



<b>CHANGE REQUEST NO. ILC-CR-00XX</b>	<b>EDMS No:</b> D*XXXX	<b>Created: 31-12-2019</b>
		<b>Last modified: 10-1-2020</b>

## SRF ACCELERATOR CRYOGENICS: HE INVENTORY

[Few sentences describing the main subject of the change request]

A change request of He inventory configuration for the ILC SRF accelerator cryogenics is provided in focus on helium resource conservation to respond to any operation and emergency modes, as follows:

- Helium (He) inventory is simply stored as He gas in multiple buffer tanks (at 20 bar<sub>-max</sub>) at each satellite plant, as a primary concept, enabling quick and full He resource recovery during any shutdown of the SRF cryogenics including primary AC power outage,
- As a complementary concept, long-term helium inventory backup is proposed in liquid/supercritical phase in a dewar/container at a specified station/plant, to reserve additional He inventory with a fraction of 10 - 20% for the full amount of He (100%) necessary to the nominal ILC SRF system operation. and to flexibly link and distribute to each satellite plant with He-gas pipelines.

## RATIONALE

[Outline briefly as possible the main reasons for requesting the change]

- LHe in the ILC SRF cryomodule has to be entirely evaporated within 3 days because of static thermal load (~ 20 W/CM) and acceptable pressure increase (limited to  $\leq 2$  bar-abs) in the cryomodules (CMs), in case of any shutdown of the cryogenics operation (see Fig. 1). Immediate recovery in gas phase is inevitable by using recovery compressors supported by emergency AC power generators.

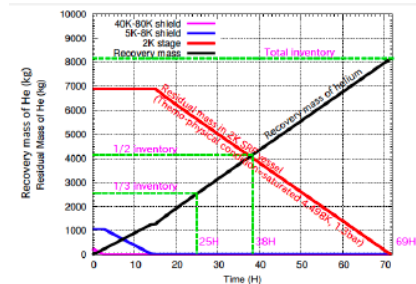
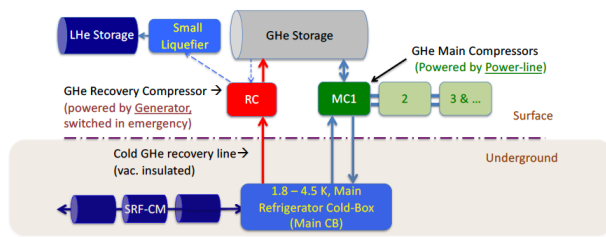


Fig. 1

- A large amount of helium resource may not be quickly delivered in particularly in Japan, because entire He resource in Japan is shipped and imported and it directly impact on the SRF accelerator operation availability. It is very important to conserve He inventory with minimum loss in any emergency modes of the cryogenics operation including AC power outage.
- Full recovery and storage of the He resource into GHe buffer tanks by using a recovery compressor system at 20 bar is a simple and very reliable strategy to conserve the He inventory.
- Just as a note, the previous CR (009) assumed that a half of He resource be liquefied and stored in a large LHe dewar. It takes one week (~7 days), and it might cause additional failure risks.

### SCOPE

[Brief description of the overall scope of the modifications being proposed, including possible impact on other areas]

- We propose to modify the helium inventory to be simply stored in He gas buffer tanks (100%) at each ML satellite system, instead of mixture of gas/liquid (50/50%) storage system, for very reliable recovery of helium gas evaporated from the ML SRF system. It requires doubling numbers of He gas buffer-tanks (6 to 12) at each satellite cryogenics station. On the other hand, it may much simplify the recovery system with no requirement for the helium liquefaction system at each satellite surface site (see Fig. 2).

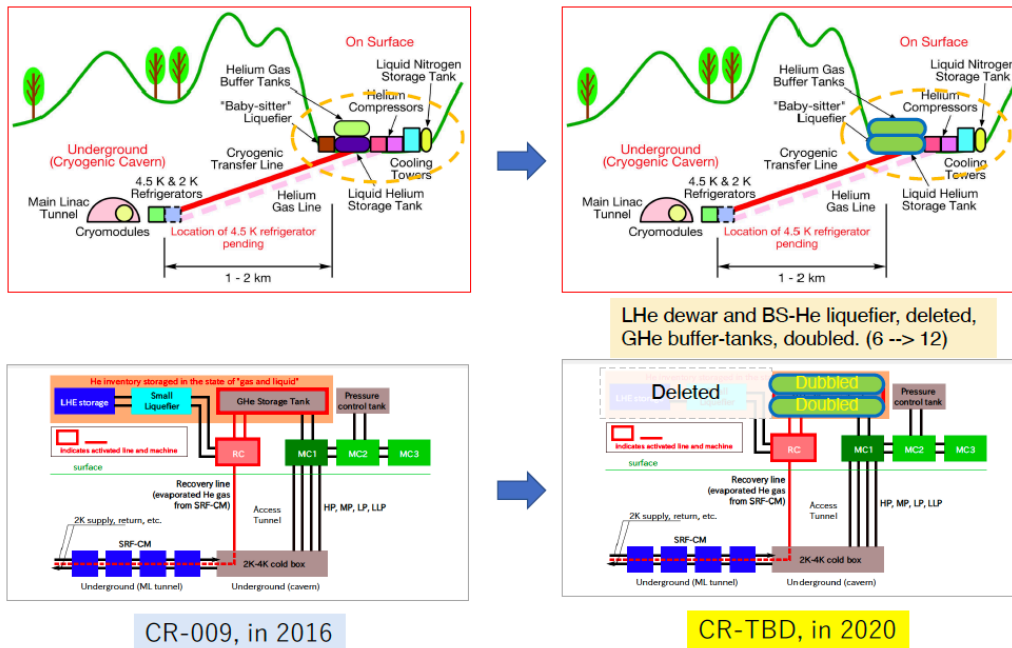


Fig. 2

- Helium inventory for long-term backup may be differently optimized by reserving possibly with LHe/supercritical phase in a large LHe container (dewar) assisted with a baby-sitter/small liquefier to maintain the helium inventory to be re-cycled/re-condensed.
- It may be placed at one location, possibly at the ILC IP/central region, and GHe inventory network/pipeline should be provided to flexibly distribute the helium resource for all satellite cryogenics plants along the ILC ML/DR (see Fig. 3).
- The station should also function as the reception to receive He resource commercially delivered possibly in a large LHe/supercritical phase.

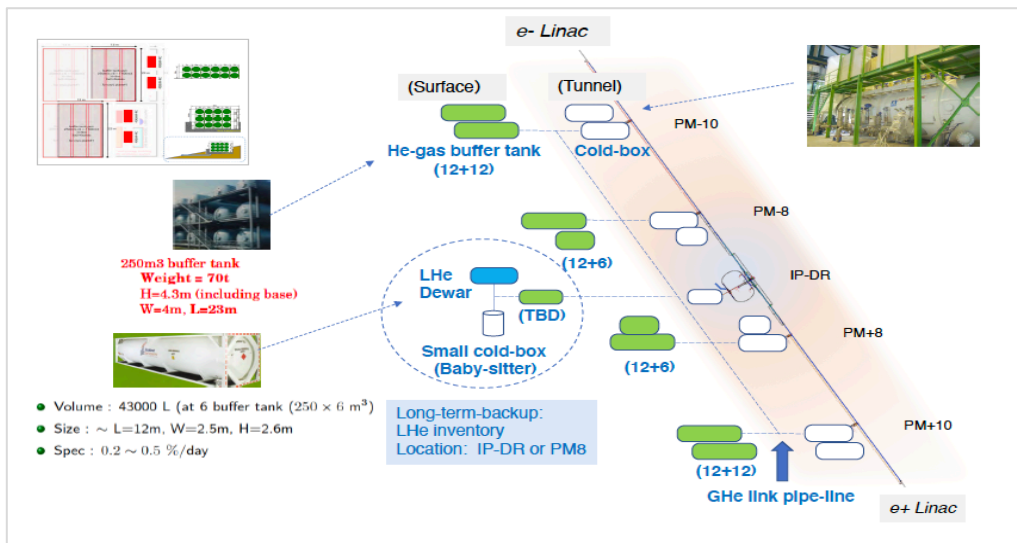


Fig. 3

- As a significant positive impact, helium resource may be very reliably conserved, and availability of the SRF accelerator operation may be much secured.
- No major effects are seen to other system, except for doubling GHe tanks including transportation to and installation work at the satellite cryo-plant site.
- Overall scope of the modification is summarized in Table 1, as follow:

Table 1.

	CR-09: current baseline	CR: proposed
<b>Quick recovery at Satellite Plant:</b>		
# GHe BufferTank	6 (3 x 2 layers)	12 (4 x 3 layers)
Emergency Recovery compressor	Yes	Yes
He liquefier for LHe storage	Yes	No
LHe Storage Reservoir	Yes	No
He recovery time:	7 days ( 2x3+a)	3 days
Emergency Power Generators:	≤ 1 MW	≤ 0.5 MW
Surface area required	≤ 1300 m <sup>2</sup>	≤ 1,300 m <sup>2</sup>
<b>Long-term He backup (10-20%)</b>		
LHe reservoir and He liquefier	Distributed at satellites	Centralized at IP-DR



### VALUE/SCHEDULE IMPACT

[Brief explanation of the estimated value figure if available. Also if know, impact on construction schedule. Value should also include explicit labour if possible]

- The estimate value figure for the He recovery and gas storage (100%) in comparisons with the current baseline (CR-09) is summarized in Table 2, as follows:

Table 2.

Subject	Current Baseline (CR-09)	New CR (proposed)
<b>Cost of ML Satellite Plant (each):</b>		
GHe buffer tanks	3.4	6.7
Recovery compressors	0.7	0.7
Small He liquefier and LHe dewar	4.4 + 1	--
LHe dewar	1	--
Transportation and unloading	0.9	1.8
Site construction (CE)	0.6	1.2
<b>Sum/plant</b>	11.4	10.8
<b>Total Cost for 2 x 3.5 (7 eq.) plants:</b>	<b>79.8</b>	<b>75.6</b>
<b>Additional Cost: Long-term He backup:</b>		
LHe dewar + He liquefier + GHe Link	+ $\alpha$	4.4+1 + $\beta$
<b>Grand total</b>	<b>80 + <math>\alpha</math></b>	<b>76 + 5 + <math>\beta</math></b>

- The overall cost is similar in both cases, and no major effect is expected.
- The impact on the construction schedule should be minor.
- The operational cost including annual maintenance/inspection would be less in the new CR, because of the simplicity in the system configuration.

(end)

Requested and prepared by: T. Okamura, H. Nakai, and A. Yamamoto





Attachments:

Number:	Original / Updated:	by:
1	Concepts of CR009 and follow-up (2016)	HN, TO, YM, AY
2	Report from WG3 on ILC-250 study (2017-7)	AY. HN. TO
3	Study of ILC ML Cryogenics, (2017-3) Originally reported at LCWS (2016)	TO, HN, AY
4	Cryogenics at CERN, ILC Cryog. WS (2013-11)	D. Delikaris
5.	Foot print: LHC-SM18, He Inventory Configuration, Image for 2 x 3 x 4 He tanks Configuration	DD, AY

Change History:

Version:	Created/modified:	by:	what:
1.0	31.12.2019	T. Okamoto, H. Nakai, A. Yamamoto	Preliminary Draft
1.1	5.1, 2020	T. Okamoto, H. Nakai, A. Yamamoto	Draft updated, including additional attachments.
1.2	8. 1, 2020	T. Okamoto, H. Nakai, A. Yamamoto	Draft updated,
1.3	10. 1, 2020	T. Okamoto, H. Nakai, A. Yamamoto	Appendix added (CERN SM18, He inventory example),



## IMPLEMENTATION PLAN

Can be left blank for first submission.

**Concerned Parties** (Work Packages, Coordinators, Suppliers etc.)

WF/Area	

Affected documents

EDMS ID	Title	Remark

## ATTACHEMENTS

[Place additional document here as needed. This can be used for adding a more detailed description of the CR]

### Attachment 1: CR009 (Nakai, Okamura, Makida, Yamamoto, 2016-2017)

#### ILC Cryogenics Layout-Design Updated in 2017 -- Change Request 09 (Originally, 2016-1)

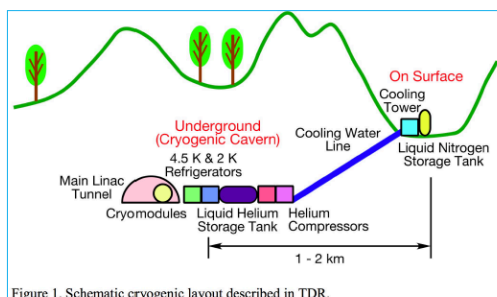


Figure 1. Schematic cryogenic layout described in TDR.

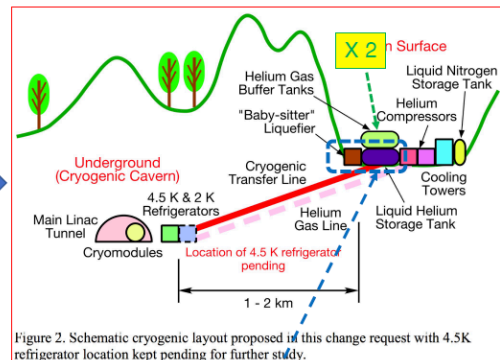
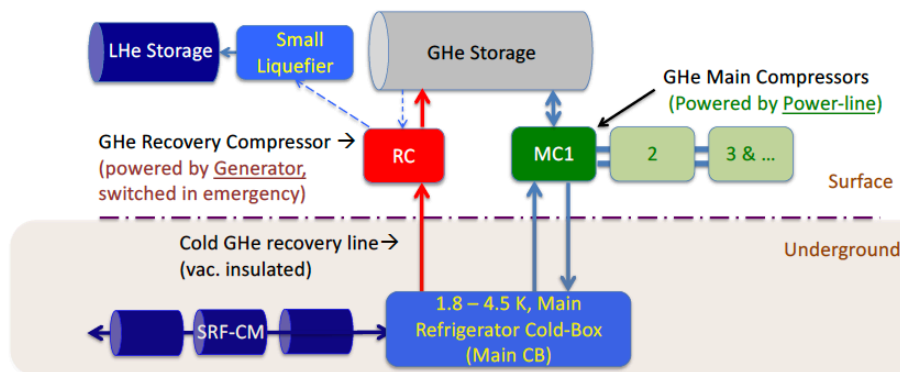


Figure 2. Schematic cryogenic layout proposed in this change request with 4.5K refrigerator location kept pending for further study.

Today (2020-1), we will discuss the emergency operation: to be simplified by doubling GHe Buffer Tanks, and eliminating a small (Baby-Sitter) He Liquefier and a LHe storage tank (reservoir)

#### He Flow Lines in Emergency to Recovery

2016-8-25  
Nakai, Okamura, Makida, and Yamamoto



##### Operation Sequence in emergency to resume steady state modes (under investigation):

1. GHe recovery using RC (powered by Generator for < 24 hrs, (electric capacity: < 1 MW / plant)
  2. Recovery of MC1 (and 2, 3, ...) and Main CB, for LHe to be kept in CM after power-recovery
  3. LHe to be produced in LHe storage for a period of 5 ~ 7 days, by using RC powered by power line
- (Note: Balance of LHe and GHe storage capacity to be further investigated and globally discussed)



## Attachment 2: Reports from ILC250 WG3 (A. Yamamoto, S. Michizono, and B. List: briefly extracted, 25 July, 2017)

### ILC Cryog. Configuration to be staged at 250 GeV Option D (ML installed, downstream)

Legend:  
 - small 2 K and 4.5 K cryoplants  
 - large 2 K cryoplants  
 - helium compressor stations

**TDR-2013**  
Configuration  
at 500 GeV  
- 5 plants/linac

**Staging  
at 250 GeV :**  
3 plants/linac,  
although the  
cooling power  
requirements to  
be reduced  
down to ~70 %.

Updated: 170724

### Staging (250 GeV) effects on the SRF Cryogenic Systems

**Electron Linac**

Station	Length (m)	Start (m)	End (m)
RTML	100.0	100.0	200.0
Damping Rings	100.0	200.0	300.0
Final Focus	100.0	300.0	400.0
Main Linac	1200.0	400.0	1600.0
5 GeV Booster	120.0	1700.0	1820.0
Detector Cryogenics	100.0	1820.0	1920.0
Undulators	100.0	1920.0	2020.0

$E = 31.5 \text{ MV/m}$ , and  $L_{eff} = 1.0385 \text{ m}$   
 $V/cavity = 32.7 \text{ MV}$   
 $V/\text{short-string} = 3 \times 21 \times 0.8505 = 53.6 \text{ GeV}$   
 $V/\text{MLU} = 32.71 \times 26 = 850.5 \text{ MV}$   
 Cryogenics unit (short string) length (3 MLU)  
 $= 3 \times 37.956 \times 2.5 = 116.368 \text{ m}$   
 RF unit: (4.5 CM) length = 56.934 m  
 MLU length (9.3 CM) =  $3 \times 12.652 = 37.956 \text{ m}$   
 CM length = 12.652 m (pitch)

	RTM L-BC	ML-CM	PM -12 -u	PM -12 -d	ML-CM	PM -10 -u	PM -10 -d	ML-CM	PM -8 -u	PM -8 -d	e+ Booster	Sum	Cost Down
<b>TDR-500</b>													
Cryo-Cost	19.05 + 29.27				58.54	58.54	58.54	58.54	58.54	58.54	32.54*	315.02	n/a
# C-Plant	$\sim 0.2 + 0.5 = 0.7 \rightarrow 1$				1	1	1	1	1	1	$> \sim 0.55*$	5.5 systems	
CP-Power (19 kW @ 4.5 K)				19 kW @ 4.5 K	19 kW @ 4.5 K	19 kW @ 4.5 K	19 kW @ 4.5 K	19 kW @ 4.5 K	19 kW @ 4.5 K	19 kW @ 4.5 K			
# CM	51	99			189	189		189	189		24	930	
E. Sum	10	28.1			53.6	53.6		53.6	53.6		5	257.5	

	RTM L-BC	ML-CM	PM -10 -u	PM -10 -d	ML-CM	PM -8 -u	PM -8 -d	e+ Booster	Sum	Cost Down
<b>Stage - 250</b>										
Cryo-Cost	19.05 + 29.27					58.54	58.54	32.54*	197.94	0
# C-Plant	$\sim 0.2 + 0.5 = 0.7 \rightarrow 1$					1	1	$\sim 0.55$	3.5 systems	
# CM	51	45				189	189	24	498	
E. Sum	10	12.8				53.6	53.6	5	135.0	

	RTM L-BC	ML-CM	PM -10 -u	PM -10 -d	ML-CM	PM -8 -u	PM -8 -d	e+ Booster	Sum	Cost Down
<b>Stage - 250 +SRF R&amp;D</b>										
Cryo-Cost					58.54	58.54 + 13 (for long distribution)		130	-68	
# C-Plant						$0.7 \times (1+0.13) + x = 0.79 + \sim 0.4 \rightarrow 1$		2 systems		
# CM & (relative TL)	51	4.5				189 (132)	189 (132)	24 (17)	457.5	
E. Sum	10	1.28				59.56	59.56	5	135.4	

### Attachment 3: ML Cryogenics (Okamura, Nakai, Yamamoto: briefly extracted, 2017)

#### ML Cryogenics

T.Okamura, H.Nakai, A.Yamamoto  
KEK  
2017/3/13

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#### Main Flow Diagram

Not including cryo system for power failure.

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#### MCS Configuration and Input Power

- 8 compressors (3 kinds of compressor)
  - 2 sub-atmospheric comp, 2 low stage comp, 4 high-stage comp
- Total input power 5 ~ 5.5 MW / plant
- too large input power to run during power failure

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#### He inventory per 1-cryo plant

**He inventory**

- 63000 liquid L/plant = about 8.2 metric tons/plant
- Fig. 3.26 (ILC Technical Design Report: Volume 3, Part II) , most of the helium inventory consists of the liquid helium which bathes the RF cavities in the helium vessels. (TDR)

**Equivalent buffer tank volume of 63000L of LHe**

- 12 buffer tanks with 250m<sup>3</sup>, 2 MPa-A (including 10% contingency)
- If 6 buffer tanks with 250m<sup>3</sup> are prepared, half of all can be stored in the buffer tanks.

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#### Basic Design Guideline during Power Failure

- No loss of Helium resource** even during a total power or cryogenics system failure
  - Unfortunately, this guideline was missing in the TDR.
  - Annual loss of helium may not be zero because of regular maintenance work, but it may be assumed to be smaller than 10 %.
  - Sudden large amount of helium resource would not be available especially in Japan.
- SRF should be protected from a damage due to pressure increment** which is induced by static heat load and loss of cooling capacity. Boil off gas should be discharged from SRF-CM so as not to be beyond allowable pressure of SRF.
  - Allowable pressure of SRF cavity is 2 bar-abs.
  - Significantly different from superconducting magnet system allowing 20 bar (as same as the cryogenics design pressure).

**Recovery system meeting the above requirements is needed!**

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#### Technical Design Guideline during Power Failure

- A QUICK ACTION is essential against the MCS stop.**
  - A simple and robust GHe recovery action made by using a dedicated GHe compressor system, immediately after the Main Compressor stop.
  - Recovery system can be operated by using natural-gas/oil generators with a capacity of 1 MW ×(1 ~ 3) days per cryo-system: meaning 2 MW ×(1 ~ 3) days per access tunnel portal point.
- MCS and MCB with 5-5.5 MW may not be restarted even though main electrical power is quickly recovered after the failure.**
  - because of unexpected problem which are generated by sudden inadequate stop due to the failure.
- Liquefaction of recovery gas should not be done.
  - it is not easy to ensure a high response and stability of liquefaction system.
- Recovery helium gas should be stored in buffer tank by means of Recovery Compressor (RC) system.**

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#### Block Diagram (during Steady State Operation)

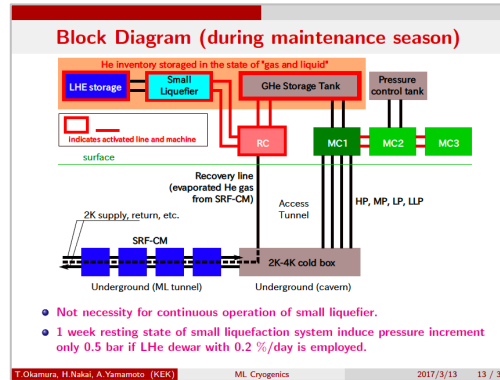
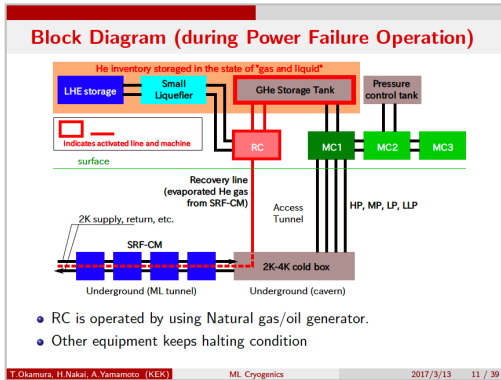
- LHe storage is almost empty during steady-state mode.
- During steady state operation, maintenance of small liquefier should be done.

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#### Block Diagram (during Warm Up Operation)

- All he inventory should be recovered on surface (recovery time ~ 1 week.)
- Small liquefaction system (Small liquefier and RC) should be operated.
- In addition, MCS and MCB have to be running state to control boil off He mass flow rate within 290 L/h which is the capacity of small liquefier system.

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### How to operate during power failure

- MCB (Main Cold Box) ⇒ NOT Restarted!
- MCS (Main Compressor System) ⇒ NOT Restarted!
- Small Liquefier and LHe Storage dewar ⇒ NOT Started!
- RC (Recovery Compressor) ⇒ Started !**
  - Not necessary for large input power
  - input power ~ 400 kW (= 71.5 g/sec).
- POSSIBLE to operate by using natural oil/gas generators**

**Requirement for recovery mass flow rate**

- Mass flow rate control within ~ 30 g/sec is essential.
  - According to our estimation, evaporated mass flow becomes much larger than 30 g/sec due to heat load increment unless some ingenuity is made.

⇒ How to reduce the mass flow rate ?

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### Evaporated mass flow control during Power Failure

How to reduce evaporated mass flow rate

- Due to the loss of cooling capacity, increment of static heat load into SRC induce evaporated mass flow increment.
- Cold boil off gas should go through radiation shield to cool down the shield temperature and to reduce heat load.
- ⇒ Enthalpy recovery of boil off gas with cryogenic temp.**

If the evaporated mass flow rate during the failure can be reduced, redundancy of recovery system during the failure can be obtained.

Information on Mass Flow Rate

- Required (Desired) ~ 30 g/sec.
- RC Capacity ~ 71.5 g/sec
  - During steady state cooling = 18 g/sec (w/o Dynamic Loss)

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### TOY Model for Evaporated Mass Flow Estimation

Following balance equations with TOY model are solved numerically.

Heat transfer Correlation

$$\bar{Q}_{ij} = h_{ij}(T_i - T_j)A_{ij}$$

$$Nu_{ij} = \frac{h_{ij}D_j}{\nu_j} Re_{ij} = \frac{\nu_j D_j}{\nu_j}$$

Dittus-Boelter Correlation

$$Nu_{ij} = 0.023 Re_{ij}^{1/2} Pr_j^{1/4}$$

Energy Balance Equation for material

$$C_i M_i \frac{dT_i}{dt} = Q_{i-1,i} - Q_{i,i+1} - \bar{Q}_{ij}$$

Energy Balance Equation for helium

$$\frac{\partial}{\partial t} (\rho_j h_j) + \frac{\partial}{\partial z} (\rho_j u_j h_j) V_j \approx -V_j \frac{\partial h_j}{\partial z} + Q_{ij}$$

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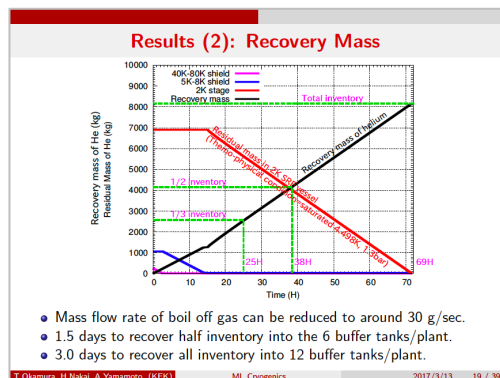
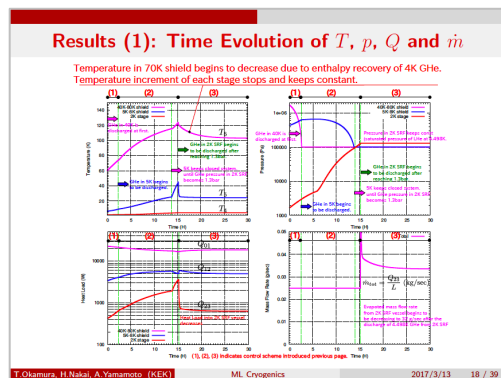
### Calculation and Control Scheme

Initial Pressure of each stage

- 40K shield = 18 bar (inlet pressure of T3)
- 5K shield = 3.6 bar (outlet pressure at HEX in the 4K subcooler)
- 2K SRF = 1.6 kPa (saturated pressure of He II)

- Helium gas in 40 K shield is discharged from 18 bar to 1 bar.
  - During this operation, 5K shield and 2K SRF keep closed system.
  - Pressure in 5K shield and 2K SRF gradually increase due to static load.
- After 40 K shield becomes 1 bar, He gas in 5K shield is discharged to 1 bar
  - Discharged He gas go through 70K shield to recover enthalpy.
  - 2K SRF keeps closed system and pressure gradually increases.
- After 5K shield becomes 1 bar and 2K SRF pressure becomes 1.3 bar from 2K, 1.5 kPa, He gas in 2K SRF begins to be recovered.
  - Discharged He gas go through 5K shield and 70 K shield.
- If residual mass in 2 K SRF becomes almost zero, calculation is finished.

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### How to set up buffer tanks

- 6 buffer tanks / plant. ⇒ 12 tanks / location.
- Transportation and unloading scheme should be considered carefully.

6 buffer tanks (each for 250m<sup>3</sup>)  
example of JFROSA (KAGA, Japan) unloading of 250m<sup>3</sup> tank at NOKA port

250m<sup>3</sup> buffer tank  
Weight = 7t  
H=4.2m (including base)  
W=6m, L=25m

Semi-refrigerated sections used as a storage shed

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### BOG behaviour during planned outage

#### Dewar Specification

- Volume : 43000 L (at 6 buffer tank (250 × 6 m<sup>3</sup>))
- Size : ~ L=12m, W=2.5m, H=2.6m
- Spec : 0.2 ~ 0.5 %/day

#### During planned outage (3days continuously shutdown)

- (1 bar, 4.2 K) ⇒ (1.60 bar, 4.70 K) (@ 0.5%/day)
- (1 bar, 4.2 K) ⇒ (1.24 bar, 4.44 K) (@ 0.2%/day)

No problem during 3 days outage

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### Small Liquefaction System (Small Liquefier)

#### Definition

Small Liquefaction System can be defined as follows.

- Compressor : (Recovery Compressor is used.)
- Small Liquefier : (Cooling capacity can be determined automatically from input power of RC.)

#### Assumption

- If 6 buffer tanks are employed, half inventory should be stored in LHE dewar.

#### Specification

- Liquefier : maximum liquefaction capacity=290 L/h  
⇒ MCB has to be continuously operated to keep this condition.
- Required mass flow : 80 g/sec (410 kW = RC power)
- Half inventory can be liquefied for 4.5 days (within 1 week).

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### Discussion on Storage Scheme

- GHe and LHE mixing storage scheme has a source of unrest shown below from the view point of inventory loss.
  - In the case of severe damage of MCB such that MCB can not be operated within 1.5 days
  - In the case of severe damage of small liquefaction system such as liquefier and LHE dewar.
- Recovery time can be reduced from 1 week to 3 days in the case of GHe storage scheme.
- Manufacturing cost without small liquefaction system is a little bit cheaper than half and half mixing storage scheme.
- Required surface area is almost same each other. (if config. shown P19 is applied)

Storage Scheme	unit : (t-h)	buffer tank	Small liquefaction system	Other, Transport etc.	Total Cost
12 buffer tanks	w/ small liquefier	6.72	0	4.1	10.82
6 buffer tanks	w/ small liquefier	3.36	5.4	2.6	11.36

Storage Scheme	unit : (m <sup>2</sup> )	buffer tank	Small liquefaction system	Other, Transport etc.	Total Area
12 buffer tanks	w/ small liquefier	40m x 25m	8m x 14m (RC)		1263
6 buffer tanks	w/ small liquefier	23m x 25m	30m x 23m (RC, Liquefier, LHe dewar)		1265

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### Summary (1)

#### Power Failure

- Instead of Storage Scheme introduced in TDR, not only LHE dewar but also GHE buffer tanks are employed for preventing loss of He inventory during power failure.
- Recovery compressor (RC) should be located on surface but its capacity should be enough small to be operated using LNG generator during the failure. Several hundreds kW can be acceptable. (MW order can not be acceptable.)
- To perform this, recovery mass flow rate during the failure should be reduced. Enthalpy recovery operation seems effective way to reduce the mass flow rate.
- According to the simulation based on toy model, mass flow rate can be reduced to around 30 g/sec. In this case, if 6 tanks with 250 m<sup>3</sup> are located on surface, resting state of MCS and MCB for 1.5 days can be acceptable.

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### Summary (2)

#### Maintenance and other operation

- When all inventory is recovered for maintenance season, small liquefier is needed. RC can also be applied to small liquefaction system.
- Fraction between Liquid and Gas can be optimized by considering site environmental condition.
  - Recently, we considered 1/2 in Gas and 1/2 in LHE.
  - to be discussed further with Tohoku group.
- Recovery time for the total inventory is within 1 week by using small liquefaction system. To perform this, MCS and MCB have to be operated continuously during recovery mode.
- Tentative stop of the Small liquefaction system such as planned outage can be acceptable. To ensure it, allowable pressure should be 10 bar or so and less heat load into the dewar such as 0.2-0.5 %/day should be used.

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Back Data

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### Detailed comparison

Comparison Item		12 buffer tanks scheme	6 buffer tanks and LHE Dewar scheme
Cryo components for recovery system	buffer tanks	12	6
	recovery compressor	400kW	400kW
	small liquefier	-	280L/h
	LHE dewar	-	42000L
	cryogenic pipe	-	4 cryo pipes (3-5m)
Piping through access tunnel	HP	318.5mm	318.5mm
	MP	508mm	508mm
	LP	406mm	406mm
	LLP	406mm	406mm
	Recovery line	165.2mm	165.2mm
exclusive area on surface(m2)	1265	1265	
necessity for building	-	necessary	
Cost	buffer tanks	6.72	3.36
	recovery compressor	0.7	0.7
	Cold box	-	4.4
	LHE dewar	-	1
	Transportation	1.8	0.9
	unloading crane	0.4	0.4
	Site construction	1.2	0.6
	SUM	10.82	11.36

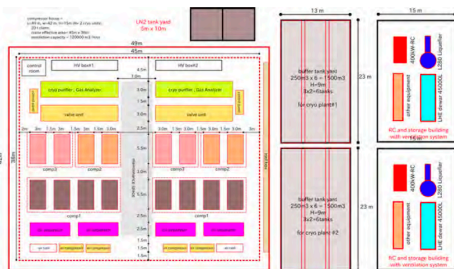
- ILC site-specific utility designs are same for each storage scheme.

- Brief cryogenic equipment is summarized in following table

			Input Power		Specification	Size	Weight		
Surface	MCS	Main Compressor System	5-5.5 MW	6.6kV	Post-2MPa	8 comps	1614 g/sec	(5.7m x W2.8m x H3.3) x 8 sets	13t x 8sets
	RC	Recovery Compressor	370-410 kW	6.6kV	Post-2MPa	1 comp	71.5-85.5 g/sec	(5.5m x W3m x H2.8m) x 1 set	18.5t
	BT	Buffer Tank			250m <sup>3</sup> x (4-2)	22000 L (BLHE)		(L2.3m x W4m x H4.3m) x 6 sets	70 t x 6 sets
	SD	Storage Dewar				44000 L @ LHE		OD: 5m x L: 13m	under investigation
Access Tunnel	SL	Small Liquefier with Turbines		3P200V	290 L/h				
	CE	Cold Evaporator		3P200V	10000 L				
	HP	High Pressure Pipe			Single, SUS304TP-A	not insulated	1606 g/sec, 300K	OD-318.5mm	
	MP	Medium Pressure Pipe			Single, SUS304TP-A	not insulated	1235 g/sec, 300K	OD-508mm	
	LP	Low Pressure Pipe			Single, SUS304TP-A	not insulated	234 g/sec, 300K	OD-406mm	
	LLP	Negative Pressure Pipe			Single, SUS304TP-A	not insulated	136 g/sec, 300K	OD-406mm	
Cryo Cavern	RP	Recovery Pipe			Single, SUS304TP-A	with drain	20g/sec, 80K-300K	OD-165.2mm	
	CR	Cable Rack				LAN Cable, Signal Cable	W600mm x 2 stage		
	Upper MCB	300K to 70K Main Cold Box		3P200V	see Flow diagram and TS diagram		L: 8.1m x W: 3.7m x H: 3.5m	34 t	
	Lower MCB	70K to 1.8K Main Cold Box		3P200V	see Flow diagram and TS diagram		L: 1.4m x W: 3.5m x H: 4m	50 t	
Access Tunnel to ML	SCR	Sub Control Box for MCB		3P200V, 2P100V			L: 5m x W: 0.5m x H: 1m		
	TCR	Tentative Control Room		2P100V			L: 4m x W: 2.5m x H: 2.5m		
	TRT	Transfer Tube			6 pipes in one Jacket / 2 for 70K shield / 2 for 5K shield / 2 for 2K shield		Jacket OD-650A-750A		
					under investigation	70K shield (suppl): OD-72mm/80mm			
					under investigation	5K shield (suppl): OD-56mm/70mm			
					under investigation	2K (suppl): OD-70mm/300mm			

- small equipment described as follows are not listed in the table.
  - air compressor for control valves
  - cryo purification system
  - Gas analyzer
  - dryer
  - vacuum pump
  - 6.6 kV High voltage control unit for MCS
  - cooling water system for MCS and turbines installed in MCB
  - etc...

### Surface Layout for 2 plants



### Evaporated mass vs Buffer tank volume

Recovery Time and Buffer tank volume are shown at around 30 g/sec.

HE Inventory (kg / plant)	evaporated mass flow (kg/sec)	recovery time (h)	Number of 250m <sup>3</sup> Buffer tank required	contingency
40K shield	246	0.03	2	0.1
5K shield	1068	0.03	10	0.4
2K SRF	6901	0.03353	57	2.4
1/3 inventory	2738	0.03	25	1.1
1/2 inventory	4108	0.03	38	1.6
Total inventory	8215	0.03291	69	2.9

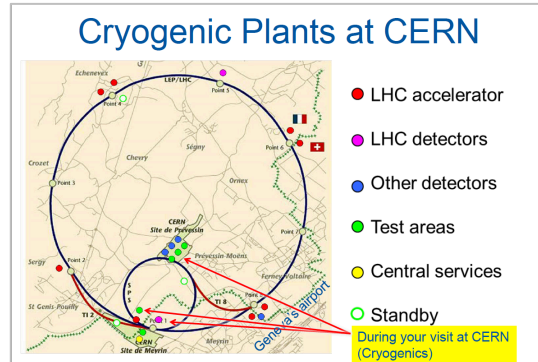
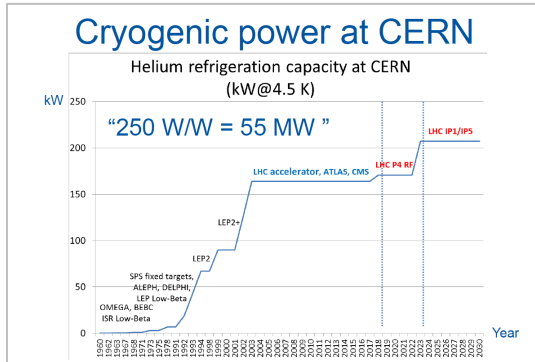
Time to fill up at 30 g/sec.

- 4+2=6 tanks (1/3 inventory) ⇒ 25H
- 6+2=8 tanks (1/2 inventory) ⇒ 38H
- 11 tanks (total inventory) ⇒ 69H

Further detailed dynamic simulation will be performed continuously instead of using TOY model.



Attachment 4. Cryogenics at CERN (by D. Delicaris: briefly extracted, 25-11-2013)



### Management of Cryogenic Fluids

- Total HELIUM inventory at CERN: 170'000 kg
- LHC (accelerator & detectors) helium full inventory: 136'000 kg
- Additional strategic permanent storage during operation: 15'000 kg

- LHC (accelerator & detectors) liquid NITROGEN needs for a full cool down: 11'500 ton
- (LHC accelerator full cool down: 10'000 ton in 33 continuous days; equivalent to 500 standard transportable containers delivered by industrial suppliers)

- In situ helium liquefaction for central services (up to 350 000 liter per year) and distribution by means of mobile containers ranging from 100 to 2'000 liter (users without dedicated cryogenic plant)

### Helium & Nitrogen Storage

Storage infrastructure (in brackets: capacity dedicated to LHC)

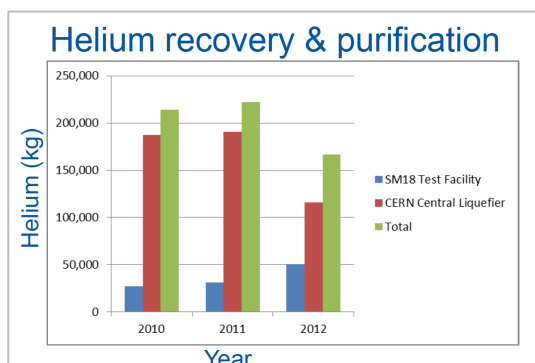
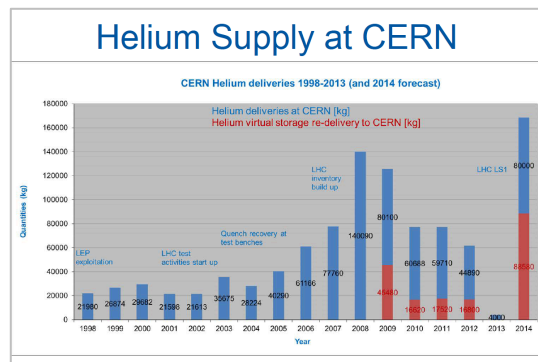
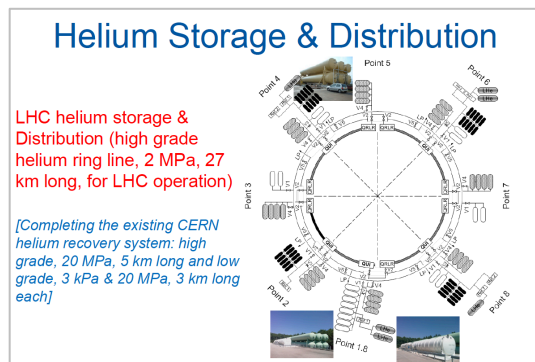
Gas & liquid helium storage capacity at CERN

Gas tank capacity [m³]	250 (at 2.1 MPa)	80 (at 1.5 & 2.1 MPa)
Number of units at CERN	58 (58)	65 (40)

Liquid tank capacity [liter]	120'000 (fixed)	25'000 (fixed)	11'000 (mobile)	6'000 (fixed)
Number of units	6	1	2	1

Liquid nitrogen storage capacity at CERN

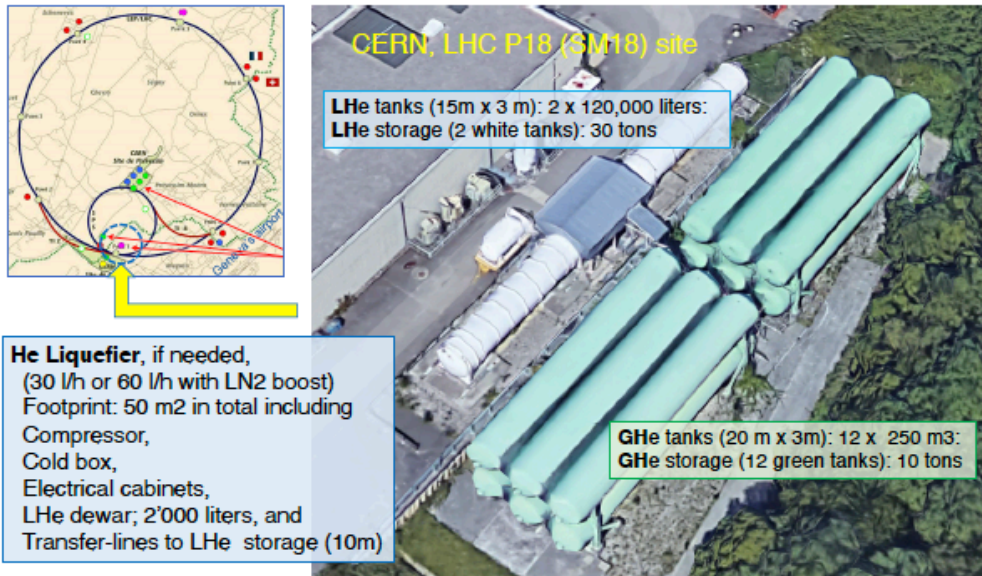
Container capacity [liter]	50'000	40'000	27'000	20'000	15'000	10'000	6'000
Number of units	14 (13)	2	1	2	2	1	7



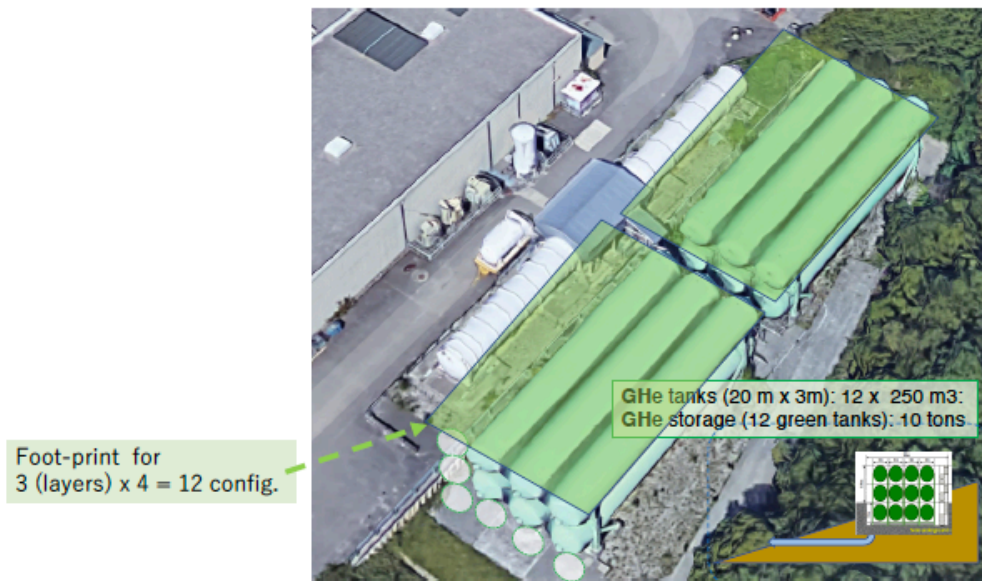
### Summary

- Cryogenics at CERN: since 1960's for cooling components on accelerators, physics detectors & test facilities
- Very large spectrum of cryogenic engineering & working conditions (applications and refrigeration capacity @ T K)
- Implementation & successful operation of "state of the art" industrial cryogenic equipment at the edge of the present technology: The LHC cryogenic system (26.7 km, cooling @1.8 K, 80 ton of He II)
- Procurement and management of very important cryogen inventory (helium and nitrogen)
- Cryogenic operation availability to the users:
  - Before the LHC era: nearly 590'000 running hours have been cumulated over 15 years with a mean availability rate of 99%
  - The present LHC mean availability is already situated around 95%; progress is very impressive! Peaks at 99% are observed for several week periods!

Attachment 5: He Inventory Configuration at CERN LHC P18 (SM18)



Current Foot-Print: LHe (2) and GHe (2 x 2 x 3) Configuration



Image, Foot-Print: GHe (2 x 3 x 4) Tanks Configuration.