

# RF DIPOLE DESIGN UPDATE

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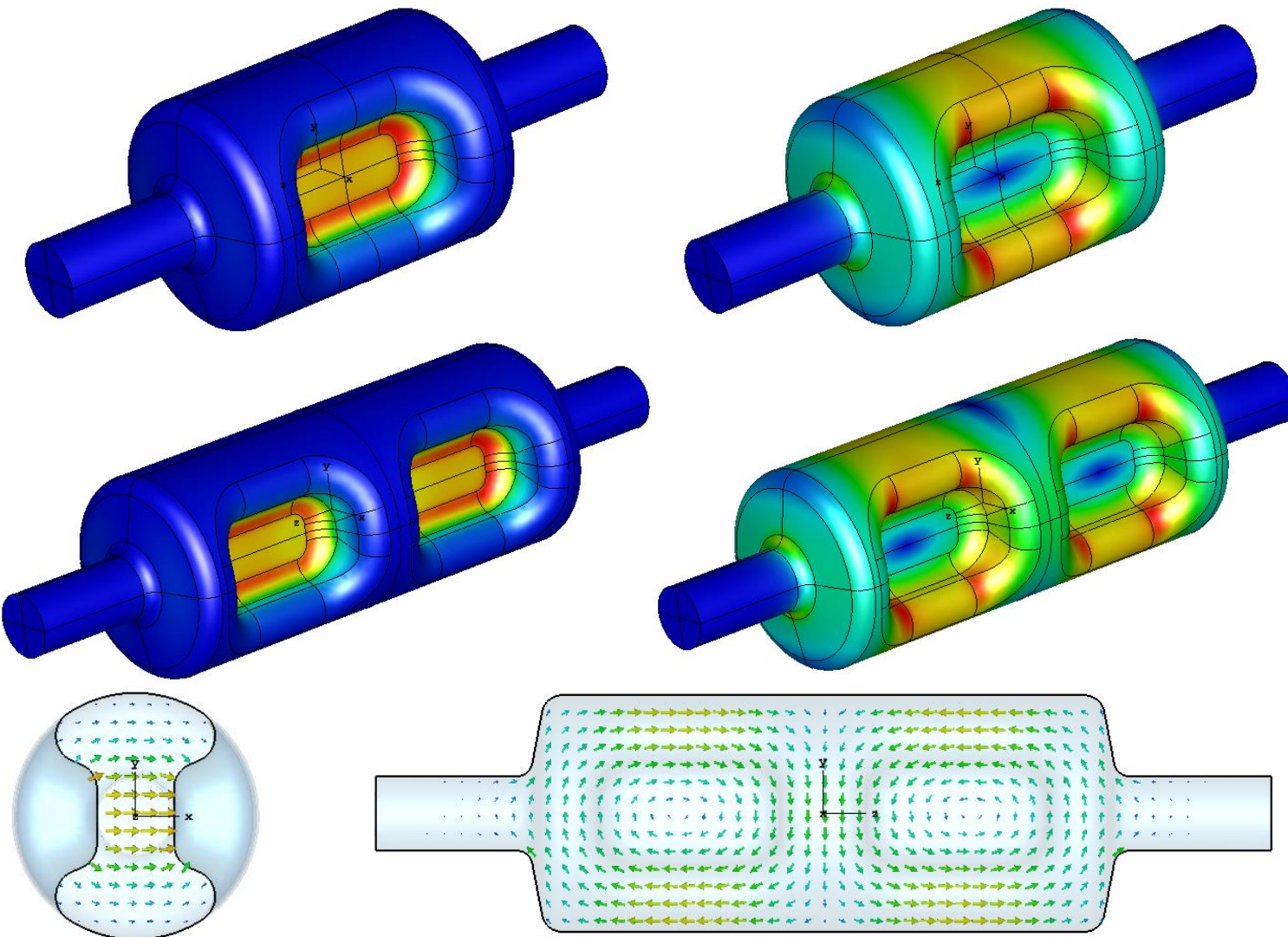
**and**

**Thomas Jefferson National Accelerator Facility**

# Outline

- 1.3 GHz RF-Dipole cavity design
- Pole separation
- 1.3 GHz RFD crab cavity for ILC
- Fundamental power coupler
- Higher order modes and impedances
- Mechanical analysis
  - Stress analysis
  - Lorentz detuning
  - Pressure sensitivity
- Summary

# 1.3 GHz RFD Cavity Design



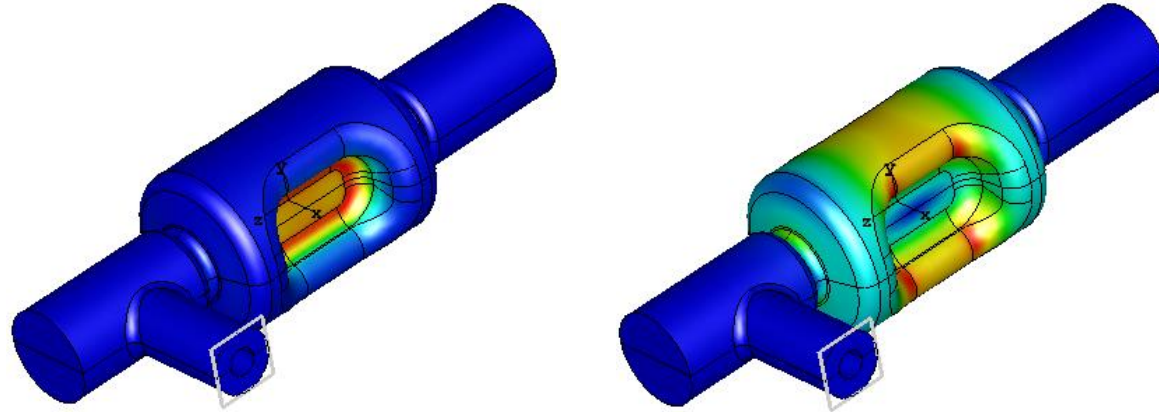
Property	1-cell	2-cell
Operating frequency [GHz]	1.3	1.3
SOM [GHz]	–	1.188
1 <sup>st</sup> HOM [GHz]	2.069	1.932
$E_p/E_t^*$	4.45	4.57
$B_p/E_t^*$ [mT/(MV/m)]	9.09	8.92
$B_p/E_p$ [mT/(MV/m)]	2.04	1.95
$G$ [ $\Omega$ ]	142.5	147.3
$R/Q$ [ $\Omega$ ] ( $V^2/P$ )	182.2	370.7
$R_t R_s$ [ $\Omega^2$ ] ( $V^2/P$ )	$2.6 \times 10^4$	$5.5 \times 10^4$
Reference length $V/E_t = \lambda/2$ (mm)	11.54	11.54
$V_t$ [MV]	1.0	2.0
$E_p$ [MV/m]	38.58	39.66
$B_p$ [mT]	78.85	77.36
Pole separation, beam aperture (mm)	36	36
Cavity Length [mm]	172.32	297.4
Cavity Diameter [mm]	128.6	114.5
Pole Length [mm]	85	85

# 1.3 GHz RFD - 36 vs 30 mm Pole Separation

Property	1-cell	2-cell
Operating frequency [GHz]	1.3	1.3
SOM [GHz]	–	1.188
1 <sup>st</sup> HOM [GHz]	2.069	1.932
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Operating frequency [GHz]	1.3	1.3
SOM [GHz]	–	1.201
1 <sup>st</sup> HOM [GHz]	2.085	1.960
$E_p/E_t^*$	3.84	3.98
$B_p/E_t^*$ [mT/(MV/m)]	8.04	7.94
$B_p/E_p$ [mT/(MV/m)]	2.10	1.99
$G$ [ $\Omega$ ]	133.0	137.2
$R/Q$ [ $\Omega$ ] ( $V^2/P$ )	280.2	556.7
$R_t R_s$ [ $\Omega^2$ ] ( $V^2/P$ )	$3.7 \times 10^4$	$7.6 \times 10^4$
Reference length $V/E_t = \lambda/2$ (mm)	11.54	11.54
$V_t$ [MV]	1.0	2.0
$E_p$ [MV/m]	33.3	34.54
$B_p$ [mT]	69.7	68.82
Pole separation, beam aperture (mm)	30	30
Cavity Length [mm]	172.32	297.4
Cavity Diameter [mm]	107.4	109.4
Pole Length [mm]	85	85

# 1.3 GHz RFD Cavity

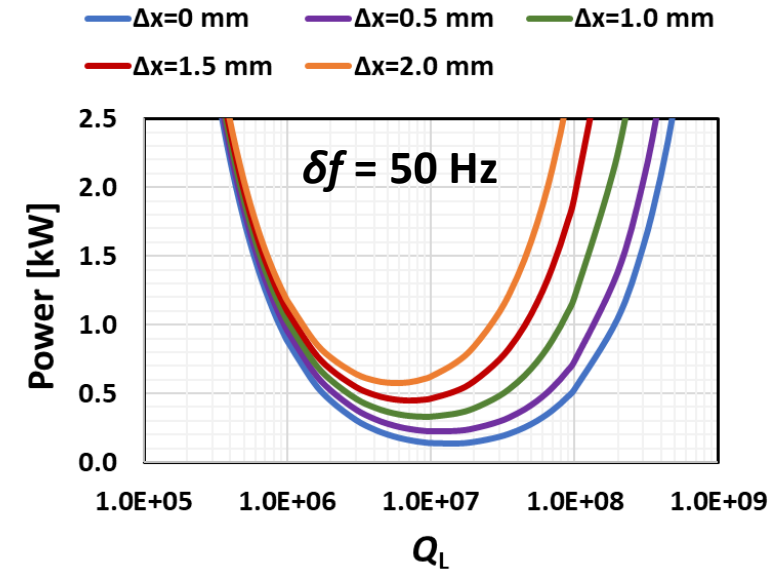
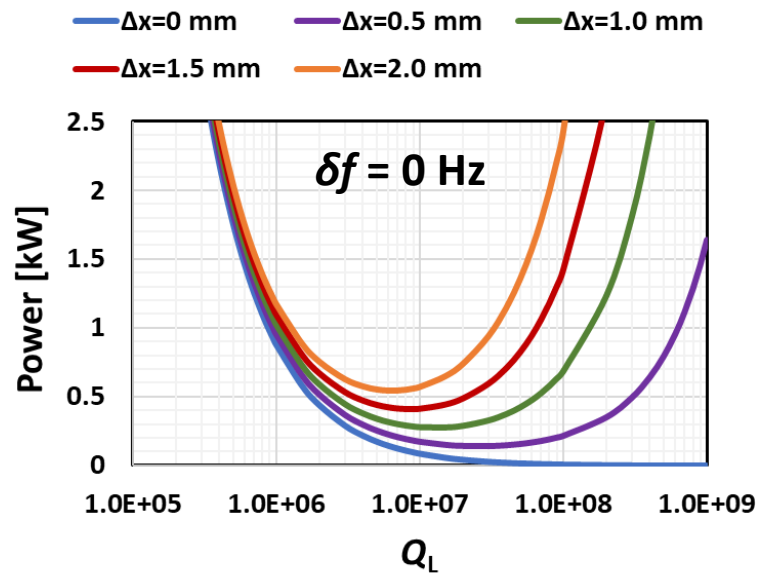
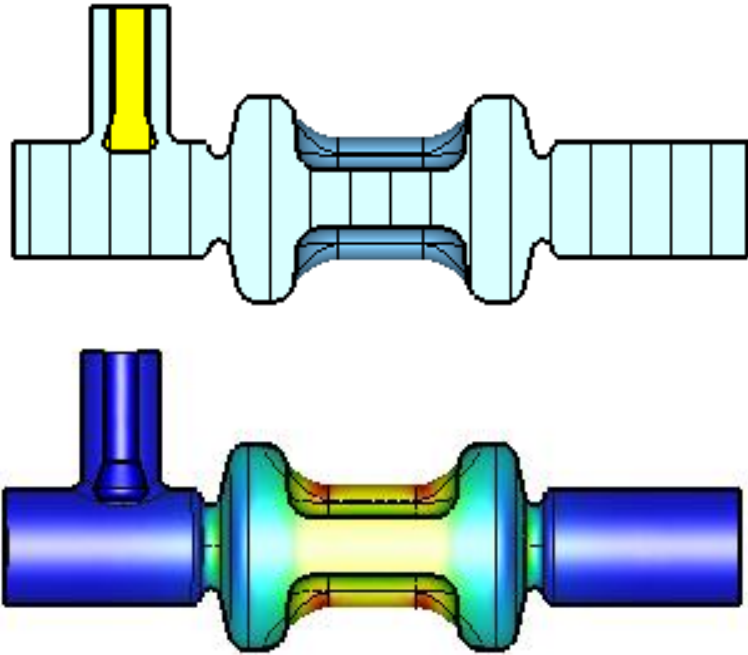


- Pole separation – 30 mm
  - Decided this pole separation from the past experience, to guarantee good high pressure rinsing
- Beam aperture – 40 mm
  - For HOM mode propagation

	250 GeV	1 TeV
$V_t$ per cavity [MV]	1.0	1.0
Total $V_t$ [MV]	1.845	7.4
Number of cavities	2	8

Property	1-cell	
Operating frequency [GHz]	1.3	
SOM [GHz]	–	
1 <sup>st</sup> HOM [GHz]	2.08	
$E_p/E_t^*$	3.87	
$B_p/E_t^*$ [mT/(MV/m)]	8.02	
$B_p/E_p$ [mT/(MV/m)]	2.07	
$G$ [ $\Omega$ ]	133	
$R/Q$ [ $\Omega$ ] ( $V^2/P$ )	285	
$R_t R_s$ [ $\Omega^2$ ] ( $V^2/P$ )	$3.8 \times 10^4$	
Reference length $V/E_t = \lambda/2$ (mm)	11.54	
$V_t$ [MV]	1.0	1.15
$E_p$ [MV/m]	34	39
$B_p$ [mT]	70	80
$P_{diss}$ [W] ( $R_s = 20$ n $\Omega$ )	0.53	0.7
Pole separation (mm)	30	
Beam aperture (mm)	40	
Cavity Length [mm]	380	
Cavity Diameter [mm]	129.0	
Pole Length [mm]	85	

# Fundamental Power Coupler



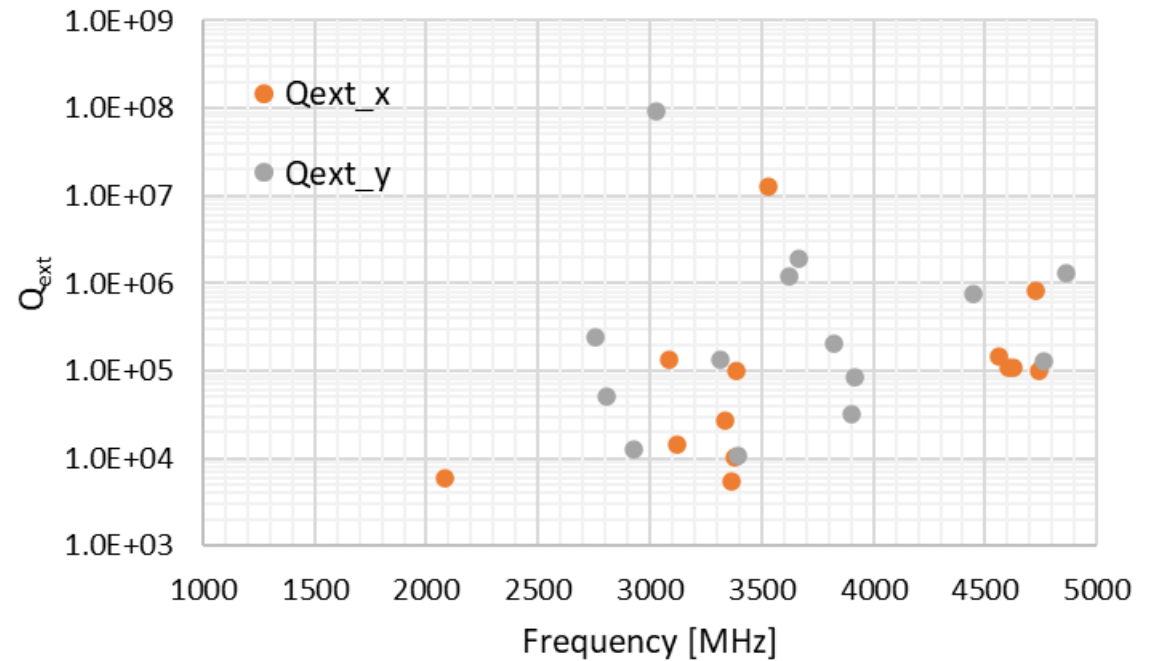
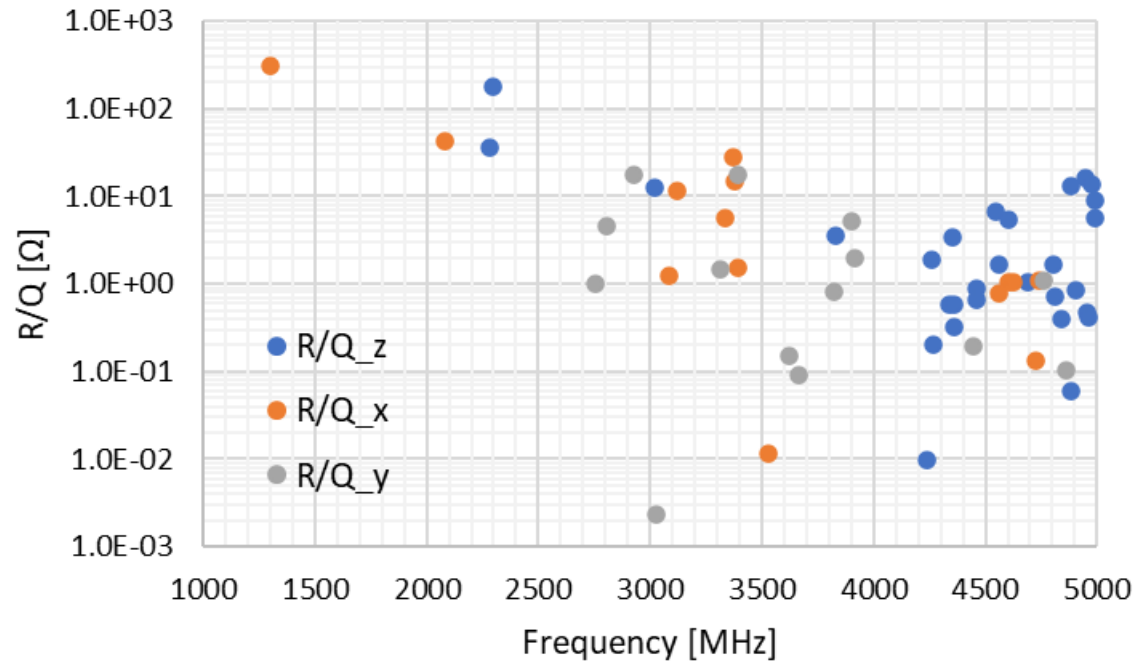
Beam and cavity parameters:

- $I_b = 10$  mA
- $R/Q = 285 \Omega$  ( $V^2/P$ )
- $V_t = 1$  MV

- Coupling using coaxial antenna
  - Similar to LCLS II power coupler
- $Q_{\text{ext}} = 1.0 \times 10^7$  at  $\Delta x = 0.5$  mm  $\delta f = 50$  Hz
- RF power  $\approx 500$  W
- RF heating at the Cu probe at 1 MV – 65 mW

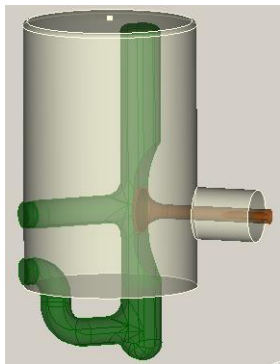
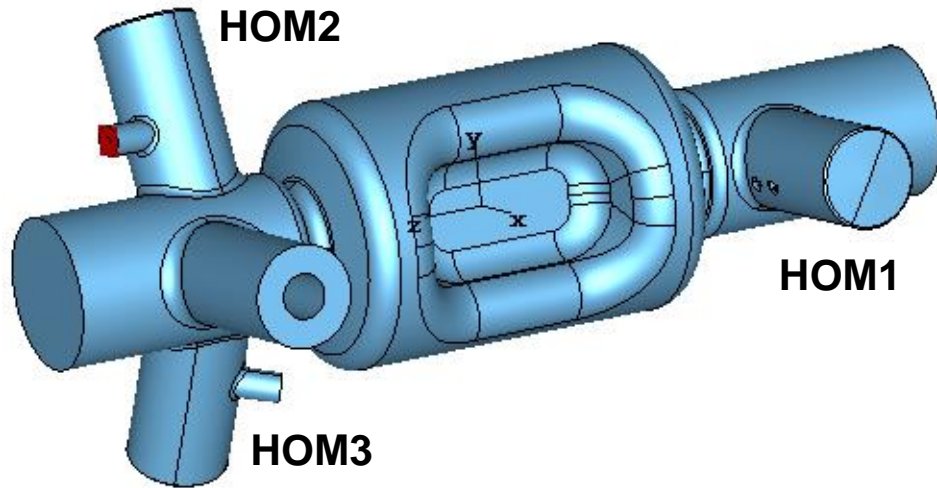
# Higher Order Modes

- Impedance threshold:  $Z_x = 48.8 \text{ M}\Omega/\text{m}$  and  $Z_y = 61.7 \text{ M}\Omega/\text{m}$
- Impedance threshold per cavity:  $Z_x = 5.42 \text{ M}\Omega/\text{m}$  and  $Z_y = 6.85 \text{ M}\Omega/\text{m}$  (9 cavities per side)



- For longitudinal modes need to evaluate loss factor for short range wakefields with  $\sigma_z = 0.3 \text{ mm}$

# Higher Order Mode Damping



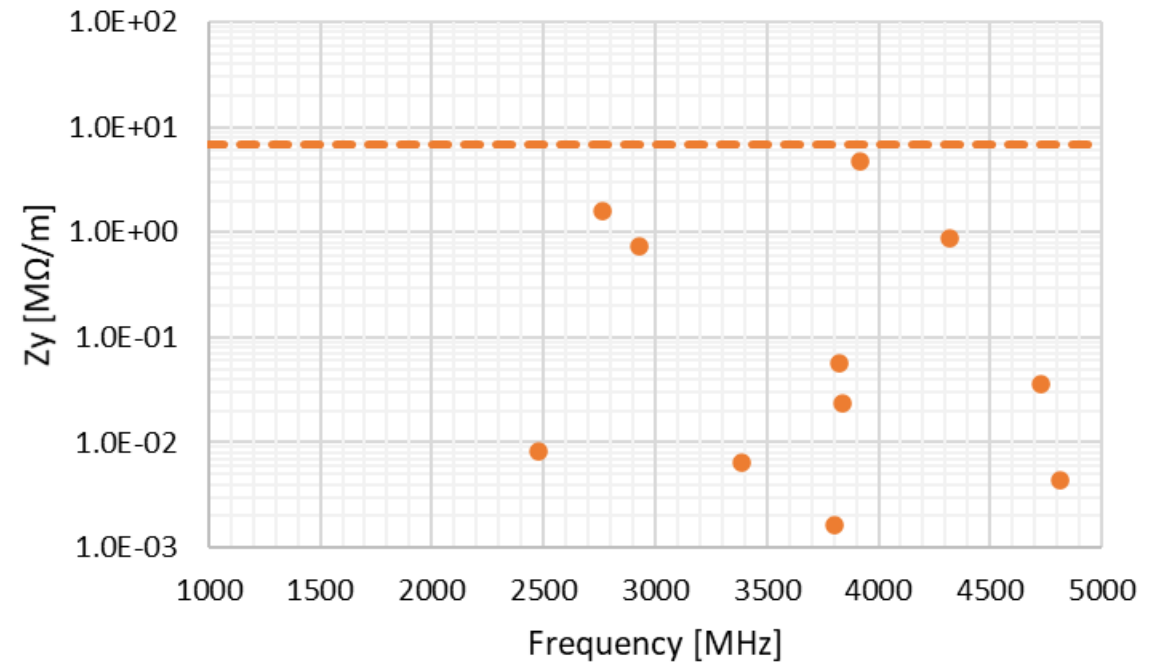
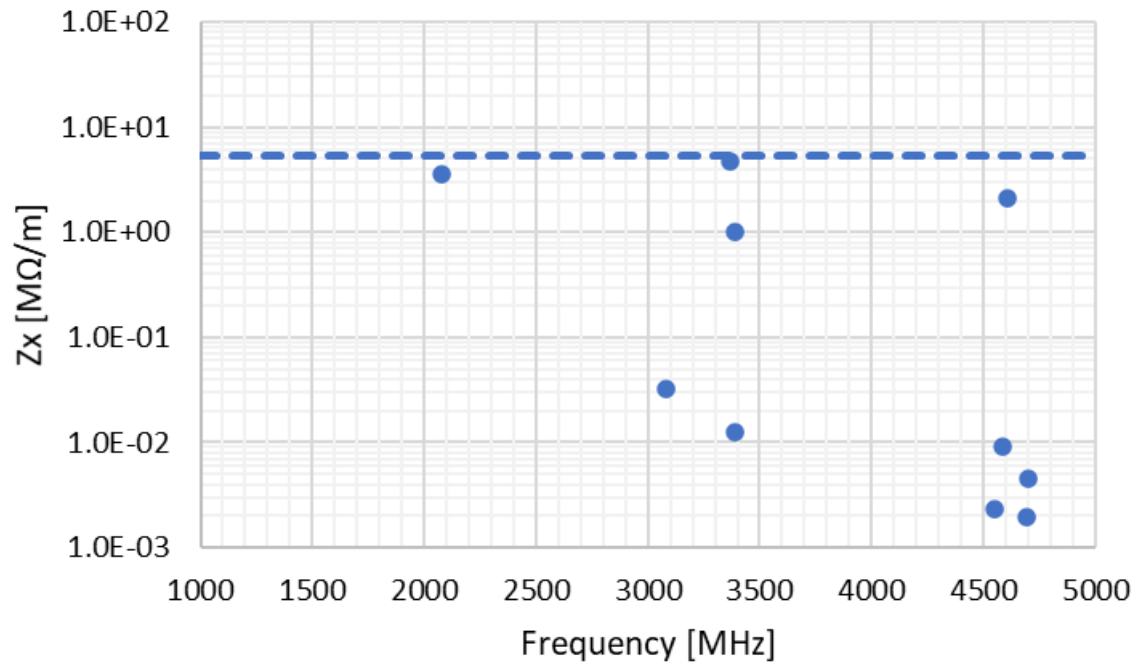
TESLA type HOM coupler

- 1<sup>st</sup> concept: Damping using 3 TESLA type HOM couplers
  - Damper design used in the LCLS II cavities
  - All the couplers are placed on the beam pipe
- Planning to investigate damping using the scaled LHC-RFD HOM coupler
- Waveguide damping is also a possible option
- Final choice will be decided based on
  - RF properties including HOM power
  - Engineering and manufacturing complexity



# Higher Order Mode Damping

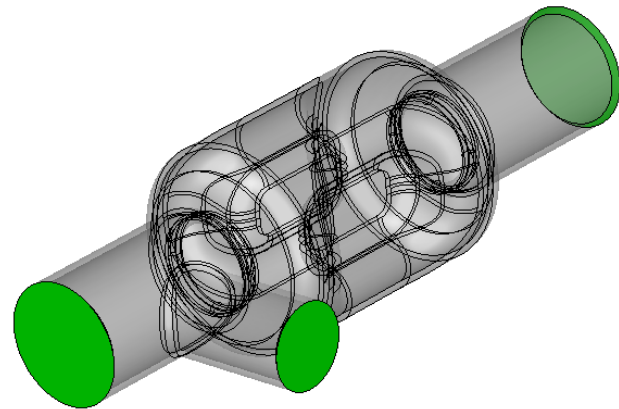
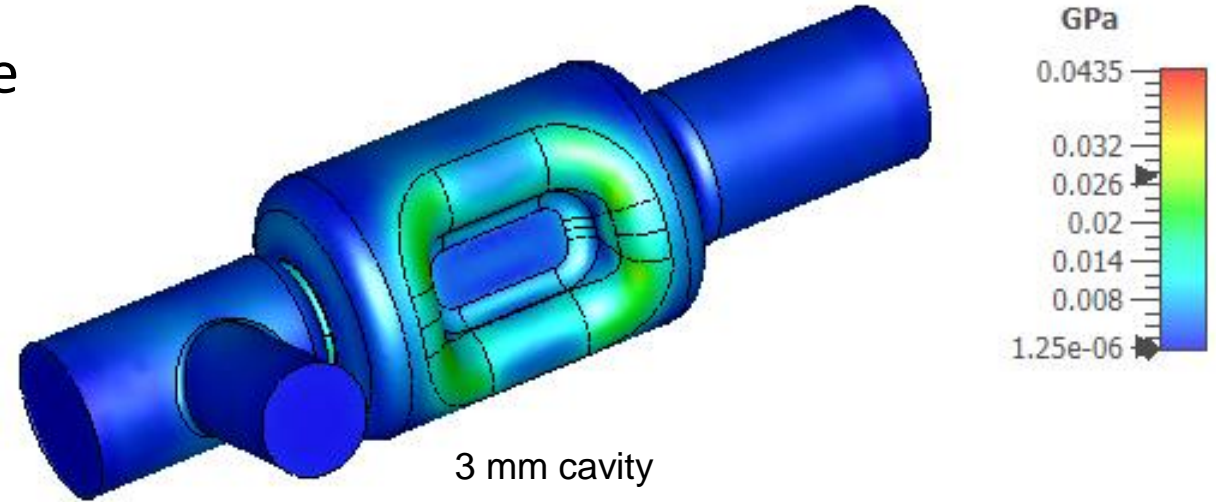
- Impedance threshold per cavity:  $Z_x = 5.42 \text{ M}\Omega/\text{m}$  and  $Z_y = 6.85 \text{ M}\Omega/\text{m}$



- Impedances calculated using circuit definition
- Need to evaluate up to  $\sim 20 \text{ GHz}$

# Stress Analysis

- Analysis at 2.2 atm external pressure
- Nb material properties at room temperature
  - (JLAB-TN-09-002 – C100 Cryomodule Niobium Cavity Structural Analysis)
  - Young's modulus – 82.7 GPa ( $1.2 \times 10^7$  psi)
  - Poisson's ratio – 0.38
- Allowable stress < 43.5 MPa



Boundary conditions

- Maximum stresses

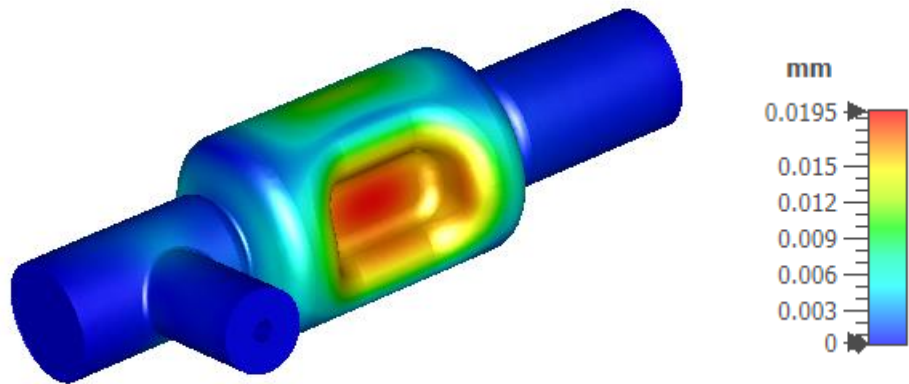
Cavity Thickness [mm]	Max. Stress [MPa]
2.5	36
3.0	27

- Initial analysis shows cavity doesn't require stiffening

# Mechanical Analysis

## Pressure Sensitivity

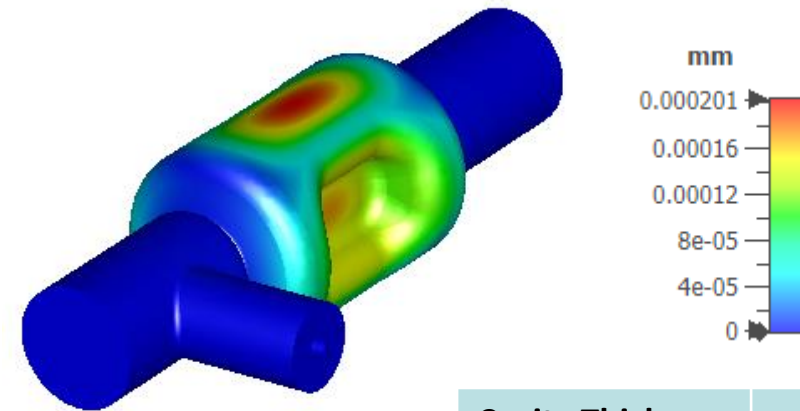
- Nb material properties at room temperature
  - Young's modulus – 82.7 GPa ( $1.2 \times 10^7$  psi)
  - Poisson's ratio – 0.38
- Stiffening at poles can reduce pressure sensitivity



Cavity Thickness [mm]	$df/dP$ [Hz/mbar]
2.5	728
3.0	509

## Lorentz Detuning

- Nb material properties at cryo temperature
  - Young's modulus – 123 GPa ( $1.79 \times 10^7$  psi)
  - Poisson's ratio – 0.38
- Lorentz detuning can be reduced by tuner
  - Tuning by push/pull at top and bottom of the cavity

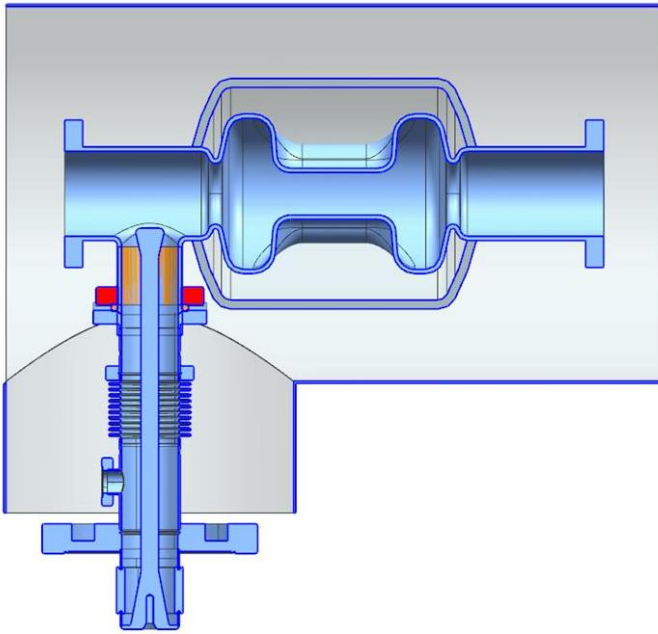


Stored energy = 0.45 J at 1 MV

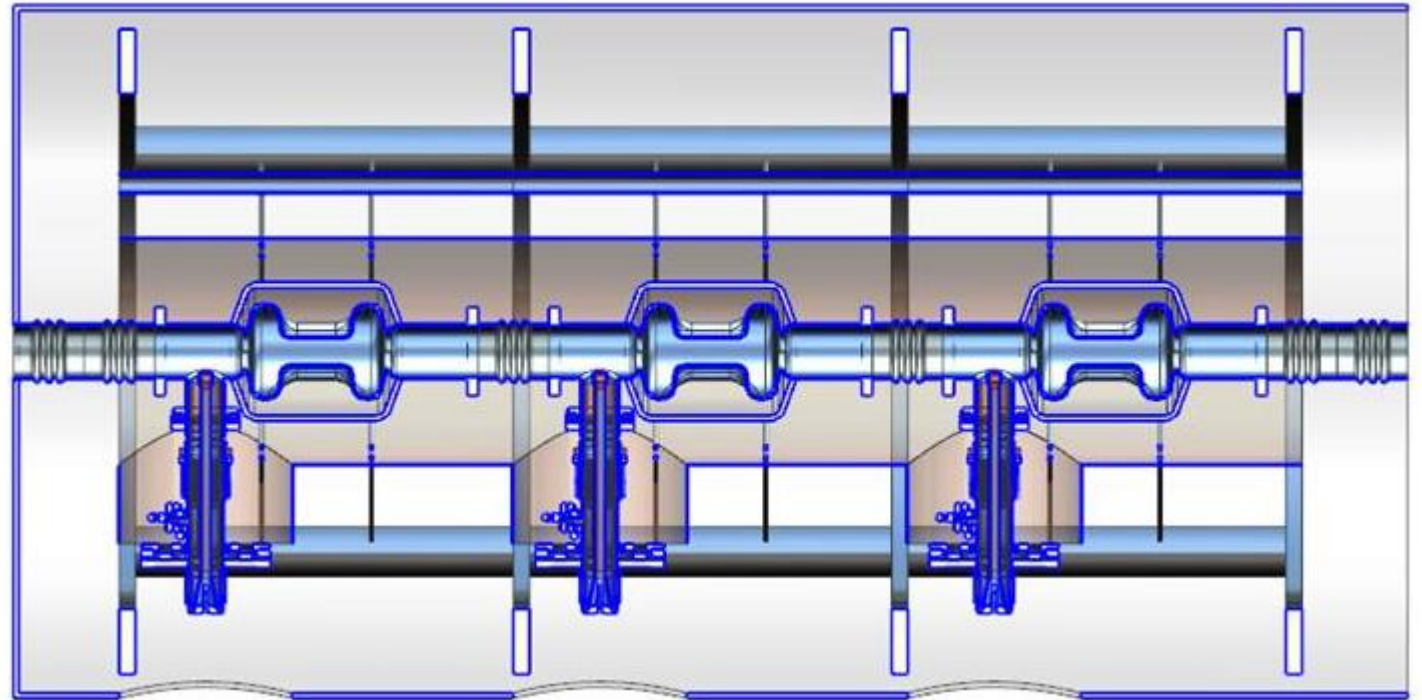
Cavity Thickness [mm]	$k_L$ [kHz/(MV) <sup>2</sup> ]
2.5	-7.44
3.0	-5.04

# Conceptual He Vessel and Cryomodule Design

- Cavity thickness – 3mm
- 3 cavities per cryomodule
- Second beam pipe:
  - 20 mm beam pipe
  - Outside the He vessel and within the cryomodule

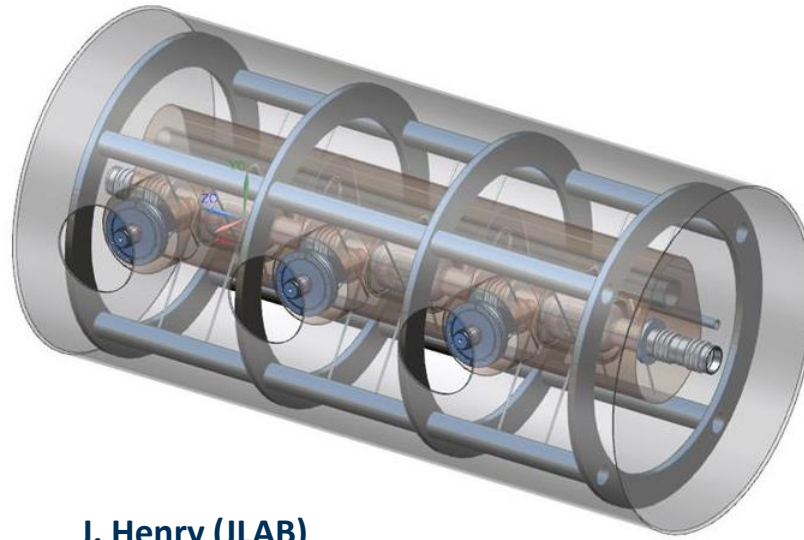
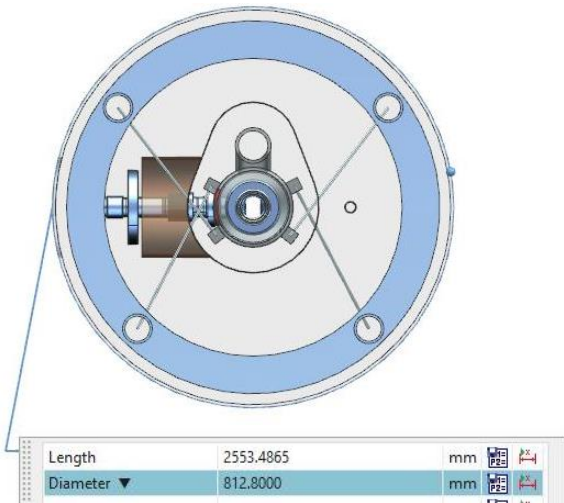
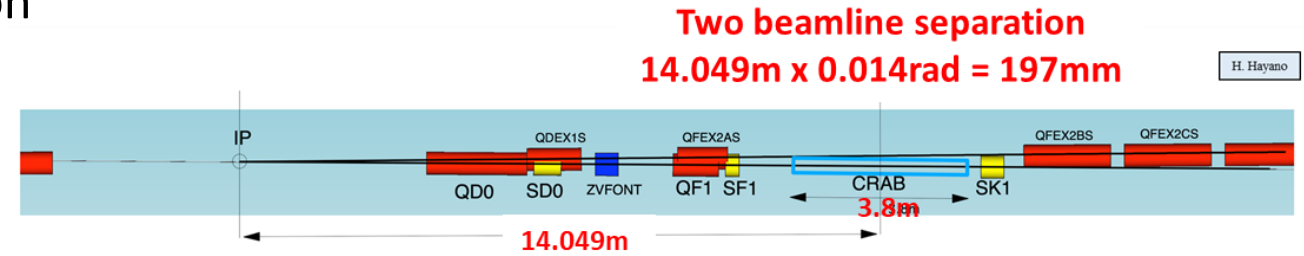


J. Henry (JLAB)



# Conceptual He Vessel and Cryomodule Design

- 1 cryomodule for 1.845 MV at 250 GeV
  - 3 cavities in a single cryomodule allow operation with a cavity failure
- 3 cryomodules for 7.4 MV at 1 TeV
- Cryomodule size: length  $\sim 1.64$  m and diameter  $\sim 0.82$  m
- Design concept follows JLab C100 cryomodule



J. Henry (JLAB)



# Summary

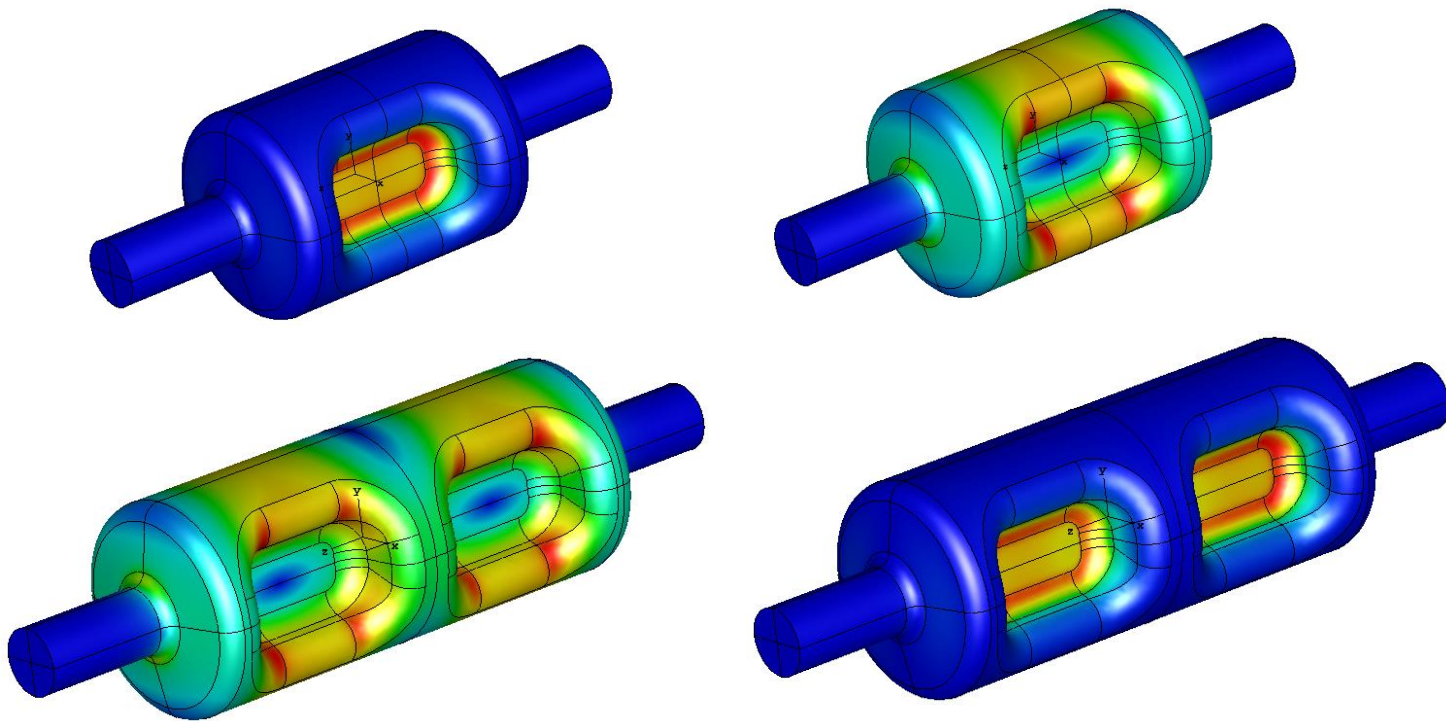
- Current work focused on the single cell 1.3 GHz RFD design for the ILC crab cavity design
  - 2-cell cavity design can be considered
- Cavity design is evaluated with 30 mm pole separation and 40 mm beam aperture
- Initial cavity design is completed with FPC
- An acceptable HOM damping mechanism is identified and further options will be evaluated
  - Longitudinal effects to be evaluated
- Preliminary mechanical analysis is completed

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## Back Up Slides

# Cavity Design

- 30 mm beam aperture
- Two designs options
  - Single cell cavity
  - 2 cell cavity

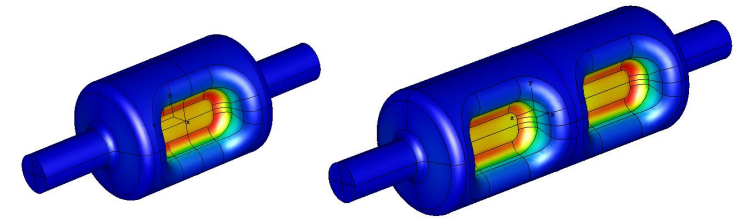
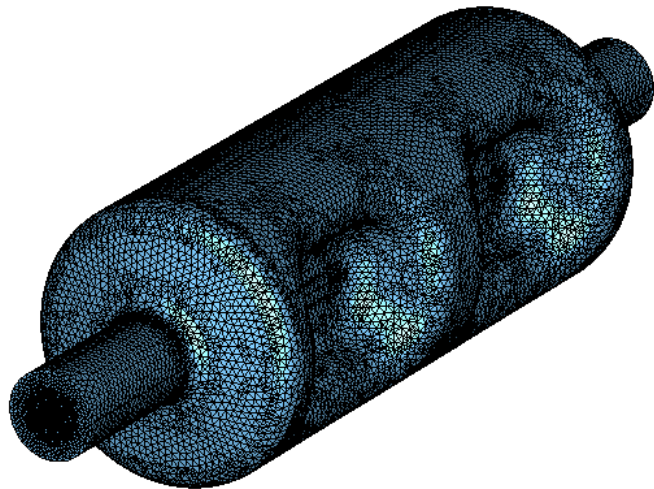


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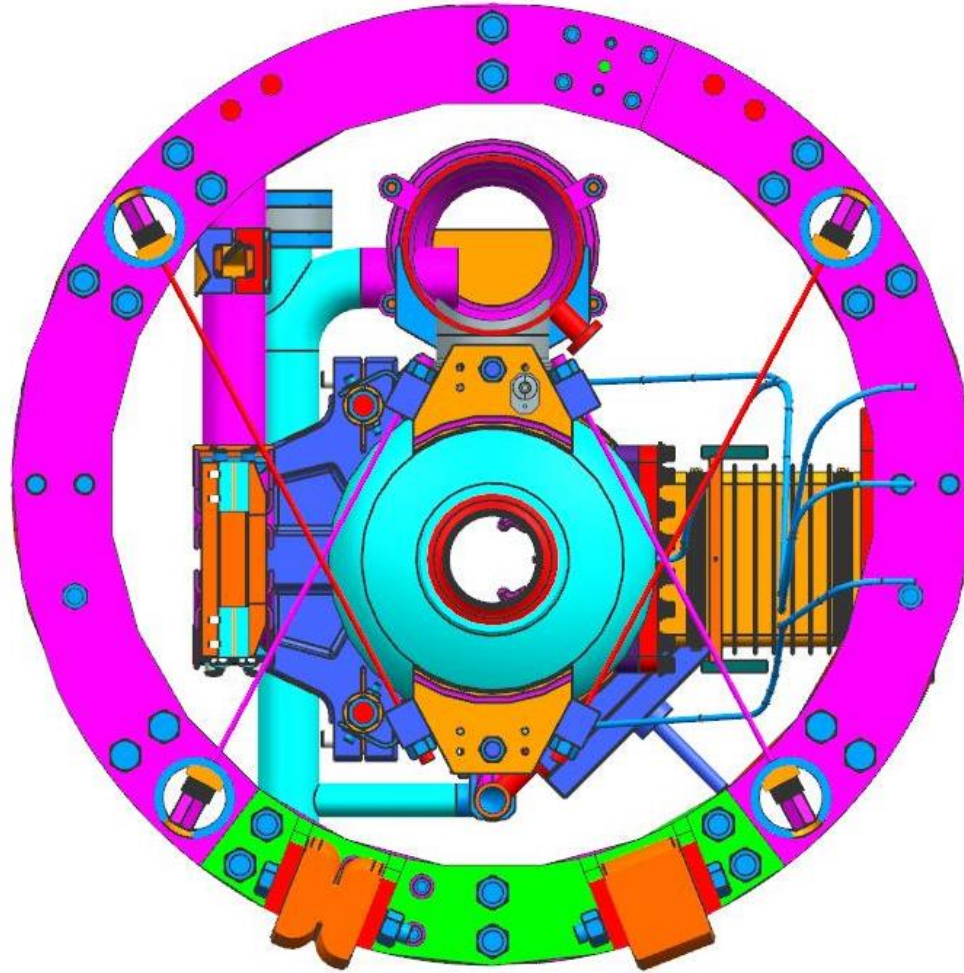
# Multipole Components

- Higher order multipole components for the bare cavity
- Requires a finer mesh along the beam center



Component	Units	1-cell	2-cell
$V_z$	[V]	0.575	-77.25
$V_t$	[V]	1.0E+06	1.0E+06
$b_0$	[mT/m <sup>2</sup> ]	0	0
$b_1$	[mT/m]	3.3	3.3
$b_2$	[mT]	-0.0013	-0.00045
$b_3$	[mT m]	2275.8	2106.6
$b_4$	[mT m <sup>2</sup> ]	9.2	3.2
$b_5$	[mT m <sup>3</sup> ]	-1.39E+6	-1.43E+6
$b_6$	[mT m <sup>4</sup> ]	-4.83E+4	-1.68E+4
$b_7$	[mT m <sup>5</sup> ]	-1.97E+9	-1.89E+9

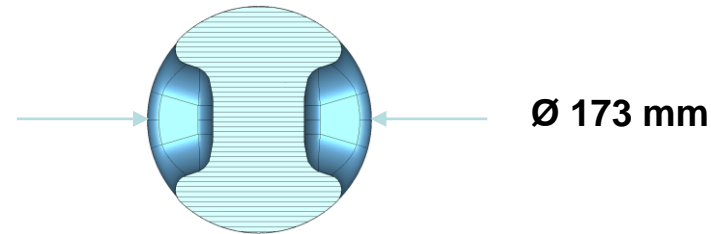
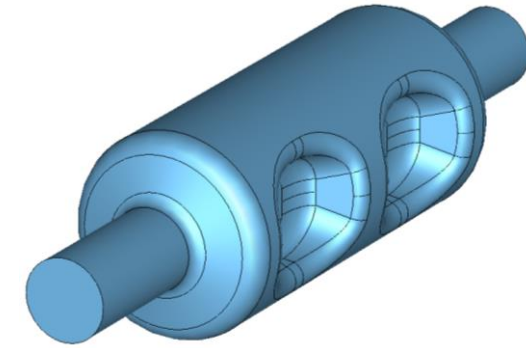
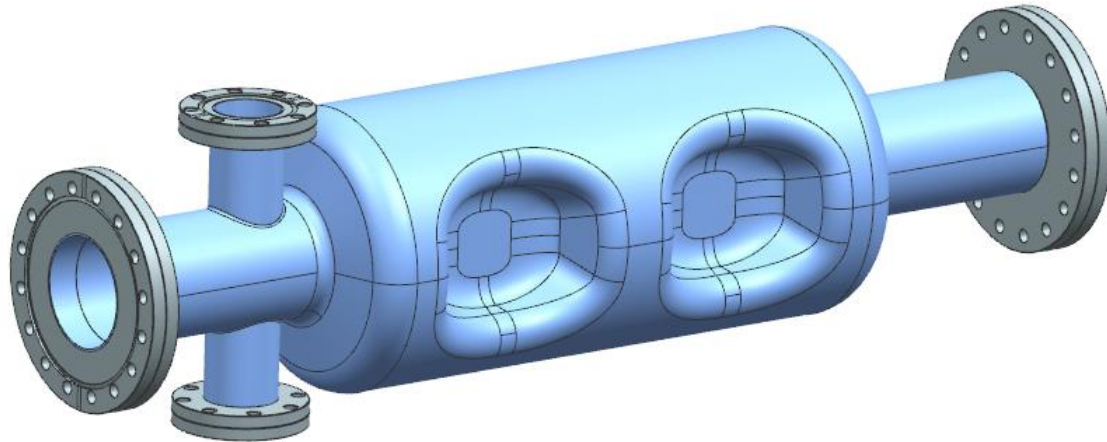
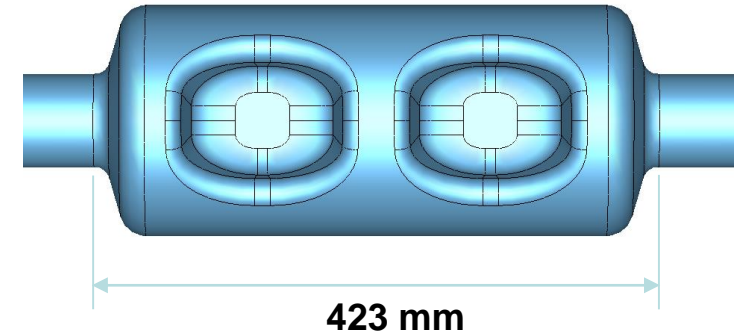
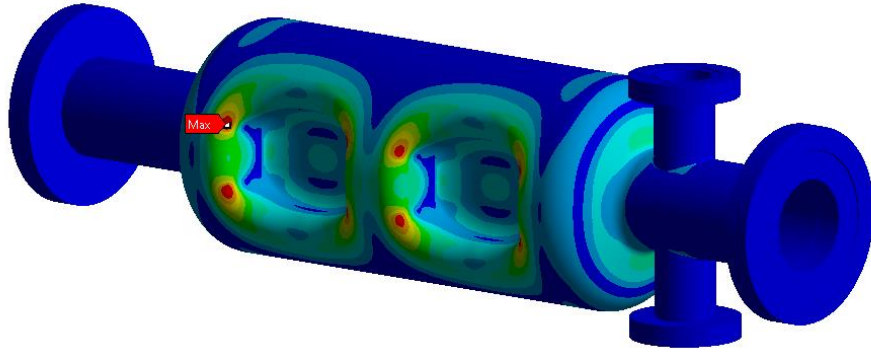
# C100 Cryomodule Design



# Final Design for JLEIC Crabbing System - 952 MHz 2-cell RFD

A: Static Structural  
Equivalent Stress  
Type: Equivalent (von-Mises) Stress  
Unit: MPa  
Time: 1

54.048 Max  
48.043  
42.037  
36.032  
30.027  
24.021  
18.016  
12.011  
6.0056  
0.00028533 Min



Subashini De Silva, HyeKyoung Park

Supported by grant from the  
state of Virginia through SURA

# 952 MHz RFD - Fabrication in Progress

- Material cost – sheet Nb forming instead of machining
- Avoid weld seams at high mechanical stress area and high surface magnetic field area
- Use of simple weld only – high production yield
- Strategy relevant to final cavity with HOM dampers

Subashini De Silva, HyeKyoung Park

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