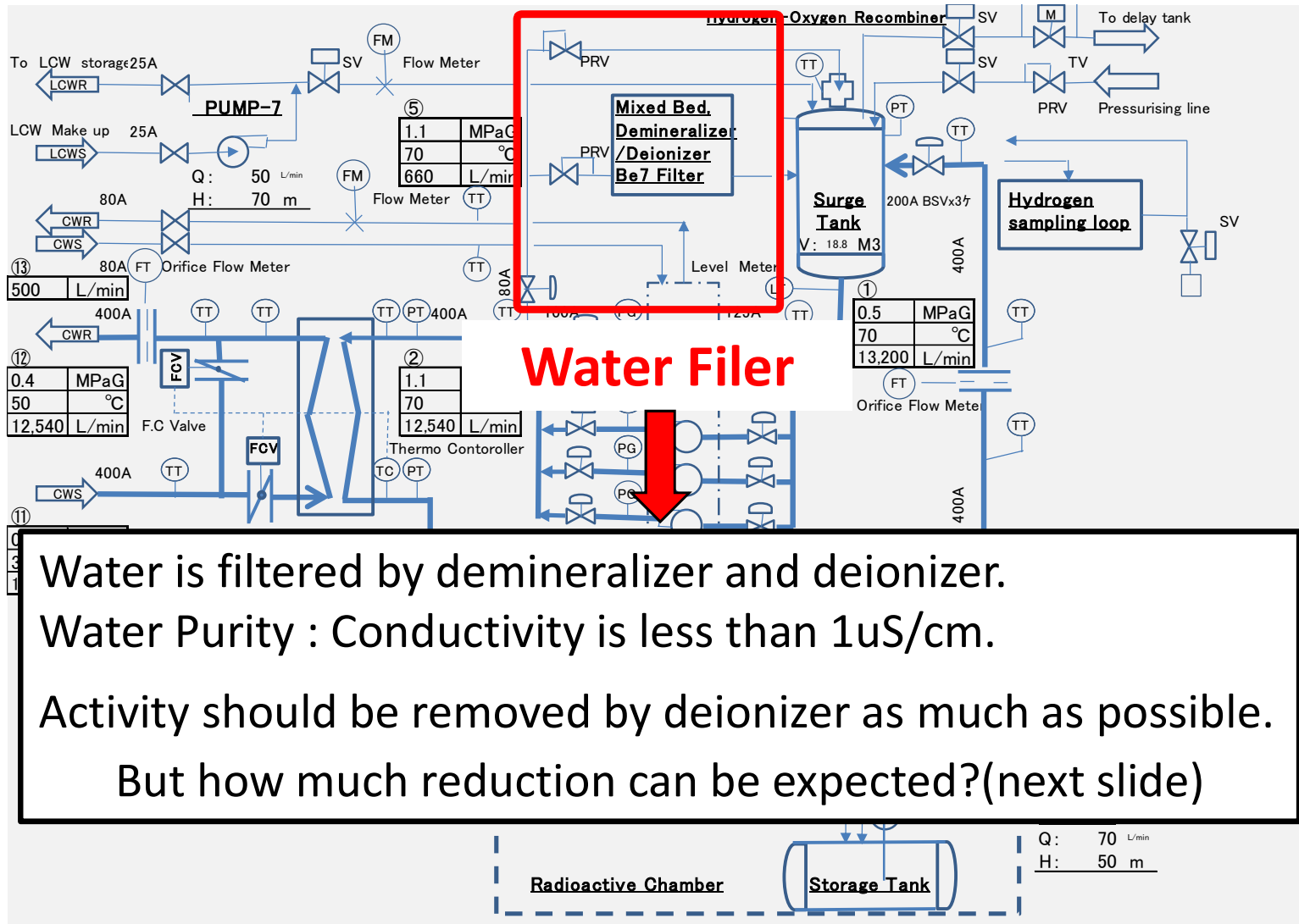
Volume fraction of H<sub>2</sub> : 2350/302350 \* 100

**0.78 vol%**

**Lower Explosion limit of H<sub>2</sub> : 4 vol%**

Required System : **Recombine Efficiency ~80%, Volume Flow ~50L/sec**

# Water Filter





# Water Activity Filtering

## ◆ Base Status with 250GeV nominal status

1year Production(5000h) : Be7=2e13(Bq), H3=2e12

Saturate Activity : Be7=2e13(Bq), H3=5.4e13

Total water volume : ~50m<sup>3</sup>

Density in water without filter : Be7 = 4e5(Bq/cm<sup>3</sup>), H3 = 1.1e6

## ◆ Deionizer Performance

From J-PARC experience\*, deionizer can remove 99.995% of Be7 in water.

(Their deionizer system achieved to reduce Be7 from ~130GBq to ~6.5MBa)

If our removal efficiency is 99.99%,,, Density in water with filter : Be7 = ~ 40(Bq/cm<sup>3</sup>)

## ◆ Deionizer Life Time and Shielding.

From J-PARC experience, deionizer can work several years.

(Especially over 5year work at Neutrino Target & Horn system\*)

Deionizer retain 2e13Bq of Be7. Be7 emit 477keV gamma ray.

⇒ Expected dose rate without shield is ~100mSv/h at 1m away(only Be7).

Deionizer module needs shielding. Tenth value layer of Fe(500keV) = ~3cm

⇒ 12cm thick of Fe can reduce dose rate from 100mSv/h to 10uSv/hour at 1m away.

Weight of deionizer (include the shield) would be several tons.

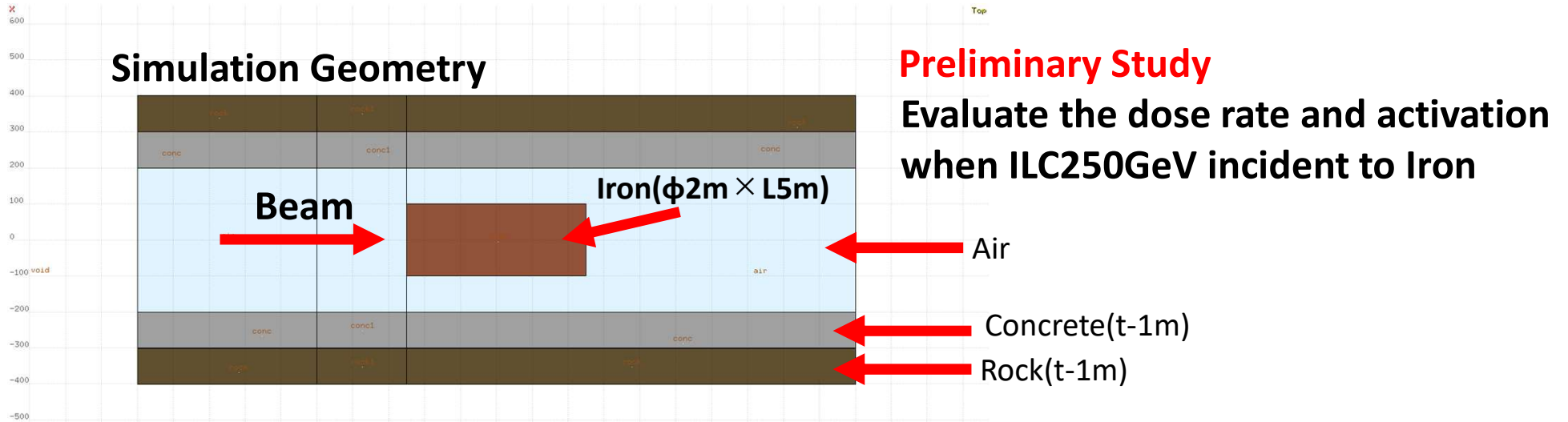
\*Y.Oyama, T2K water drainage / exhaust air, Neutrino Beam Instruments 2014.



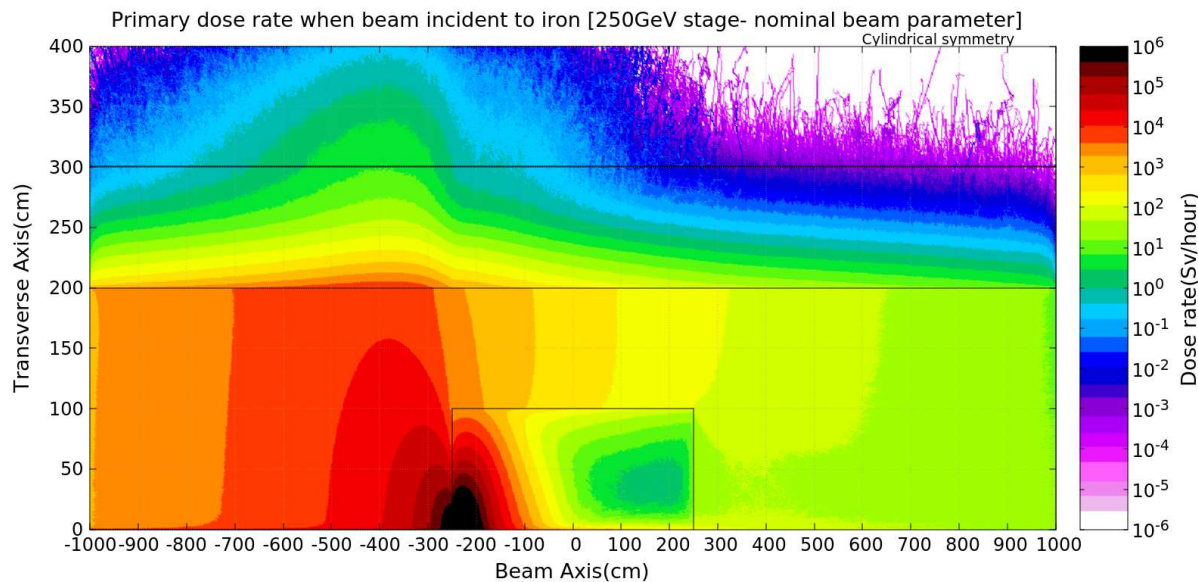
# How much shield thickness is required?

## ◆ How much we should shield dose rate in operation?

Relation between Dose rate in operation and activation.



## Total dose in operation

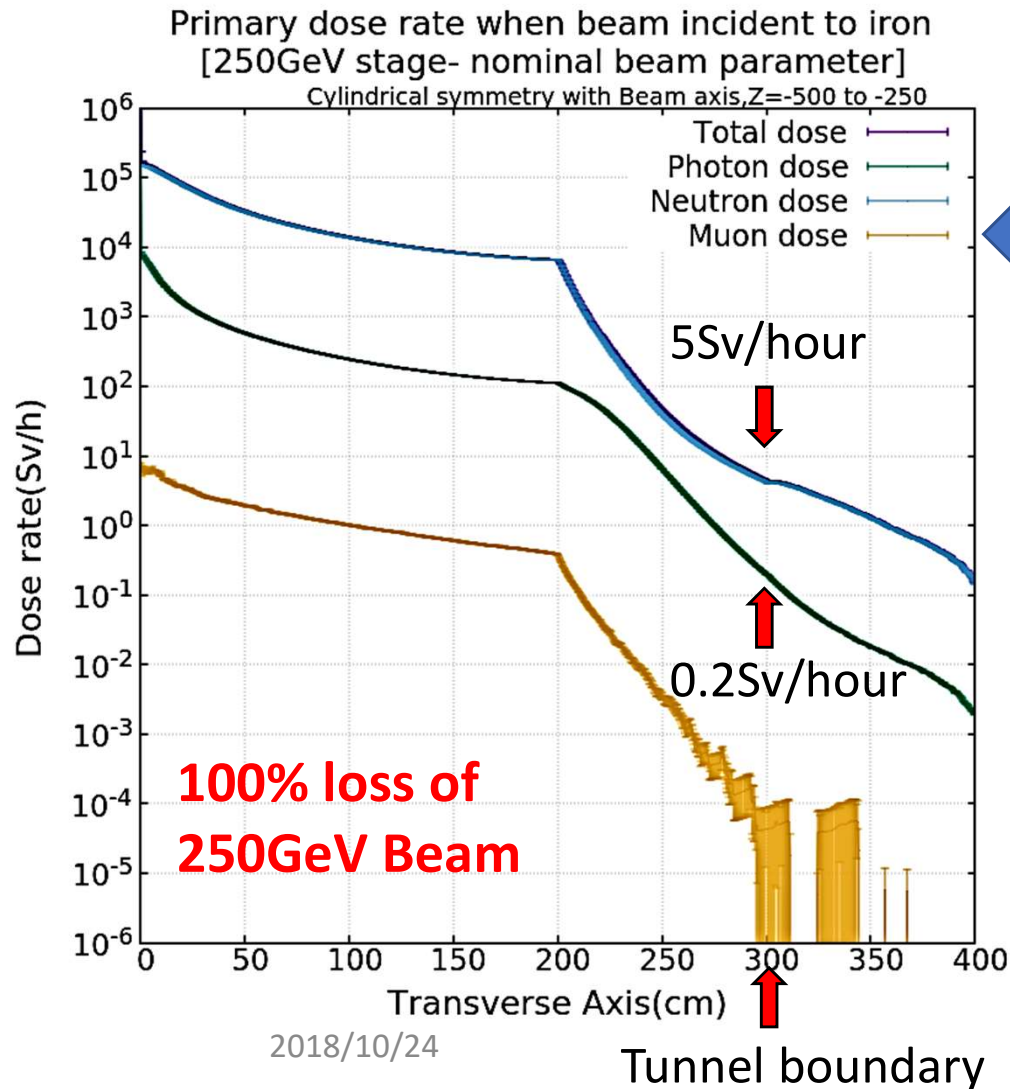




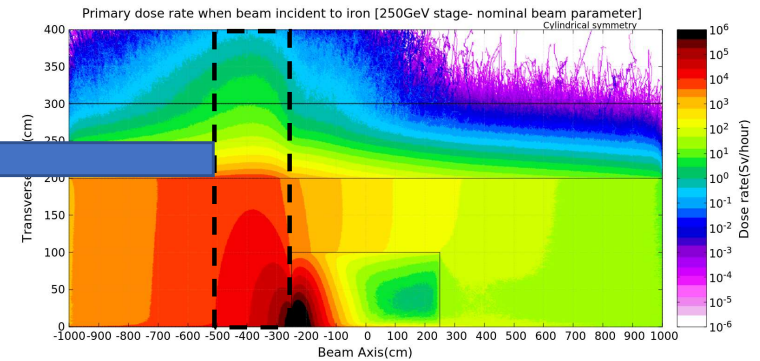
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Relation between Dose rate in operation and activation.



## Preliminary Study



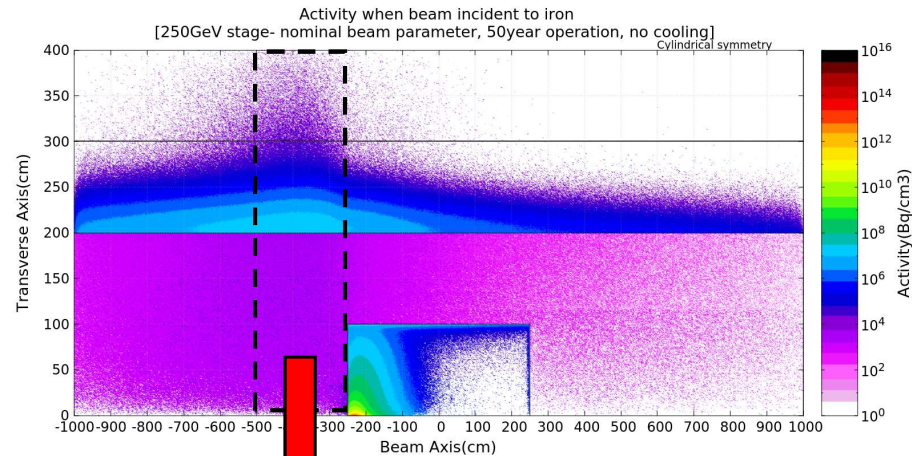
At tunnel boundary

Neutron is dominant : 96%



# Total Activity in outside tunnel

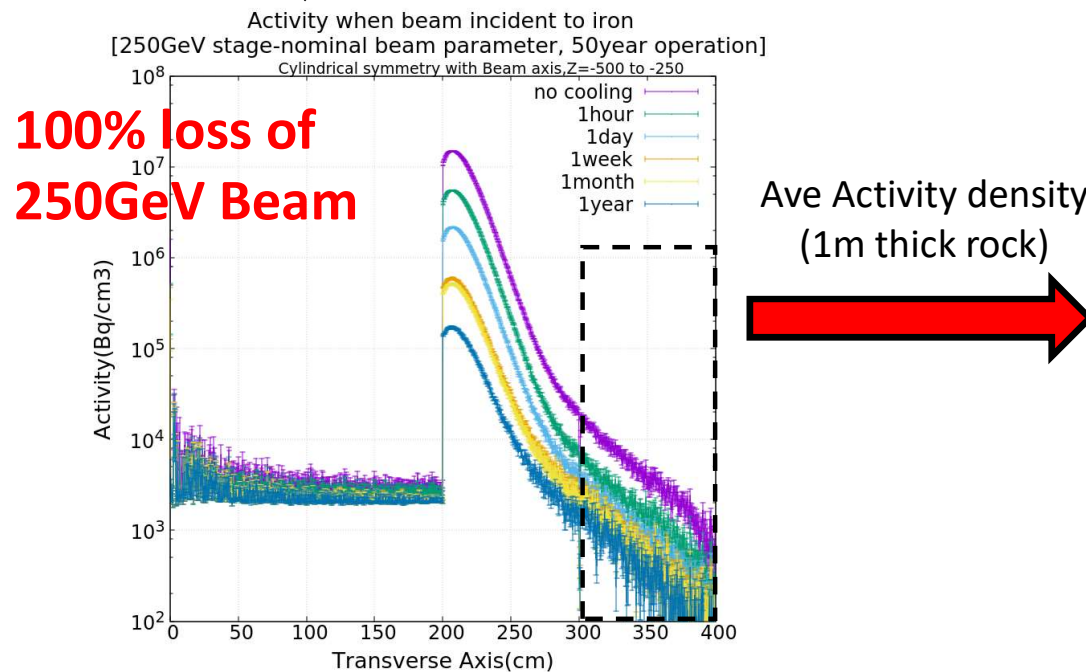
## ◆ Relation between Dose rate in operation and Activation.



Preliminary Study

Total activity - 50year operation

Conversion to 5mSv/hour at boundary (0.1% loss)



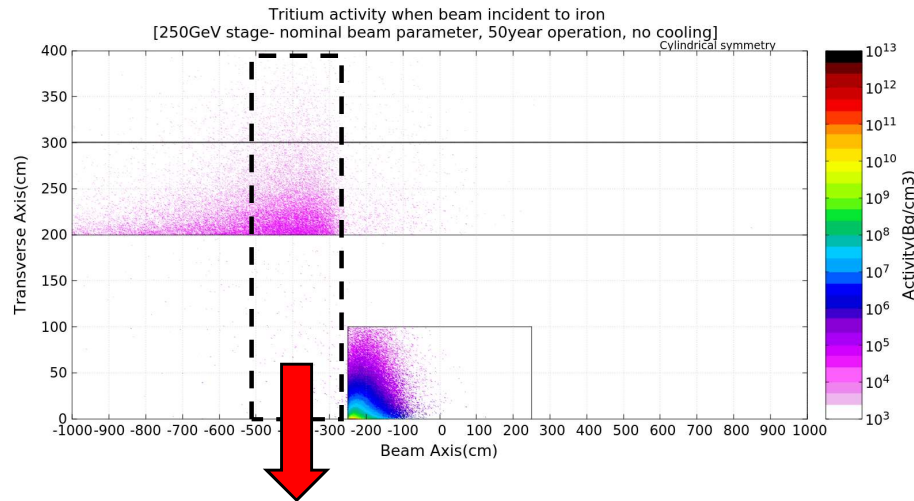
Cooling	Average Activity(Bq/g) in Rock(t=1m)
None	2.23
1hour	0.82
1day	0.46
1week	0.32
1month	0.29
1year	0.20



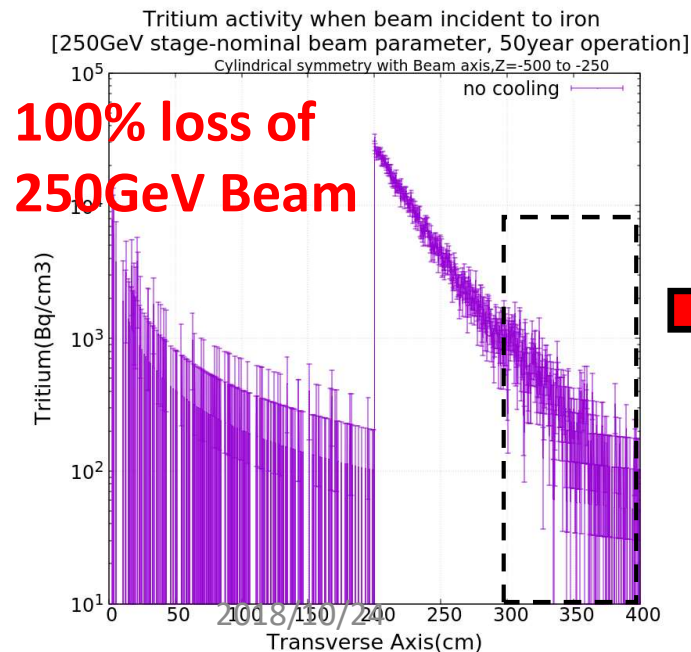


# H3 Activity in outside tunnel

## ◆ Relation between Dose rate in operation and Activation.



**Preliminary Study**  
**H3 activity - 50year operation**



**100% loss of  
250GeV Beam**

Ave Activity density  
(1m thick rock)

**Conversion to 5mSv/hour at  
boundary (0.1% loss)**

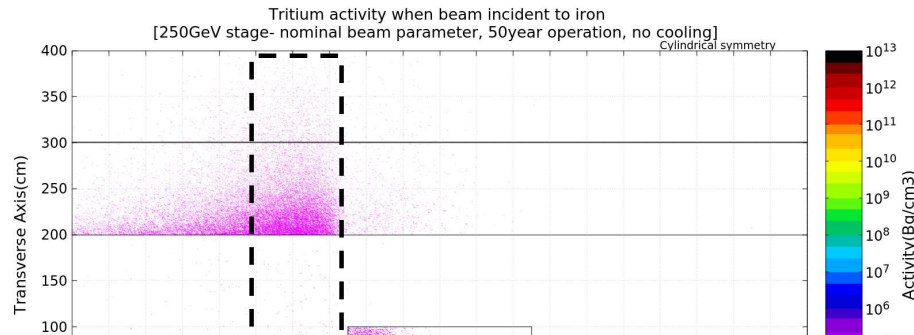
**Average Activity(Bq/g)  
in Rock(t=1m)**

0.14



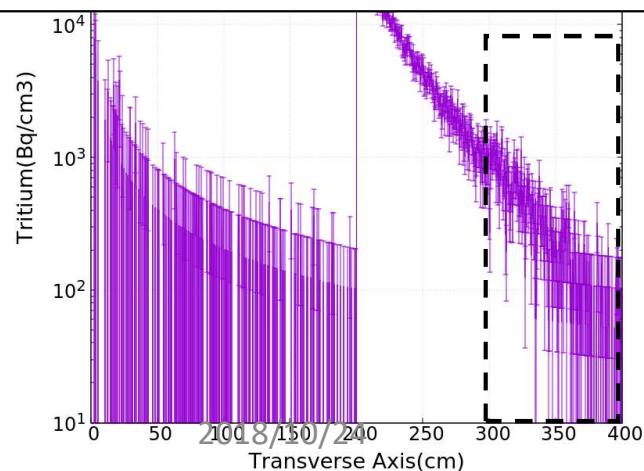
# H3 Activity in outside tunnel

## ◆ Relation between Dose rate in operation and Activation.



Preliminary Study  
H3 activity - 50year operation

If Neutron dose rate at boundary = 5mSv/h is acceptable,  
Main Dump shielding would be **iron 0.5 & concrete 4m**(1TeV OK)  
(Detail : ALCW2018 “CFS consideration on the Main Dump and around”)



Average Activity(Bq/g)  
in Rock(t=1m)

0.14



# Summary

Totally, situation is relaxed,,,

	250GeV nominal	1TeV-TDR
Max Temp in water	~70°C	~145°C
Required Pressure at dump	3.2bar at least	10bar But cavitation will occur
Window Heat Load per window thickness	14W/mm	25W/mm

(Relaxed factors are not only above)

Required systems are estimated and each one is not so special.

In 250GeV nominal stage, main dump can work with enough margin.  
And we can check and learn many practical issues  
for Luminosity and Energy upgrade !!