

# RF DIPOLE DESIGN UPDATE

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**and**

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# Outline

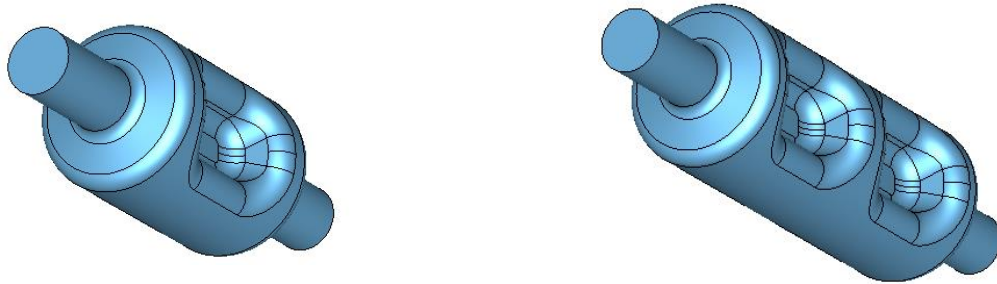
- 1.3 GHz RFD crab cavity design options for ILC
- Fundamental power coupler
- Higher order modes and impedances
- Multipacting analysis
- Mechanical analysis
- Preliminary cryomodule layout
- Summary

# Main Goals of the Study

- Transverse voltage: 1.845 MV for 250 GeV and 7.4 MV for 1 TeV
- Cryostat length flange to flange < 3.25 m
- Peak surface fields:  $E_p < 45$  MV/m and  $B_p < 80$  mT
- Total transverse impedance threshold:
  - Horizontal: 48.8 M $\Omega$ /m
  - Vertical: 61.7 M $\Omega$ /m

# 1.3 GHz RFD Cavity Design

- Pole separation – 25 mm
- Beam aperture – 30 mm
- Two cavity options considered: 1-cell and 2-cell

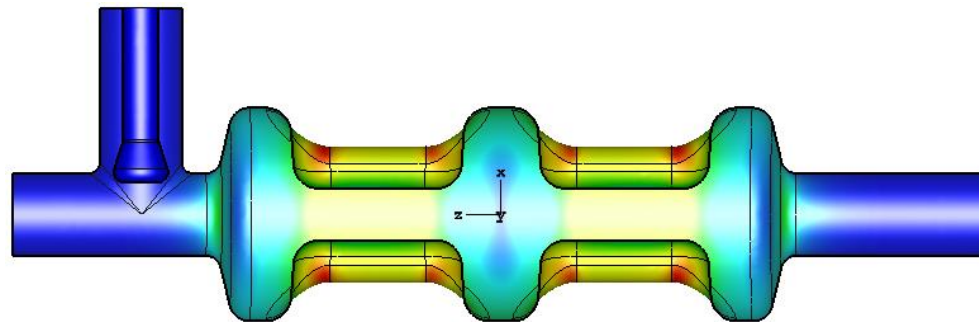
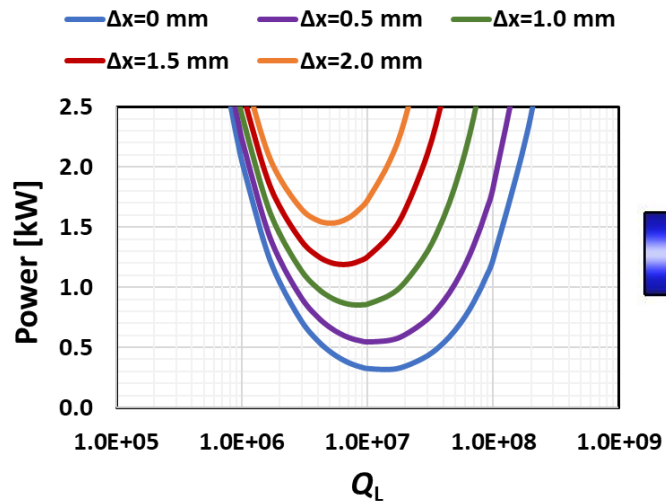
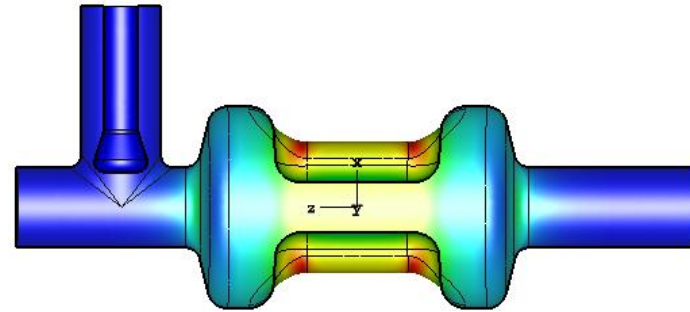
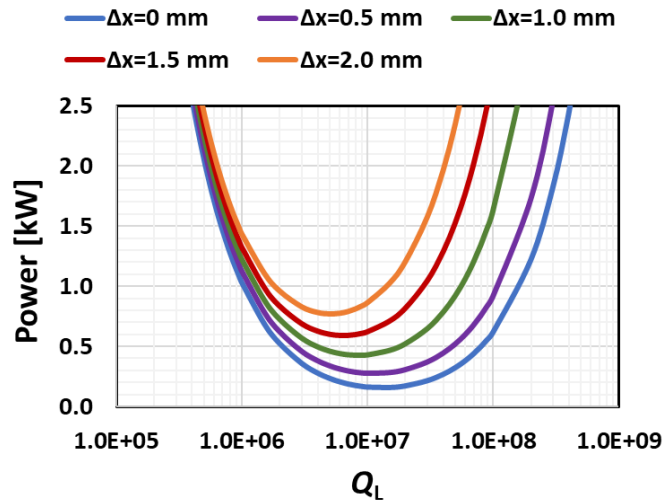


- Meet peak surface field requirements:  $E_p < 45$  MV/m and  $B_p < 80$  mT

	250 GeV		1 TeV	
Cavity type	1-cell	2-cell	1-cell	2-cell
Max $V_t$ per cavity [MV]	1.35	2.70	1.35	2.70
Total $V_t$ [MV]	1.845		7.4	
Number of cavities	2	1	6	3
$V_t$ per cavity [MV]	0.9225	1.845	1.234	2.467

Property	1-cell	2-cell
Operating frequency [GHz]	1.3	1.3
SOM [GHz]	–	1.198
1 <sup>st</sup> HOM [GHz]	2.142	2.039
$E_p/E_t^*$	3.83	3.85
$B_p/E_t^*$ [mT/(MV/m)]	6.84	6.84
$B_p/E_p$ [mT/(MV/m)]	1.79	1.78
$G$ [ $\Omega$ ]	129.9	132.2
$R/Q$ [ $\Omega$ ] ( $V^2/P$ )	444.8	892.7
$R_t R_s$ [ $\Omega^2$ ] ( $V^2/P$ )	$5.78 \times 10^4$	$1.18 \times 10^4$
Reference length $V/E_t = \lambda/2$ [mm]	115.3	115.3
$V_t$ [MV]	1.35	2.70
$E_p$ [MV/m]	44.8	45.0
$B_p$ [mT]	80.1	80.0
Pole separation [mm]	25	
Beam aperture [mm]	30	
Cavity Length [mm] (flange-to-flange)	310	450
Cavity Diameter [mm]	100.3	103.4
Pole Length [mm]	80	80

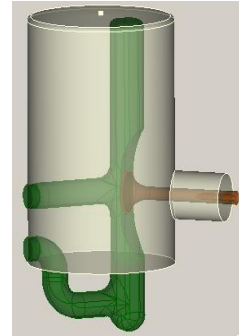
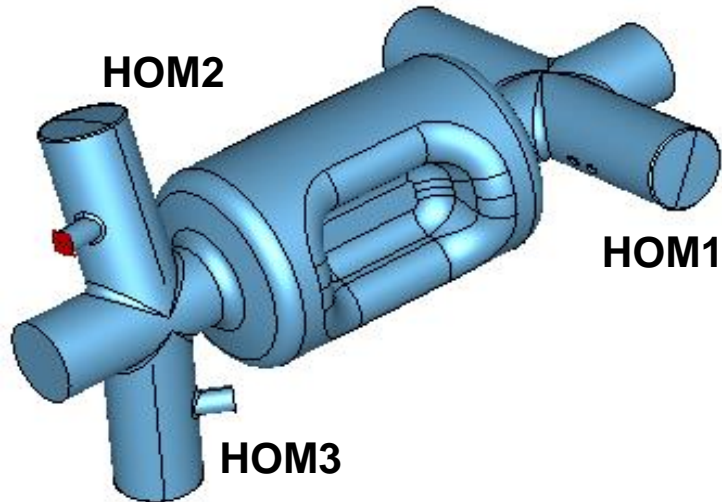
# Fundamental Power Coupler



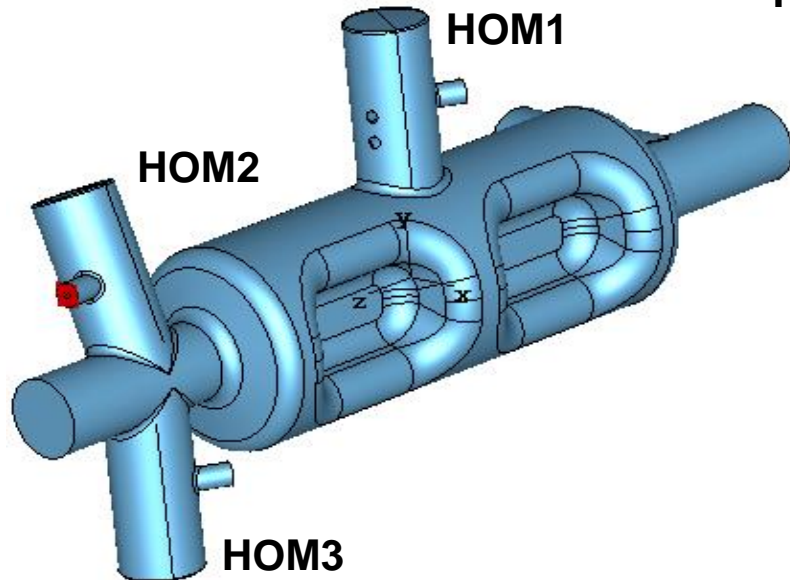
- Coupling using coaxial antenna
  - Similar to LCLS II power coupler
- Beam current:  $I_b = 10$  mA
- Beam offset:  $\Delta x = 0.5$  mm
- Microphonics:  $\delta f = 50$  Hz
- Cavity parameters:

	1-cell	2-cell
$R/Q$ [ $\Omega$ ]	444.8	895.6
$V_t$ per cavity [MV]	1.35	2.7
$Q_{ext}$	$1.5 \times 10^7$	
RF Power at the cavity [W]	300	600
RF heating at Cu probe [W]	1.2	2.22

# Higher Order Mode Damping



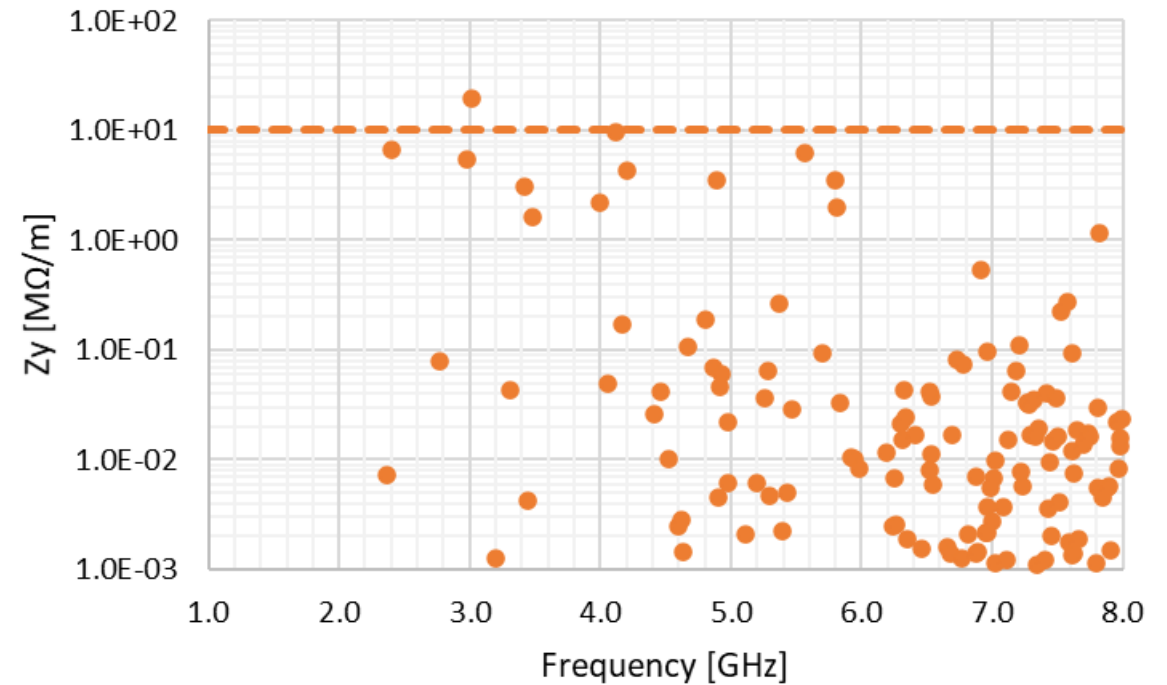
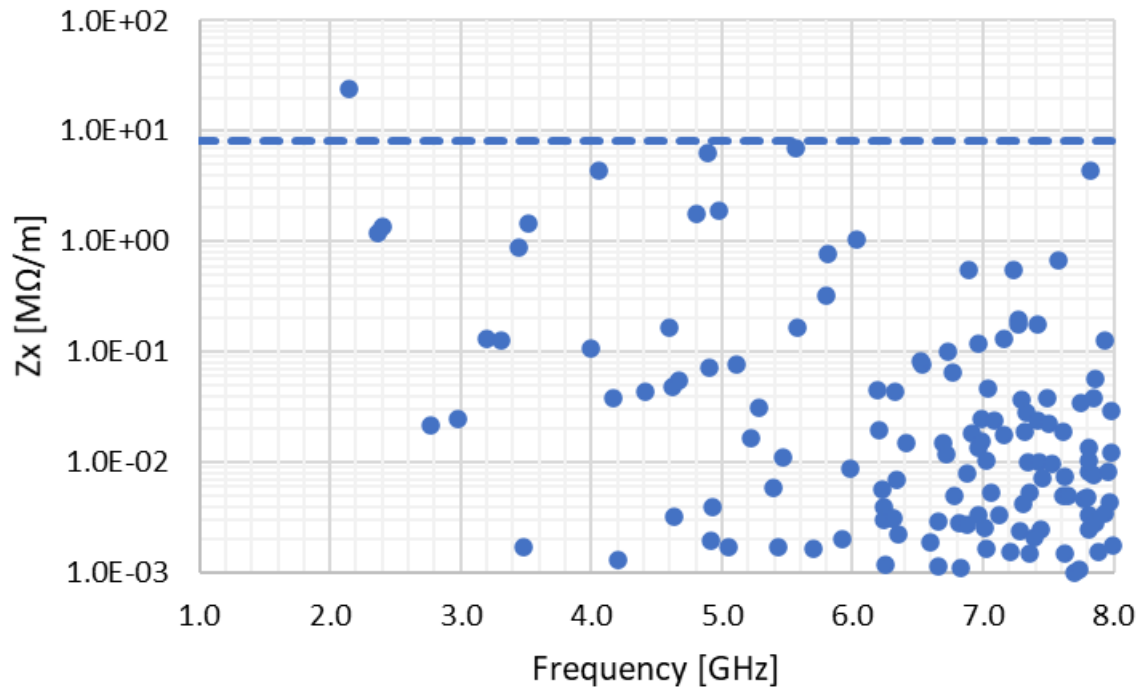
TESLA type  
HOM coupler



- Damping using 3 TESLA type HOM couplers
  - Damper design used in the LCLS II cavities
  - 1-cell cavity: All the couplers are placed on the beam
  - 2-cell cavity: Single coupler on cavity body to couple to the trapped modes between the poles
- Further HOM damping schemes to be explored
  - LHC-RFD HOM coupler option
  - Waveguide damping option
- Final choice will be decided based on
  - RF properties including HOM power
  - Engineering and manufacturing complexity

# Preliminary Transverse HOM Damping – 1-cell Cavity

- Impedance threshold:  $Z_x = 48.8 \text{ M}\Omega/\text{m}$  and  $Z_y = 61.7 \text{ M}\Omega/\text{m}$
- Impedance threshold per cavity:  $Z_x = 8.14 \text{ M}\Omega/\text{m}$  and  $Z_y = 15.425 \text{ M}\Omega/\text{m}$  (6 cavities)

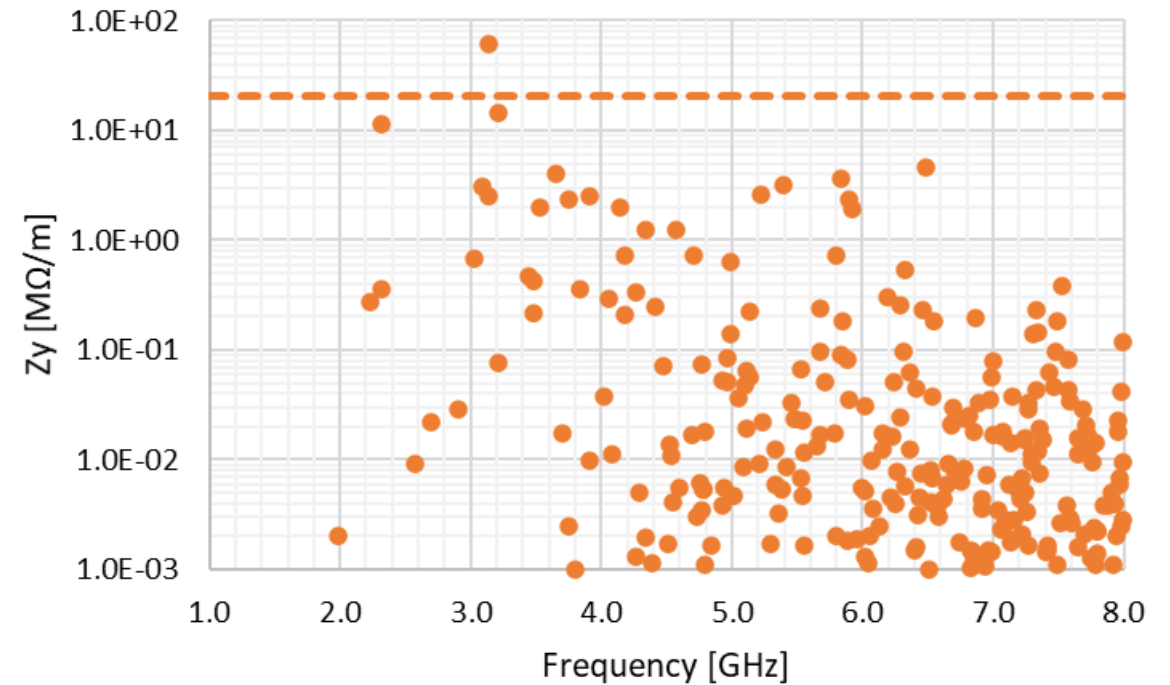
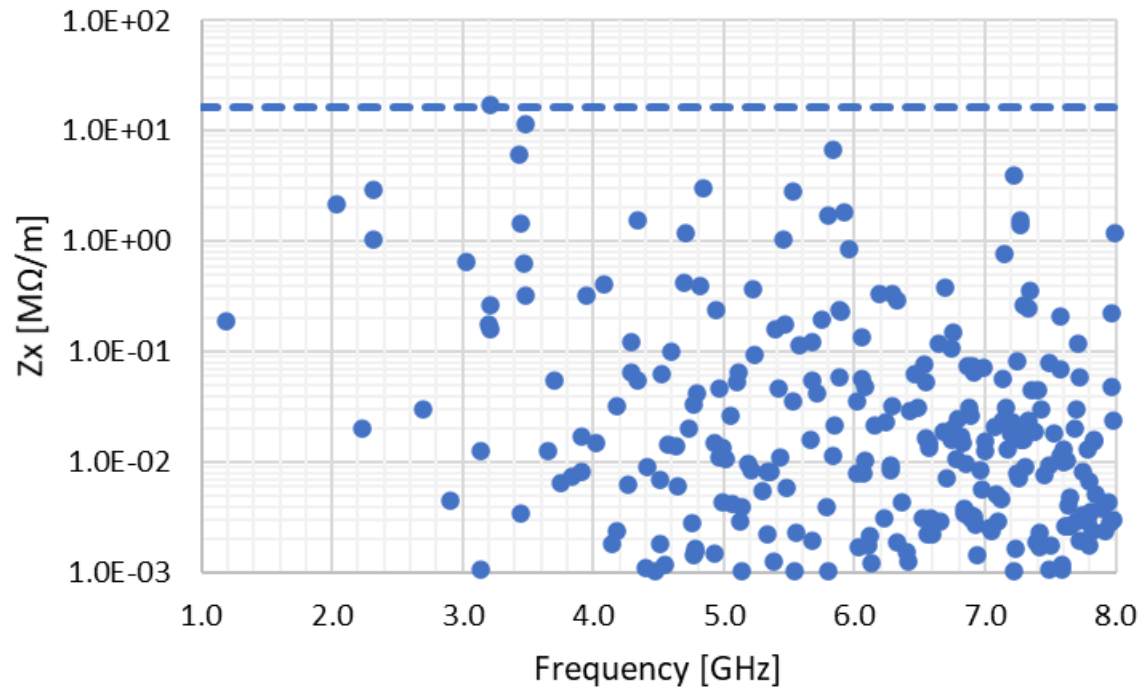


- Impedances calculated using circuit definition
- Modes calculated up to beam pipe aperture cut off frequency



# Preliminary Transverse HOM Damping – 2-cell Cavity

- Impedance threshold:  $Z_x = 48.8 \text{ M}\Omega/\text{m}$  and  $Z_y = 61.7 \text{ M}\Omega/\text{m}$
- Impedance threshold per cavity:  $Z_x = 16.27 \text{ M}\Omega/\text{m}$  and  $Z_y = 20.57 \text{ M}\Omega/\text{m}$  (3 cavities)

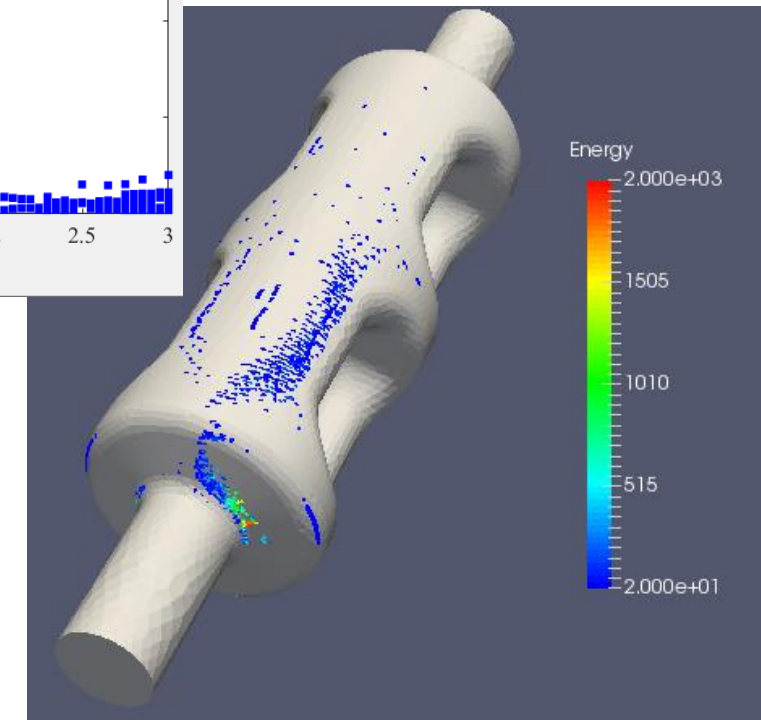
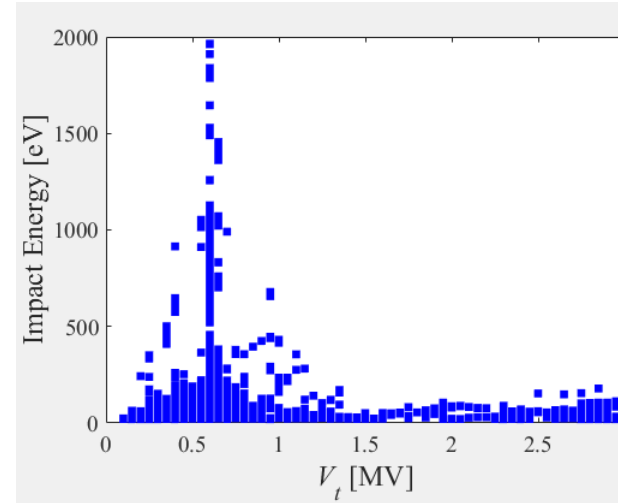
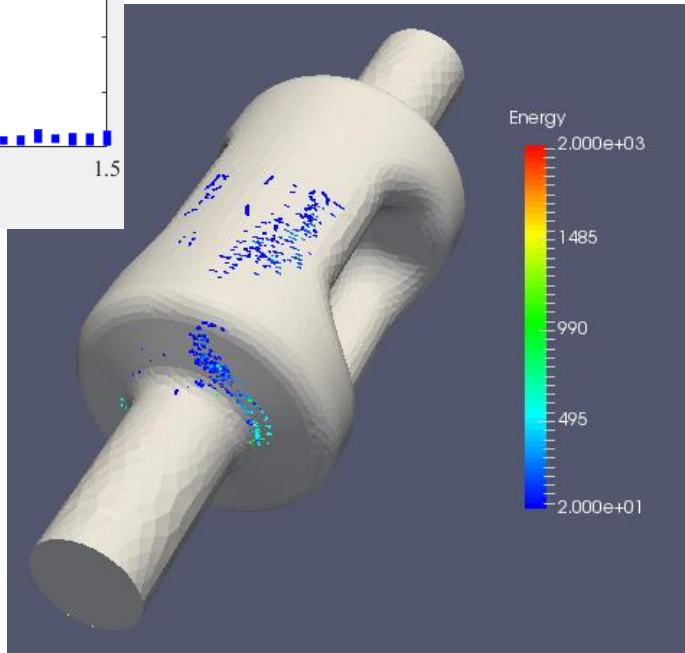
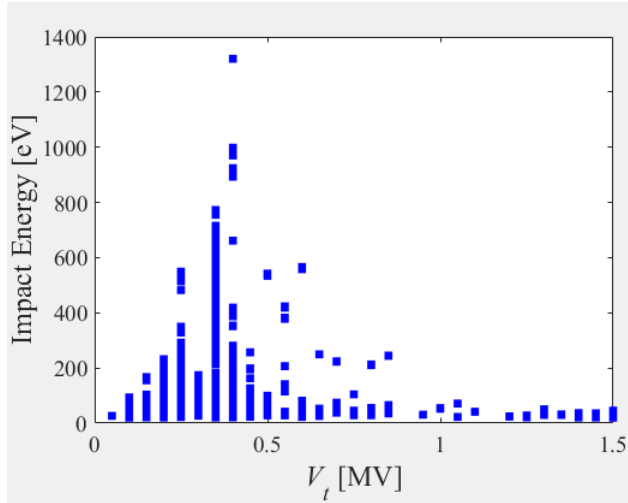


- Impedances calculated using circuit definition
- Modes calculated up to beam pipe aperture cut off frequency



# Multipacting Analysis

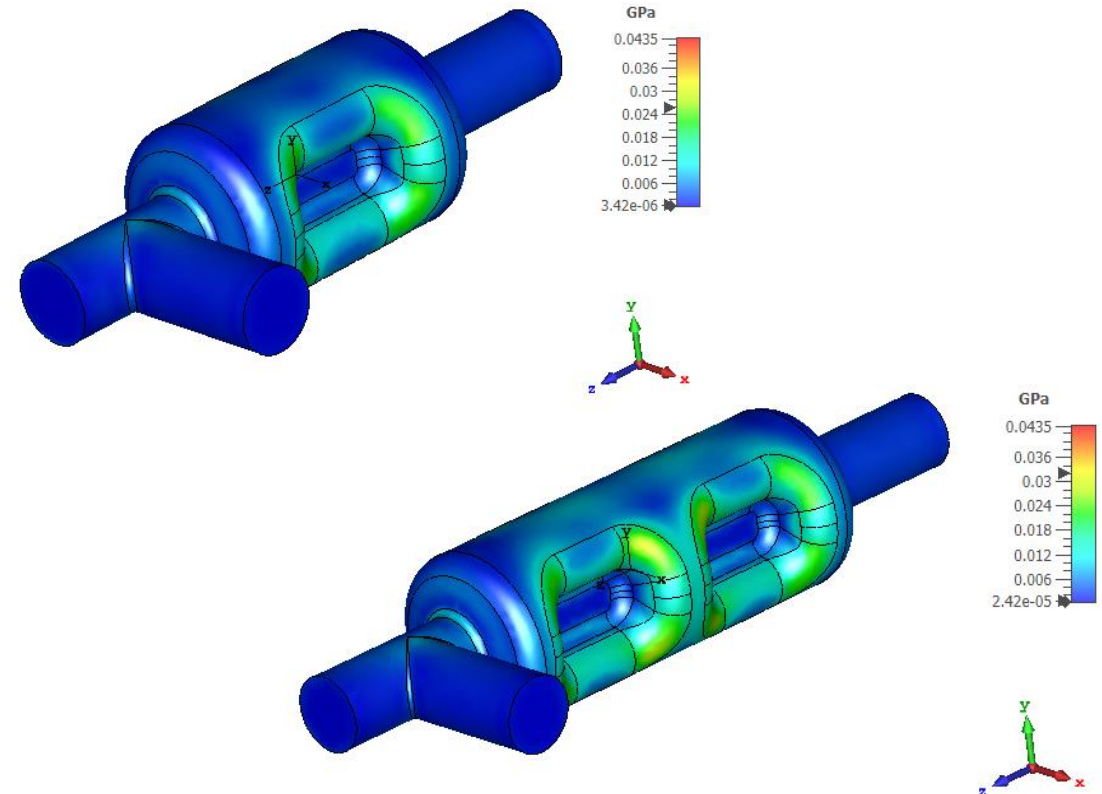
- Resonant particles traced for 50 rf cycles with impact energy 20-2000 eV
- Simulated for a 1/8<sup>th</sup> surface area



# Stress Analysis

- Analysis at 2.2 atm external pressure
- Nb material properties at room temperature
  - (JLAB-TN-09-002 – C100 Cryomodule Niobium Cavity Structural Analysis)
  - Young's modulus – 82.7 GPa ( $1.2 \times 10^7$  psi)
  - Poisson's ratio – 0.38
- Cavity thickness – 3 mm
- Boundary conditions – Cavity constrained at beam pipes and FPC
- Allowable stress < 43.5 MPa
- Maximum stress
- Initial analysis shows cavity doesn't require stiffening
- Cavity can be machined with varying thickness

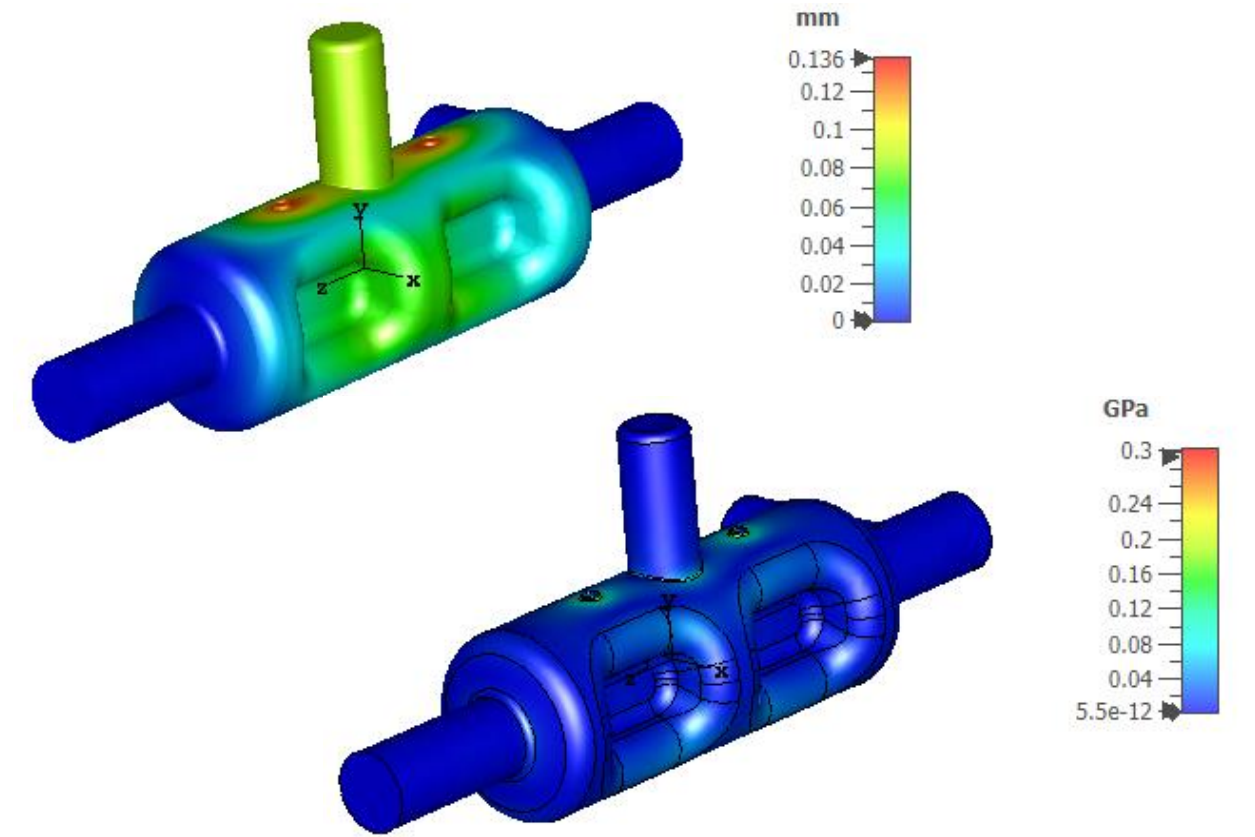
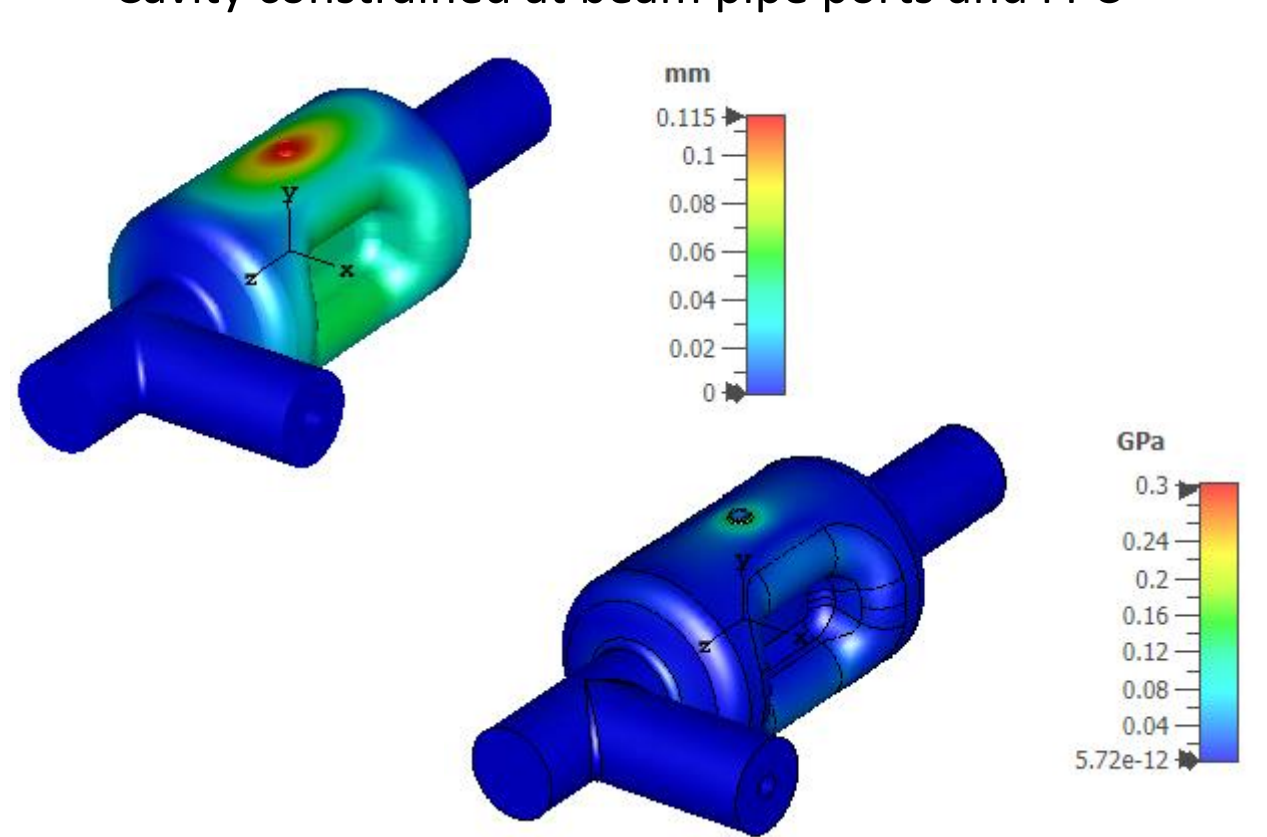
Cavity Type	Max. Stress [MPa]
1-cell	25
2-cell	32



# Tuning Sensitivity

- Nb material properties at cryo temperature
  - Young's modulus – 123 GPa ( $1.79 \times 10^7$  psi)
- Cavity thickness – 3mm
- Cavity constrained at beam pipe ports and FPC

Cavity Type	Total Displacement	Tuning Sensitivity	Tuning Range
1-cell	0.23 mm	8.5 MHz/mm	1.96 MHz
2-cell	0.27 mm	4.1 MHz/mm	2.23 MHz

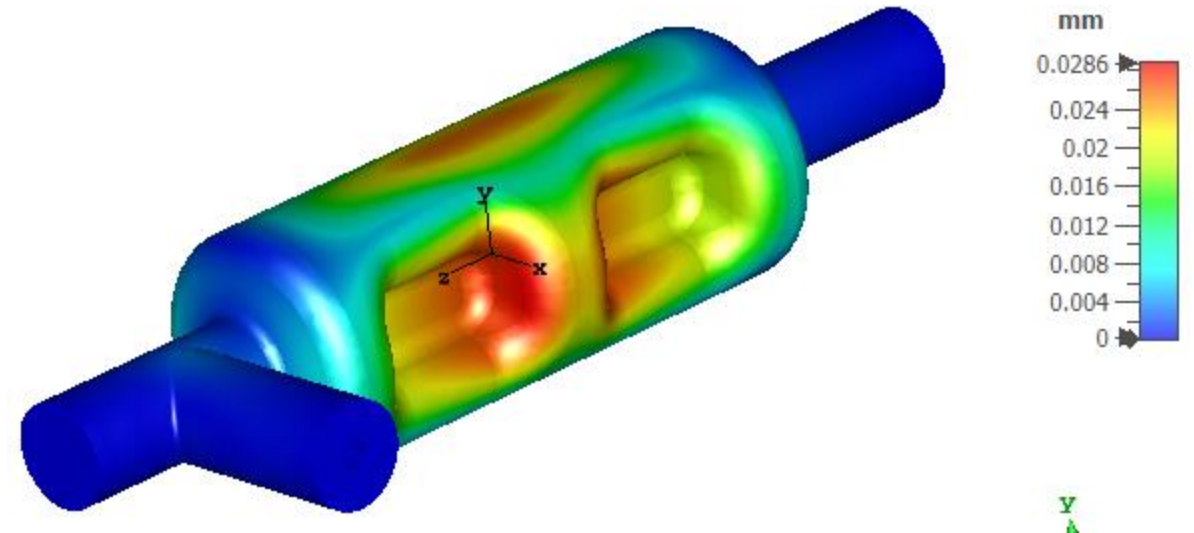
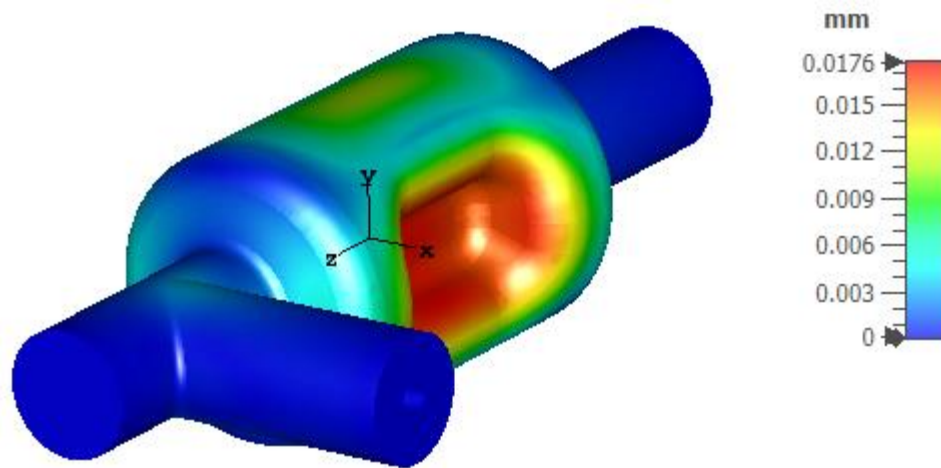


# Pressure Sensitivity

- Nb material properties at room temperature
  - Young's modulus – 82.7 GPa ( $1.2 \times 10^7$  psi)
  - Poisson's ratio – 0.38
- Cavity thickness – 3mm
- Cavity constrained at beam pipe ports and FPC
- Stiffening at poles can reduce pressure sensitivity

Cavity Type	$df/dP$ [Hz/mbar]
1-cell	561.3
2-cell	751.5

- Stiffening at poles can reduce pressure sensitivity

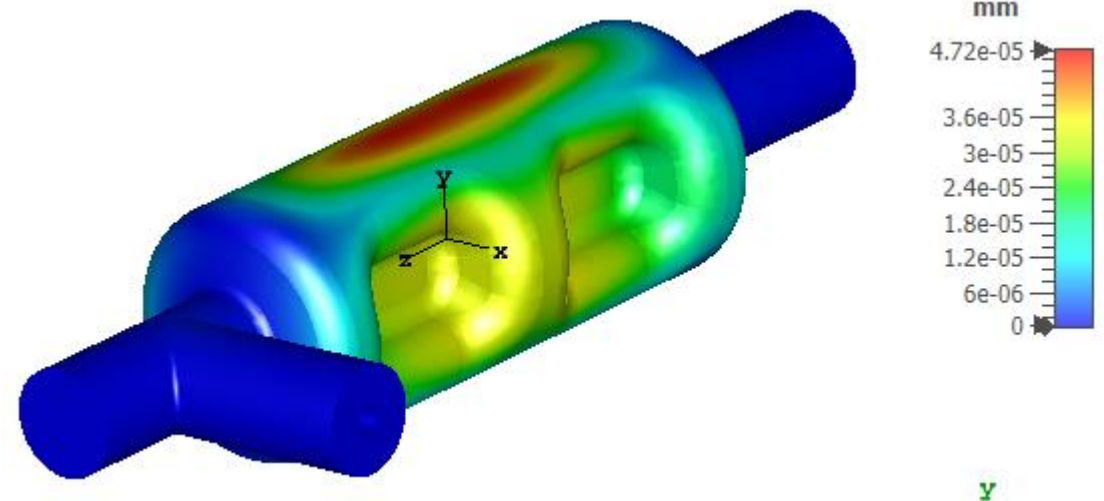
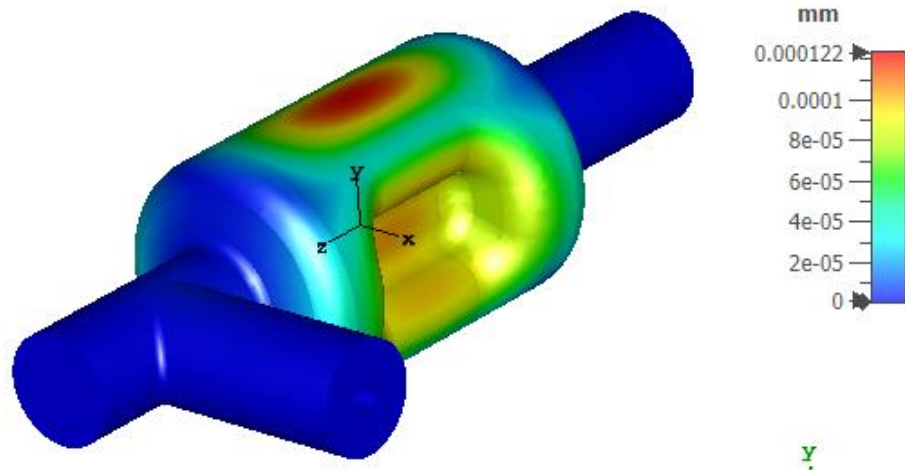




# Lorentz Detuning

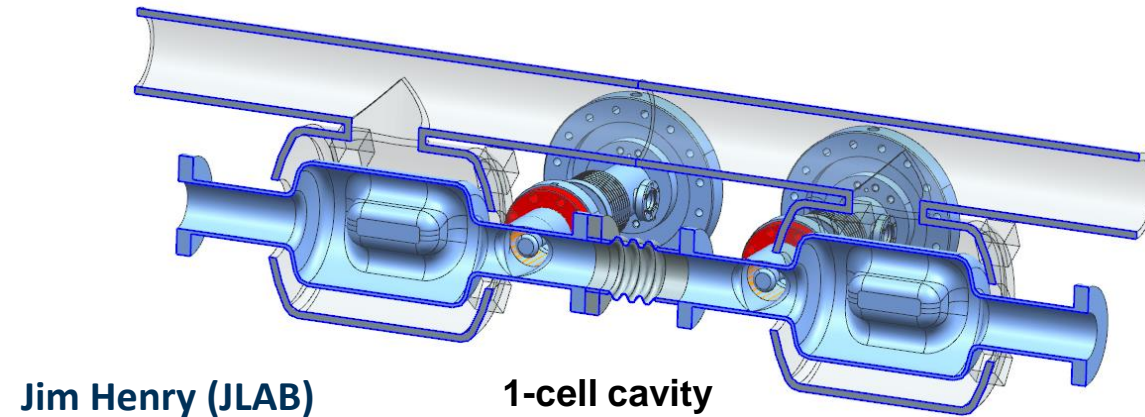
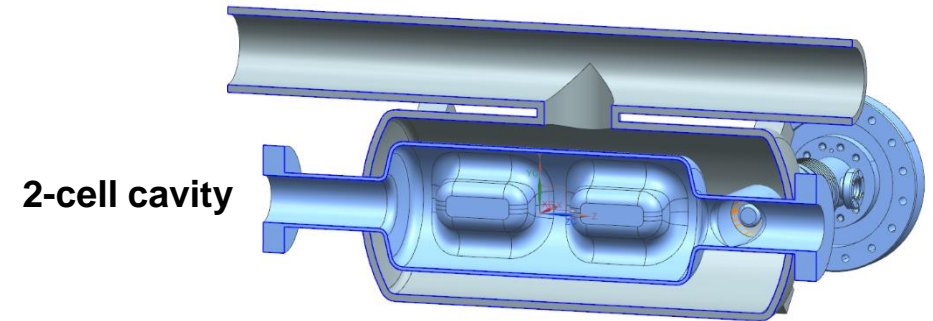
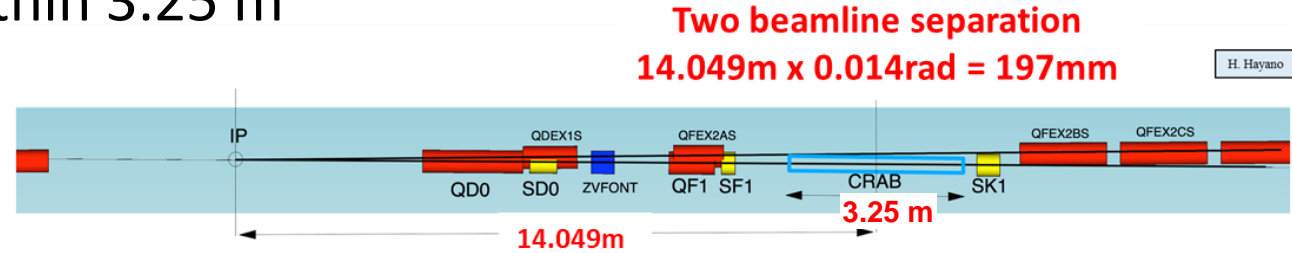
- Nb material properties at cryo temperature
  - Young's modulus – 123 GPa ( $1.79 \times 10^7$  psi)
  - Poisson's ratio – 0.38
- Cavity thickness – 3mm
- Cavity constrained at beam pipe ports and FPC
- Lorentz detuning can be reduced by tuner
  - Tuning by push/pull at top and bottom of the cavity

Cavity Type	$k_L$ [kHz/(MV) <sup>2</sup> ]	Vt [MV]	$\Delta f$ [kHz]
1-cell	-3.67	1.35	6.7
2-cell	-1.11	2.7	8.1



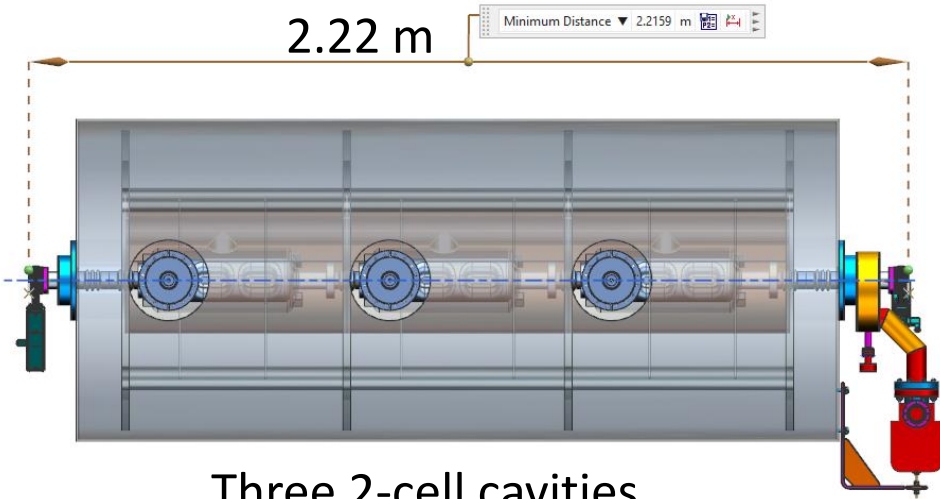
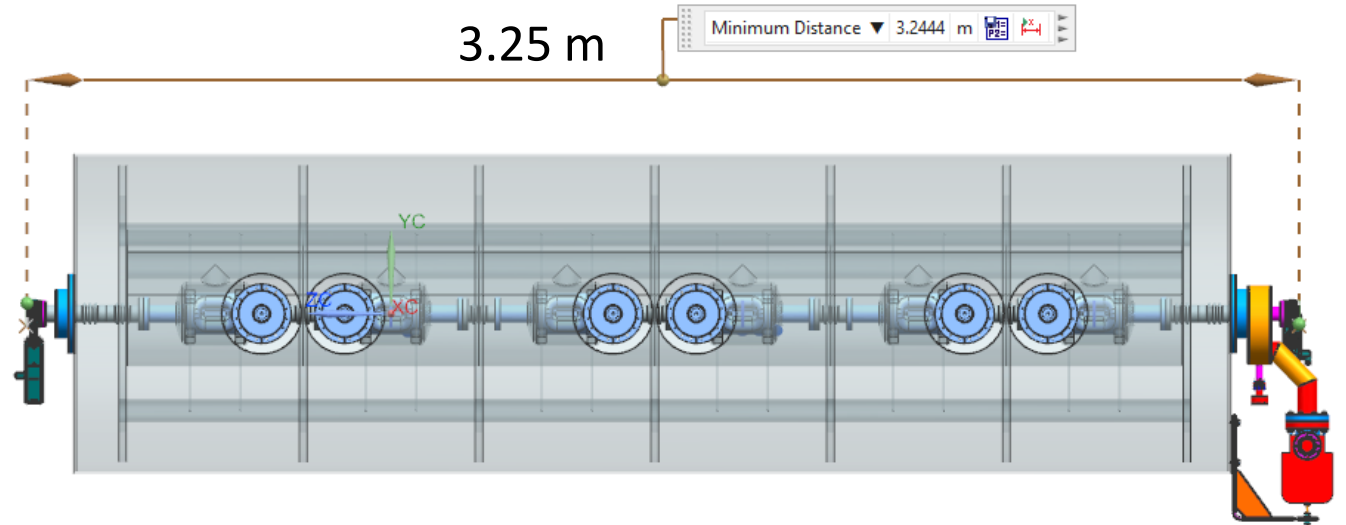
# Conceptual He Vessel and Cryomodule Design

- At 1 TeV – Cryomodule required to fit in within 3.25 m
- 1-cell cavity
  - 6 cavities in a single cryomodule
  - 10% extra margin
- 2-cell cavity
  - Minimum 3 cavities in a single cryomodule will deliver required  $V_t$
  - Space available for 4 cavities in a single cryomodule
  - 30% extra margin available with 4 cavities
- Cavity thickness – 3mm
- Design concept follows JLab C100 cryomodule
- Second beam pipe – 20 mm beam pipe

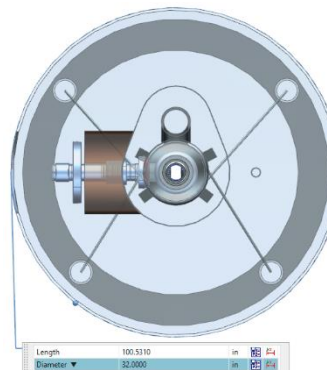


# Conceptual He Vessel and Cryomodule Design

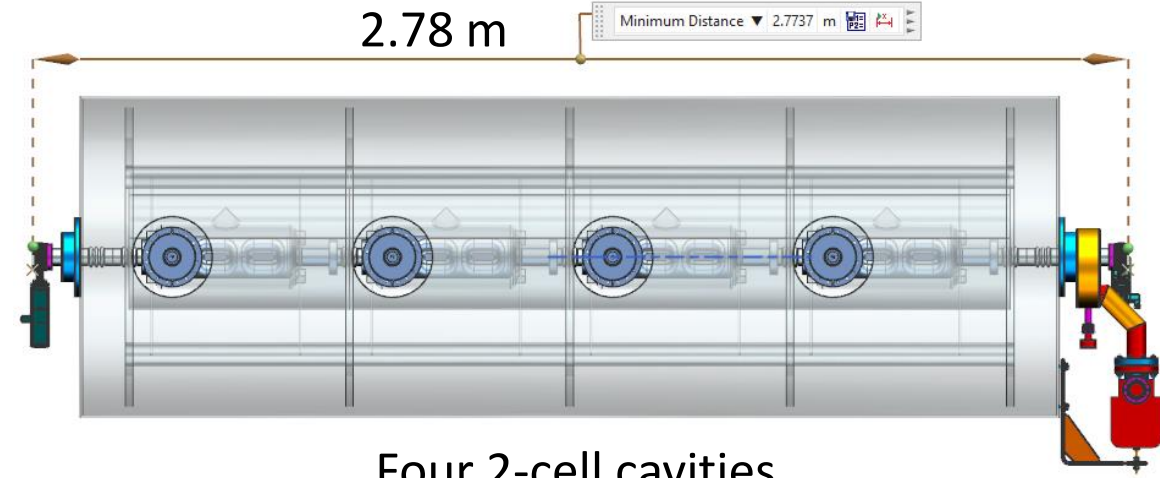
- Six 1-cell cavities
- Total achievable  $V_t = 8.1$  MV
- Cryomodule length = 3.25 m
- Cryomodule diameter = 0.82 m



Three 2-cell cavities  
Total achievable  $V_t = 8.1$  MV



Jim Henry (JLAB)



Four 2-cell cavities  
Total achievable  $V_t = 10.8$  MV



# Summary

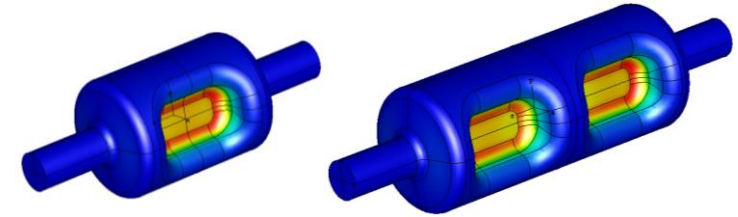
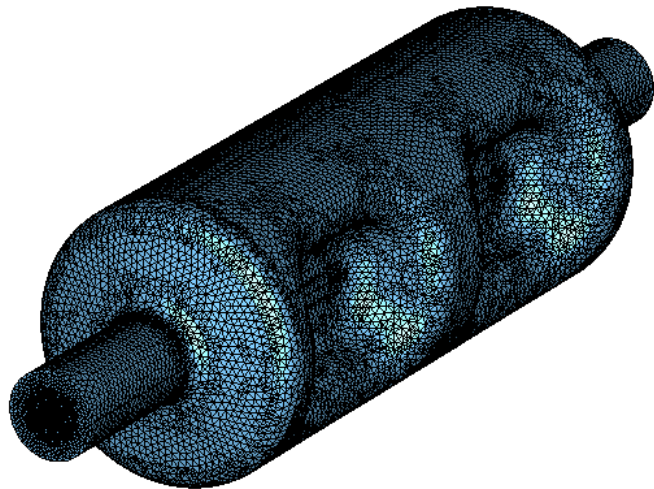
- Two 1.3 MHz rf-dipole cavity options were developed following the reduced beam line space of 3.25 m
  - Cavity design was evaluated with 25 mm pole separation and 30 mm beam aperture
- Both 1-cell and 2-cell designs meet current specifications in:
  - Dimensional requirements, peak surface fields with required transverse voltage
  - An acceptable HOM damping mechanism is identified
  - Requires further analysis on HOM damping
  - Longitudinal effects to be evaluated
- Initial cavity designs are completed with FPC
- Preliminary mechanical analysis is completed
- Several cavity options allows trade off between maximum voltage and margin

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## Back Up Slides

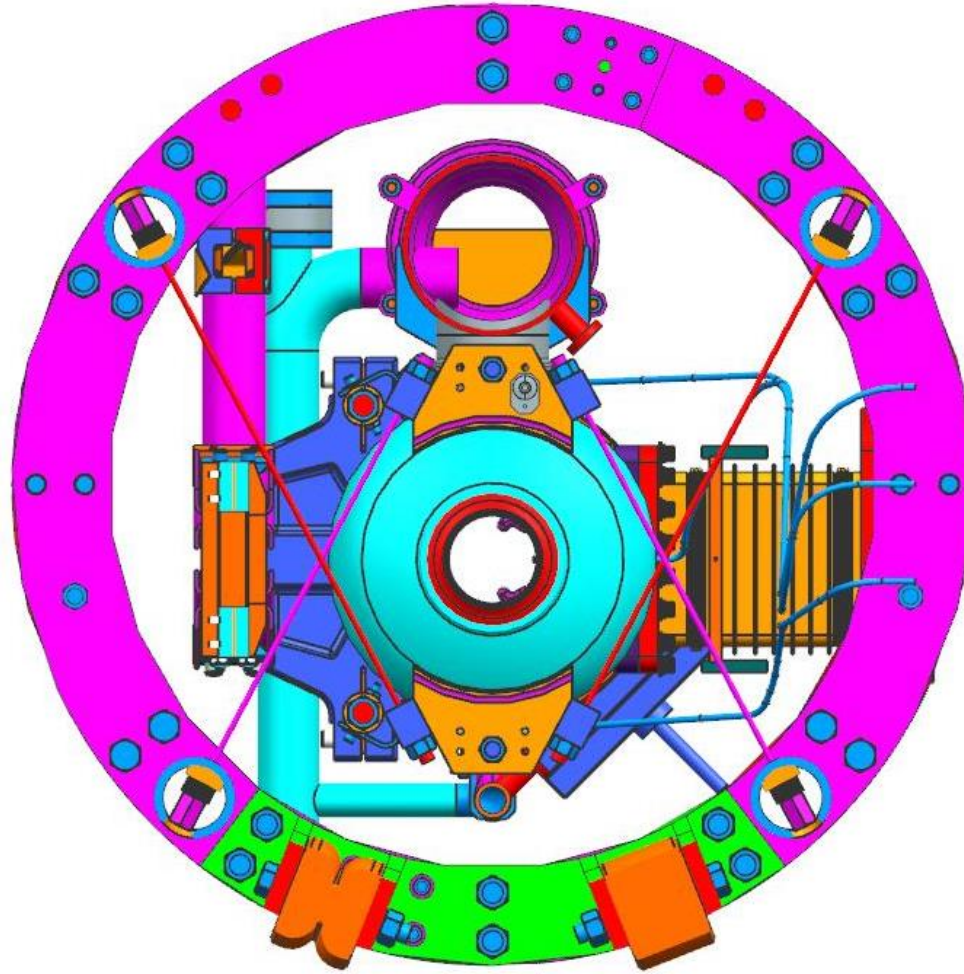
# Multipole Components

- Higher order multipole components for the bare cavity
- Requires a finer mesh along the beam center



Component	Units	1-cell	2-cell
$V_z$	[V]	0.575	-77.25
$V_t$	[V]	1.0E+06	1.0E+06
$b_0$	[mT/m <sup>2</sup> ]	0	0
$b_1$	[mT/m]	3.3	3.3
$b_2$	[mT]	-0.0013	-0.00045
$b_3$	[mT m]	2275.8	2106.6
$b_4$	[mT m <sup>2</sup> ]	9.2	3.2
$b_5$	[mT m <sup>3</sup> ]	-1.39E+6	-1.43E+6
$b_6$	[mT m <sup>4</sup> ]	-4.83E+4	-1.68E+4
$b_7$	[mT m <sup>5</sup> ]	-1.97E+9	-1.89E+9

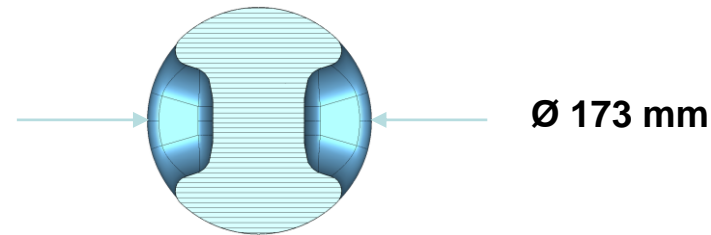
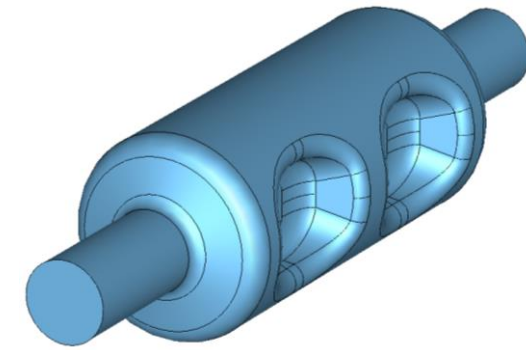
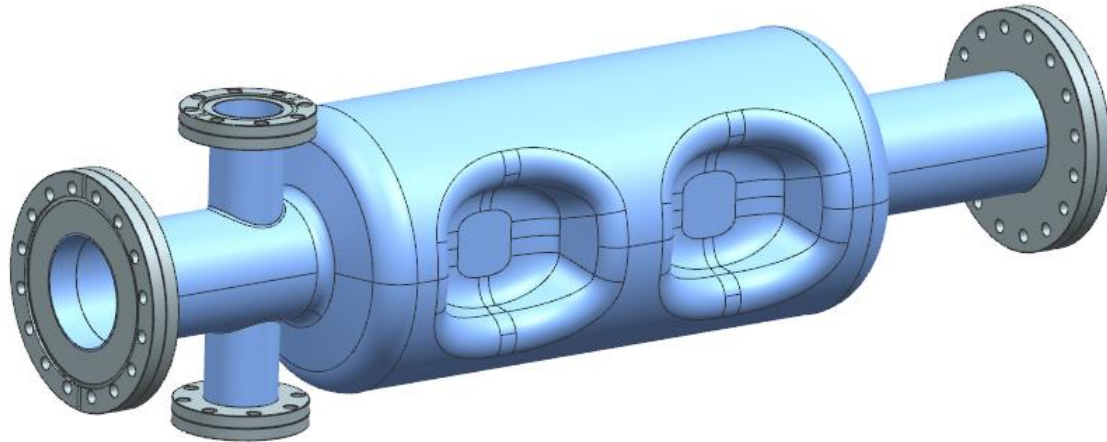
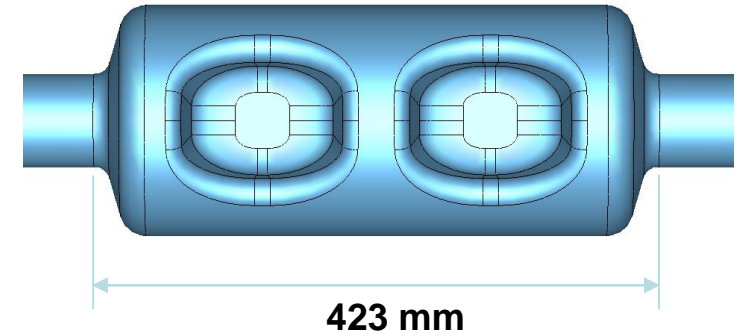
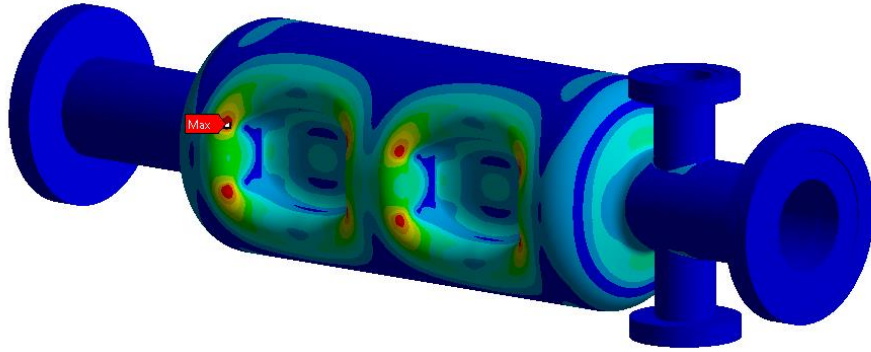
# C100 Cryomodule Design



# Final Design for JLEIC Crabbing System - 952 MHz 2-cell RFD

A: Static Structural  
Equivalent Stress  
Type: Equivalent (von-Mises) Stress  
Unit: MPa  
Time: 1

54.048 Max  
48.043  
42.037  
36.032  
30.027  
24.021  
18.016  
12.011  
6.0056  
0.00028533 Min



Subashini De Silva, HyeKyoung Park

Supported by grant from the  
state of Virginia through SURA



# 952 MHz RFD - Fabrication in Progress

- Material cost – sheet Nb forming instead of machining
- Avoid weld seams at high mechanical stress area and high surface magnetic field area
- Use of simple weld only – high production yield
- Strategy relevant to final cavity with HOM dampers

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