



Meeting ILD Electronics and Cooling



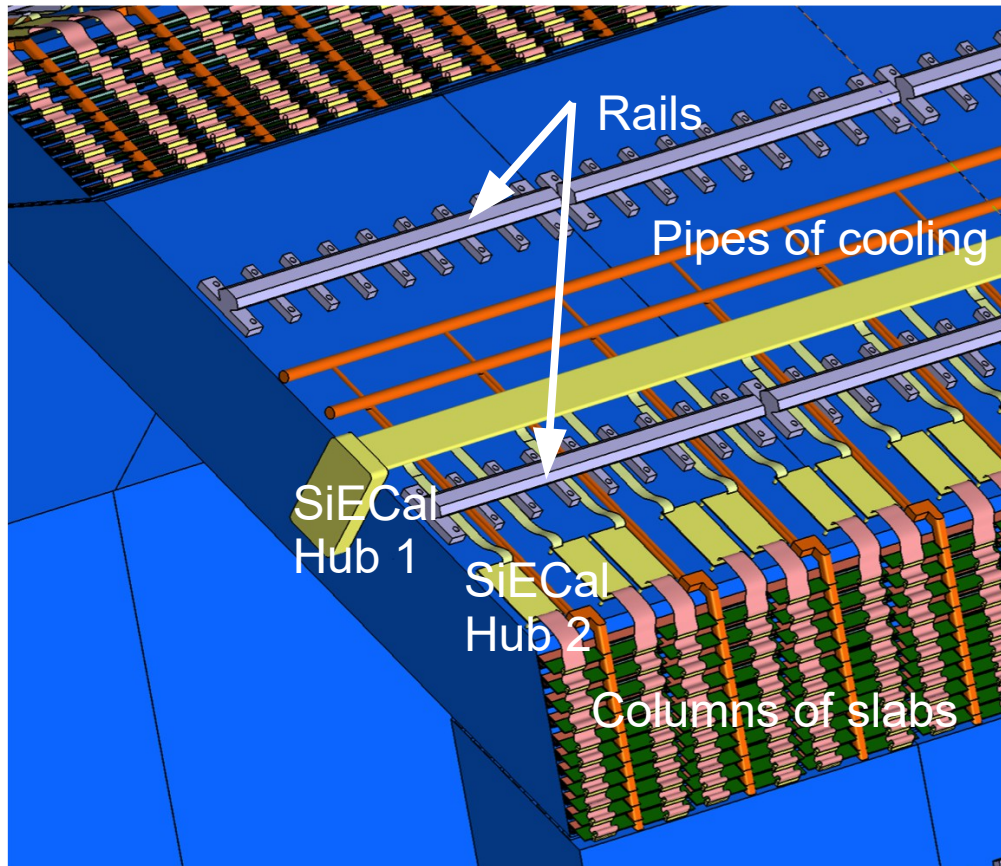
Roman Pöschl,



LAL Orsay Feb. 2018

- Coordination of integration of Ecal services (electronics and cooling) is pending since a while
 - Progress on both sides
 - Hardware development
 - Cooling loop and heat exchangers at LPSC
 - SL-Board at LAL
- > Morning 1: Understand how to bring these devices together
Which constraints and how to remedy them?
- Design
 - Considerations on power and cabling needs for Ecal
- => Morning 2: Occupation of space between Ecal and Hcal by Electronics Hubs and cooling circuitry
- Technical drawing for cooling system of barrel and endcaps
- => Afternoon 2: Does the cooling system comply with current constraints of ILD in general and the Ecal in particular

Remark: Today concentration (mainly) on Ecal barrel



Current “design”

- SiEcal Hub 1
(hub to external supplies and DAQ)

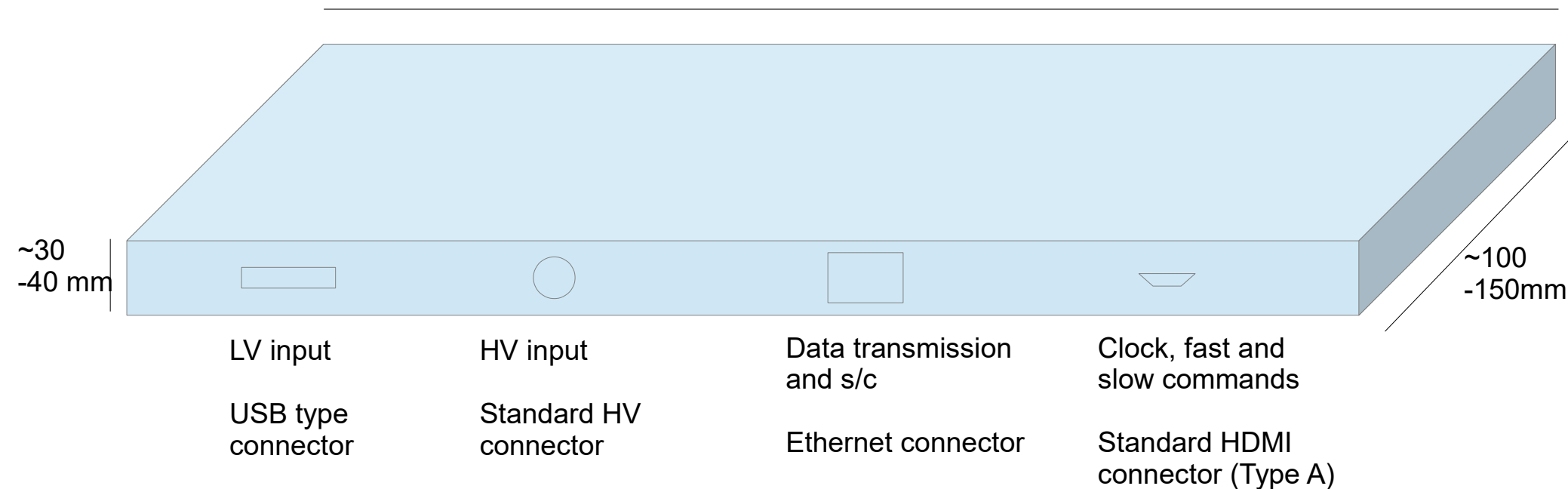
SiEcal internal components

- SiEcal Hub2
(internal hub to be checked whether heat source)

“Old and obsolete drawing by R.P. but hopefully instructive for discussion

Hub1 front side

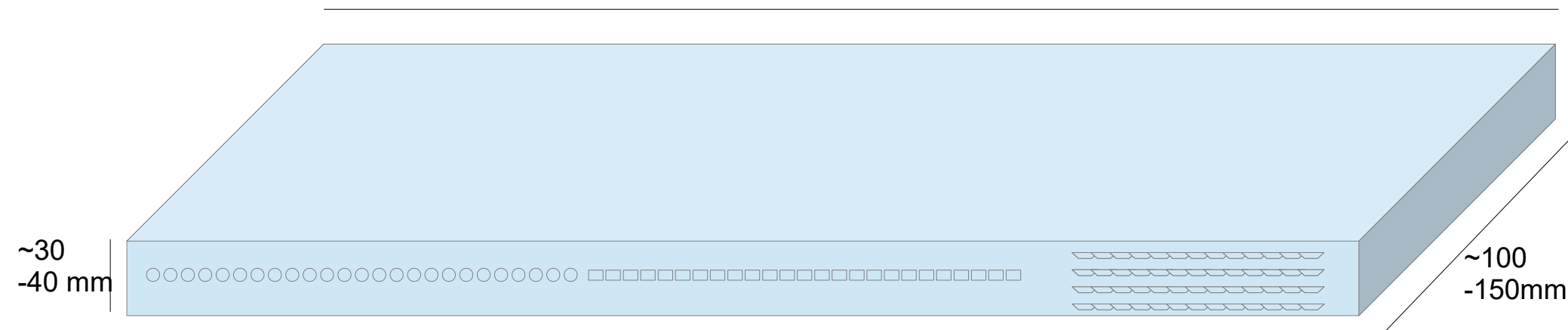
~1000m



“Old and obsolete drawing by R.P. but hopefully still instructive for discussion

Hub1back side

~1000m



HV out

Ethernet

Upper two rows:
 LV, micro USB
 Lower two rows:
 Clock etc,
 micro HDMI (Type C)

Inside Hub1:

- HV/LV distribution (1-many)
- Ethernet hub
- Clock fan out, fast signal distribution

- In this design Hub1 supplies all 25 columns of a stave
=> Huge number of cables

- May be doable if enough space available but ... Fixation of TPC needs to be taken into account

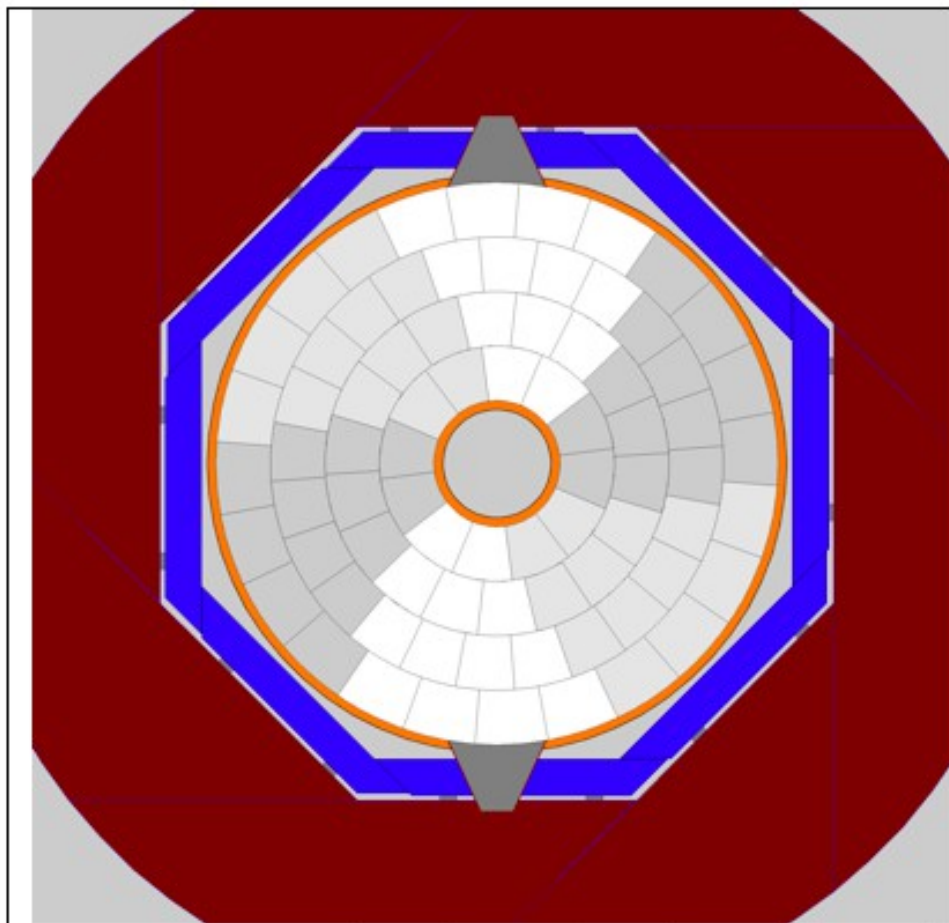


Figure 3. The TPC is shown hanging from the HCal. The ECal barrel is also represented with its rails.

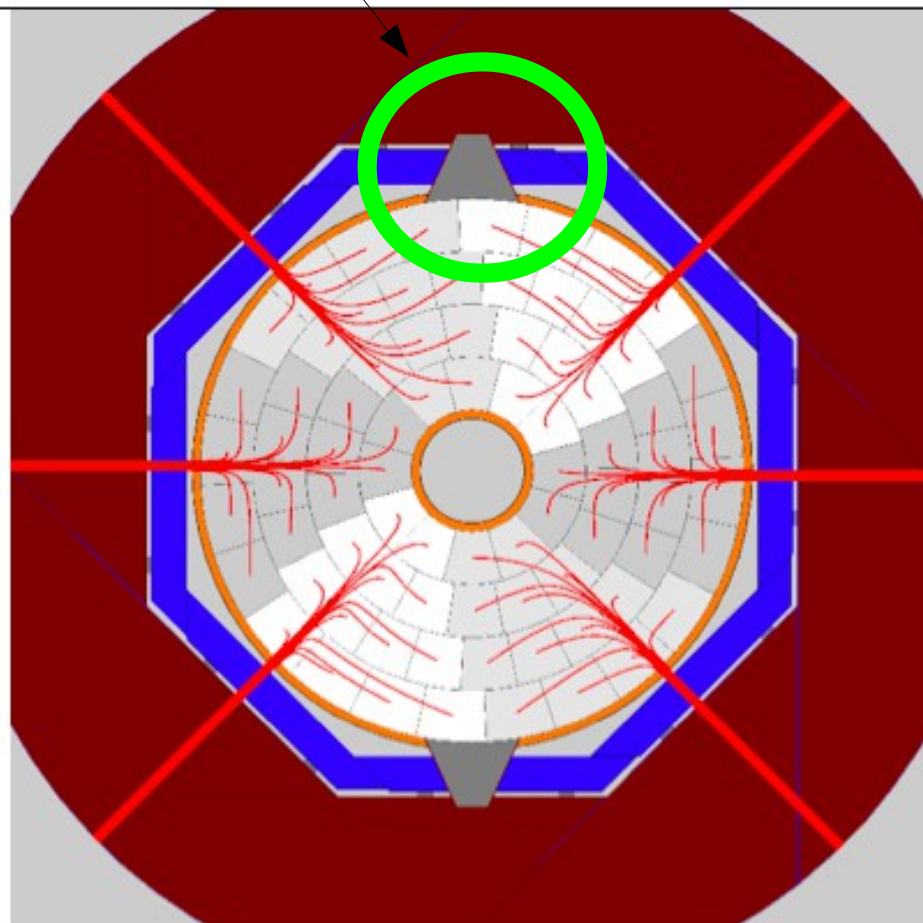


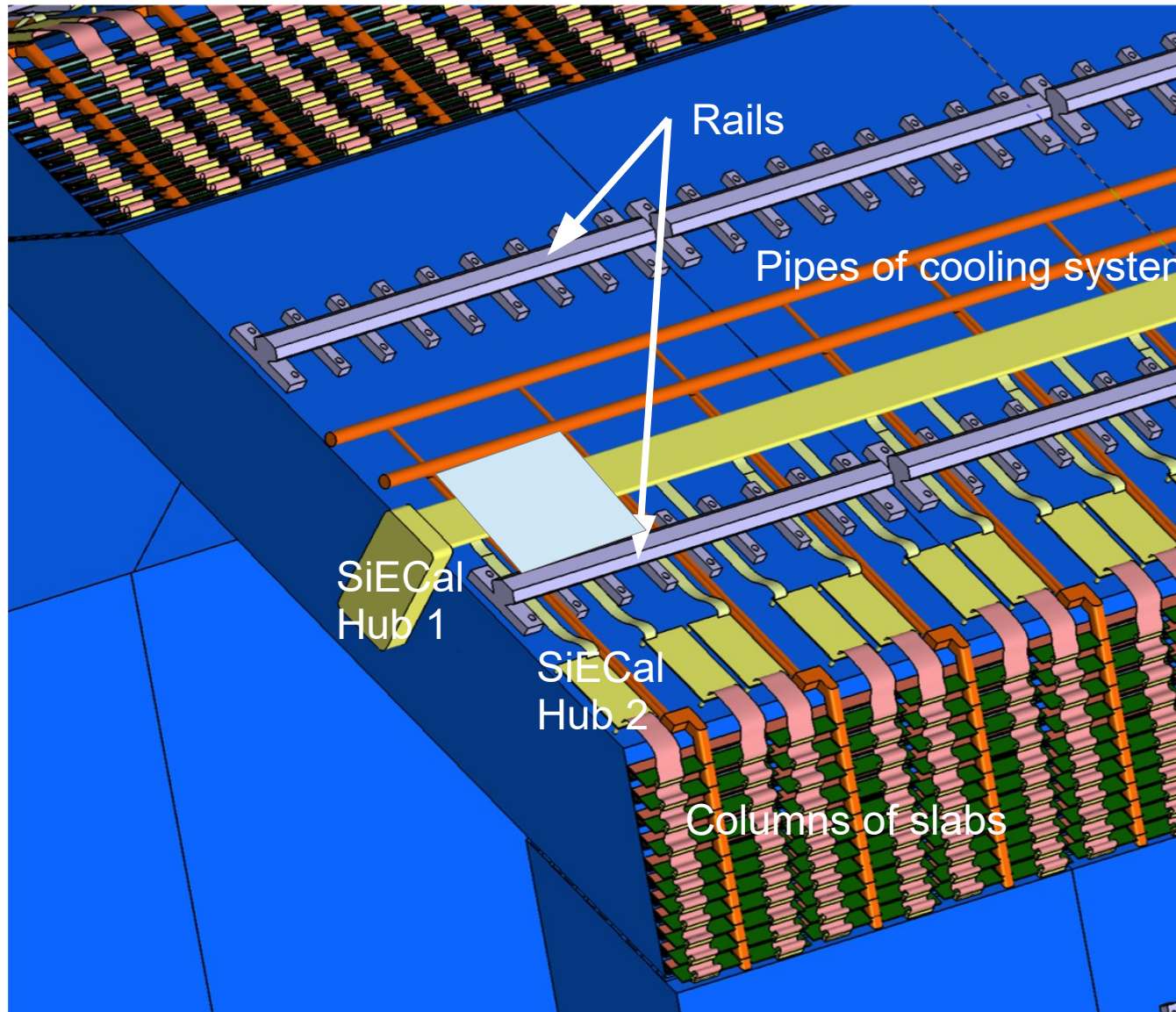
Figure 4. Getting the services out of the TPC. An example.

Summary of constraints:

- 1) TPC Fixation will most likely limit space available for Ecal Hub1
- 2) Huge number of outgoing and incoming cables renders design very difficult

Consequences:

- 1) Reduce what is now Hub1 to simple patch panel that receive and fan out limited number of service cables (LV, HV, data transfer)
- 2) Integrate a very much “slimmed” Hub1 in space between Ecal and Hcal that serves Hub2
Hub1
In: 48 V LV, 150 V HV, optical fibres for clock and data transfer
Out: 12 V LV (after DCDC Conversion), 150 V HV, optical fibres for clock and data transfer



New hub sitting between pipes of cooling system

Latest (?) drawings from AIDA2020 delivery report:

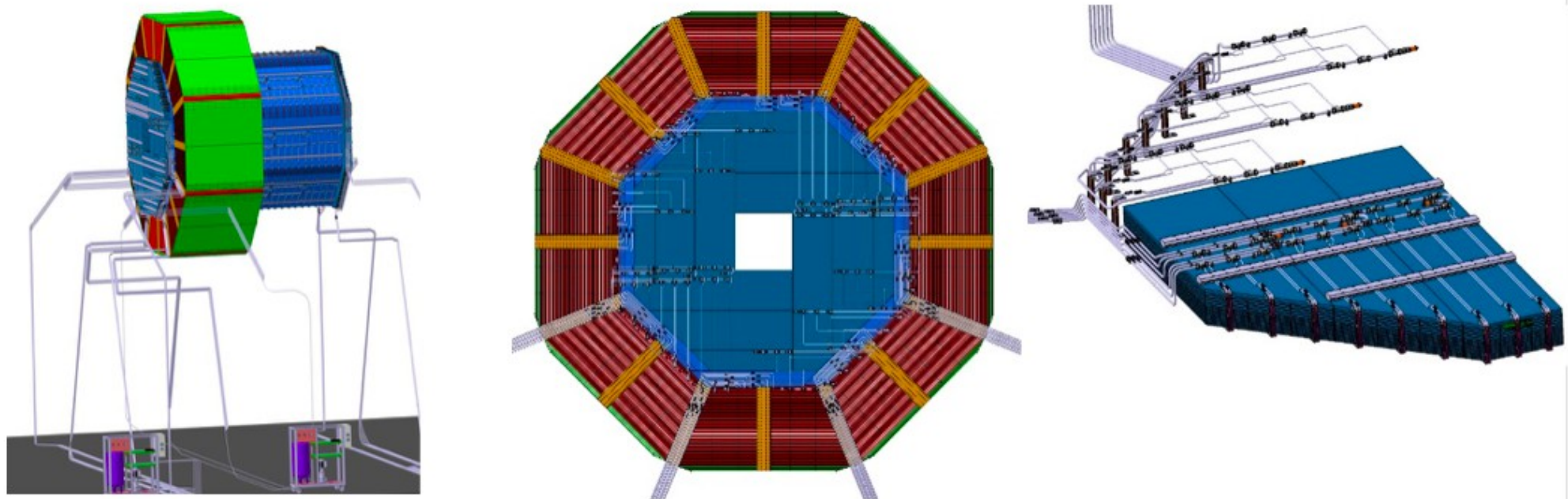
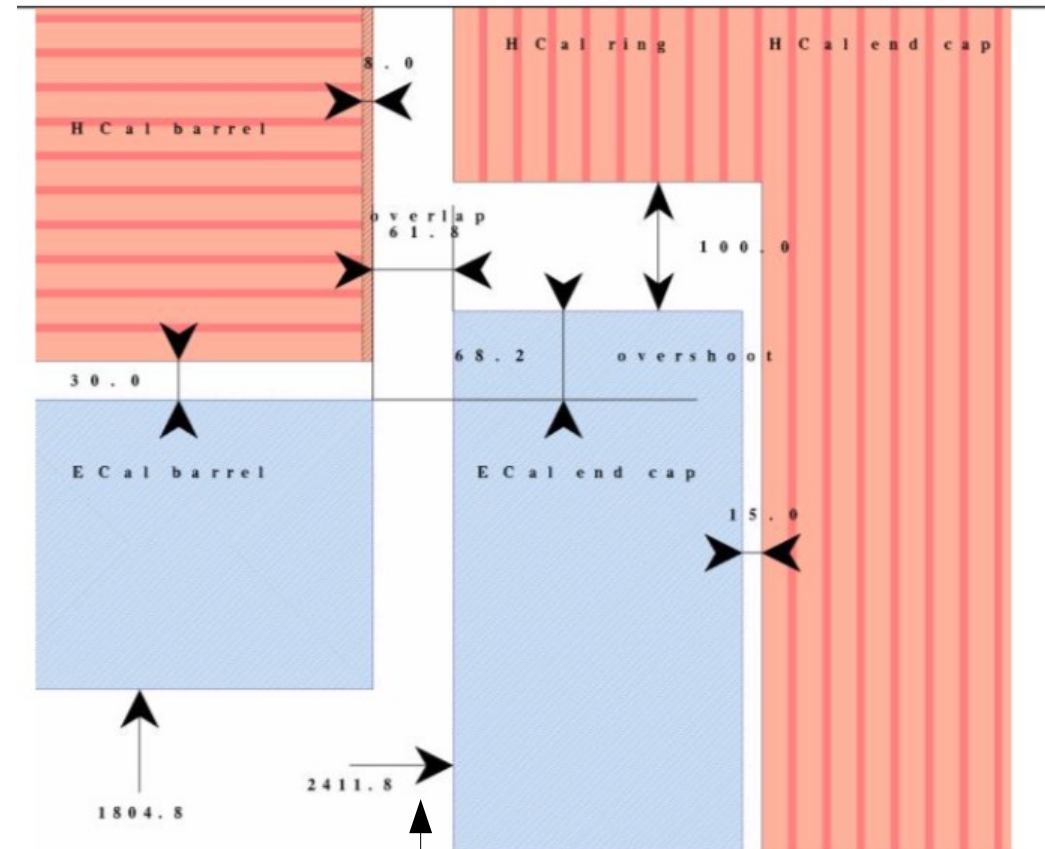
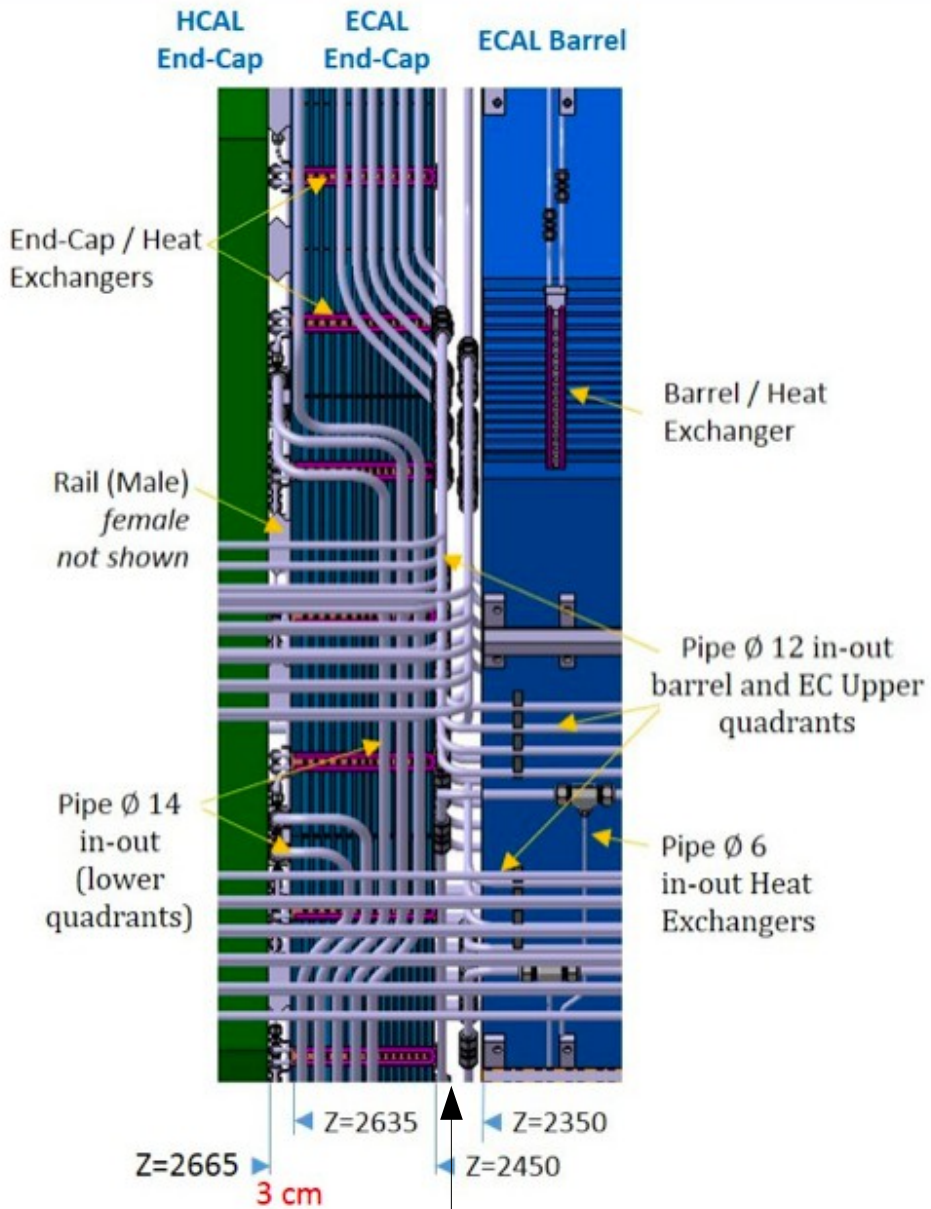


Figure 4: – (Left) Schematics of a general cooling distribution network of SiECAL for 1 Barrel and 2 EndCaps (Middle) Four main cooling lines arriving at the bottom, trough AHCAL, due to sub atmospheric configuration specific distribution network for leak-less cooling (Right) local cooling network on 2 EndCap Quadrants.

Question: Do cooling pipes for barrel enter only on one side of the barrel

Cooling system in ILD

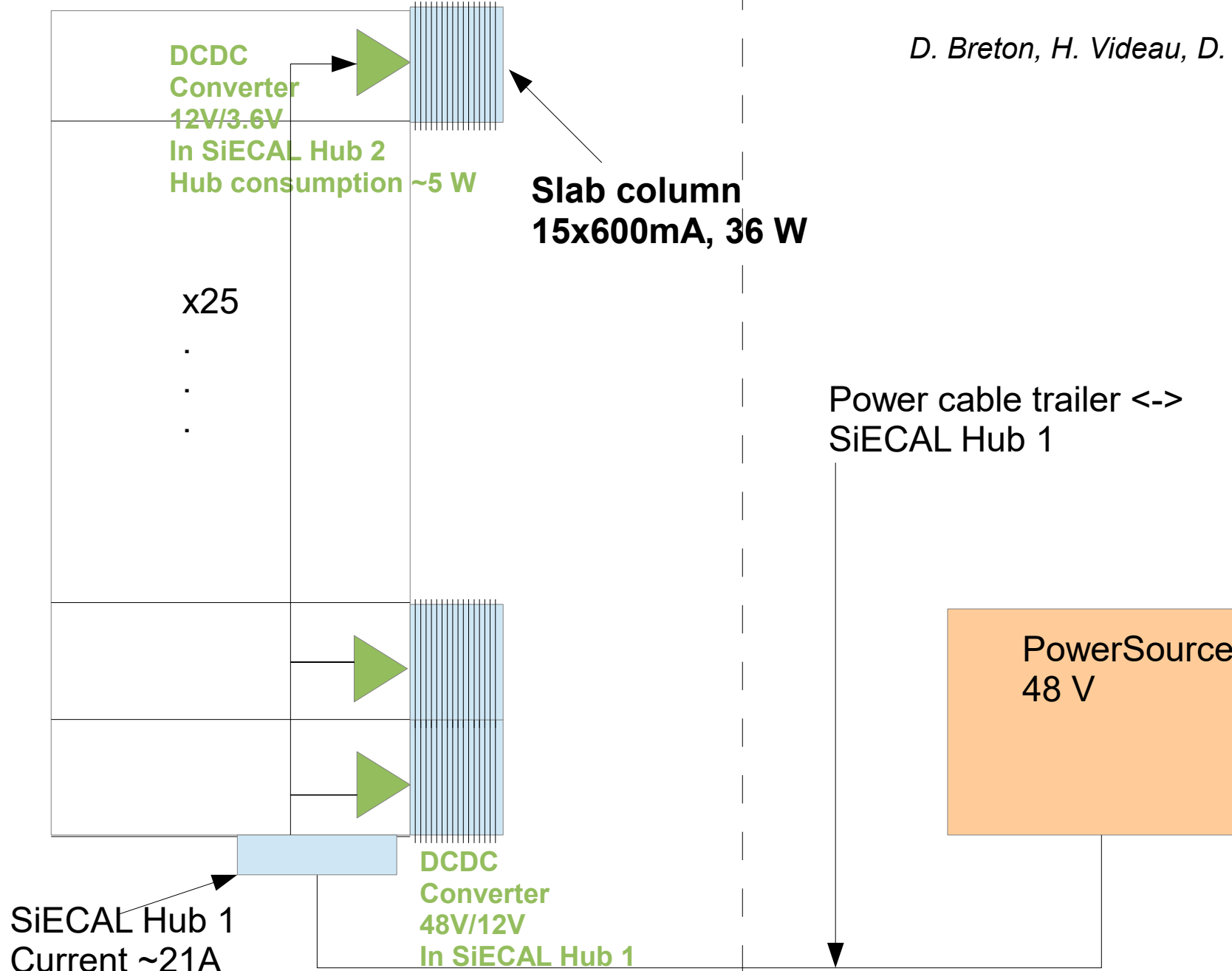


62.8mm

100mm

- Comment: Drawing with cooling pipes found in early version of AIDA2020 Report (maybe obsolete)
- If not obsolete: No compliance with current ILD Design

D. Breton, H. Videau, D. Zerwas, R.P.



1) The total power consumption of a stave 41 W (=25 columns) is about

$$25 \times 41\text{W} = 1000 \text{ W}$$

2) These 1000W have to be provided by the main power supply of 48 W

=>current drawn from the power supply is

$$1000\text{W}/48\text{V} = 21 \text{ A} \text{ (Note that these are average currents, peak current scale with DCDC conversion)}$$

These 21 A arrive at the SiECAL Hub 1

3) 21 A require a cable with a cross section of about 1.5 mm² maybe 2.5 mm².

Voltage drop:

$$\Delta U = (0.0171/1.5)\text{Ohm} \times 21\text{A} = 0.24 \text{ Volt} \Rightarrow \sim 5 \text{ Volt after 20m in case of } 1.5 \text{ mm}^2$$

with a thermal dissipation of $0.24\text{V} \times 21\text{A} \sim 5\text{W/m}$

$$\Delta U = (0.0171/2.5)\text{Ohm} \times 21\text{A} = 0.14 \text{ Volt} \Rightarrow \sim 3 \text{ Volt after 20m in case of } 2.5 \text{ mm}^2$$

with a thermal dissipation of $0.14\text{V} \times 21\text{A} \sim 3\text{W/m}$

$$\Delta U = (0.0171/4)\text{Ohm} \times 21\text{A} = 0.09 \text{ Volt} \Rightarrow \sim 1.8 \text{ Volt after 20m in case of } 4 \text{ mm}^2$$

with a thermal dissipation of $0.09\text{V} \times 21\text{A} \sim 2\text{W/m}$

Cable thickness subject to compromise between material budget and thermal dissipation

=> Propose to choose 2.5 mm² (requires coordination with other detector components)

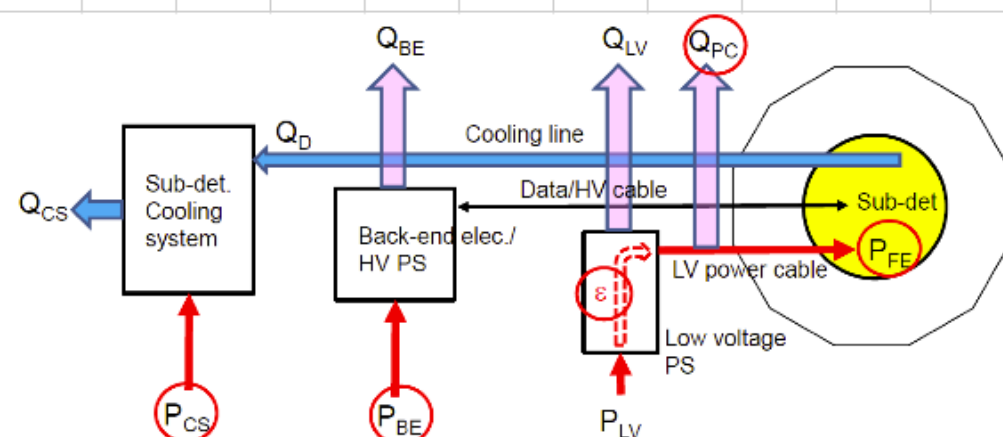
Remark: Numbers agree with the ones provided by C. Clerc and R. Cornat for DBD

Distributed by Yasuhiro beginning of September

Example SiEcal Power

05/09/18

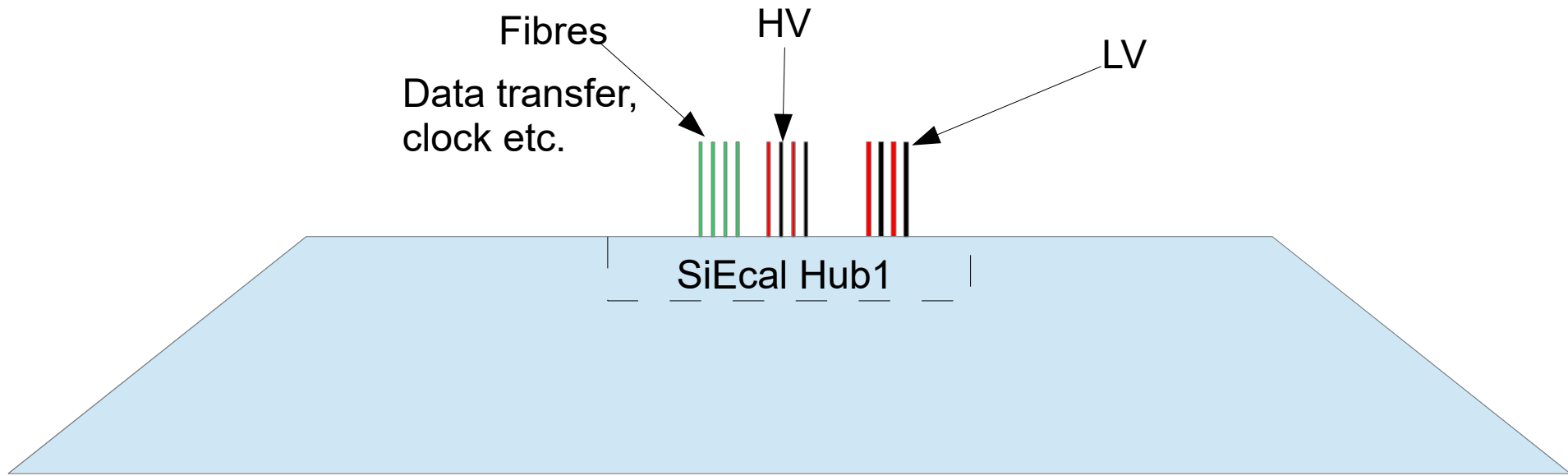
	Sub-detector name	ECAL
P_FE	Power consumption of Front-end Electronics	17 kW
Q_PC	Heat loss in Power Cables	1 kW
e	Efficiency of low voltage power supply	90%
P_BE	AC Power input to Back-end Electronics	kW
P_CS	Electric power to drive Cooling System	8 kW
	Type of cooling water for cooling system	Chilled water
P_LV	AC Power input to Low Voltage power supply	20 kW
Q_LV	Heat loss in Low Voltage power supply	2 kW
Q_BE	Heat loss in Back-end Electronics	0 kW
Q_CS	Heat to be extracted from cooling system	25 kW



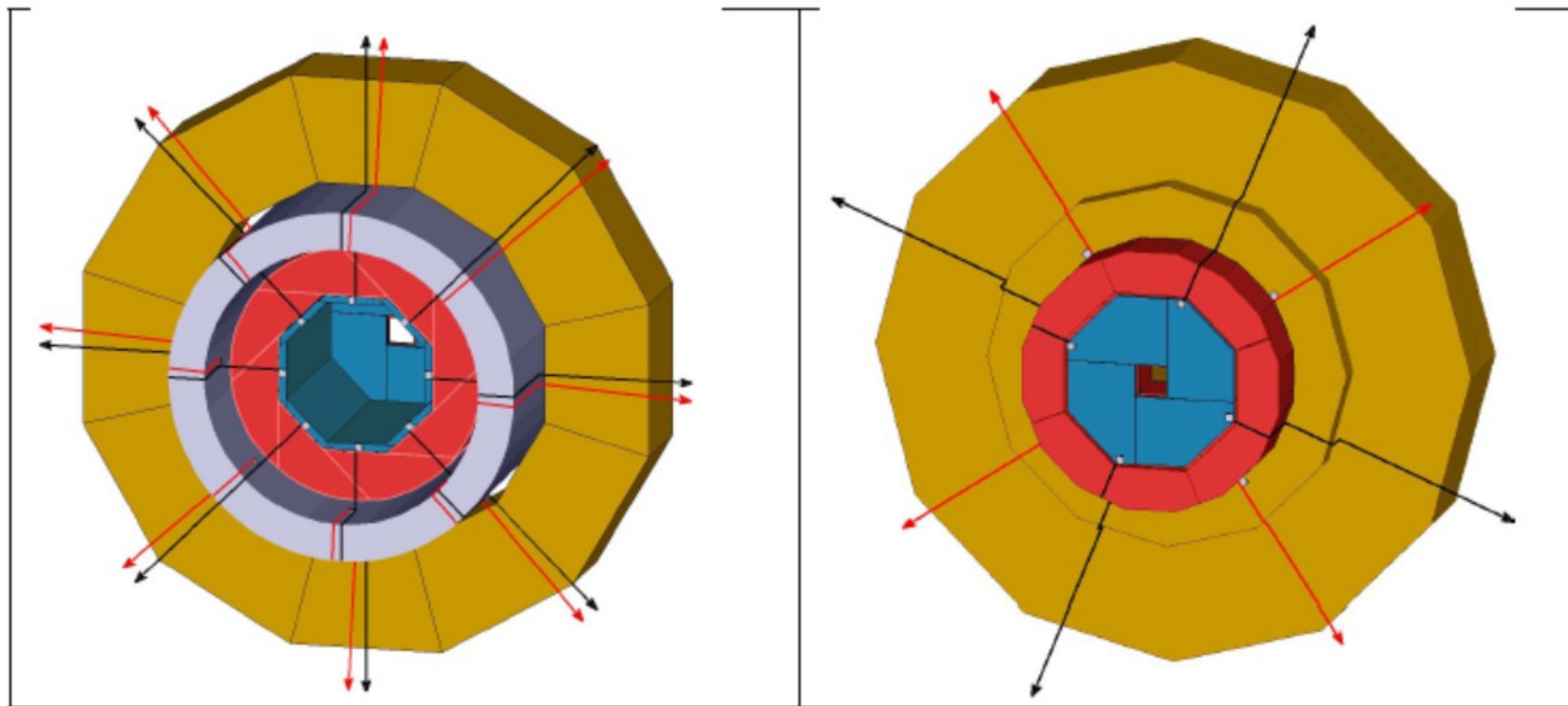
- P_{FE} : Power consumption of sub-detector Front-end Electronics
- Q_D : Heat loss in sub-det. ($= P_{FE}$)
- Q_{PC} : Heat loss in power cables
- P_{LV} : AC power input to LV PS
- ε : Efficiency of LV PS ($P_{LV} \cdot \varepsilon = P_{FE} + Q_{PC}$)
- Q_{LV} : Heat loss in the LV PS ($= (1 - \varepsilon) \cdot P_{LV}$)
- P_{BE} : AC power input to back-end elec./HV power supply
- Q_{BE} : Heat loss in the BE/HV PS ($= P_{BE}$)
- P_{CS} : Electric power to drive the cooling system
- Q_{CS} : Heat to be extracted from cooling system ($= Q_D + P_{CS}$)

Numbers were pre-filled but seem about to be correct

Note that this survey contains all subdetectors



- Not to scale!!!
- Number of cables include redundancy
 - LV cables will constitute a block of about $10 \times 2.0 \text{ mm}^2$
 - HV cables can be even thinner since they don't carry current $O(10 \text{ mA})$
 - Space consumption by optical fibres is also negligible
- Professional CAD drawing will be provided by A. Gonnin at the beginning of November
- SiEcal Hub1 has to be designed

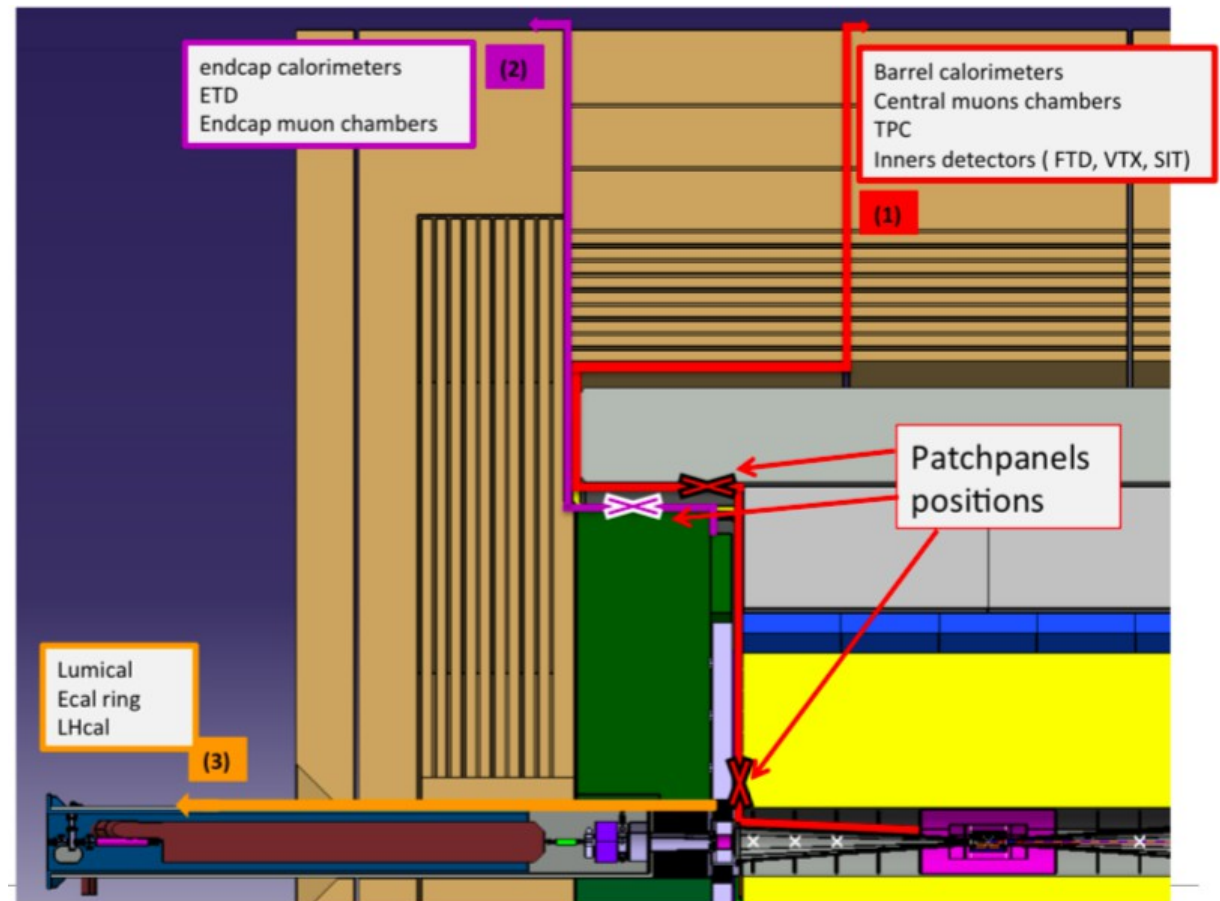


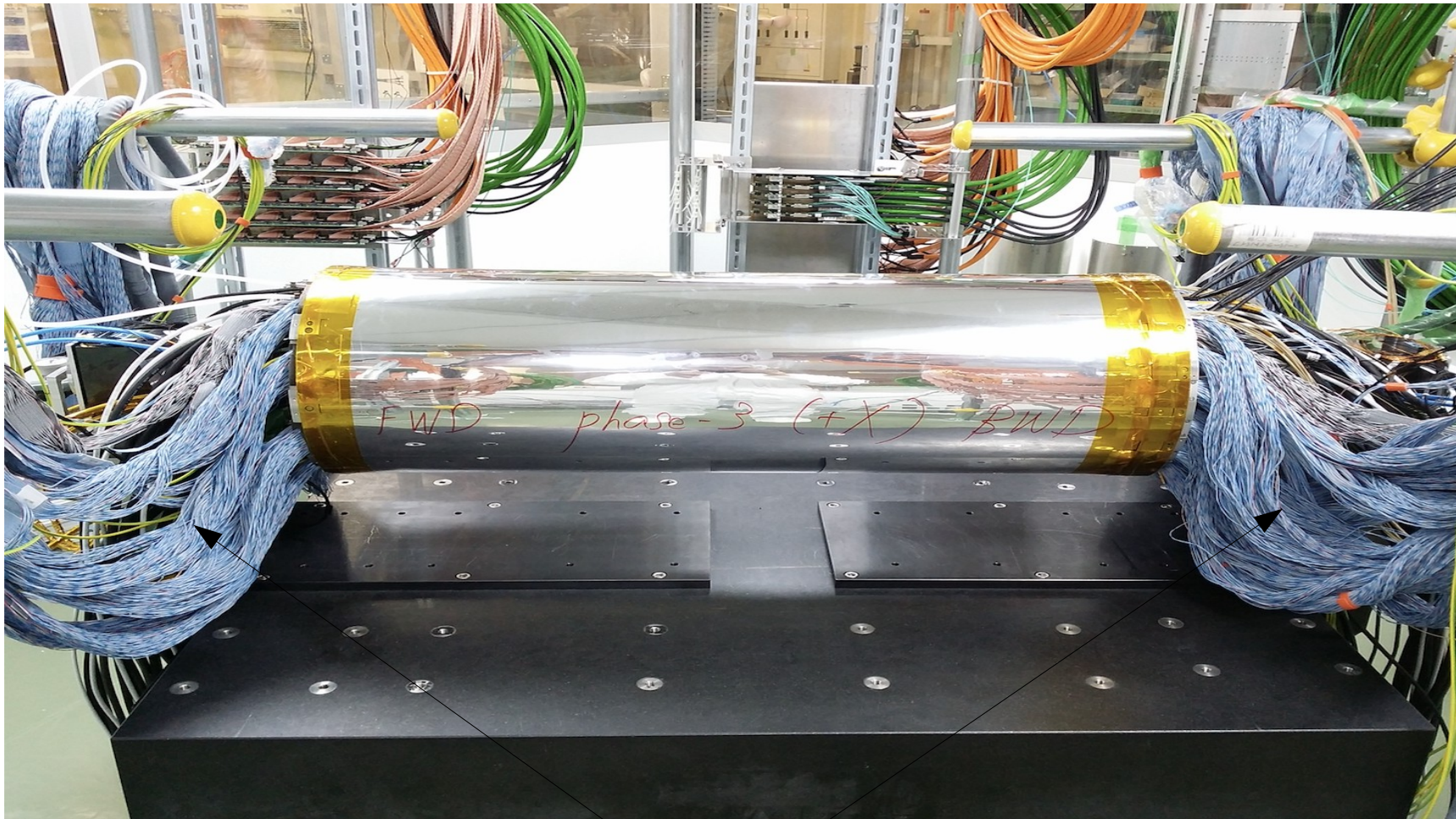
- Service lines leaving from barrel

- Service lines leaving from endcap

Drawing by Henri

- Drawing as shown by Karsten in Fukuoka
- Coordination of review of Cable and services by R.P.
- Preferred to do “my” homework before annoying others
- Take this talk as the first call to send me “your” updated cabling schemes

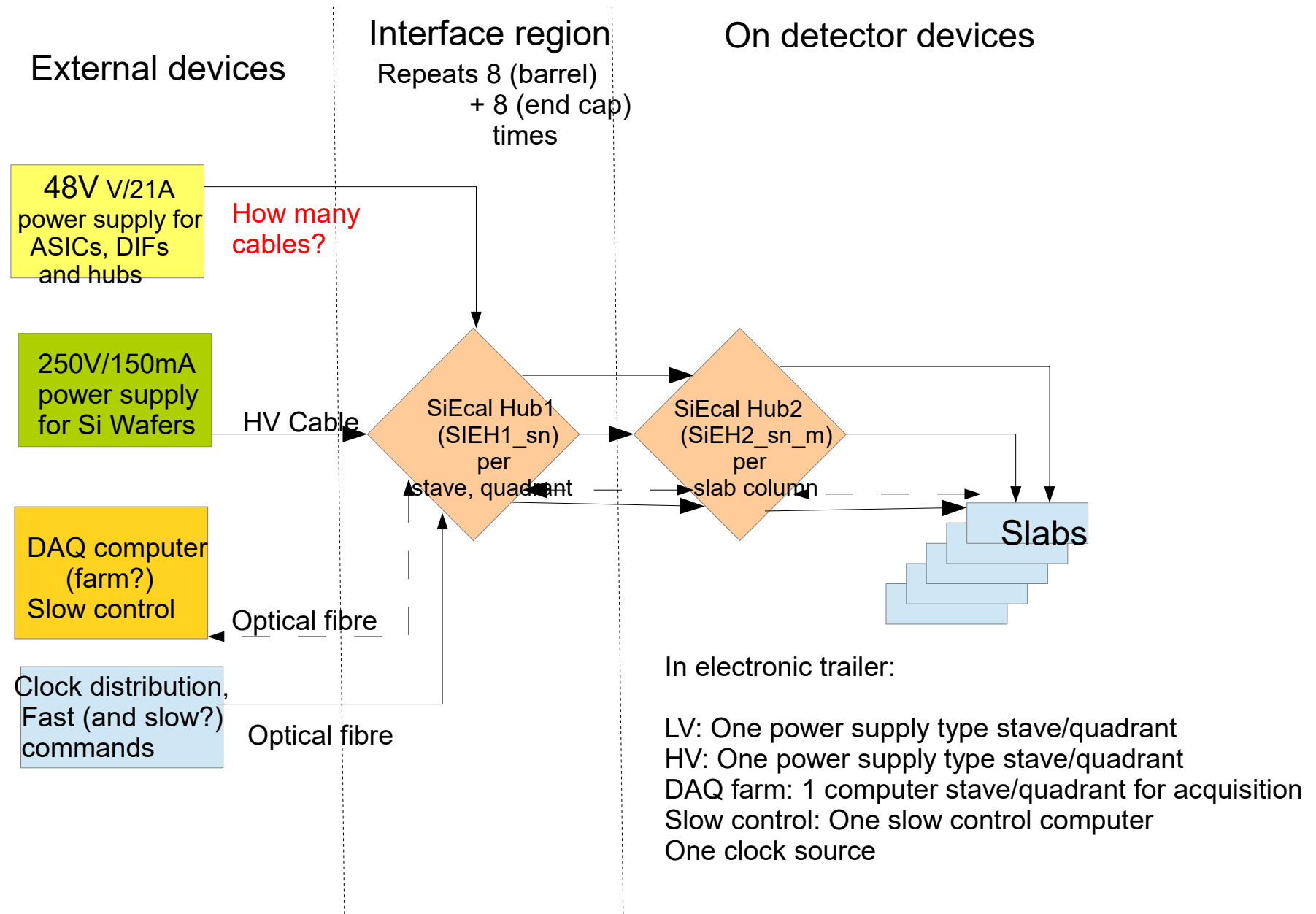


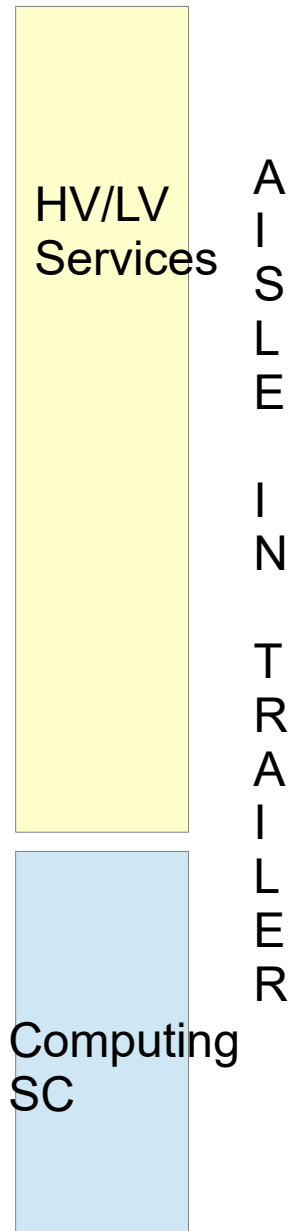


Cables!!!!
Thin but many

- Have to assume my charge and coordinate cable and service revision
- Started with understanding system requirements for Ecal and to request updated technical drawings for SiEcal
 - First step: From trailer to first hub
 - Power consumption agreed very well with pre-filled number in survey by Yasuhiro
 - Numbers on cable thicknesses agree with those from DBD (not a miracle but good to know)
 - Numbers don't look critical
- SiEcal power scheme (most likely) requires DCDC Converters
 - Basis of current considerations but subject of technical decision
 - (Not today) survey on possible products by D. Breton over summer
 - DCDC converter is pulsed device that operates in magnetic field
 - Some negative experience in CMS
- Considerations for other detectors not using DCDC Converters exist
- Power dissipation and influence on other detectors to be understood
 - e.g. Ecal \rightarrow Hcal ≤ 5 W/m, can this be cooled away by Hcal cooling?
 - Subject to discussion
- The list is for sure much longer and sorry for being late ...

Backup



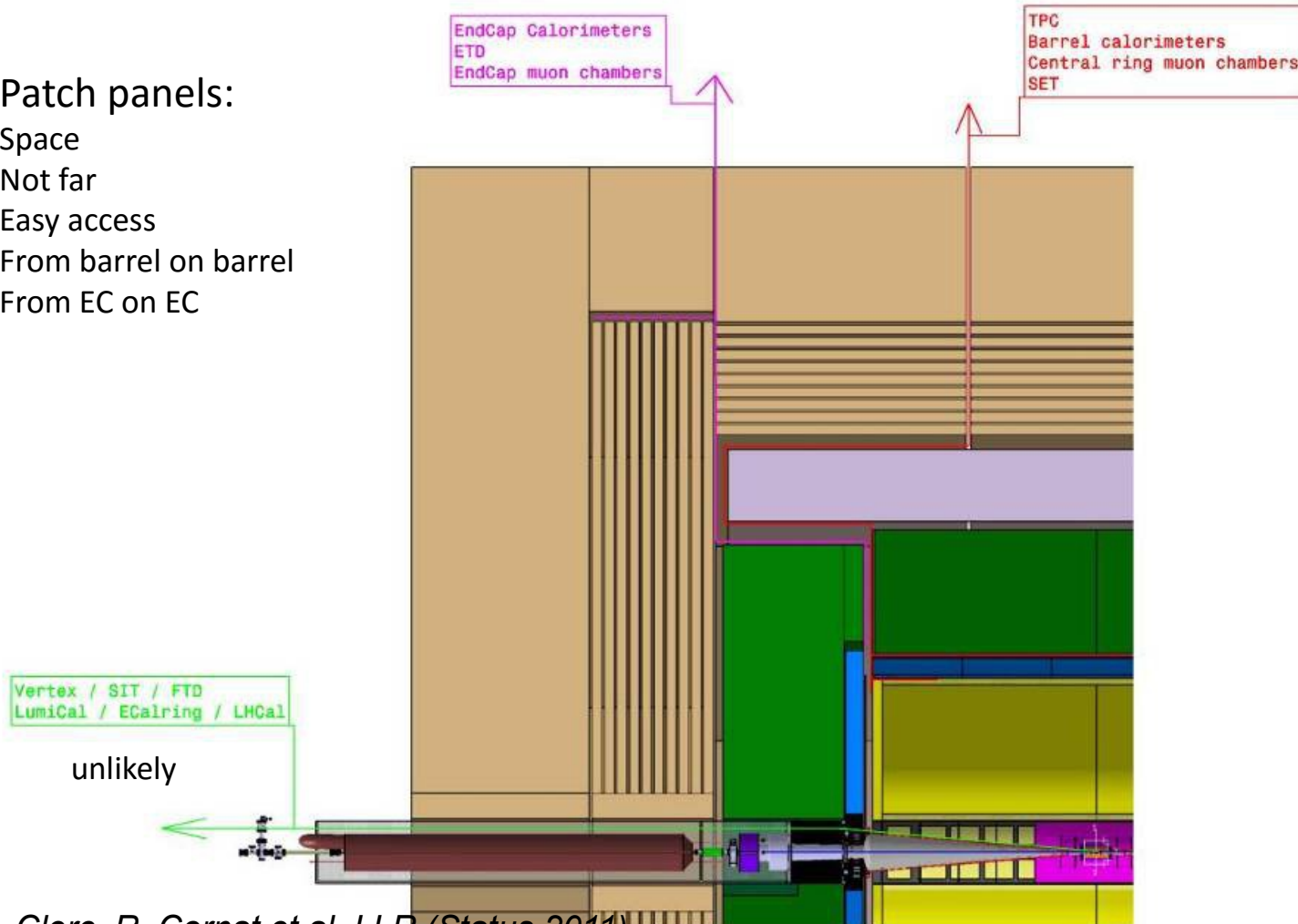


One aisle should be enough
Add a second as safety margin

A reminder

Patch panels:

- Space
- Not far
- Easy access
- From barrel on barrel
- From EC on EC



C. Clerc, R. Cornat et al. LLR (Status 2011)

Study for DBD needs regular update!!!!
Use ICD

... a poor man's point of view

- The advantage of a DCDC converter is that it realises the step down of the voltage **without** ohmic losses (in contrast to a “simple” linear regulator)
- From a “crash course” on DCDC converters I have learned that energy is stored in an inductor during time t_{on} and released during a time t_{off}
The output of a (Buck) DCDC Converter is $V_{out} = V_{in} \times t_{on} / (t_{on} + t_{off})$
The duty cycle V_{out} / V_{in} determines the average current that is drawn from the power source V_{in}
- At each layer the voltage 4V is available from a 12V/4V DCDC Converter.
The total current of a layer is 200mA (regard SL-Boards only for simplicity)
- Therefore the average current drawn from the power source is in this case
 $(4/12) \times 200\text{mA} = 66\text{mA}$