Main Linac Basics

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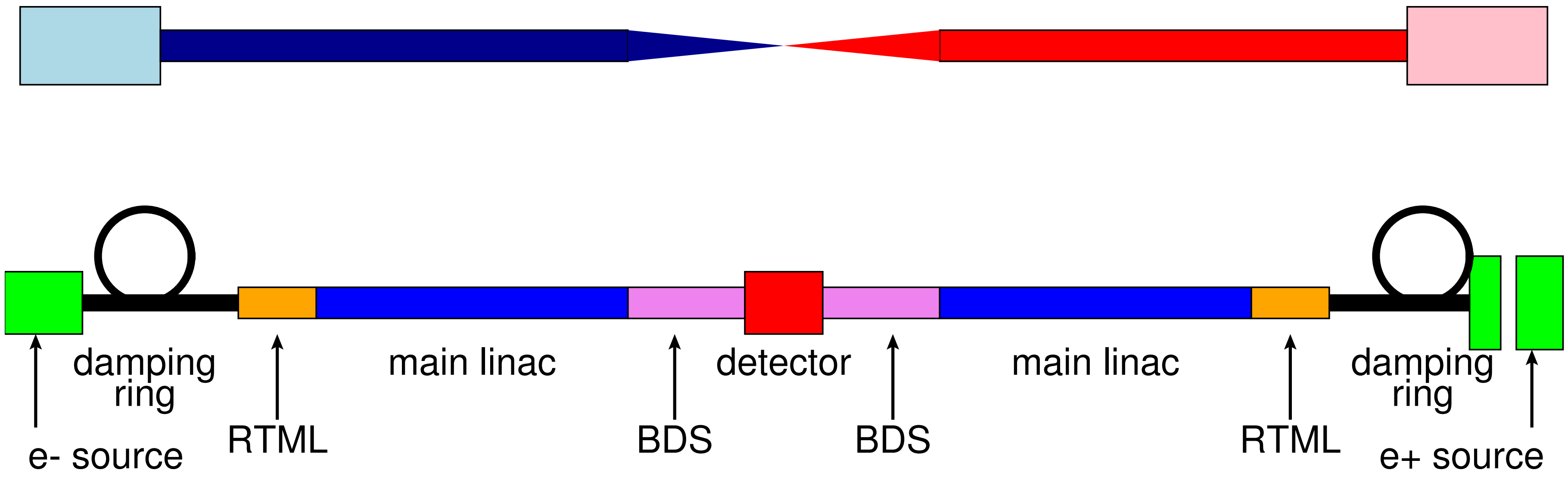
Introduction

Stepping Stones

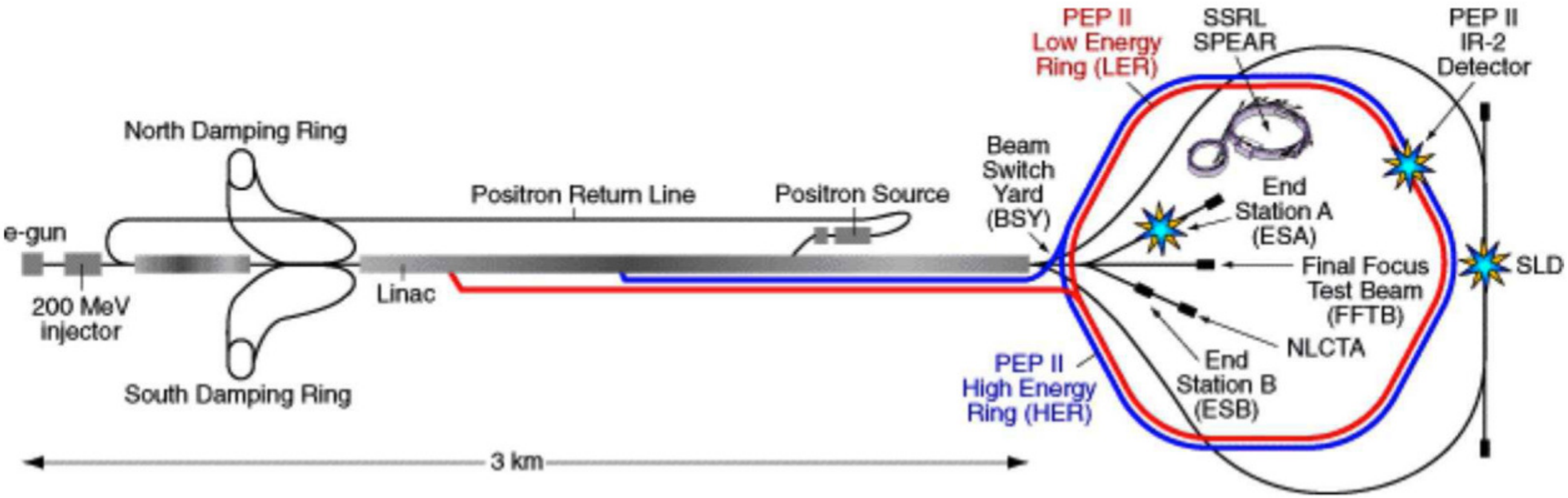
- Introduction
- Accelerating structures
- Power efficiency
- Beam parameters
  - single bunch longitudinal wakefield and energy spread
  - beam transport and emittance
  - transverse wakefields and beam break-up
- Imperfections
- Structure challenges
- Parameter optimisation

Generic Linear Collider Design



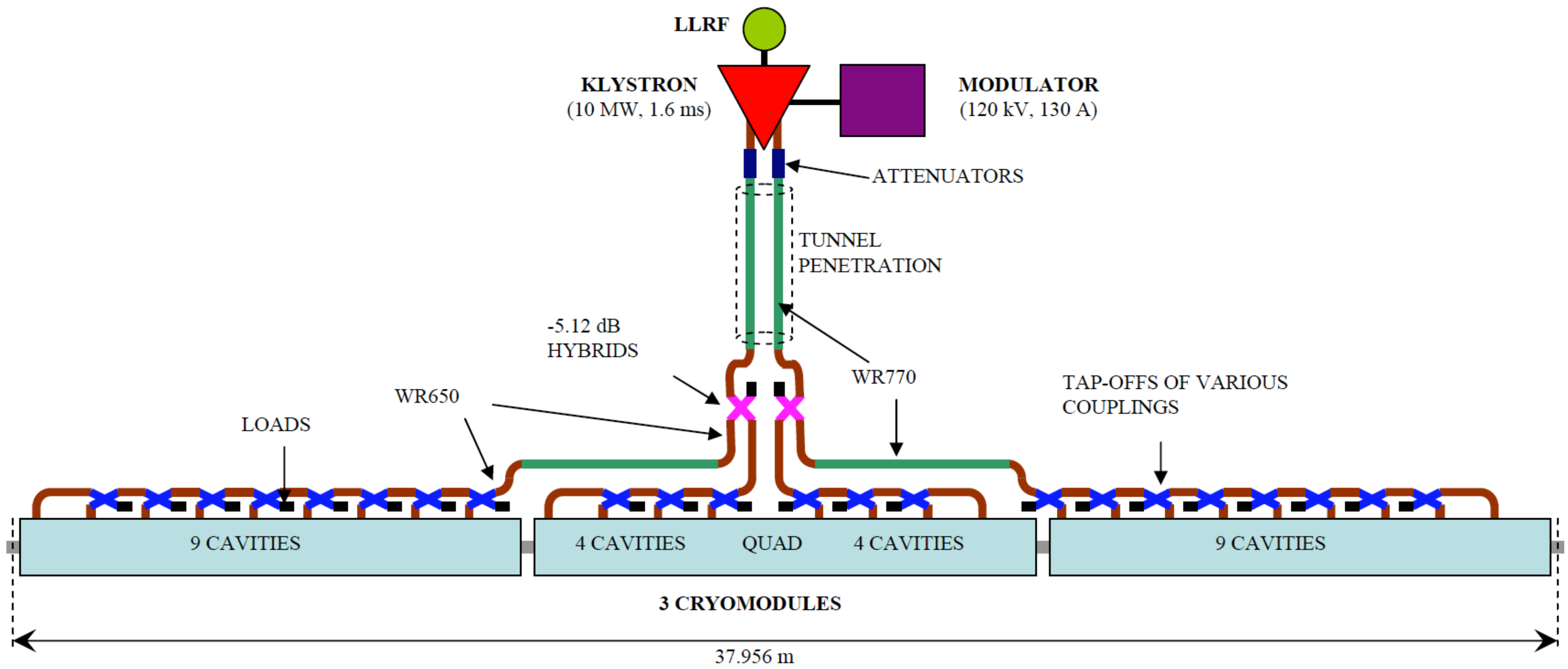
SLC

- The only linear collider so far
- Has been used as a Z_0 factory
- Now used as X-FEL



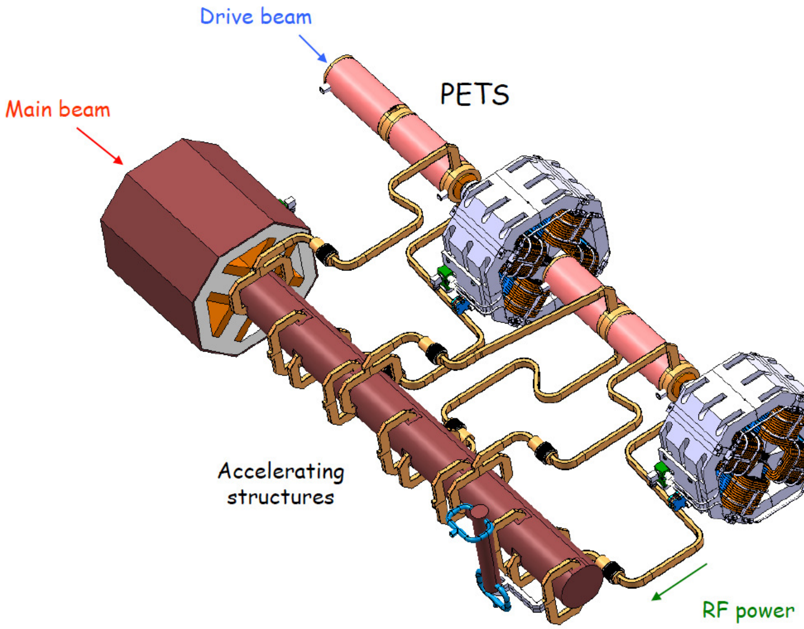
Module Design (ILC)

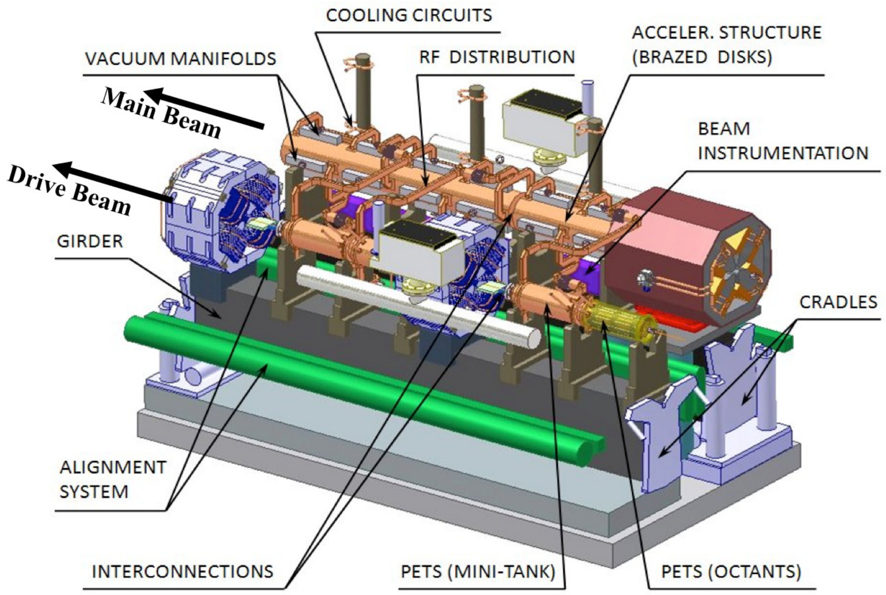
RF Unit Design (ILC, old from RDR)



- Most relevant components for the beam
  - accelerating structures
  - quadrupoles
  - beam position monitors (BPMs) and correctors

Module Design (CLIC)





- Five types of main linac modules
- Drive beam module is regular
- Most relevant components for the beam
  - accelerating structures
  - quadrupoles
  - beam position monitors (BPMs) and correctors

Why is the Main Linac Important?

- Two main parameters that are important for the physics experiments
  - collision energy
  - luminosity, a measure for the rate of events at the interaction point
- The main linac is the main component to accelerate the beam

  ⇒ it is responsible for the beam energy
  - the main relevant parameter is the accelerating gradient
- The main linac is the main consumer of power

  ⇒ it is an important limitation for the beam current
  - the luminosity depends on the beam current
- The main linac is one of the main sources of emittance growth

  ⇒ the emittance is a parameter that affects the luminosity
- There is a third parameter which the main linac affects very much, the cost
  - is the society willing to pay for it?

Cost Impact

- In ILC 60% of the cost is in the ML
- The long tunnel is expensive
  - and important for the schedule (tunnel boring machines)
- The installed components are expensive
- The linac drives other machine components
  - large damping rings in ILC to be able to store the full bunch train
  - drive beam complex in CLIC

Luminosity Impact

- Use normal luminosity formula for LC

$$\mathcal{L} = H_D \frac{N^2}{4\pi\sigma_x\sigma_y} n_b f_r$$

- Rewrite as

$$\mathcal{L} = H_D \frac{N}{\sigma_x} n_b N f_r \frac{1}{\sigma_y}$$

- And find for classical beamstrahlung

$$\mathcal{L} \propto H_D \, n_\gamma \, \eta_{RF->beam} \frac{P_{RF}}{E_{cm}} \frac{1}{\sigma_y}$$

- And for quantum beamstrahlung

$$\mathcal{L} \propto H_D \frac{n_\gamma^{3/2}}{\sqrt{\sigma_z}} \eta_{RF->beam} \frac{P_{RF}}{E_{cm}} \frac{1}{\sigma_y}$$

- Remember

$$\sigma_y = \sqrt{\beta_y \epsilon_y / \gamma}$$

Some Fundamental Parameters

parameter	symbol	SLC	ILC	CLIC
centre of mass energy	E_{cm} [GeV]	92	500	3000
luminosity	$\mathcal{L}$ $[10^{34}\ \mathrm{cm}^{-2}\mathrm{s}^{-1}]$	0.0003	1.8	5.9
luminosity in peak	$\mathcal{L}_{0.01}$ $[10^{34}\ \mathrm{cm}^{-2}\mathrm{s}^{-1}]$	0.0003	1.1	2
gradient	G [MV/m]	20	31.5	100
charge per bunch	N $[10^9]$	37	20	3.72
bunch length	σ_z [μm]	1000	300	44
beam size	$\sigma_{x,y}$ [nm]	1700/600	474/5.9	40/1
vertical emittance	ϵ_y [nm]	3000	35	20
bunches per pulse	n_b	1	1312	312
distance between bunches	Δ_b [ns]	–	554	0.5
repetition frequency	f_r [Hz]	120	5	50

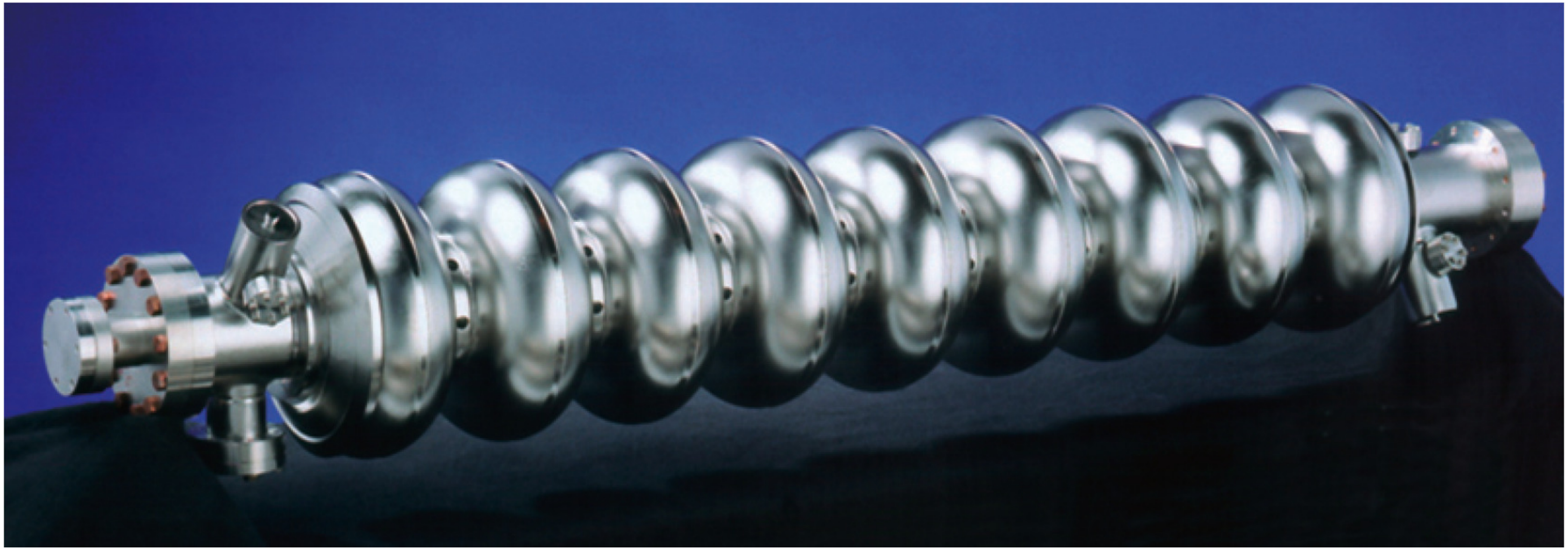
$\Rightarrow$ Beam Parameters are very different

- in particular time structure
- this also affects the experiments

- We will see that this is driven by the main linac

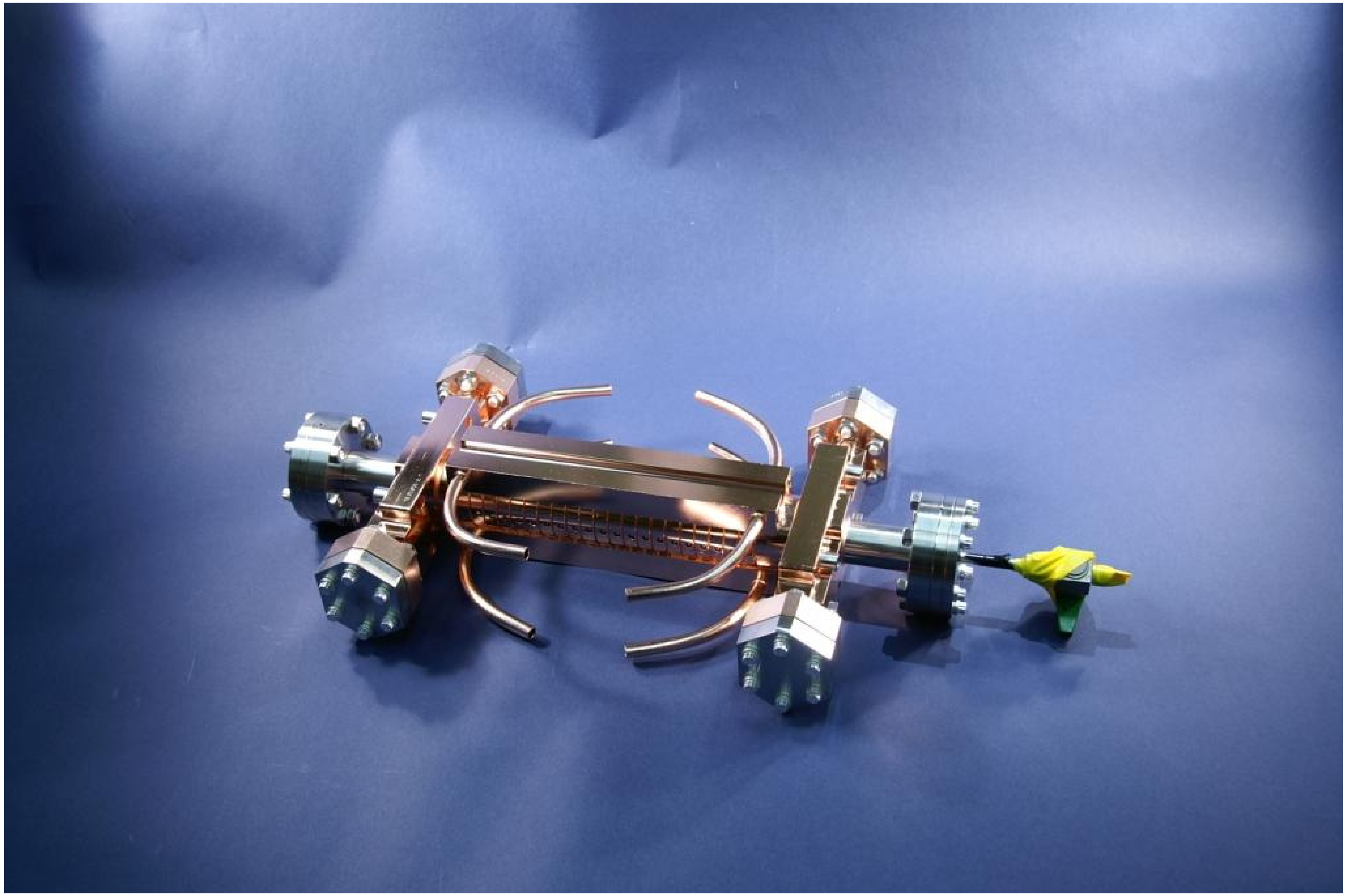
Accelerating Structures

Accelerating Structure (ILC)



- About $1\,\mathrm{m}$ long, super-conducting, $1.3\,\mathrm{GHz}$, standing wave, constant impedance, $31.5\,\mathrm{MV/m}$

Accelerating Structure (CLIC)



- About $23\,\mathrm{cm}$ long, normal-conducting, $12\,\mathrm{GHz}$, travelling wave, constant gradient (almost), $100\,\mathrm{MV/m}$

Types of Structures

- Accelerating structures can be normal-conducting or super-conducting
  - in a super-conducting structure very little power is lost in the walls
  - in a normal conducting structure a significant power is lost in the walls (in most cases)
- They can be standing wave or travelling wave structures
  - in standing wave the energy is trapped and the RF wave is reflected at the ends creating the standing wave
  - in a travelling wave structure power is coupled into one end and extracted at the other
- They can be constant impedance structures of constant gradient structures (or something else)
  - all cells can be the same design or the design differs along the structure

Choice of Material

- The material is the most fundamental design choice

- Super-conducting structures

  - allow a small beam current

  ⇒ low background per unit time in IP

  ⇒ intra-pulse feedback is possible everywhere

- Normal conducting structures

  - allow for high gradient

  ⇒ high centre-of-mass energy

  - need high beam current

  ⇒ significant wakefield effects

  - use short pulses

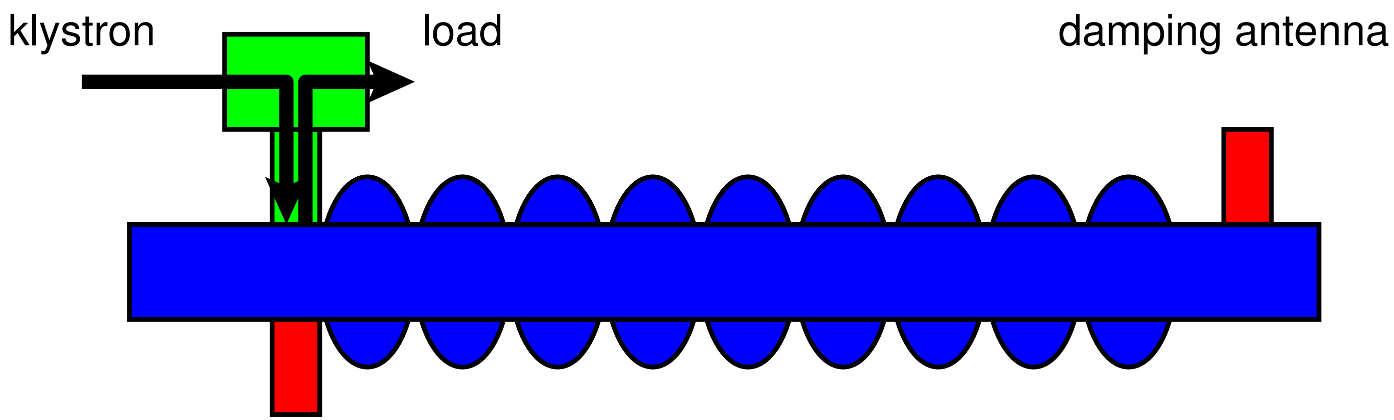
  ⇒ smaller damping ring

Standing Wave Structures

- The power is feed into one end
  - the power is reflected at the coupler
  - as the power in the cavity is increasing, the reflection is reduced
- there is a level when there is no reflection

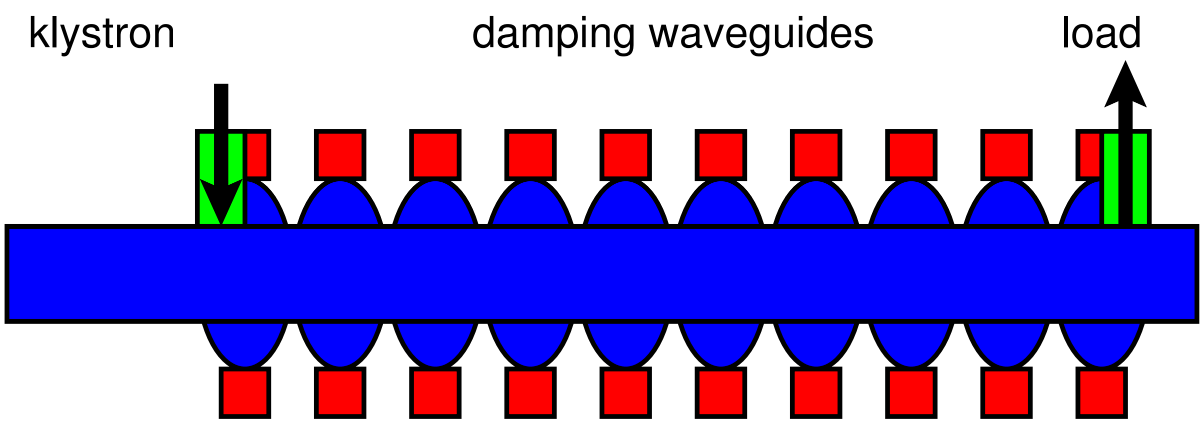
⇒ now switch on the beam

Film
Film



Travelling Wave Structures

- The power is feed into one end
  - no reflection if designed properly
- It slowly moves through the structure
  - group velocity is typically a few percent of the speed of light



Film

Choice of Structure Design

- In a super-conducting structure little power is lost in the wall
  - so can afford a small beam current
  - little power is extracted but over long times
  - natural choice is standing wave structures, to avoid all the power draining out at the end
  - no need to compensate extraction of energy along the structure
- For a normal conducting structure all four options (constant impedance/constant gradient and standing/travelling wave) could be used
  - for CLIC travelling wave, constant gradient structures have been chosen
  - travelling wave structures avoid recirculators to keep the energy in the structures
  - constant gradient allows to reach higher effective gradients

Choice of Frequency

- Obviously the frequency choice differs
  - CLIC: $12\,\mathrm{GHz}$
  - ILC: $1.3\,\mathrm{GHz}$
- So what drives the choice?
- ILC uses super-conducting structures
  - high frequencies lead to higher surface resistance
  - high frequencies lead to higher wakefield amplitudes $W_L \propto f^2$, $W_\perp \propto f^3$
  - a very low frequency makes the structures expensive (dimension $\propto \lambda$)

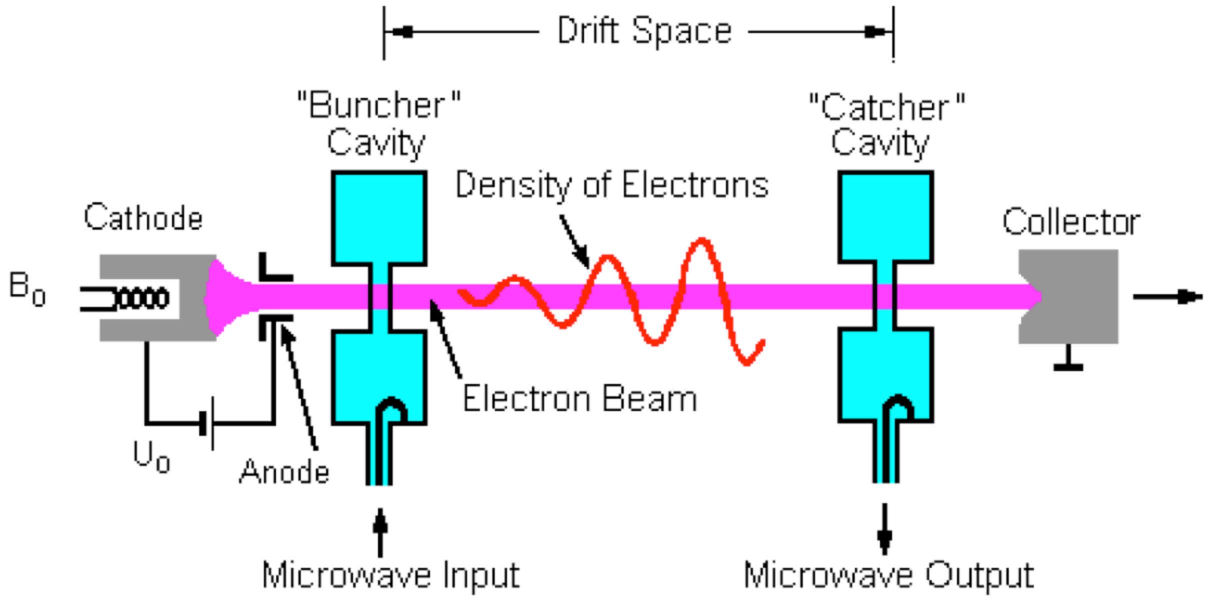
  $\Rightarrow$ so a frequency with existing power sources has been picked
- CLIC uses normal-conducting structures
  - higher frequencies help in reaching high gradients
  - but also lead to higher wakefields

  $\Rightarrow$ full optimisation of the design has been performed to achieve the lowest cost for a fixed energy and luminosity target

RF Power Generation

Klystron

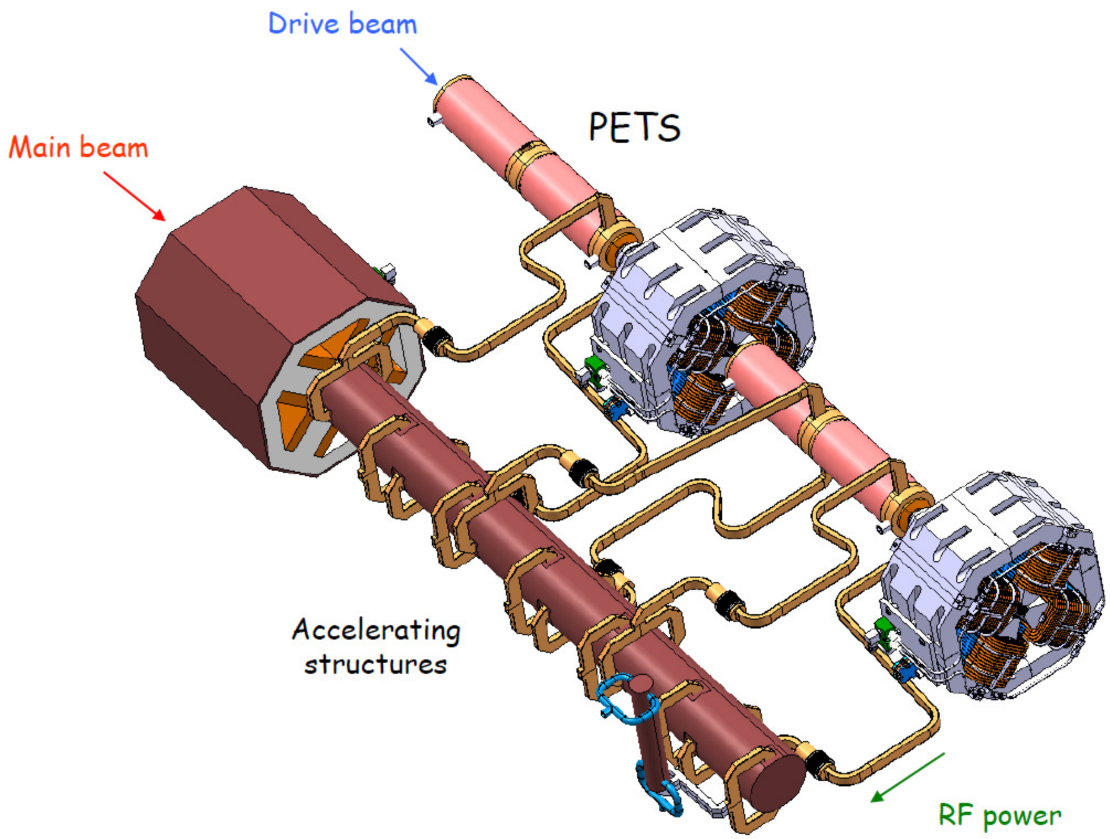
- Usually the input RF power for the accelerating structures is provided by klystrons
- In ILC klystrons are used to directly power the main beam
- In CLIC they power the drive beam accelerator
  - would be difficult in main linac



- Klystrons tend to be more efficient at low frequencies and long pulses
  - perfect for ILC ($1.3\,\mathrm{GHz}$, $1.5\,\mathrm{ms}$) and the CLIC drive beam accelerator ($1\,\mathrm{GHz}$ and $140\,\mu\mathrm{s}$)

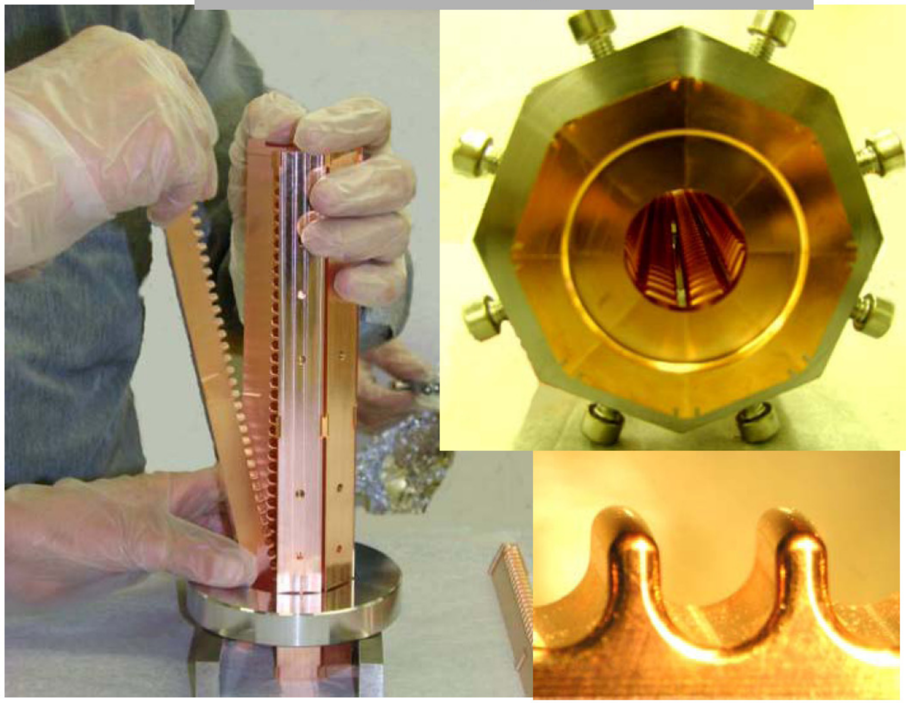
Drive Beam (CLIC)

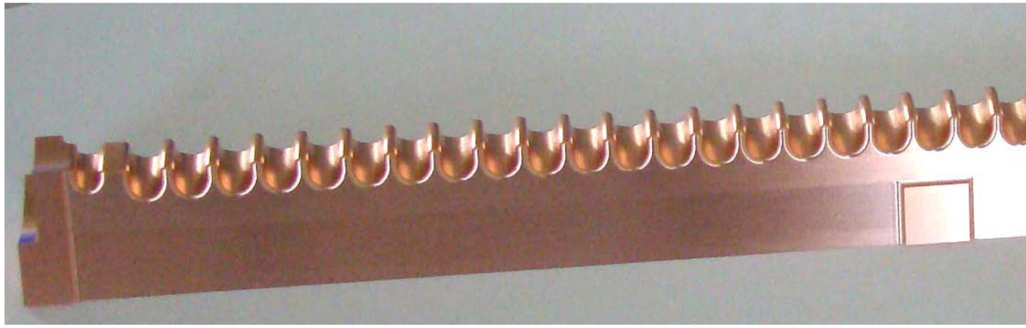
- In CLIC power is produced by a high current drive beam (100A)
  - decelerated in a low impedance structure
- Beam loading is used for acceleration



PETS

Assembly of the eight PETS bars.





Power Efficiency

Coordinate Systems

- We use two frames, the laboratory frame and the beam frame
- The nominal direction of motion of the beam is called s in the laboratory frame, the beam moves toward increasing s
- The same direction is called z in the beam frame, with smaller z moving ahead of particles with larger z
- A particle preserves its longitudinal position within the beam
- The transverse dimensions are x in the horizontal and y in the vertical plane, in both coordinate systems
- People use different systems so find out what they talk about

Beam Power

- Power consumption of the main linac is a prime consideration
  - electricity cost
  - equipment cost
- Examples of total beam power
  - ILC

$$P_{beam} = 2n_b f_r N E \approx 11\,\mathrm{MW}$$

  - CLIC

$$P_{beam} \approx 28\,\mathrm{MW}$$

- Wall plug power can be transformed into RF power with limited efficiency
- The efficiency of transforming RF power into beam power depends on
  - structure design
  - the gradient
  - the beam parameters
- The structures need to be cooled (especially in a super-conducting machine)

RF to Beam Power Efficiency

- Efficiency is

$$\eta_{RF\to beam} = \frac{\text{Energy taken by one beam pulse}}{\text{Energy in each RF pulse}}$$

  Assuming constant RF pulse power we can calculate

$$\eta_{RF\to beam} = \frac{\tau_{beam}}{\tau_{RF}} \cdot \frac{P_{beam}}{P_{RF}}$$

  This can be calculated on the basis of a single cavity/structure

- We simplify

$$\eta_{RF\to beam} = \frac{\tau_{beam}}{\tau_{beam} + \tau_{fill}} \cdot \frac{P_{beam}}{P_{beam} + P_{loss} + P_{out}}$$

  Note what I call τ_{fill} contains several components of which the fill time is the most important; RF experts will learn more

RF to Beam Power Efficiency

$$\eta_{RF\to beam} = \frac{\tau_{beam}}{\tau_{beam}+\tau_{fill}} \cdot \frac{P_{beam}}{P_{beam}+P_{loss}+P_{out}}$$

- RF pulse needs to be longer than beam pulse in order to fill the structures with energy before the beam arrives

- In a super-conducting cavity
  - little RF power is lost in the walls during the pulse
  - but the cooling requires some significant overhead
  - some cooling is also needed against heating from the environnement

$$\eta_{RF\to beam} = \frac{\tau_{beam}}{\tau_{beam}+\tau_{fill}}$$

- In normal conducting structures
  - A significant fraction of the RF power is lost into the walls
  - some power will be draining out of the travelling wave structure (usually)

$$\eta_{RF\to beam} = \frac{\tau_{beam}}{\tau_{beam}+\tau_{fill}} \cdot \frac{P_{beam}}{P_{beam}+P_{loss}+P_{out}}$$

Shunt Impedance R and P_{loss}

Note: the concept of shunt impedance will be important for all efficiency effects

The field in a structure induces losses in the walls

The loss is described by R, the shunt impedance, defined as

$$R = \frac{\text{effective voltage}^2}{\text{ohmic power loss}} = \frac{V^2}{P_{loss}} = \frac{(GL)^2}{P_{loss}}$$

Note: the impedance is here given in “Linac Ohms” , in “Circuit Ohms” the number would be only 50%: 1”Linac Ohm”= 0.5”Circuit Ohm”

So one obtains easily the power

$$P_{loss} = \frac{(GL)^2}{R}$$

⇒ High R means little losses

Losses vs. Acceleration

Power loss per unit length in the wall

$$P'_{loss} = \frac{G^2}{R'}$$

Power per unit length given to the beam

$$P'_{beam} = IG$$

The ratio is

$$\frac{P'_{beam}}{P'_{loss}} = R'\frac{I}{G}$$

⇒ For high efficiency want

- lower gradient G
- higher current I
- higher shunt impedance R'

- The average beam current is determined bzy the luminosity goal
- The machines are pulsed to increase the beam current while the RF is on
- So what limits the shunt impedance and the beam current?

Shunt Impedance

The shunt impedance R depends on three main factors

- structure geometry
- structure material
- RF frequency

The energy stored in the structure is only a function of the geometry

- all energy is in the vacuum
- described by R/Q (and ω)

The rate of losses depends on the surface material, the shape and the RF frequency

- material is most important
- described by Q

Hence, the value of R can be written as

$$R = \frac{R}{Q} Q$$

Stored Energy R/Q

- We can simply calculate R/Q

$$R = \frac{\text{effective voltage}^2}{\text{ohmic power loss}} = \frac{(GL)^2}{P_{loss}}$$

$$Q = \frac{\text{stored energy}}{\text{ohmic energy loss per radian of RF circle}} = \frac{E}{P_{loss}}\omega$$

- Hence

$$(R/Q) = \frac{(GL)^2}{P_{loss}}\frac{P}{E\omega} = \frac{(GL)^2}{E\omega}$$

so one can calculate

$$E = \frac{(GL)^2}{(R/Q)\omega}$$

$\Rightarrow$ The structure geometry defines R/Q and does not depend on the material

Remark: Scaling of R/Q

The structure geometry defines

$$\left(\frac{R}{Q}\right) = \frac{(GL)^2}{E\omega}$$

Energy in the structure (same gradient) scales with the volume

$$E \propto \lambda^3$$

the energy gain GL scales with

$$GL \propto \lambda$$

and the frequency ω as

$$\omega = 1/\lambda$$

Hence

$$\Rightarrow \frac{R}{Q} = \frac{(GL)^2}{E}\frac{1}{\omega} \propto \frac{\lambda^2}{\lambda^3}\frac{\lambda}{1} = \mathrm{const}$$

A typical value for superconducting cavities is 100Ω per cell

Quality Factor Q

- The internal quality factor Q (here the same as Q_0) is defined as

$$Q = \frac{\text{stored energy}}{\text{ohmic energy loss per radian of RF circle}} = \frac{E}{P_{loss}}\omega$$

this allows to easily write the decay of the energy due to ohmic losses

$$E(t) = E_0 \exp(-\omega t/Q)$$

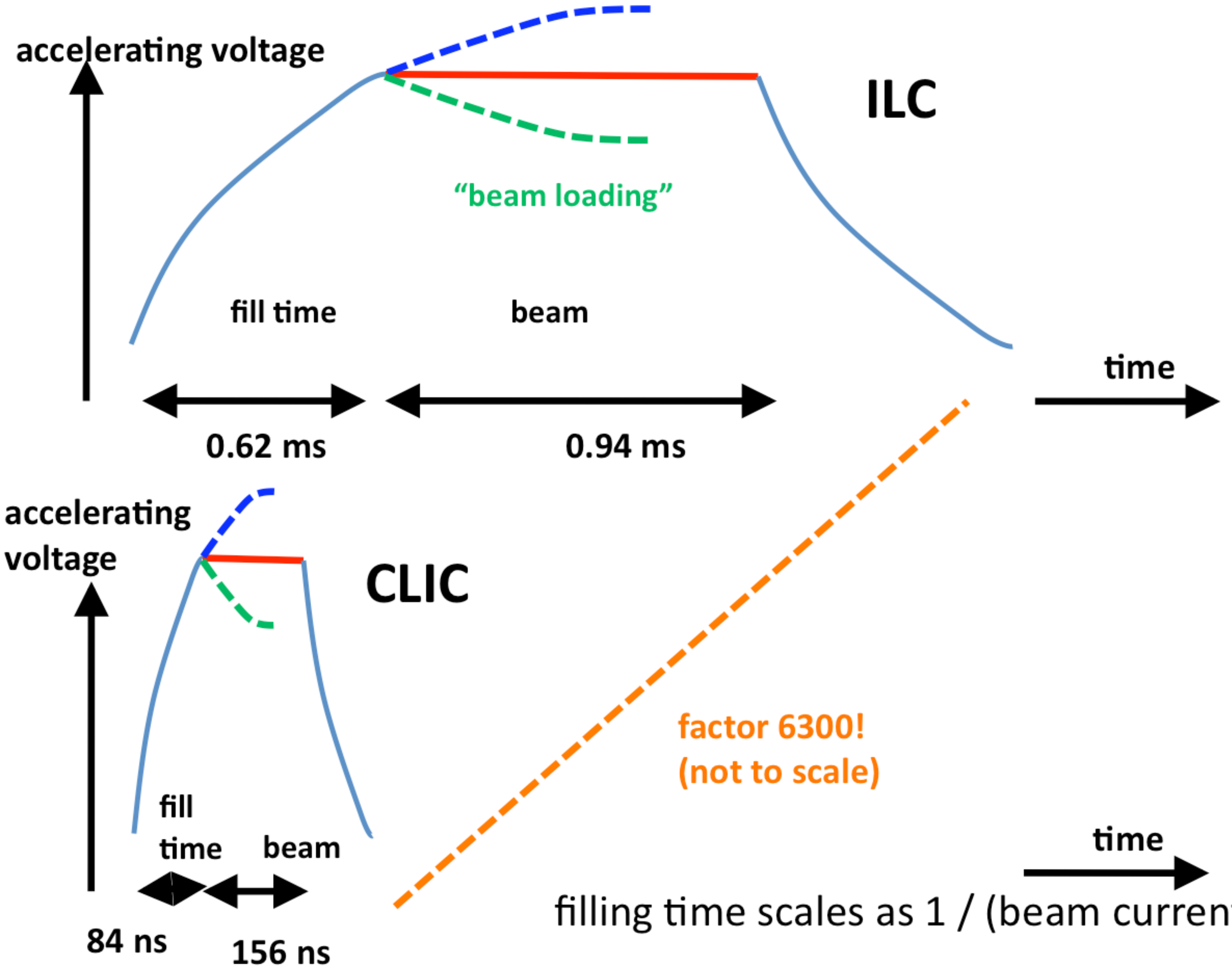
⇒ High Q indicates little losses

Example values are

- $O(10^{10})$ for superconducting
- $O(10^4)$ for normal conducting structures

- Scaling is
  - $\propto \omega^{-2}$ for superconducting structures (but upper limit from other resistivity)
  - $\propto \sqrt{\omega^{-1}}$ for normal conducting structures

Required RF Pulse Length (Outdated Numbers)



filling time scales as 1 / (beam current)

Filling a Standing Wave Cavity

- Once filled, the energy should be kept in the cavity

  ⇒ can only allow little coupling to the outside, i.e. large Q_E

$$E(t) = E(t_0)\exp\left(-\frac{t-t_0}{Q_E}\omega\right) \qquad G(t) = G(t_0)\exp\left(-\frac{t-t_0}{2Q_E}\omega\right)$$

  ⇒ RF power sent to the structure can be reflected

⇒ So we need to match the coupling to have no reflection at nominal gradient

- First we chose the input power to correspond to the power extracted by the beam (neglecting losses in the wall)

$$P_{in} = G_{target} L I_{beam}$$

Filling a Standing Wave Cavity (cont.)

- Now we determine the required coupling Q_E

  The reflected voltage for input power P_{in} is given by

$$V_{refl} = \sqrt{aP_{in}}$$

  The stored energy causes a power flow in direction of the reflected wave

$$P_{cavity} = \frac{E\omega}{Q_E}$$

  This causes a field outside of the coupler iris

$$V_{out} = -\sqrt{aP_{out}}$$

  This yields the voltage for the load V_{load}:

$$V_{load} = V_{refl} + V_{out} = \sqrt{aP_{in}} - \sqrt{a\frac{E_{target}}{Q_E}\omega}$$

  In order to have no power going to the load we require

$$V_{load} = 0$$

$$\Rightarrow P_{in} = P_{out} = \frac{E_{target}}{Q_E}\omega$$

$$\Rightarrow Q_E = \frac{E_{target}}{P_{in}}\omega$$

Filling a Standing Wave Cavity (cont.)

- Now we calculate the fill time

  To simplify, we define

$$t_c = \frac{E_{target}}{P_{in}}$$

  We will not go through the calculation here but present the result

  The gradient in the structure is given by

$$G = 2G_{target} \left(1 - \exp\left(-\frac{t}{2t_c}\right)\right)$$

  Hence the target gradient is reached after the fill time t_{till}:

$$t_{fill} = \ln(4) t_c$$

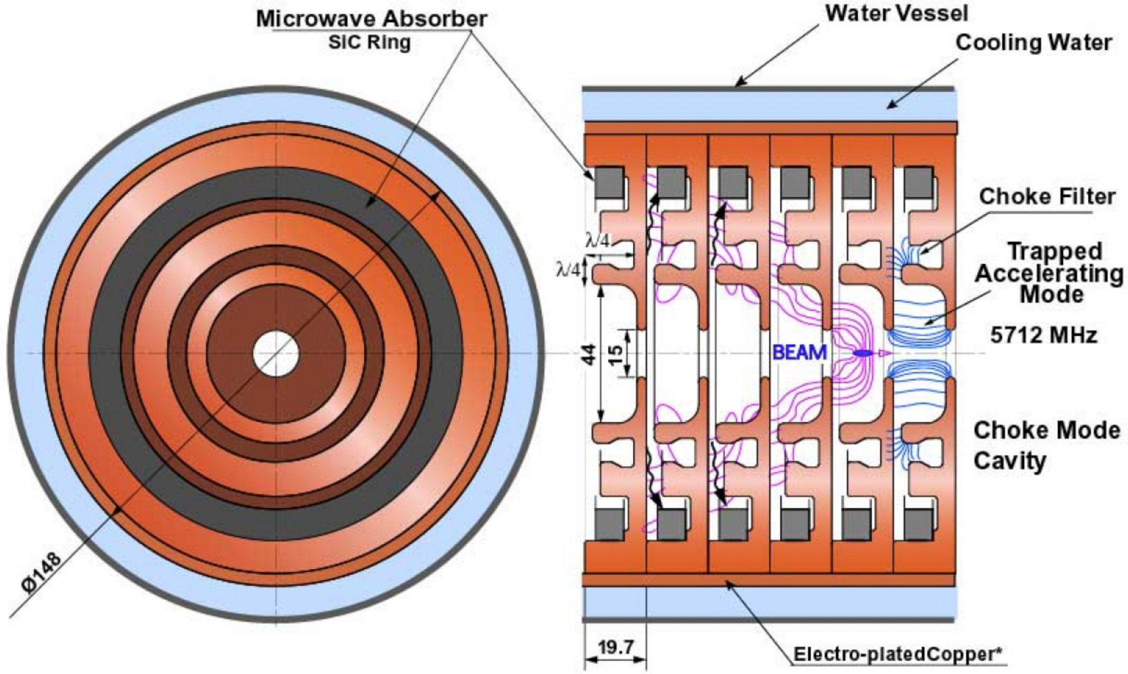
Filling A Travelling Wave Cavity

- In a travelling wave, normal conducting structure the fill time is the time for an energy to flow from input coupler to output coupler
  - in principle need to add rise time (but for RF experts)

  $\Rightarrow$ get your number from the RF expert
- We will discuss the wakefield view of the beam loading to understand
  - reason for output power
  - beam loading compensation

Passage of a Particle

- A particle in the structure will
  - $\Rightarrow$ extract or leave energy (depending on energy in structure)
  - induce electromagnetic wakefields
    - $\Rightarrow$ cosine-like longitudinal (monopole) and sine-like transverse (dipole) modes for offset driving particles
    - $\Rightarrow$ the wakefield does not depend on the energy in the structure



- The longitudinal wakefield $W_L(z)$ expresses the average acceleration of a particle at time z along the structure $[V/mC]$
- The transverse wakefield $W_\perp(z)$ expresses the average transverse deflection of a particle at time z along the structure $[V/m^2C]$

Wakefield

- The field seen by a following particle depends on the time and position along the structure

$$G_{wake}(s, z)$$

- For most purposes we average this field for the passage through the structure
- A bunch with charge Ne and transverse offset δ is followed at distance z by a witness electron
  - Energy change is $\Delta P_L c \approx \Delta E = Ne\, W_L(z) L\, e$
  - Transverse deflection $\Delta P_\perp c = Ne\, W_\perp(z) L\delta\, e$
- Analytic longitudinal wake for iris radius a

$$W_L(z \to 0) = \frac{Z_0 c}{\pi a^2}$$

- Analytic transverse wake

$$W_\perp(z \to 0) = \frac{2 Z_0 c}{\pi a^4} z$$

- For larger distances one has to perform simulations

Wakefield and Power Extraction

- Why can a wakefield model be used for the beam loading?
  - i.e.

$$\Delta G(q) = \mathrm{const}\ q$$

- The energy stored per unit length in the accelerating structure is

$$E'(s) = \frac{G(s)^2}{(R'/Q)(s)\omega}$$

- The reduction of acclerating field due to the passing charge q is $-\Delta G(s)$
- This yields for the energy lost by the structure

$$\Delta E'_{lost}(s) = \frac{G^2(s) - (G(s) - \Delta G(s))^2)}{(R'/Q)(s)\omega} \quad \Rightarrow \Delta E'_{lost}(s) = \frac{2G(s)\Delta G(s) - (\Delta G(s))^2}{(R'/Q)(s)\omega}$$

- The beam extracts an energy

$$\Delta E'_{beam}(s) = q\left(G(s) - \frac{1}{2}\Delta G(s)\right)$$

hence

$$q\left(G(s) - \frac{1}{2}\Delta G(s)\right) = \frac{2G(s)\Delta G(s) - (\Delta G(s))^2}{(R'/Q)(s)\omega}$$

$$\Rightarrow \Delta G(s) = \frac{(R'/Q)(s)\omega}{2}q$$

$\Rightarrow$ The gradient change depends only on the charge not the initial gradient, as expected

- Note: I simplified a bit (sorry, but this is easier with cheating)

Beam Loading in Travelling Wave Structure

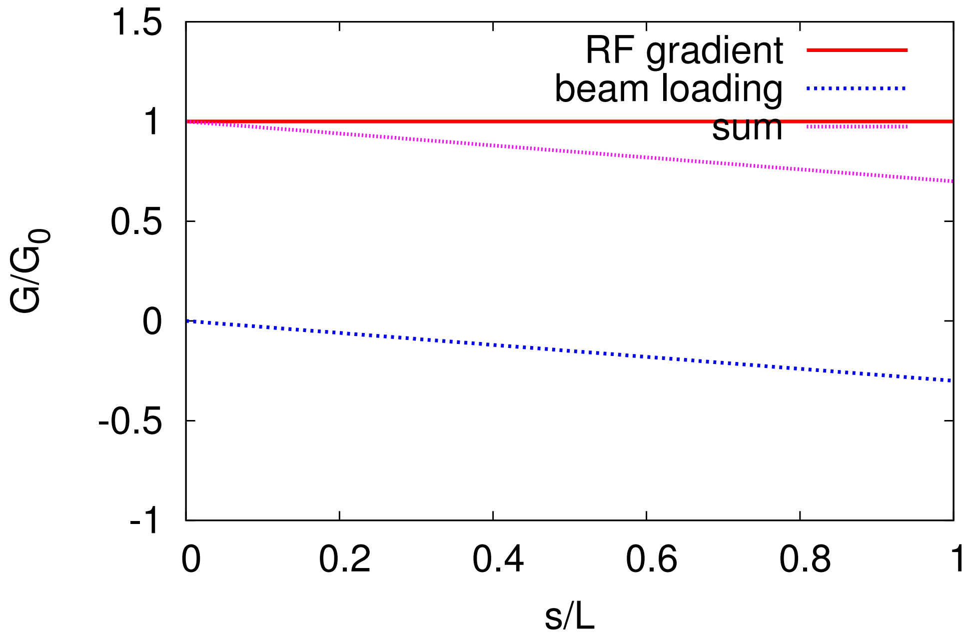
- Consider constant impedance, $Q = \infty$
- Field induced by passing bunch is moving forward
  - as is external RF

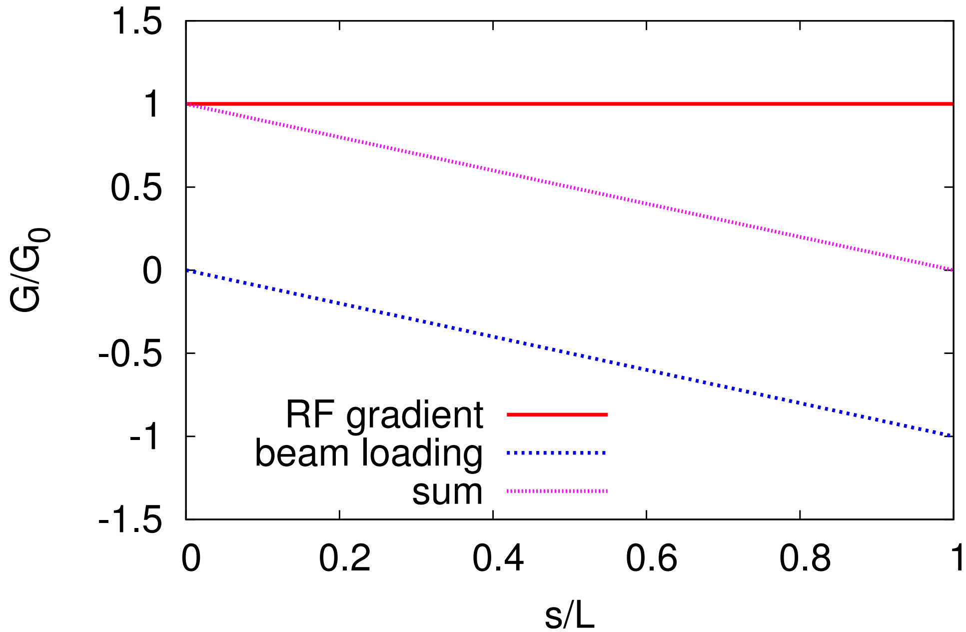
  $\Rightarrow$ beam loading fields build up along the structure
- The RF loses power in the wall

$\Rightarrow$ The gradient decreases along the structure

Film

- Warning: simplified flying saussage model, not strictly correct but good for some understanding

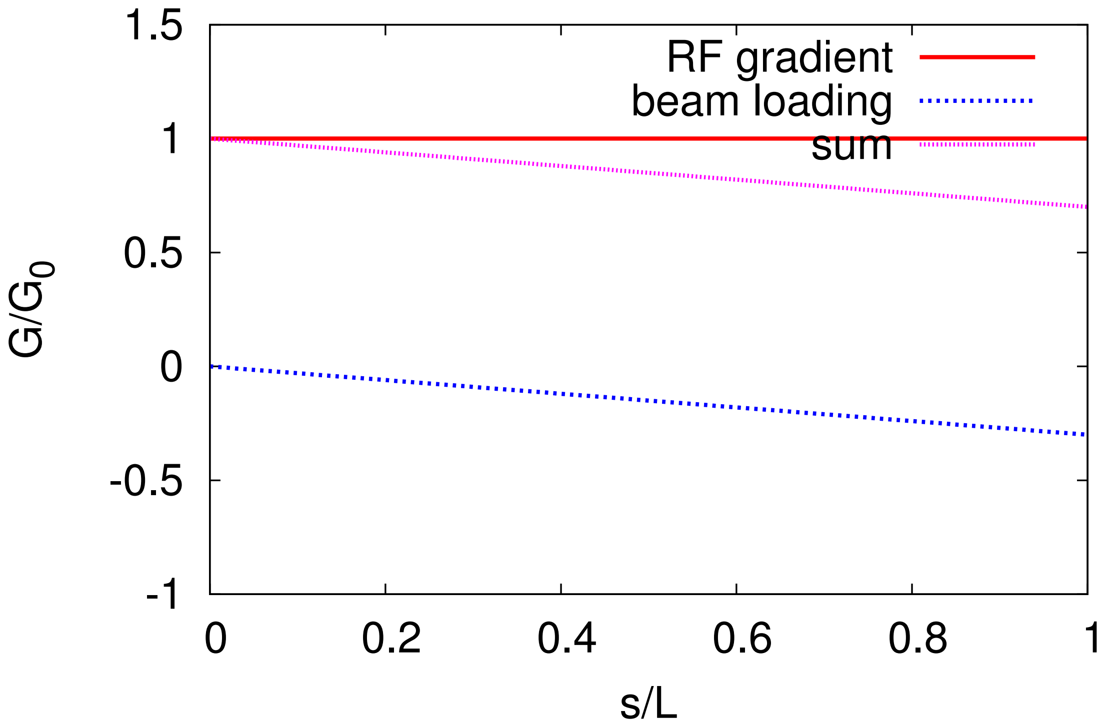




Beam Loading Compensation

- Constant impedance example with losses into the walls
- The first bunch sees no beam loading

⇒ We need to shape the RF pulse accordingly



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Structure Tapering

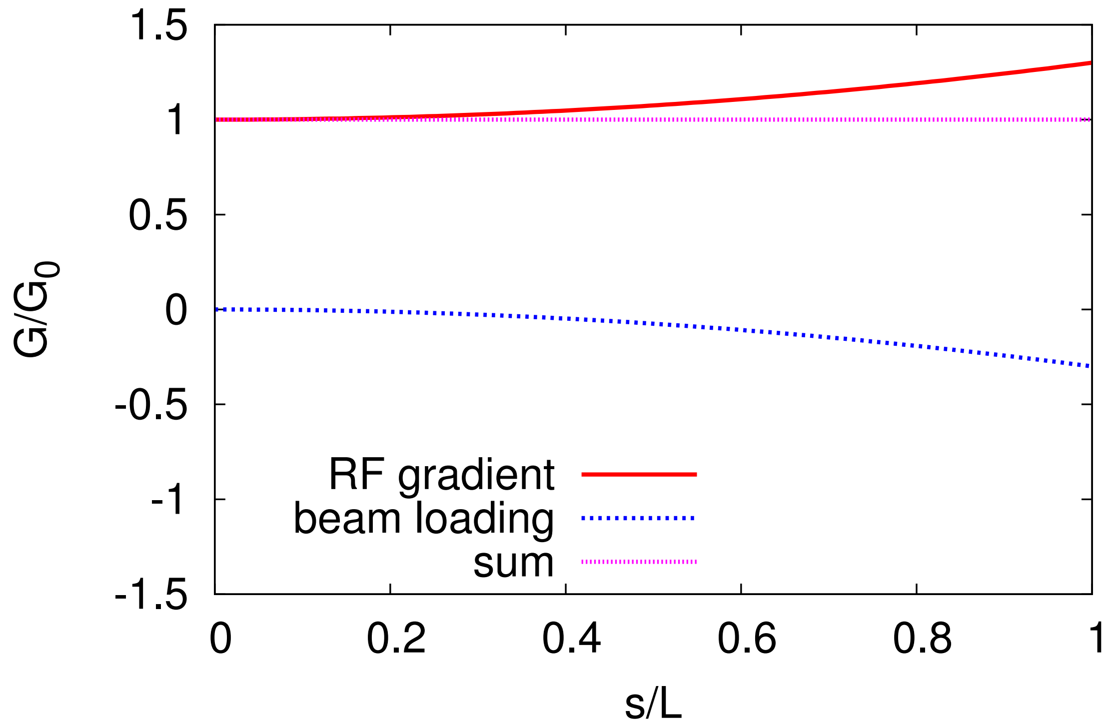
- By decreasing the along the structure iris radius the local R/Q increases

⇒ The unloaded gradient increases along the structure

⇒ The loaded gradient remains constant

- In practice we have to ensure that the RF constraints are fulfilled in each cell

- Note: beam loading could reduce breakdown rate



- Note: in CLIC about 20% of the RF power are lost in the loads during the flat top

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Constant Impedance vs. Constant Gradient

- In a travelling wave structure, the beam extracts energy during its passage

  ⇒ the gradient will be lower at the end of the structure

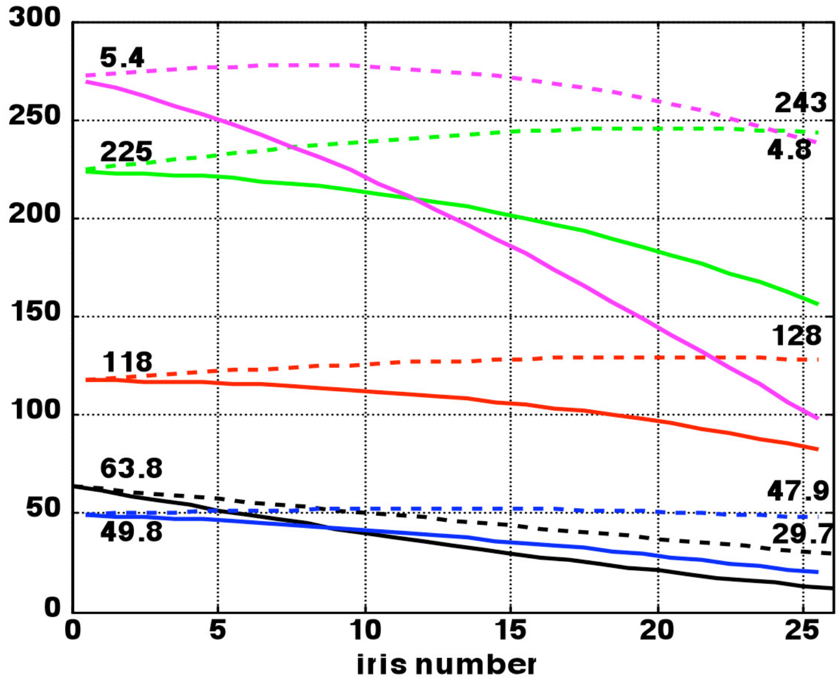
- This can be avoided by reducing the iris radius along the structure (tapering)

  - the smaller irises produce more gradient per power flowing through them

- An additional difference exists for the long-range transverse wakefields

  - in a constant impedance structure one strong wakefield mode exists

  - in a tapered structure many small modes exist which reduces the effective wakefield



RF to Beam Power Efficiency Summary

parameter	CLIC	ILC (RDR)
R'/Q	$\approx 11\,\mathrm{k\Omega/m}$	$1.036\,\mathrm{k\Omega/m}$
Q	≈ 6000	$\approx 10^{10}$
R'	$\approx 66\,\mathrm{M\Omega/m}$	$\approx 10^{7}\,\mathrm{M\Omega/m}$

- ILC: $I \approx 5.8\,\mathrm{mA}$

$\Rightarrow$

$$\frac{P'_{beam}}{P'_{wall}} \approx 1650$$

- CLIC: $I \approx 1.2\,\mathrm{A}$

$\Rightarrow$

$$\frac{P'_{beam}}{P'_{wall}} \approx 0.8$$

- Efficiency is

$$\eta = \frac{\tau_{beam}}{\tau_{beam} + \tau_{fill}} \frac{P_{beam}}{P_{beam} + P_{loss} + P_{out}}$$

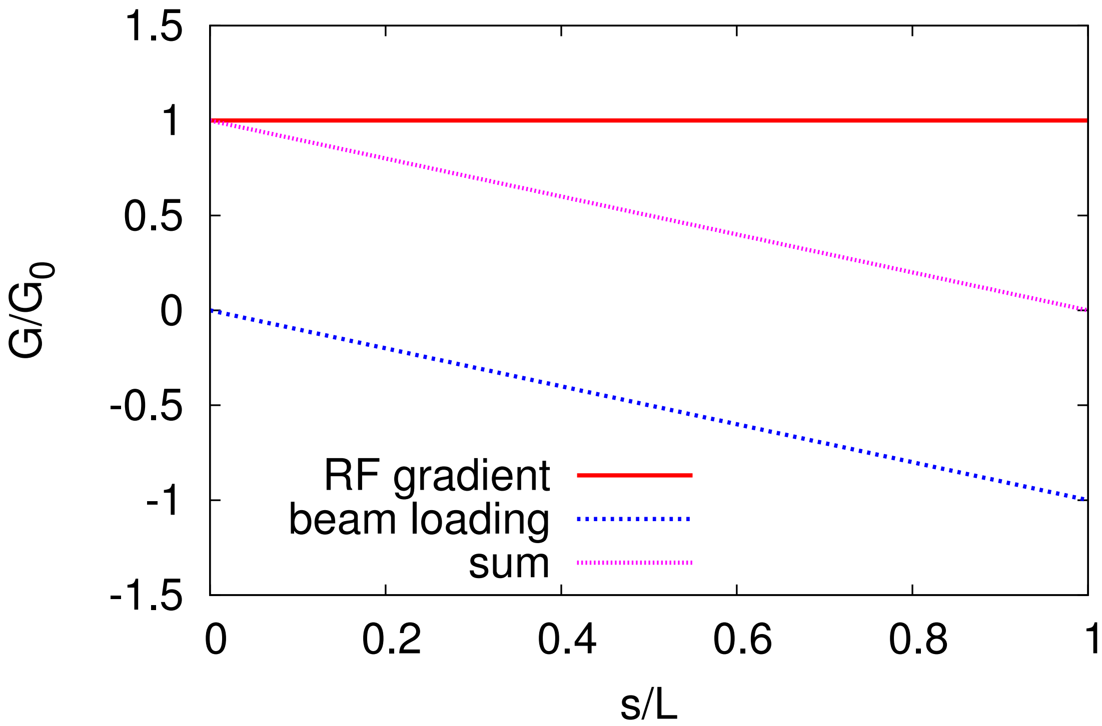
- Plugging in numbers for ILC

$$\eta \approx \frac{730\,\mu\mathrm{s}}{730\,\mu\mathrm{s} + 900\,\mu\mathrm{s}} \approx 0.45$$

- Plugging in (slightly older) numbers for CLIC

$$\eta = \frac{156\,\mathrm{ns}}{156\,\mathrm{ns} + 83\,\mathrm{ns}} \cdot \frac{27\,\mathrm{MW}}{27\,\mathrm{MW} + 25\,\mathrm{MW} + 12\,\mathrm{MW}} \approx 0.65 \cdot 0.42 \approx 0.277$$

Remark: Drive Beam Accelerator



- High current at low gradient allows high efficiency

$$\frac{P'_{beam}}{P'_{wall}} = \frac{R'I}{G}$$

- Acceleration at low frequency is efficient
  - Q is high $Q \propto 1/\sqrt{\omega}$
  - klystrons are efficient
- In CLIC $\eta \approx 97.5\%$ expected

- Structure needs to be long enough not to have power leaking out

$$G = G_{RF} + G_{BL} \quad G = \frac{1}{2} G_{RF}$$

$$G_{BL} \propto LI$$

ILC Limiting Factors for Efficiency

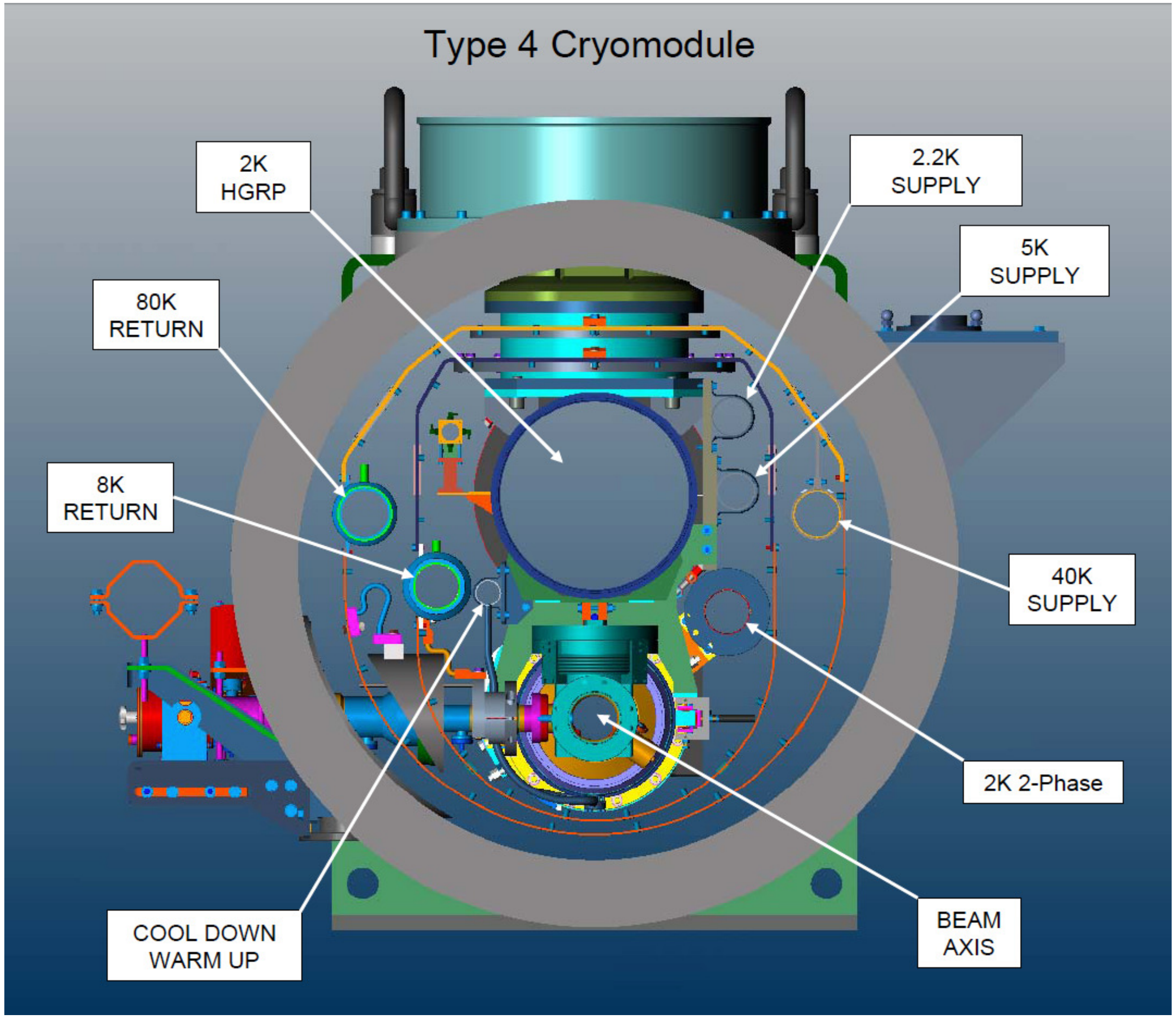
- The transfer of RF to the beam is almost perfect during the pulse
- The main power consumption is for the cooling
  - to cool $1\,\mathrm{W}$ at $2\,\mathrm{K}$ requires about $700\,\mathrm{W}$

  remember Carnot process, in best case

$$\frac{P_{cool}}{P_{source}} \geq \frac{T_2 - T_1}{T_1}$$

- Additionally a number of other sources exist
  - higher order modes induced by the beam
  - static losses through the cryostat

$\Rightarrow$ Cooling power is about twice the beam power ($35\,\mathrm{kW}$)



	40–80 K		5–8 K		2 K		Total
	Static	Dynamic	Static	Dynamic	Static	Dynamic	
Heat load (W)	177.6	270.3	31.7	12.5	5.1	29.0	
Installed power (kW)	4.4	6.2	9.6	3.5	8.1	28.5	60.4

CLIC Limiting Factors for the Efficiency

- A lower gradient G
  - leads to a longer main linac hence to higher cost
  - requires reducing the current
- A higher shunt impedance R'
  - leads usually to larger wakefields also in the transverse hence to a less stable beam
- A higher beam current I
  - leads to a less stable beam
- An optimisation can be performed of the whole machine
  - varying G and R' and adjusting the current to the highest possible value
  - selecting the best combination taking into account luminosity and cost
- This optimisation has indeed been performed for CLIC

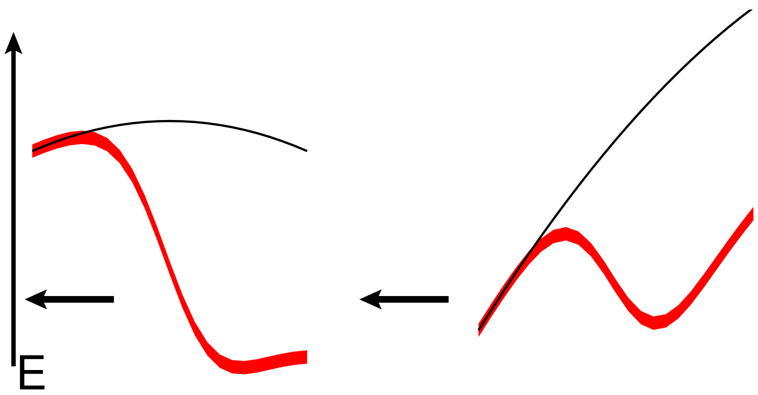
$\Rightarrow$ let us see which is the highest current for a given structure and gradient

Beam Parameters: Longitudinal Wake and Bunch Charge Limits

Wakefields and Bunch Length

- Aim for shortest possible bunch to reduce transverse wakefield effects
- Energy spread into the beam delivery system should be limited to about 1% full width or 0.35% rms
- Multi-bunch beam loading compensated by RF
- Single bunch longitudinal wakefield needs to be compensated

  $\Rightarrow$ accelerate off-crest



- Limit around average $\Delta\Phi \leq 12^\circ$

  $\Rightarrow \sigma_z = 44\,\mu\text{m}$ for $N = 3.72 \times 10$

Specific Wakefields

- Longitudinal wakefields contain more than the fundamental mode
- We will use wakefields based on fits derived by Karl Bane

  l length of the cell

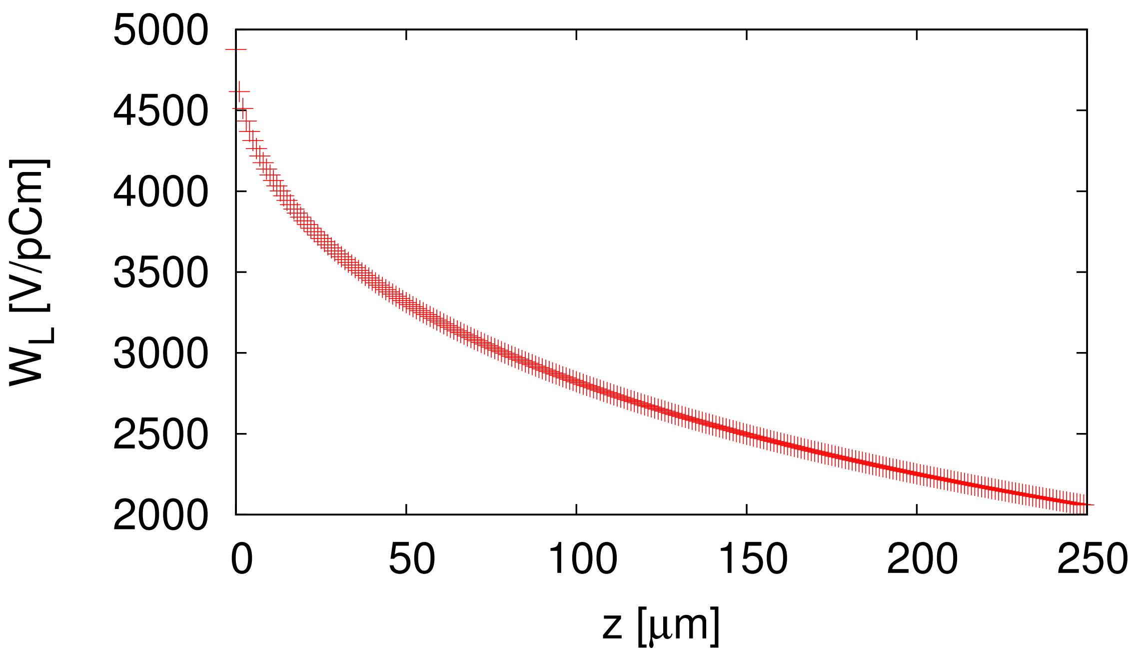
  a radius of the iris aperture

  g length between irises

$$z_0 = 0.41 a^{1.8} g^{1.6} \left(\frac{1}{l}\right)^{2.4}$$

$$W_L(z) = \frac{Z_0 c}{\pi a^2} \exp\left(-\sqrt{\frac{z}{z_0}}\right)$$

- Use CLIC structure parameters

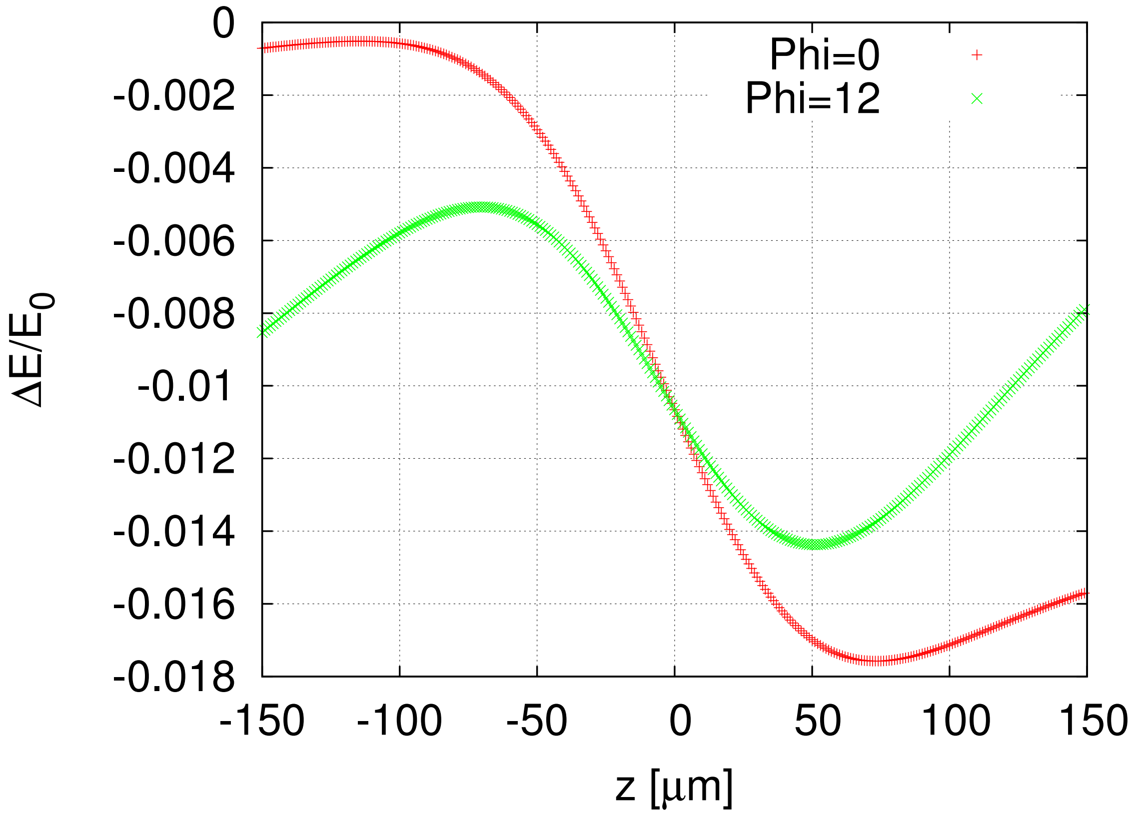


- Summation of an infinite number of cosine-like modes
  - calculation in time domain or approximations for high frequency modes

Energy Spread at End of Linac

- We use a constant RF phase along the linac
- Have to fold the longitudinal wakefield with bunch charge distribution

$$\delta G(z_0) = \int_{-\infty}^{z_0} \rho(z) W_L(z_0 - z) dz$$



Recipe for Choosing the Bunch Parameters

- Decide on the average RF phase
  - OK, we fix 12°
  - smaller values give less bunch charge, larger values give more sensitivity to phase jitter
- Decide on an acceptable energy spread at the end of the linac
  - OK, we choose 0.35%
  - mainly from BDS and physics requirements
- Determine $\sigma_z(N)$
  - choose a bunch charge
  - vary the bunch length until the final energy spread is acceptable
  - choose next charge
- Determine which bunch charge (and corresponding bunch length) can be transported stably

Simplified Treatment

Assume

- $W_z(s) = W_z = \mathrm{const}$
- uniform bunch with length $L \ll \lambda$
- and use linear approximation

Field seen by first particle

$$G_H = G\cos\left(\phi - \frac{L}{2}\frac{2\pi}{\lambda}\right) \approx G\left(\cos(\phi) - \frac{L}{2}\frac{2\pi}{\lambda}\sin(\phi)\right)$$

Field seen by last particle

$$G_T = G\cos\left(\phi + \frac{L}{2}\frac{2\pi}{\lambda}\right) \approx G\left(\cos(\phi) + \frac{L}{2}\frac{2\pi}{\lambda}\sin(\phi)\right) - NeW_z$$

We require (this automatically solves the equation for all other particles)

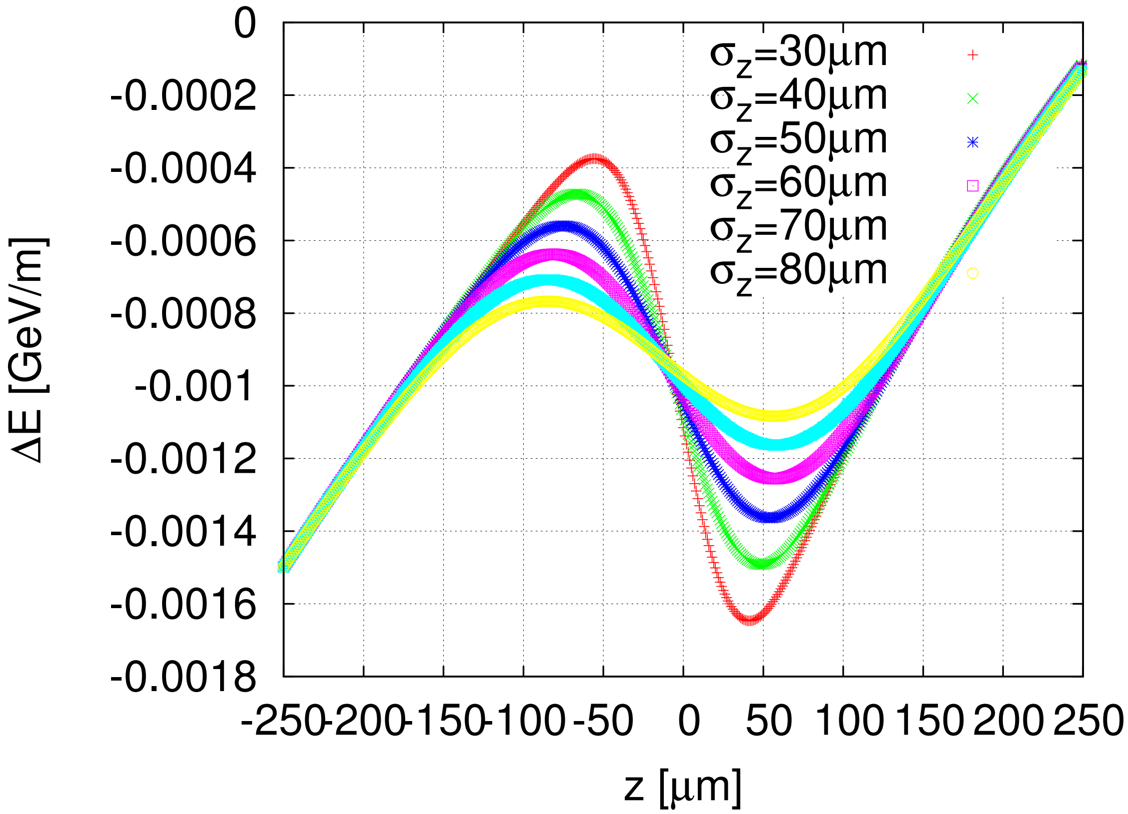
$$G_H = G_T$$

which leads to

$$L = \frac{NeW_z}{G}\frac{\lambda}{2\pi\sin(\phi)}$$

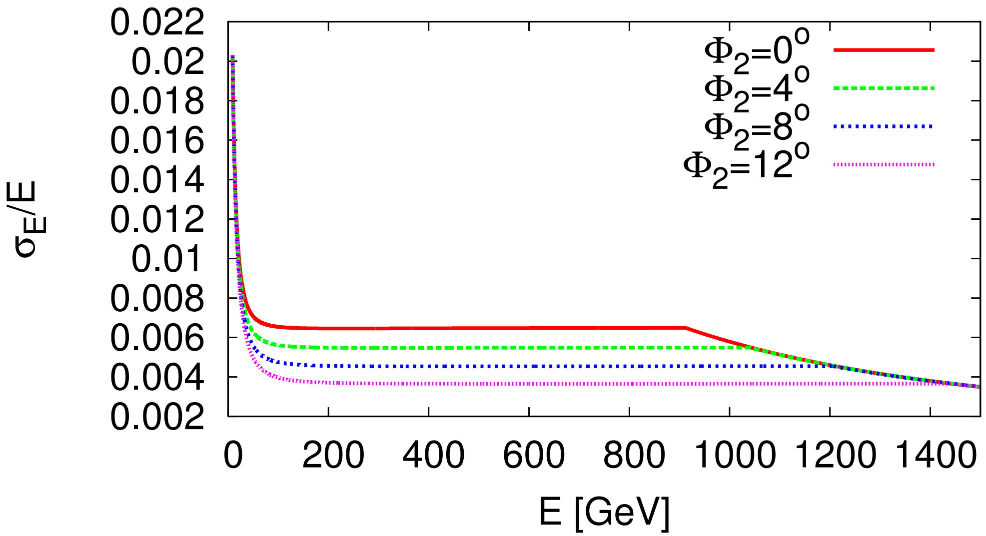
Dependence of Energy Spread on Bunch Length

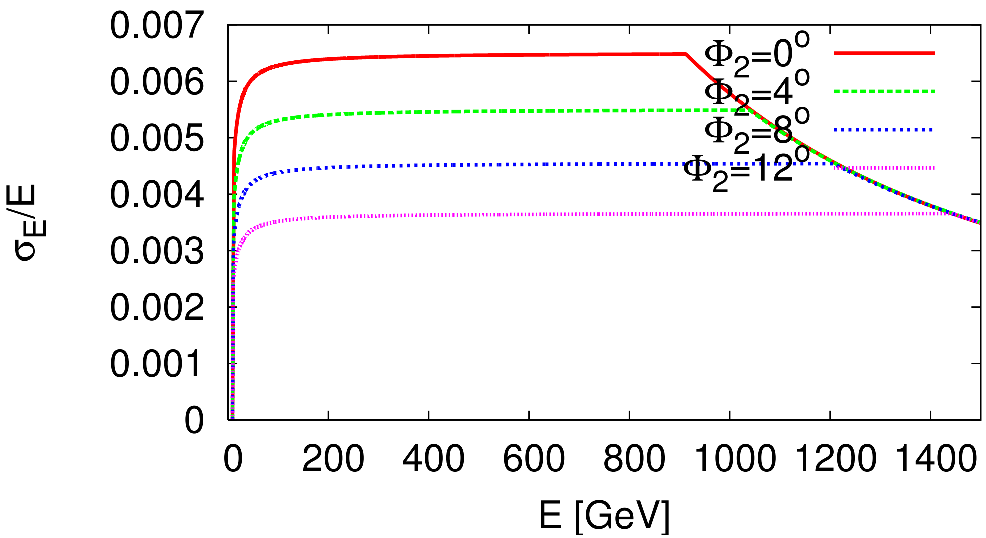
- For a given charge and phase the bunch length is varied



Note: Energy Spread Along Linac

- Three regions
  - generate
  - maintain
  - compress
- Configurations are named according to RF phase in section 2
- Trade-off in fixed lattice
  - large energy spread is more stable
  - small energy spread is better for alignment





Beam Parameters: Beam Transport and Emittance

Know $\sigma_z(N)$ but current limit will depend on wakefields and lattice design, important problem

Emittance

- The beam particles do not have identical coordinates
  - they occupy some phase space
- According to Liouville theorem (from the Liouville equation)

$$\frac{d\rho}{dt} = \frac{\partial\rho}{\partial t} + \sum_{i=1}^{N}\left[\frac{\partial\rho}{\partial q_i}\dot{q}_i + \frac{\partial\rho}{\partial p_i}\dot{p}_i\right] = 0$$

  the density in phase space around a trajectory remains constant in an unperturbed system

- For some reason particles are conventionally not described by (x, y, z, p_x, p_y, p_z) but by (x, y, z, x', y', E)

  $\Rightarrow$ in this representation the "phase space" changes

- We use the emittance to describe the phase space volume
  - geometric emittance is the actual size in $x\ x'$ and changes with acceleration
  - the normalised emittance is size in $x\ x'$ for $\gamma = 1$ and is constant

Why is the Emittance Important?

- The luminosity can be written as

$$\mathcal{L} = H_D \frac{N^2 n_b f_r}{4\pi \sigma_x^* \sigma_y^*}$$

H_D a factor usually between 1 and 2, due to the beam-beam forces
N the number of particles per bunch
n_b the number of bunches per beam pulse (train)
f_r the frequency of trains
σ_x^* and σ_y^* the transverse dimensions at the interaction point

- We will see that $\sigma_{x,y}$ can be written as the function of two parameters

$$\sigma_{x,y} = \sqrt{\frac{\beta_{x,y}\epsilon_{x,y}}{\gamma}}$$

$\epsilon_{x,y}$ is the normalised emittance, a beam property
$\beta_{x,y}$ is the beta-function, a lattice property

Main Linac Emittance Growth

- The vertical emittance is most important since it is much smaller than the horizontal one (10 nm vs. 600 nm, 24 nm vs. 8400 nm)
- For a perfect implementation of the machine the main linac emittance growth would be negligible
- Two main sources of emittance growth exist
  - static imperfections
  - dynamic imperfections
- The emittance growth budget is 5 nm for static imperfections
  - i.e. 90% of the machines must be better
- For dynamic imperfections the budget is 5 nm
  - but short term fluctuation must be smaller to avoid problems with luminosity tuning

Low Emittance Transport Challenges

- Static imperfections

  errors of reference line, elements to reference line, elements. . .

  excellent pre-alignment, lattice design, beam-based alignment, beam-based tuning

- Dynamic imperfections

  element jitter, RF jitter, ground motion, beam jitter, electronic noise,. . .

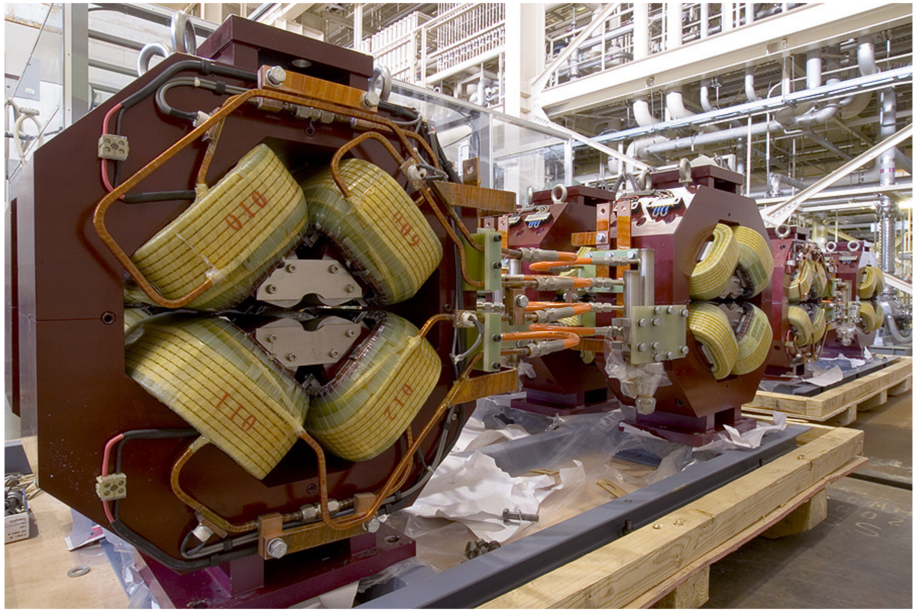
  lattice design, BNS damping, component stabilisation, feedback, re-tuning, re-alignment

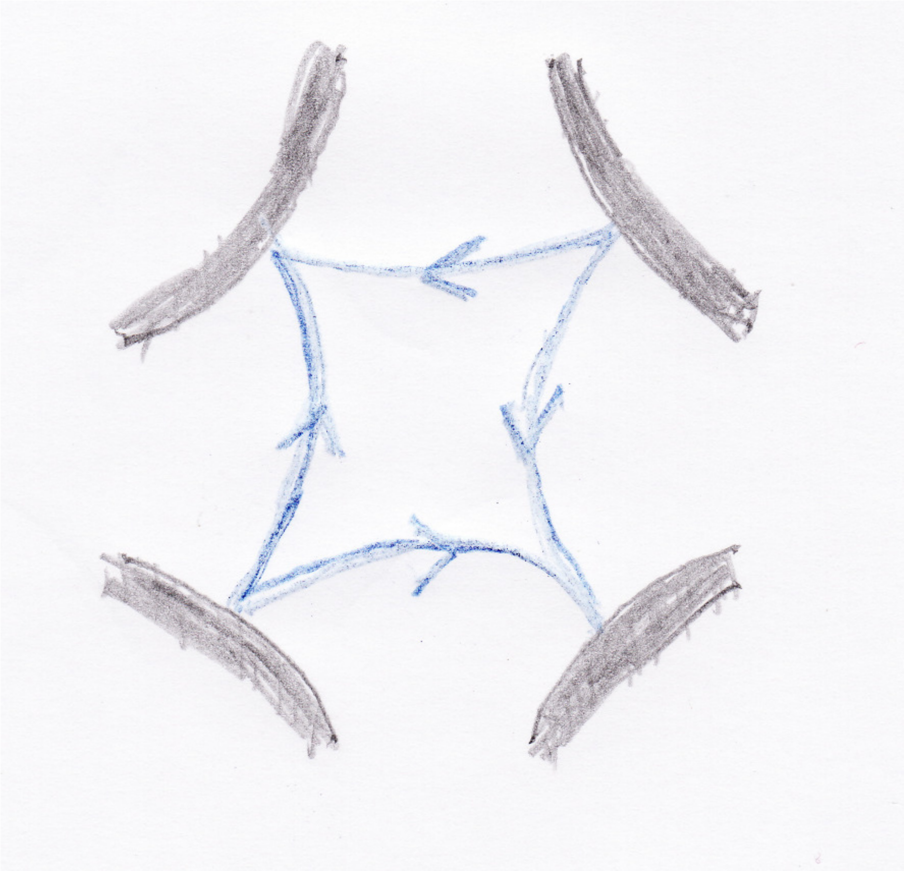
- Combination of dynamic and static imperfections can be severe

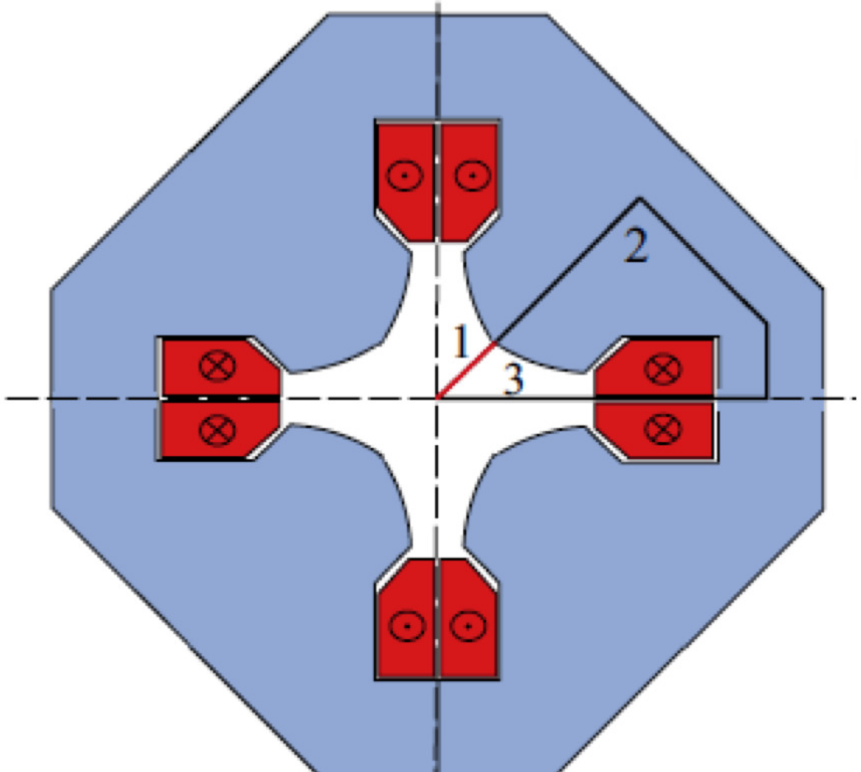
- Lattice design needs to balance dynamic and static effects

Guiding the Beams: Quadrupoles

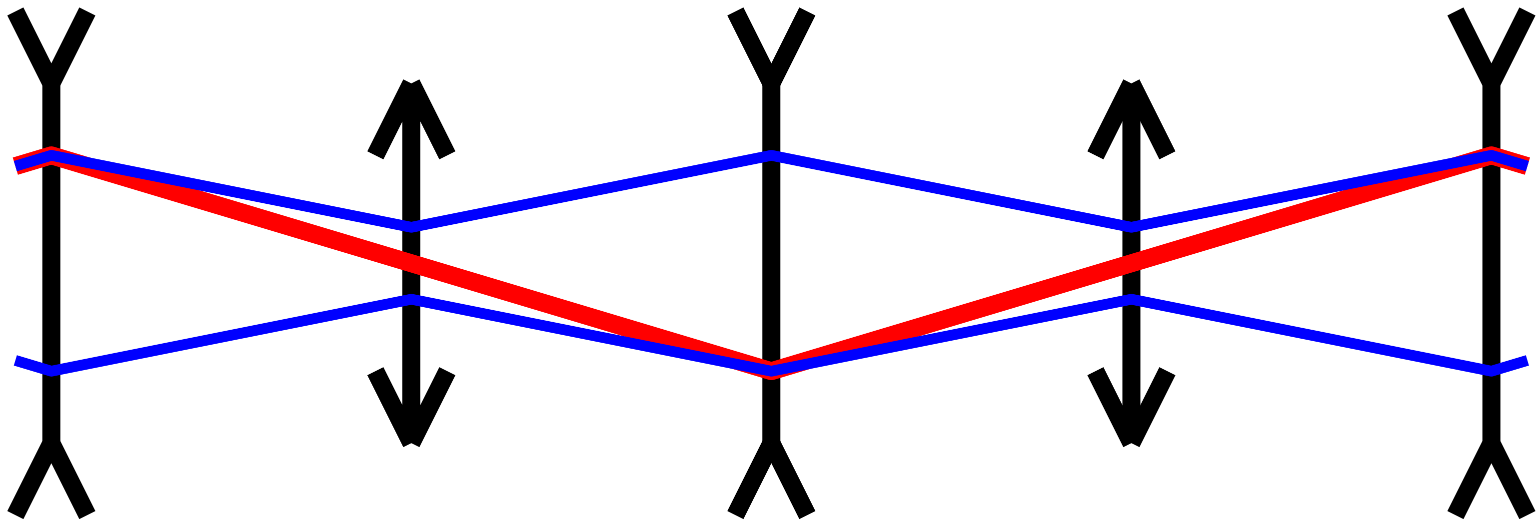
- The focusing is provided by quadrupoles
- They focus in one plane but defocus in the other planes
  - octopoles would focus in x and y but defocus in the planes at $45°$
  - also their magnetic field is not linear







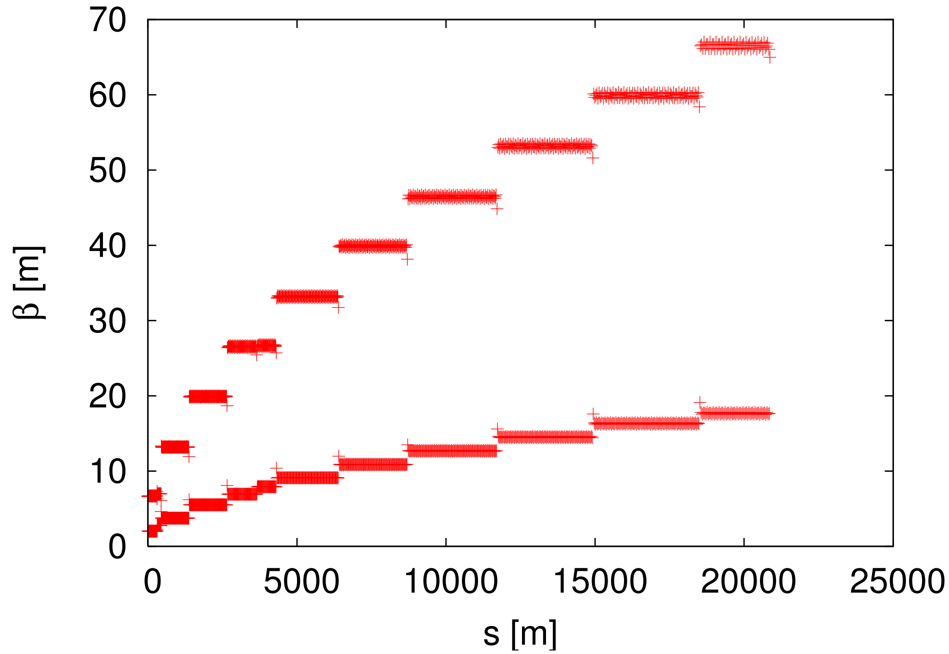
FODO Lattice



- Focusing is achieved by alternating focusing and defocusing quadrupoles

CLIC Lattice Design

- Used $\beta \propto \sqrt{E}$, $\Delta\Phi = \mathrm{const}$
  - balances wakes and dispersion
  - roughly constant fill factor
  - phase advance is chosen to balance between wakefield and ground motion effects
- Preliminary lattice
  - made for $N = 3.7 \times 10^9$
  - quadrupole dimensions need to be confirmed
  - some optimisations remain to be done
- Total length 20867.6m
  - fill factor 78.6%

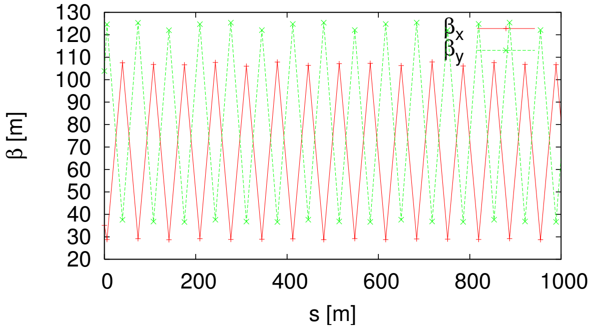


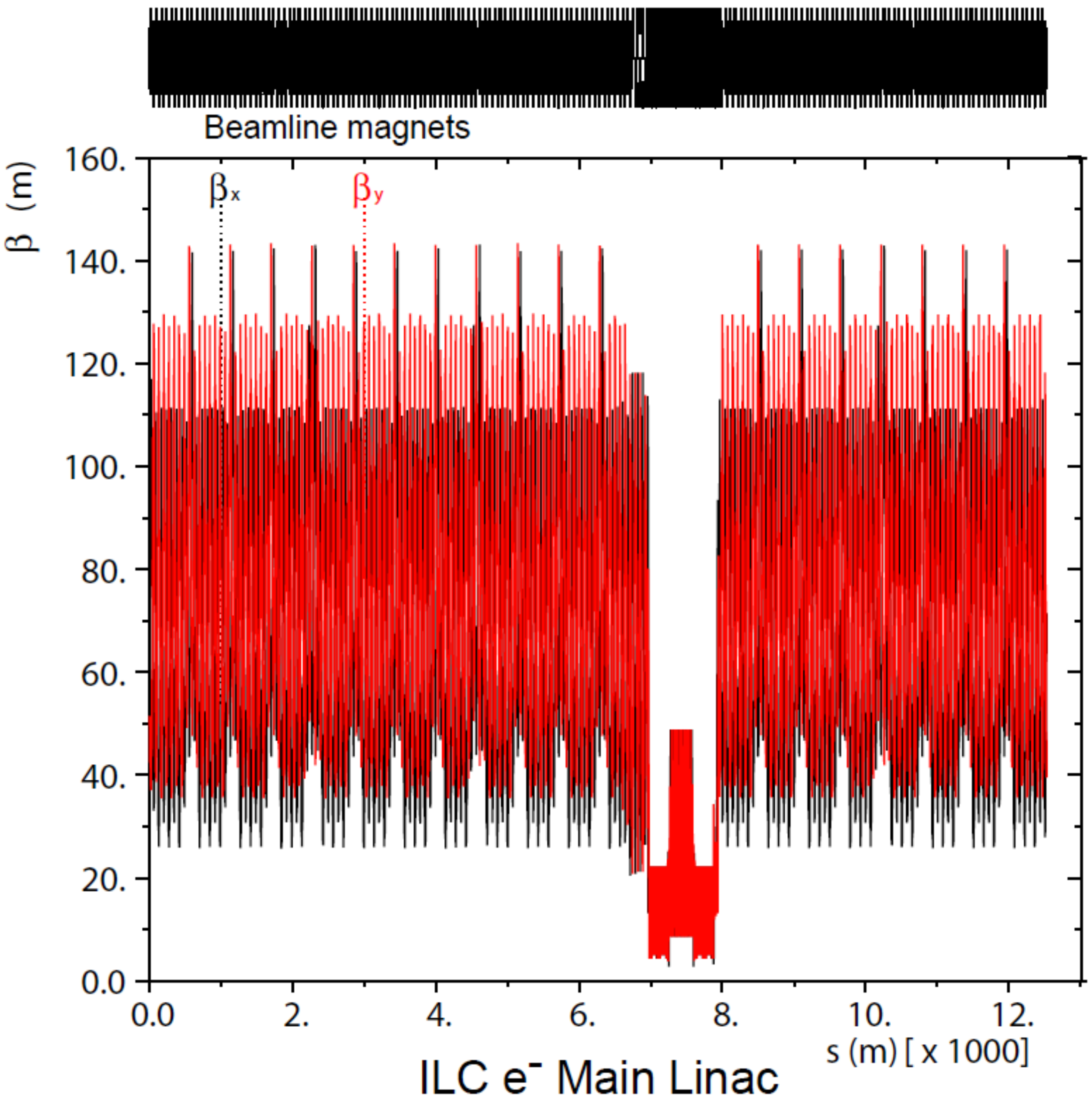
- 12 different sectors used
- Matching between sectors using 7 quadrupoles to allow for some energy bandwidth

  Note: fill factor = active length/total length

ILC Lattice

- In the ILC constant quadrupole spacing is chosen
- The phase advance per cell is constant
- The phase advance is different in the two planes
  - reduces some coupling effects between the two planes





Hill's Equation and Beta-Functions

- In many interesting cases the particle motion can be described by Hill's equation

$$x''(s) + K(s)x(s) = 0$$

i.e. a harmonic ascillator with varying spring constant
The solutions for this equation can be formulated as

$$x(s) = \sqrt{\epsilon\beta(s)}\cos(\phi(s) + \phi_0)$$

$$x'(s) = \sqrt{\frac{\epsilon}{\beta(s)}}\left[\frac{\beta'}{2}\cos(\phi(s) + \phi_0) - \sin(\phi(s) + \phi_0)\right]$$

where

$$\phi(s) = \int_0^s \frac{1}{\beta(s')}ds'$$

and β has to fulfill

$$\frac{\beta''\beta}{2} - \frac{\beta'^2}{4} + K\beta^2 = 1$$

- The solution can be easily verified
- It depends partially on the particle (ϵ, ϕ_0) and partially on the lattice (β)

Phase Space Representation

$$x(s) = \sqrt{\epsilon\beta(s)}\cos(\phi(s)+\phi_0)$$

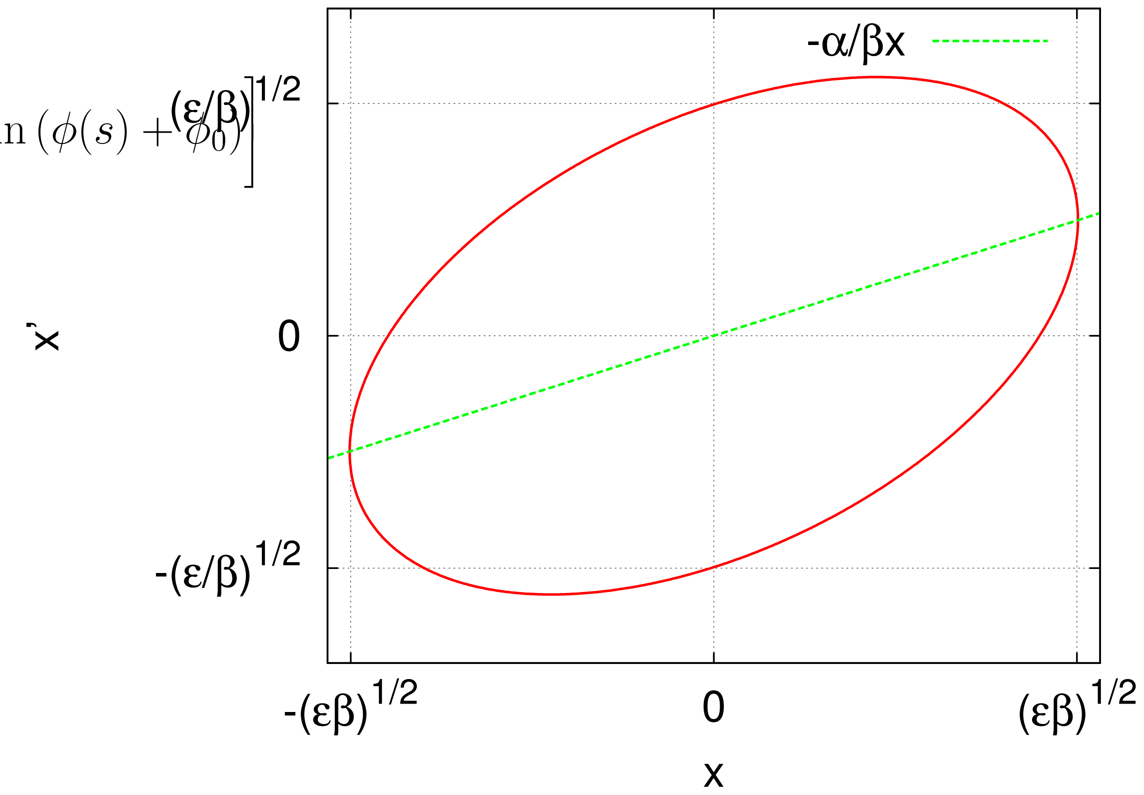
$$x'(s) = \sqrt{\frac{\epsilon}{\beta(s)}}\left[\frac{\beta'(s)}{2}\cos(\phi(s)+\phi_0) - \sin(\phi(s)+\phi_0)\right]$$

As homework you will show that $K(s) = const$ leads to $\beta = const$

$$x(s) = \sqrt{\epsilon\beta}\cos\left(\frac{s}{\beta}+\phi_0\right)$$

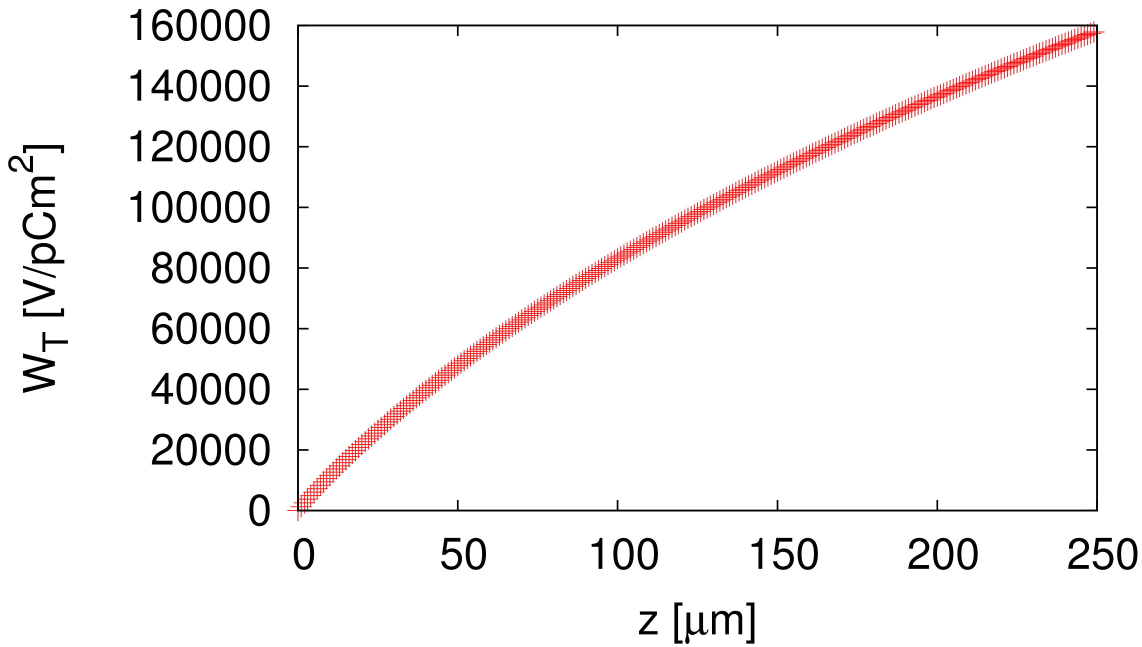
$$x'(s) = -\sqrt{\frac{\epsilon}{\beta}}\sin\left(\frac{s}{\beta}+\phi_0\right)$$

⇒ You can understand most things assuming a harmonic oscillator and some average beta-function



Beam Parameters: Transverse Wakefields and Beam Break-up

Example of Single Bunch Transverse Wakefield (CLIC)



- Fit obtained by K. Bane
- For short distances the wakefield rises linear
- Summation of an infinite number of sine-like modes with different frequencies

$$W_\perp(z) = 4\frac{Z_0 c z_0}{\pi a^4}\left[1 - \left(1 + \sqrt{\frac{z}{z_0}}\right)\exp\left(-\sqrt{\frac{z}{z_0}}\right)\right]$$

$$z_0 = 0.169 a^{1.79} g^{0.38}\left(\frac{1}{l}\right)^{1.17}$$

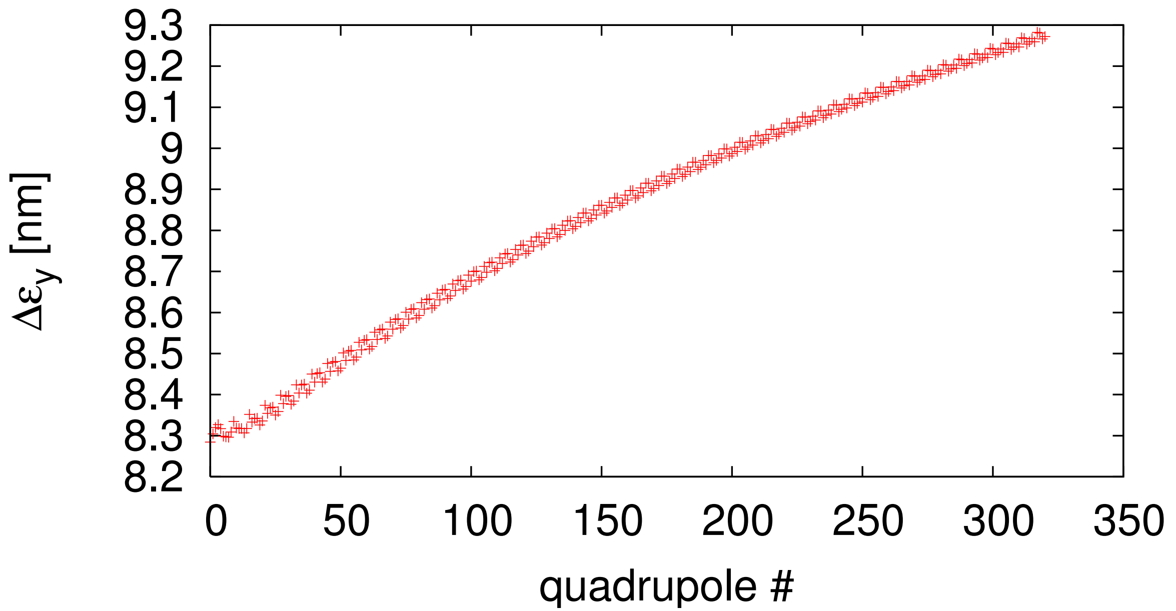
$$W_\perp(z \ll z_0) \approx 2\frac{Z_0 c}{\pi a^4} z$$

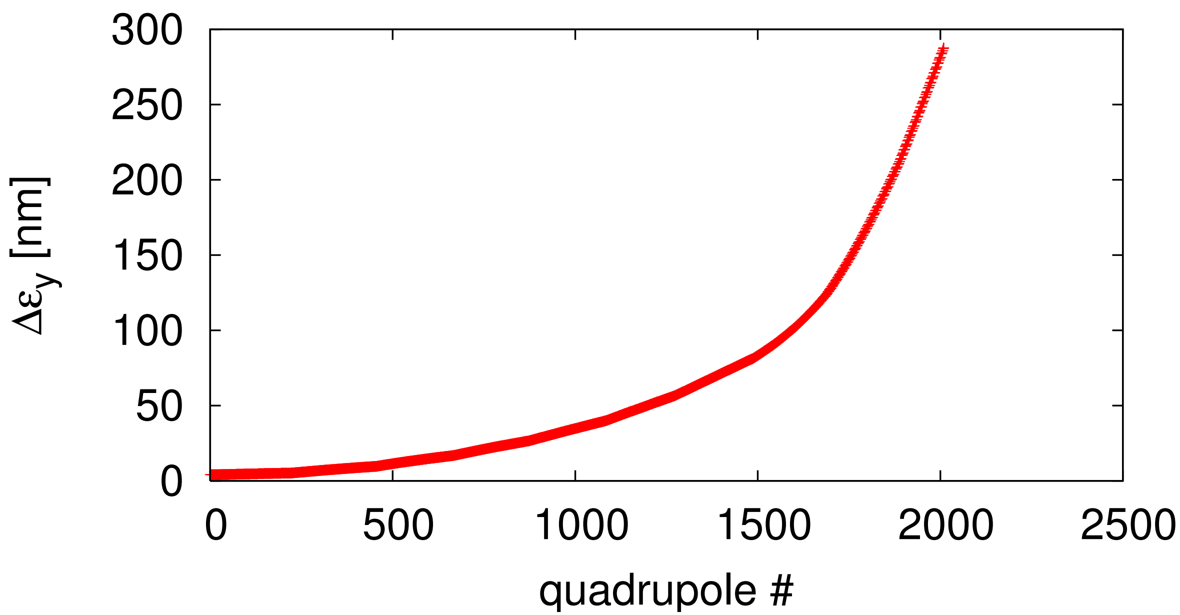
Beam Stability

- Transverse stability of a beam with initial offset of σ_y
  - no energy spread assumed in the beam
  - emittance with respect to the beam axis is shown

$\Rightarrow$ acceptable for ILC (top)

$\Rightarrow$ would be intolerable for CLIC (bottom)





Achieving Beam Stability

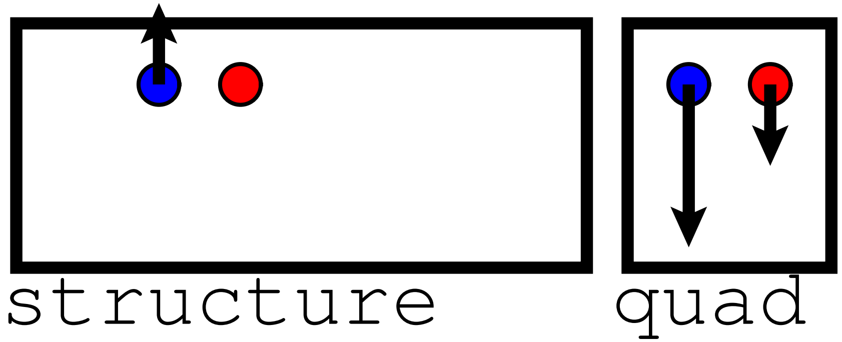
- Transverse wakes act as defocusing force on tail

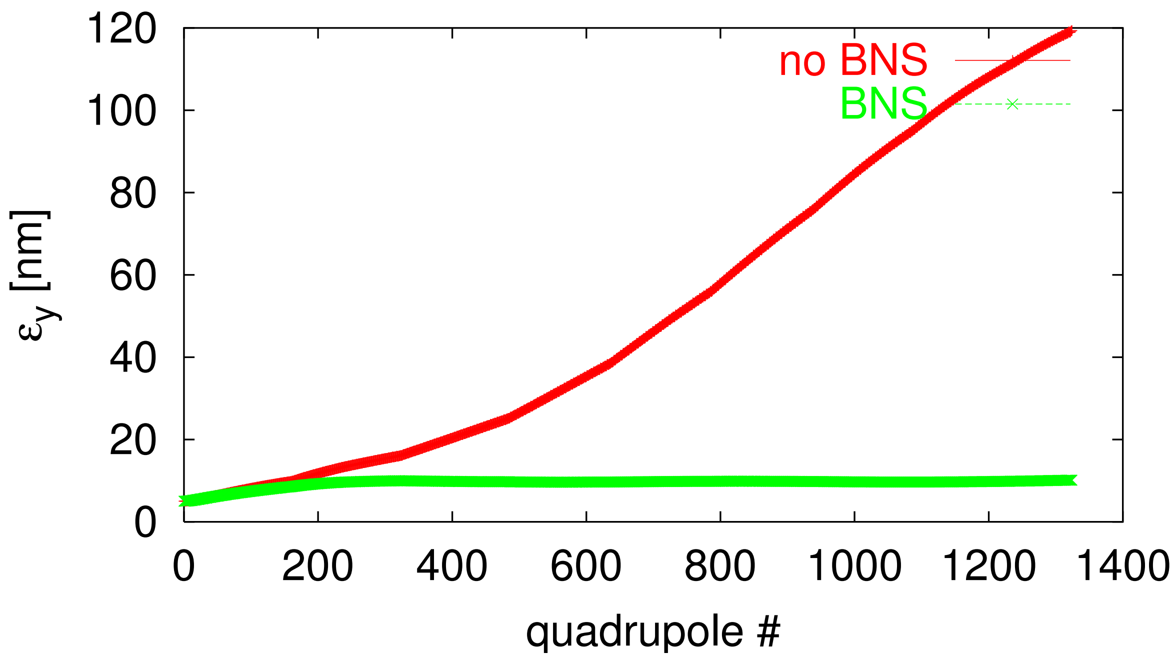
  ⇒ beam jitter is exponentially amplified

- BNS (Balakin, Novokhatsky, and Smirnov) damping prevents this growth

  - manipulate RF phases to have energy spread

  - take spread out at end





Two-Particle Wakefield Model

- Assume bunch can be represented by two particles and constant $K(s) = 1/\beta^2$
  - second particle is kicked by transverse wakefield
  - initial oscillation

$$x_1'' + \frac{1}{\beta^2}x_1 = 0 \qquad x_2'' + \frac{1}{\beta^2}x_2 = \frac{Ne^2W_\perp}{P_Lc}x_1$$

$$x_1 = x_0 \cos\left(\frac{s}{\beta}\right) \quad x_2(0) = x_0 \quad x_2'(0) = 0$$

$$x_2'' + \frac{1}{\beta^2}x_2 = x_0\frac{Ne^2W_\perp}{P_Lc}\cos\left(\frac{s}{\beta}\right)$$

- Solution is simple with an ansatz

$$x_2 = x_0 \cos\left(\frac{s}{\beta}\right) + \left(\frac{x_0Ne^2W_\perp\beta}{2E}s\right)\sin\left(\frac{s}{\beta}\right)$$

$\Rightarrow$ Amplitude of second particle oscillation is growing

$\Rightarrow$ The bunch charge and length matter as well as the lattice

$\Rightarrow$ Have a closer look into wakefields

BNS Damping solution

- First particle performs a harmonic oscillation

$$x_1(s) = x_0 \cos\left(\frac{s}{\beta_1}\right)$$

- We want the second particle to perform the **same** oscillation
- Modify unperturbed oscillation frequency of second particle

$$x_2 = x_0 \cos\left(\frac{s}{\beta_2}\right)$$

- Leads to

$$x_2'' + \frac{1}{\beta_2^2} x_2 = x_0 \frac{Ne^2 W_\perp}{P_L c} \cos\left(\frac{s}{\beta_1}\right) = x_1 \frac{Ne^2 W_\perp}{P_L c}$$

- Assuming (can be achieved by changing energy of second particle)

$$\frac{1}{\beta_2^2} = \frac{1}{\beta_1^2} + \frac{Ne^2 W_\perp}{P_L c}$$

- Yields simple solution

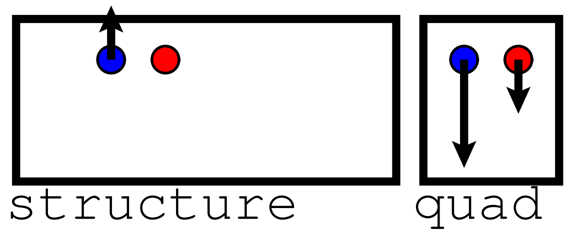
$$x_2 = x_0 \cos\left(\frac{s}{\beta_1}\right) = x_1$$

⇒ No more wakefield effect

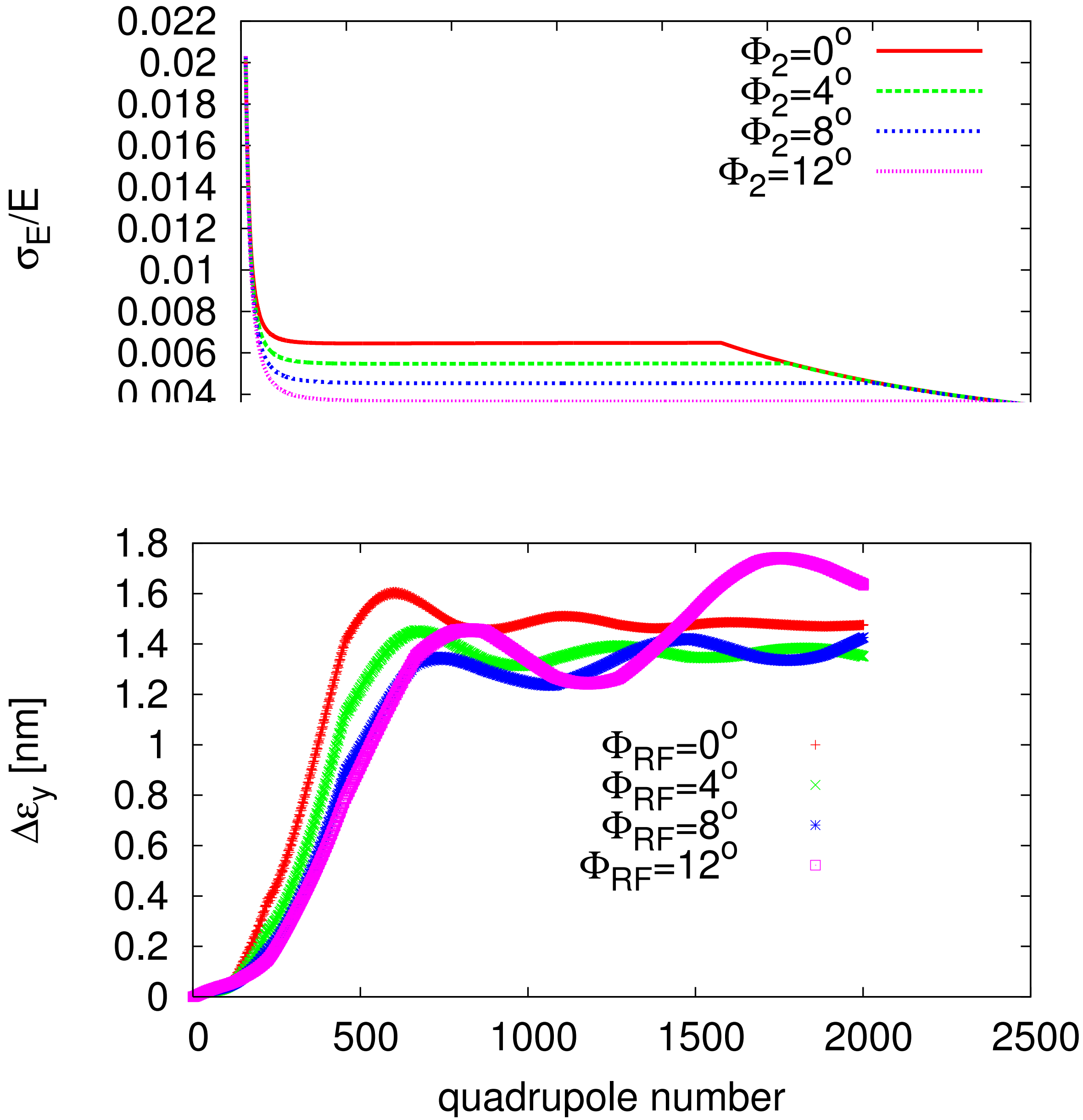
Energy Spread and Beam Stability

- Trade-off in fixed lattice
  - large energy spread is more stable
  - small energy spread is better for alignment

⇒ Beam with $N = 3.7 \times 10^9$ can be stable

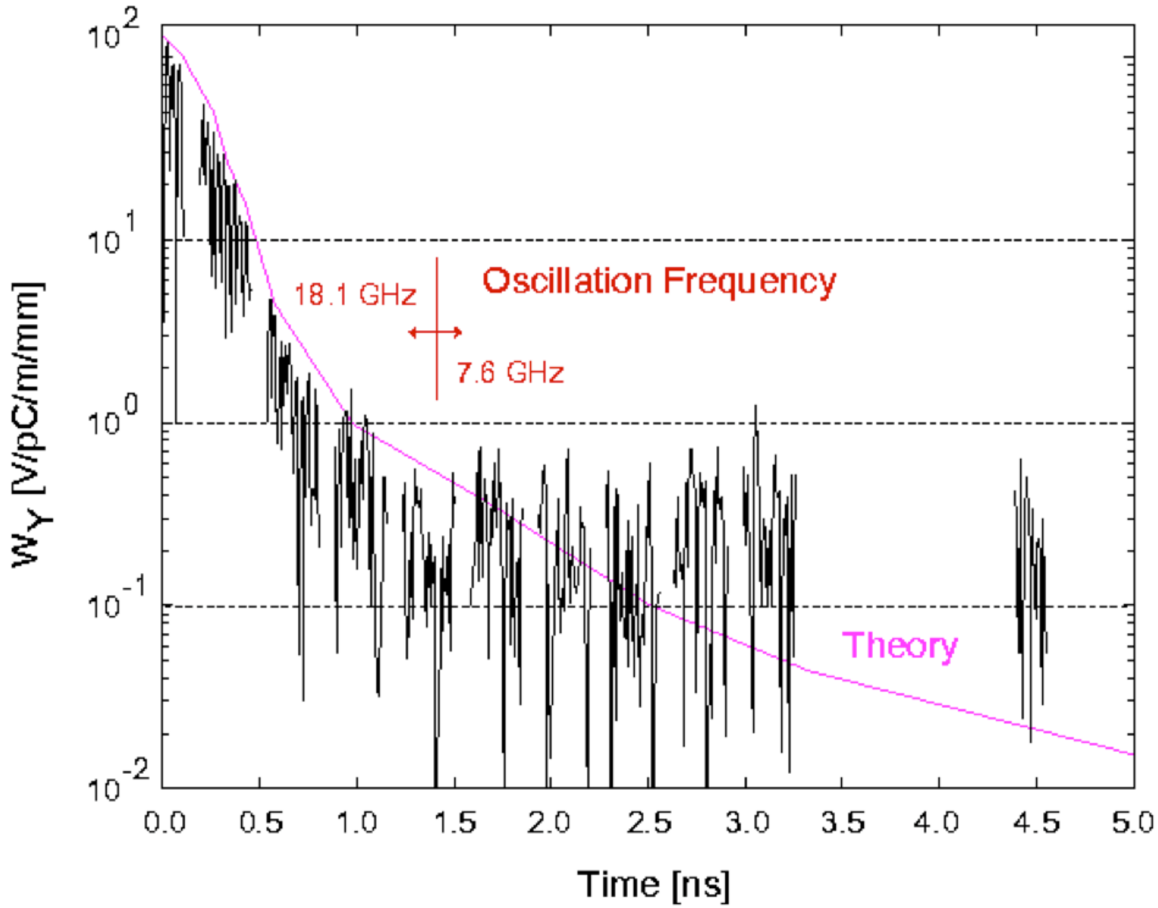


⇒ Tolerances are not a unique number



Multi-Bunch Wakefields

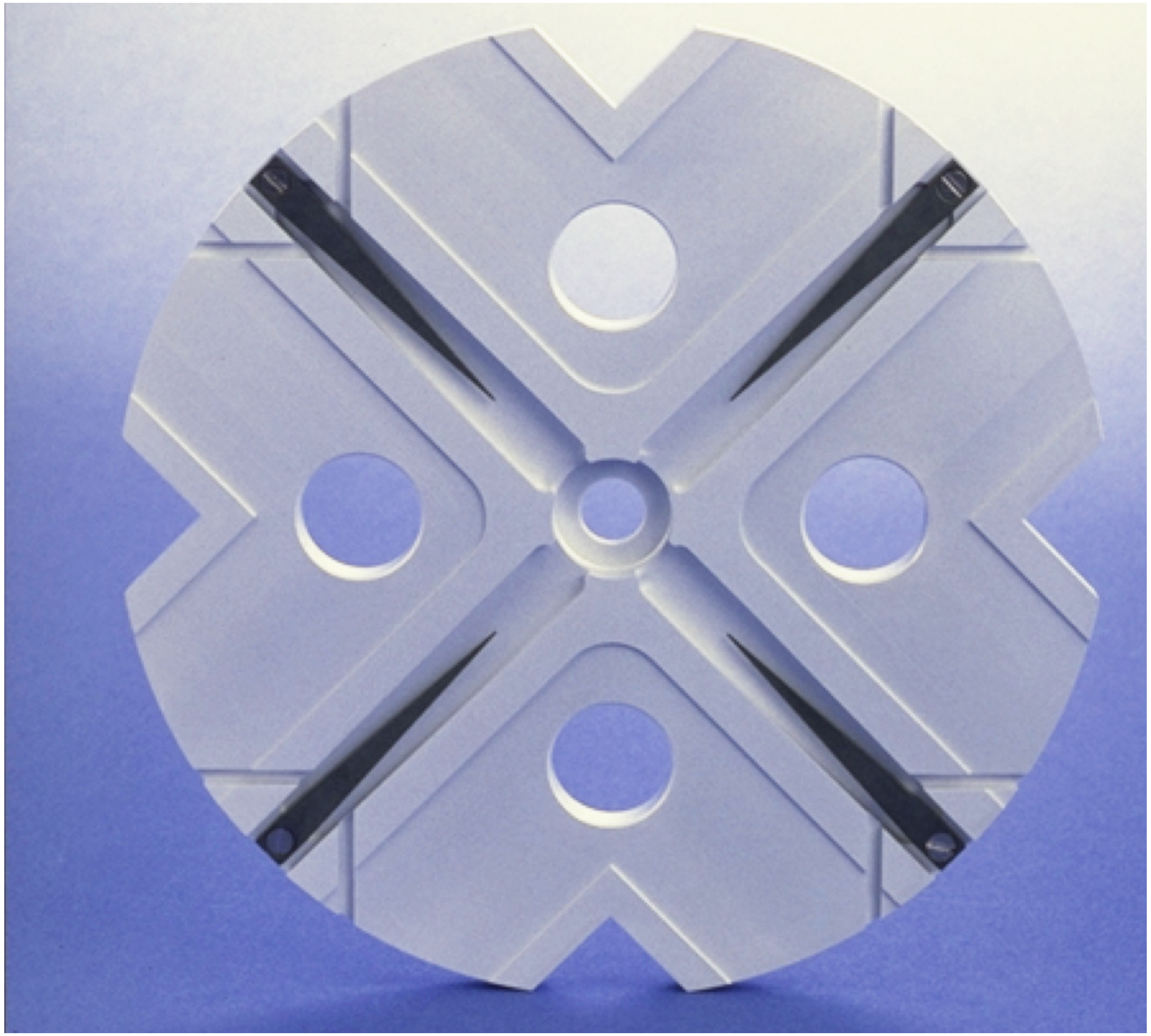
- Long-range transverse wakefields are sine-like
- They can be reduced by
  - damping
  - detuning



$$W_{\perp}(z) = \sum_i^{\infty} 2k_i \sin\left(2\pi \frac{z}{\lambda_i}\right) \exp\left(-\frac{\pi z}{\lambda_i Q_i}\right)$$

Damping

- Damping can be achieved by extracting the power of transverse modes from the structure
- In CLIC each cell has waveguides for this purpose
  - the fundamental mode cannot escape
- ILC has antennas at the end
  - weaker damping but bunch distance is larger
- Note: the difference has since been understood



Detuning

To make our life simple we neglect damping

We split the wakefield $W(z) = a\sin(kz)$ into two modes

$$W(z) = W_0 \frac{\sin((k+\Delta)z) + \sin((k-\Delta)z)}{2}$$

the resulting amplitude is

$$W(z) = W_0 \sin(kz)\cos(\Delta z)$$

integrating over a Gaussian distribution yields

$$W(z) = W_0 \sin(kz) \int_0^\infty \frac{2}{\sqrt{2\pi}\sigma_\Delta} \exp\left(-\frac{\Delta^2}{2\sigma_\Delta^2}\right) \cos(\Delta z) d\Delta$$

$$\Rightarrow W(z) = W_0 \sin(kz) \exp\left(-\frac{(z\Delta)^2}{2}\right)$$

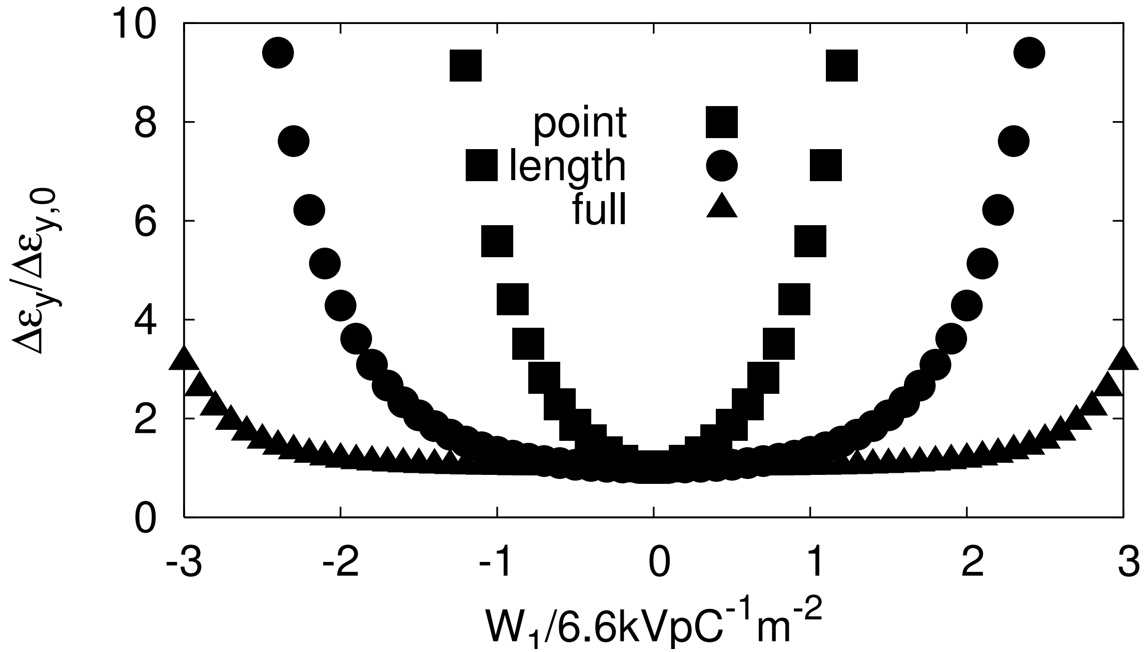
- For a limited number of modes, recoherence can occur

  $\Rightarrow$ damping is also needed

- In ILC detuning is important

Multi-Bunch Jitter Emittance Growth (CLIC)

- Multi-bunch effects can be calculated analytically for point-like bunches
  - an energy spread leads to a more stable case
- Simulations show
  - point-like bunches
  - bunches with energy spread due to bunch length
  - including also initial energy spread



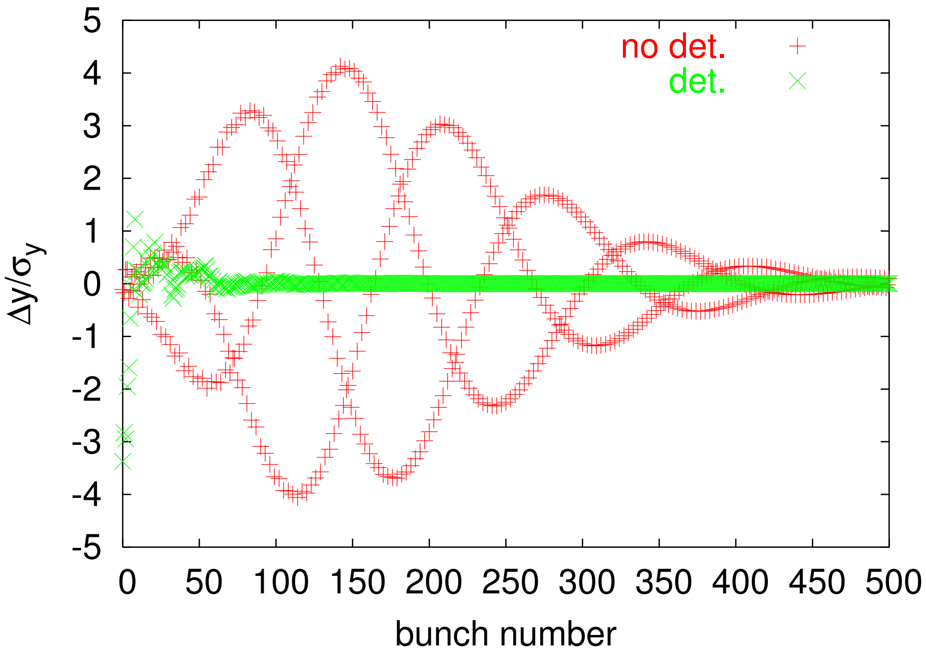
⇒ Point-like bunches is a pessimistic assumption for the dynamic effects

Static Multi-Bunch Effects (ILC)

- Simulation of long-range transverse wakefield effects
  - with no detuning
  - with random detuning from cavity to cavity

⇒ Cavity detuning is essential

⇒ Need to ensure that this detuning is present
  - it does happen naturally
  - but also if you depend on it?



All main linac cavities are scattered by 500 μm

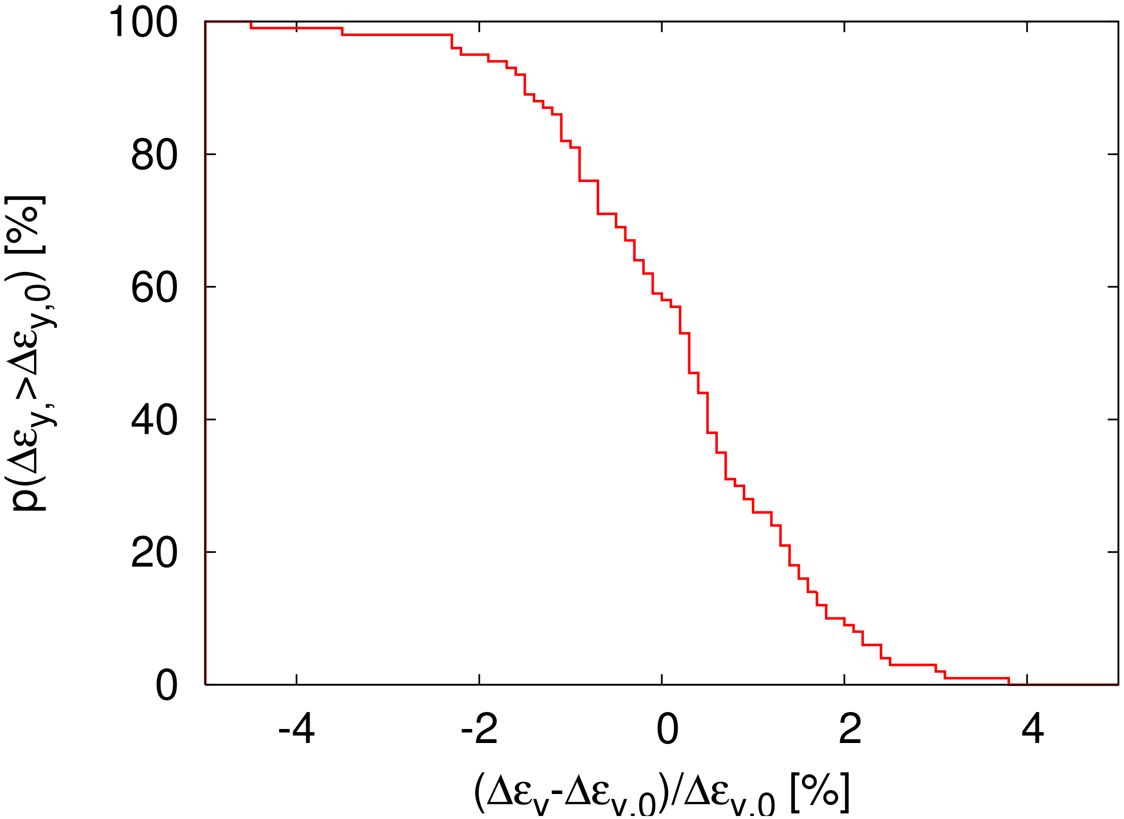
Long-range wakefields are represented by a number of RF modes

$$W_\perp(z) = \sum_{i=0}^{n} a_i \sin\left(\frac{2\pi z}{\lambda_i}\right) \exp\left(-\frac{\pi z}{\lambda_i Q_i}\right)$$

- Note: results depend on exact frequency of transverse modes
  - some uncertainty in the prediction
  - but not a worry with detuning

Beam Jitter (ILC)

- Perfect machines used
- 100 machines simulated
  - TESLA wakefields with 0.1% RMS frequency spread
  - beam set to an offset
  - 5% bunch-to-bunch charge variations in uncorrected test beam
  - additional relative emittance growth due to multi-bunch is determined



Imperfections

Introduction

- Have now been able to design a lattice that can transport the beam
- Need to determine how the imperfections in the machine affect the emittance preservation
- Will discuss the misalignment of elements
  - most important source of static emittance growth
- Have two ways to deal with tight tolerances for imperfections
  - work on the lattice to loosen tolerances
  - push R&D to satisfy tighter tolerances
  - e.g. in CLIC strong effort is ongoing to push imperfections down by about an order of magnitude

Element Misalignments

- Pre-Alignment imperfections can be roughly categorised into short-distance and long-distance errors
- To first order, the imperfections can be treated as independent
  - as long as a linear main linac model is sufficient
- The short-distance misalignments give largest emittance contribution
  - misalignment of elements is largely independent
  - simulated by scattering elements around a straight line
  - or slightly more complex local model
- The long-distance misalignments are dominated by the wire system

$\Rightarrow$ ignore short-distance misalignments and simulate wire errors only

- Combined studies are mainly for completeness

Simulation Rational

- One can understand the effects qualitatively
  - some can be calculated analytically
  - some can be approximated analytically
  - but things soon become complex

⇒ Beam dynamics tracking code is used for studies (choose your favorite one)

- Implemented models are usually very flexible
  - e.g. linear and non-linear effects
- Script language used to steer the simulation
- The art is in using minimum model
  - as little as possible
  - as much as necessary

⇒ Cannot say what is in the code but rather what is in each individual study

Main Linac Static Tolerances

Element	error	with respect to	tolerance CLIC	tolerance ILC
Structure	offset	beam	$5.8\,\mu\mathrm{m}$	$\approx 700\,\mu\mathrm{m}$
Structure	tilt	beam	$220\,\mu\mathrm{radian}$	$\approx 1000\,\mu\mathrm{radian}$
Quadrupole	offset	straight line	—	—
Quadrupole	roll	axis	$240\,\mu\mathrm{radian}$	$190\,\mu\mathrm{radian}$
BPM	offset	straight line	$0.44\,\mu\mathrm{m}$	$15\,\mu\mathrm{m}$
BPM	resolution	BPM center	$0.44\,\mu\mathrm{m}$	$15\,\mu\mathrm{m}$

- All tolerances for 1nm growth after one-to-one steering
- Goal is to have 90% of the machines achieve an emittance growth due to static effects of less than 5 nm

Assumed Survey Performance

Element	error	with respect to	alignment ILC	CLIC
Structure	offset	girder	$300\ \mu m$	$5\ \mu m$
Structure	tilts	girder	$300\ \mu radian$	$200(*)\ \mu m$
Girder	offset	survey line	$200\ \mu m$	$9.4\ \mu m$
Girder	tilt	survey line	$20\ \mu radian$	$9.4\ \mu radian$
Quadrupole	offset	girder/survey line	$300\ \mu m$	$17\ \mu m$
Quadrupole	roll	survey line	$300\ \mu radian$	$\leq 100\ \mu radian$
BPM	offset	girder/survey line	$300\ \mu m$	$14\ \mu m$
BPM	resolution	BPM center	$\approx 1\ \mu m$	$0.1\ \mu m$
Wakefield mon.	offset	wake center	—	$5\ \mu m$

- In ILC specifications have much larger values than in CLIC
  - more difficult alignment in super-conducting environment
  - dedicated effort for CLIC needed
- Wakefield monitors are currently only foreseen in CLIC
  - but could be an option also in ILC

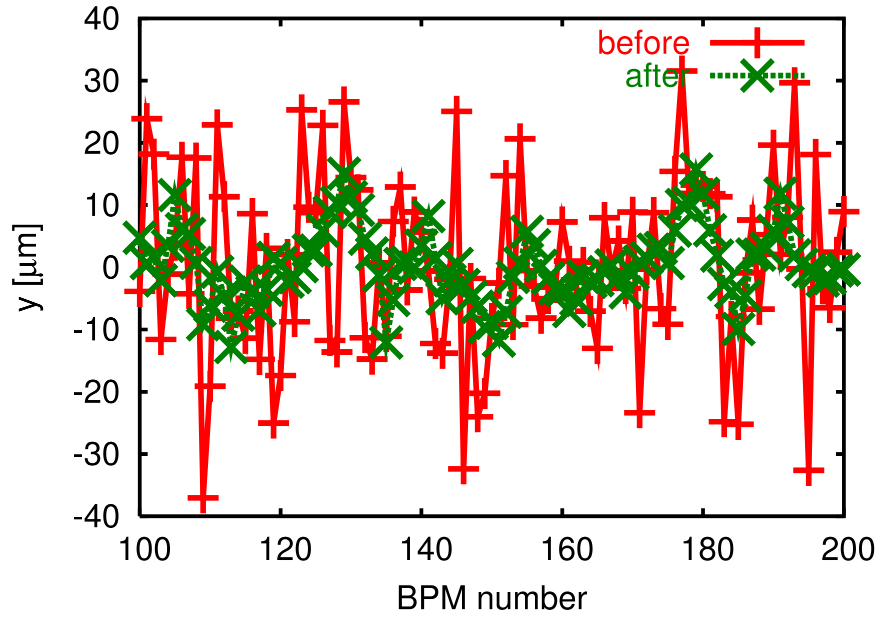
Beam-Based Alignment and Tuning Strategy

- Make beam pass linac
  - one-to-one correction
- Remove dispersion, align BPMs and quadrupoles
  - dispersion free steering
  - ballistic alignment
  - kick minimisation
- Remove residual wakefield and dispersive effects
  - accelerating structure alignment (CLIC only)
  - emittance tuning bumps

- Tune luminosity
  - tuning knobs

Dispersion Free Correction

- Basic idea: use different beam energies
- NLC: switch on/off different accelerating structures
- CLIC (ILC): accelerate beams with different gradient and initial energy
  - try to do this in a single pulse (time resolution)



- Optimise trajectories for different energies together:

$$S = \sum_{i=1}^{n} \left(w_i (x_{i,1})^2 + \sum_{j=2}^{m} w_{i,j} (x_{i,1} - x_{i,j})^2 \right) + \sum_{k=1}^{l} w'_k (c_k)^2$$

- Last term is omitted
- Idea is to mimic energy differences that exist in the bunch with different beams

Emittance Growth (ILC)

Error	with respect to	value	$\Delta\gamma\epsilon_y$ [nm]	$\Delta\gamma\epsilon_{y,121}$ [nm]	$\Delta\gamma\epsilon_{y,dfs}$ [nm]
Cavity offset	module	$300\ \mu\mathrm{m}$	3.5	0.2	$0.2(0.2)$
Cavity tilt	module	$300\ \mu\mathrm{radian}$	2600	< 0.1	$1.8(8)$
BPM offset	module	$300\ \mu\mathrm{m}$	0	360	$4(2)$
Quadrupole offset	module	$300\ \mu\mathrm{m}$	700000	0	$0(0)$
Quadrupole roll	module	$300\ \mu\mathrm{radian}$	2.2	2.2	$2.2(2.2)$
Module offset	perfect line	$200\ \mu\mathrm{m}$	250000	155	$2(1.2)$
Module tilt	perfect line	$20\ \mu\mathrm{radian}$	880	1.7	—

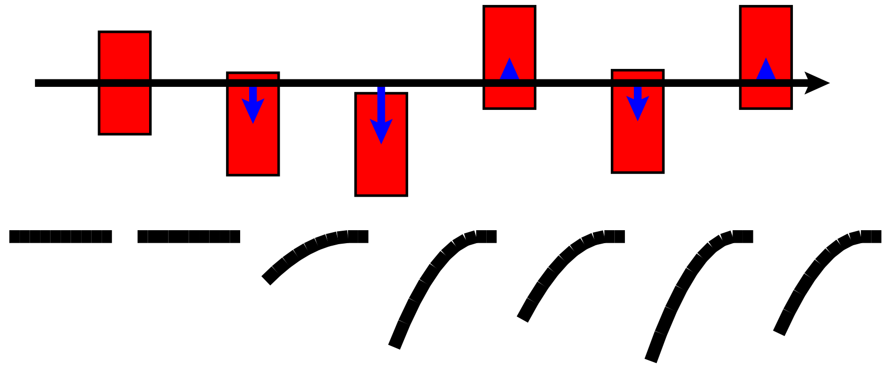
- The results of the reference DFS method is quoted, results of a different implementation in brackets
- Note in the simulations the correction the quadrupoles had been shifted, other wise some residual effect of the quadrupole misalignment would exist

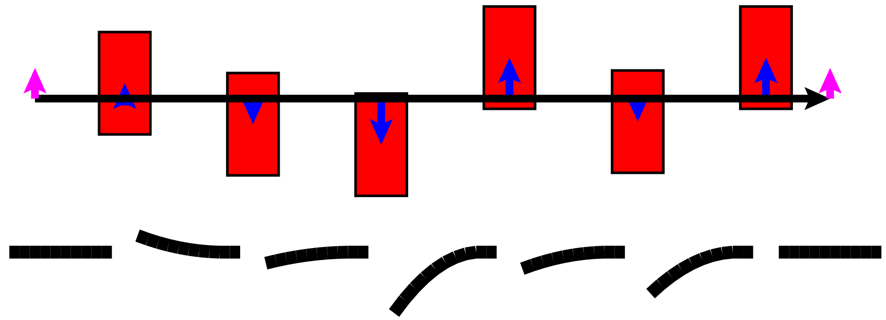
Beam-Based Structure Alignment (CLIC)

- Each structure is equipped with a wakefield monitor (RMS position error $5\,\mu\mathrm{m}$)
- Up to eight structures on one movable girders

$\Rightarrow$ Align structures to the beam

- Assume identical wake fields
  - the mean structure to wakefield monitor offset is most important
  - in upper figure monitors are perfect, mean offset structure to beam is zero after alignment
  - scatter around mean does not matter a lot
- With scattered monitors
  - final mean offset is $\sigma_{wm}/\sqrt{n}$
- In the current simulation each structure is moved independently
- A study has been performed to move the articulation points
- Girder step size $< 1\,\mu m$

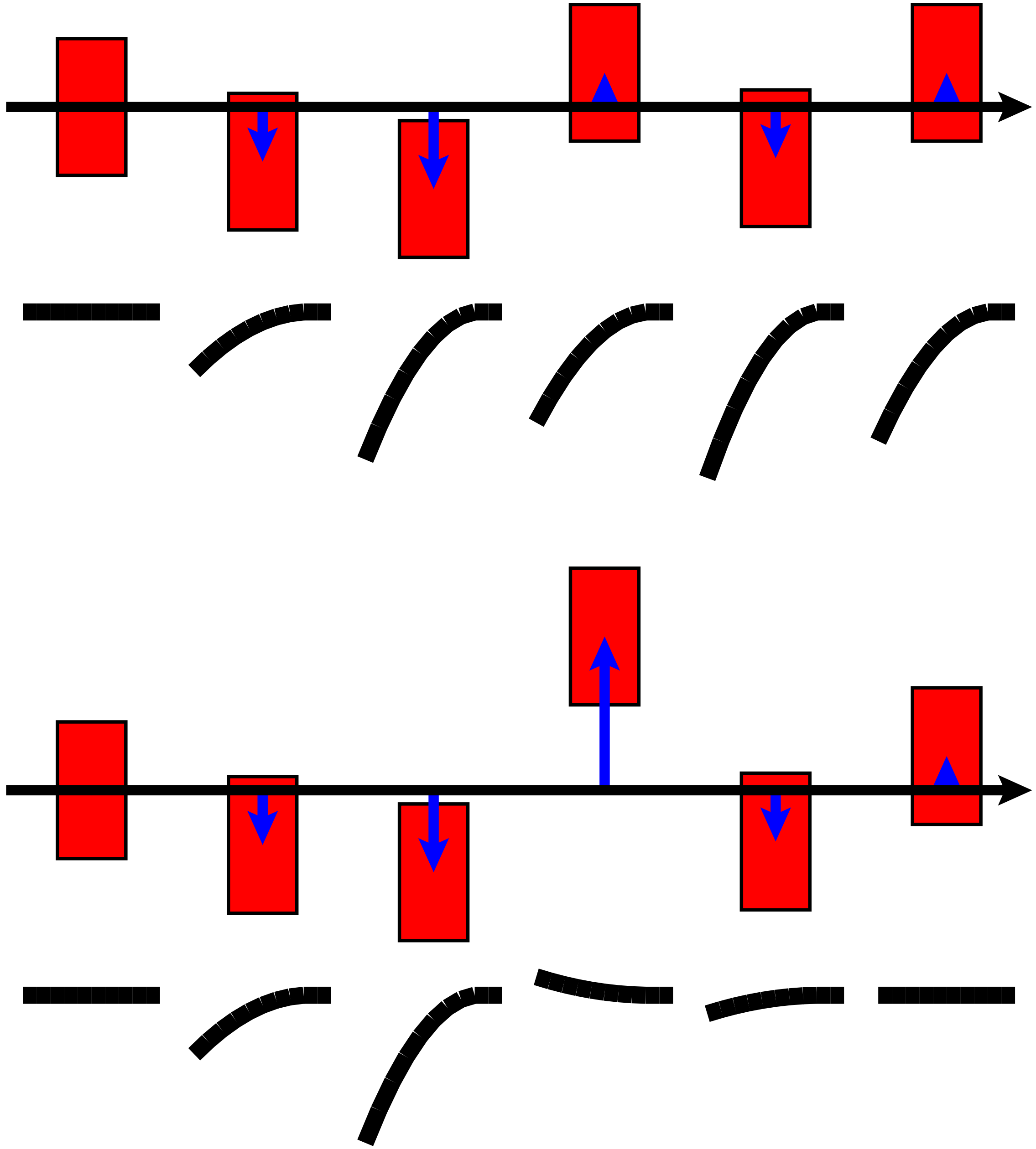




- For our tolerance $\sigma_{wm} = 5\,\mu\mathrm{m}$ we find $\Delta\epsilon_y \approx 0.5\,\mathrm{nm}$
  - some dependence on alignment method

Emittance Tuning Bumps

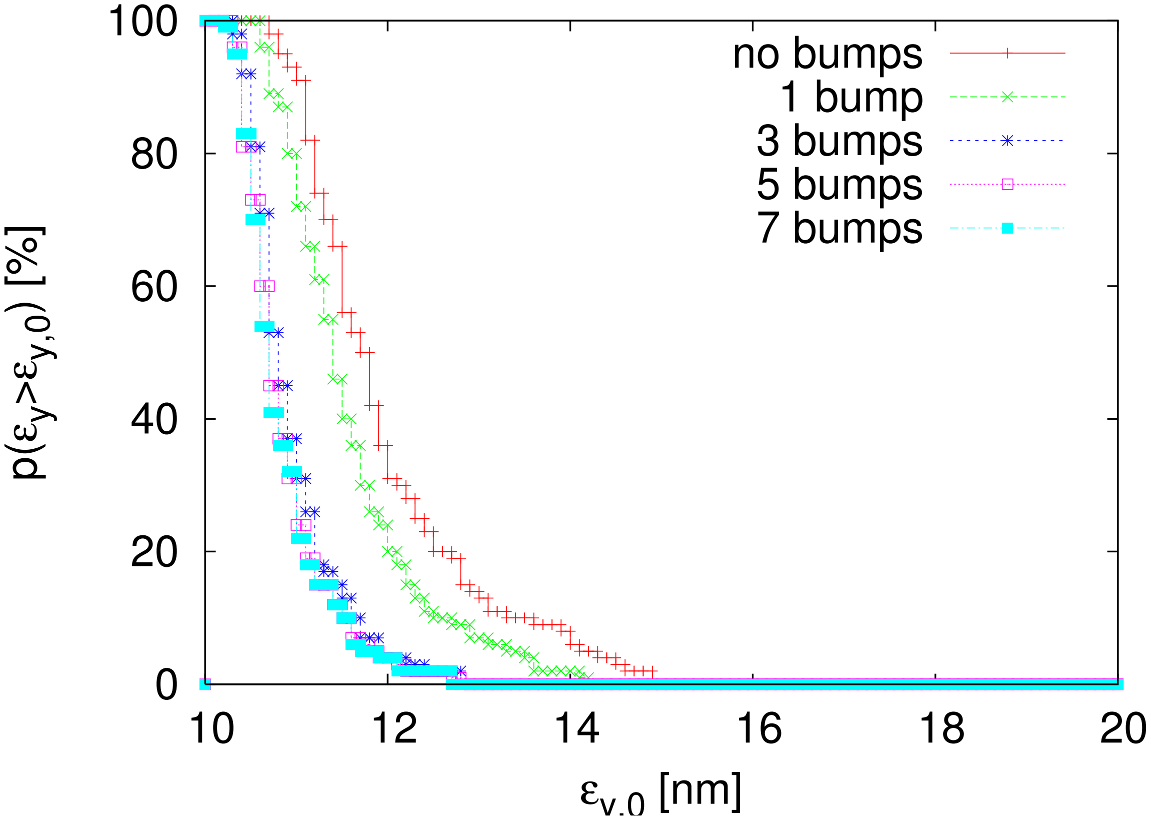
- Emittance (or luminosity) tuning bumps can further improve performance
  - globally correct wake-field by moving some structures
  - similar procedure for dispersion
- Need to monitor beam size
- Optimisation procedure
  - measure beam size for different bump settings
  - make a fit to determine optimum setting
  - apply optimum
  - iterate on next bump



Final Emittance Growth (CLIC)

imperfection	with respect to	symbol	value	emitt. growth
BPM offset	wire reference	σ_{BPM}	14 μm	0.367 nm
BPM resolution		σ_{res}	0.1 μm	0.04 nm
accelerating structure offset	girder axis	σ_4	10 μm	0.03 nm
accelerating structure tilt	girder axis	σ_t	200 μradian	0.38 nm
articulation point offset	wire reference	σ_5	12 μm	0.1 nm
girder end point	articulation point	σ_6	5 μm	0.02 nm
wake monitor	structure centre	σ_7	5 μm	0.54 nm
quadrupole roll	longitudinal axis	σ_r	100 μradian	≈ 0.12 nm

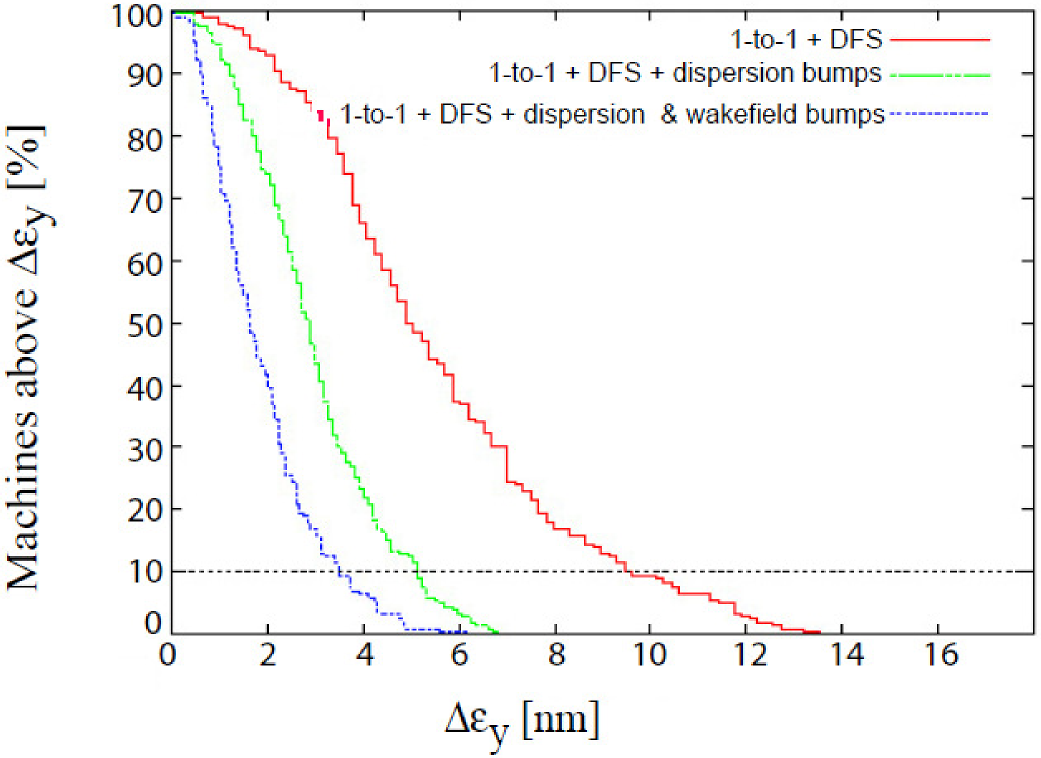
- Selected a good DFS implementation
  - trade-offs are possible
- Multi-bunch wakefield misalignments of $10\,\mu\text{m}$ lead to $\Delta\epsilon_y \approx 0.13\,\text{nm}$
- Performance of local prealignment is acceptable



Results (ILC)

- DFS brings us close to the required performance
- Tuning of the dispersion helps a lot
- Even wakefield tuning helps us
- The remaining emittance growth is to a significant extent due to quadrupole roll

  ⇒ should add a tuning bump for this effect as well



Dependence on Weights (Old CLIC Parameters)

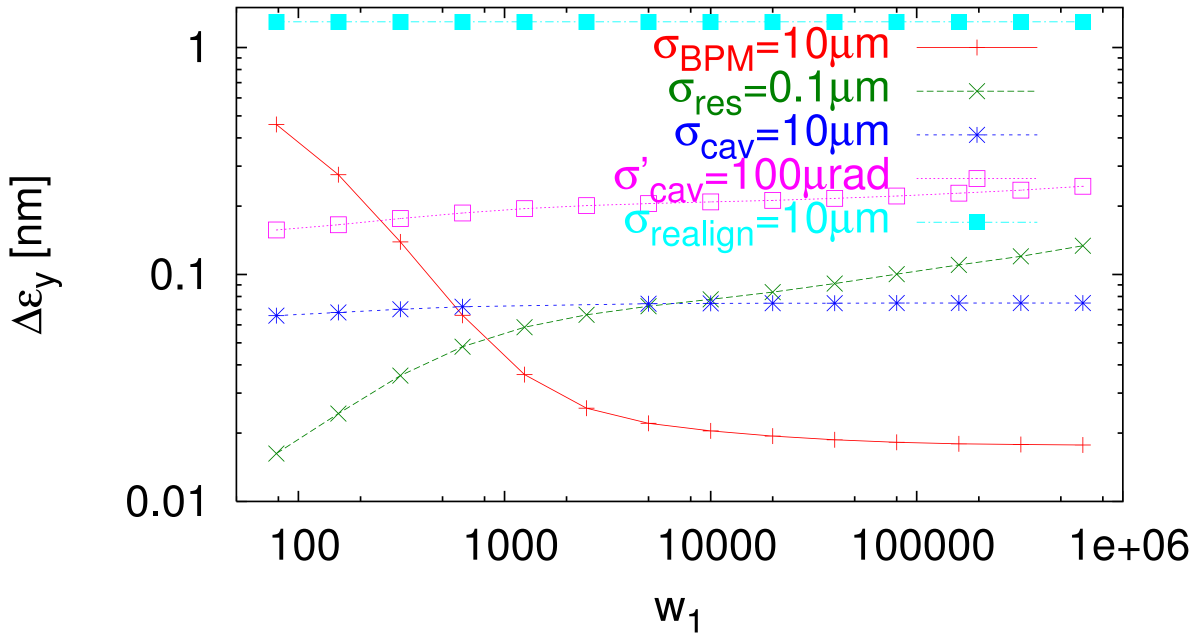
- For TRC parameters set
- One test beam is used with a different gradient and a different incoming beam energy

⇒ BPM position errors are less important at large w_1

⇒ BPM resolution is less important at small w_1

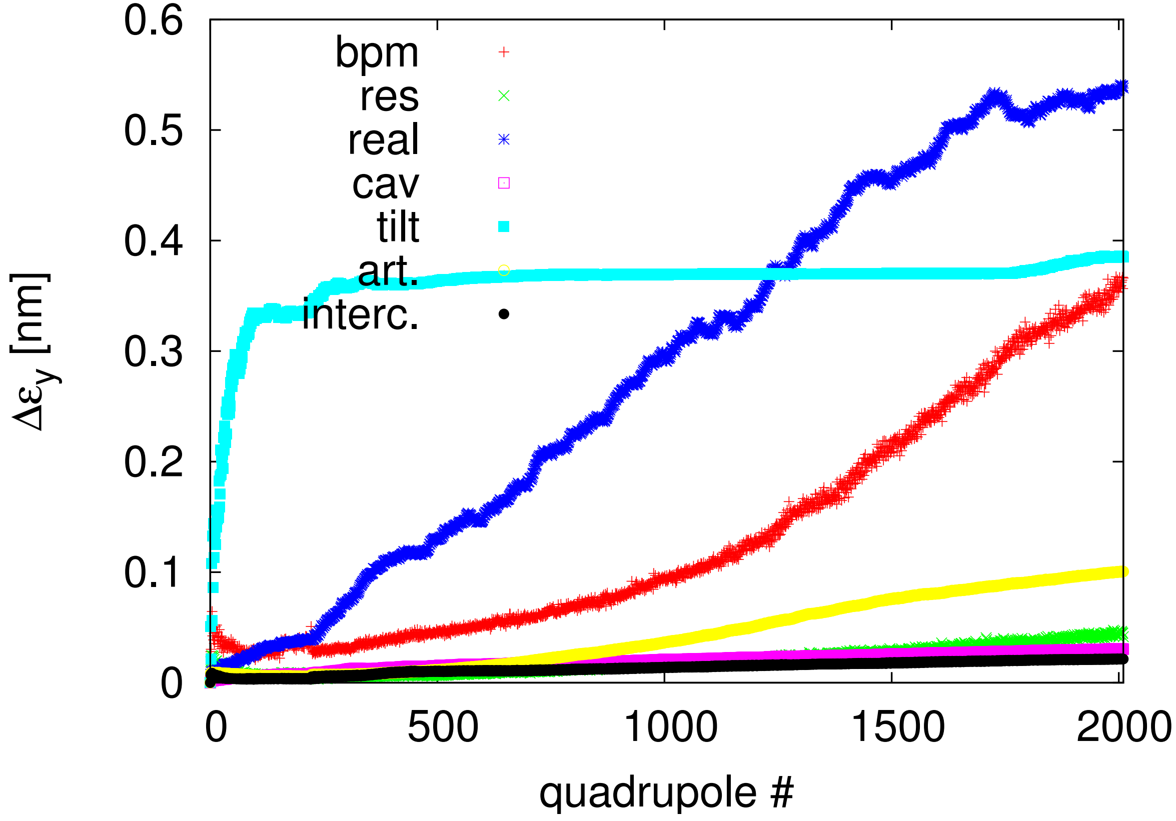
⇒ Need to find a compromise

⇒ There is no such thing as “the” tolerance for one error source

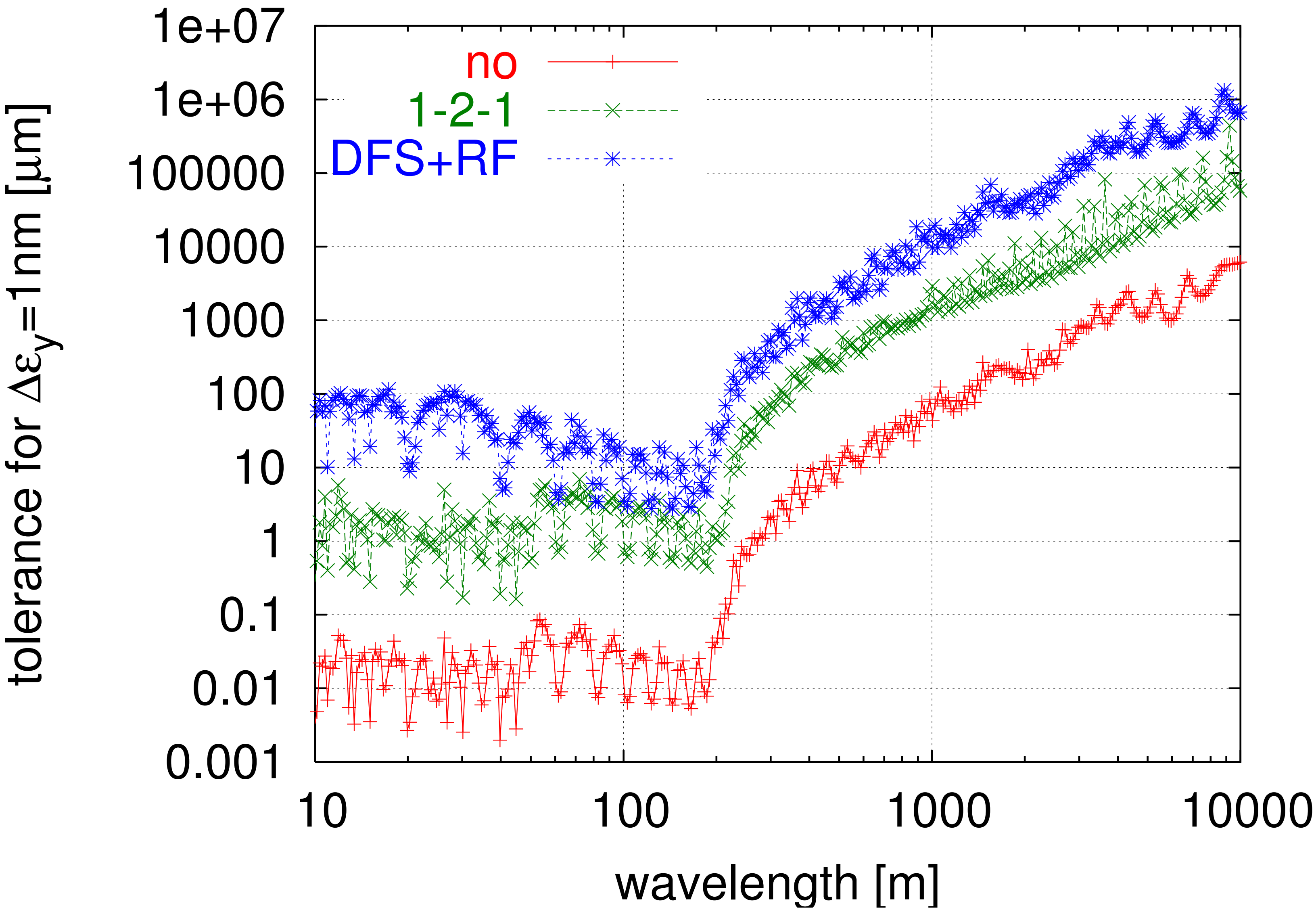


Growth Along Main Linac (CLIC)

- Emittance growth along the main linac due to the different imperfections
- Growth is mainly constant per cell
  - follows from first principles applied during lattice design
- Exception is structure tilt
  - due to uncorrelated energy spread
  - flexible weight to be investigated
- Some difference for BPMs
  - due to secondary emittance growth



Sensitivity to Survey Line Errors (CLIC)



- Cosine-line misalignments, beta-functions clearly visible

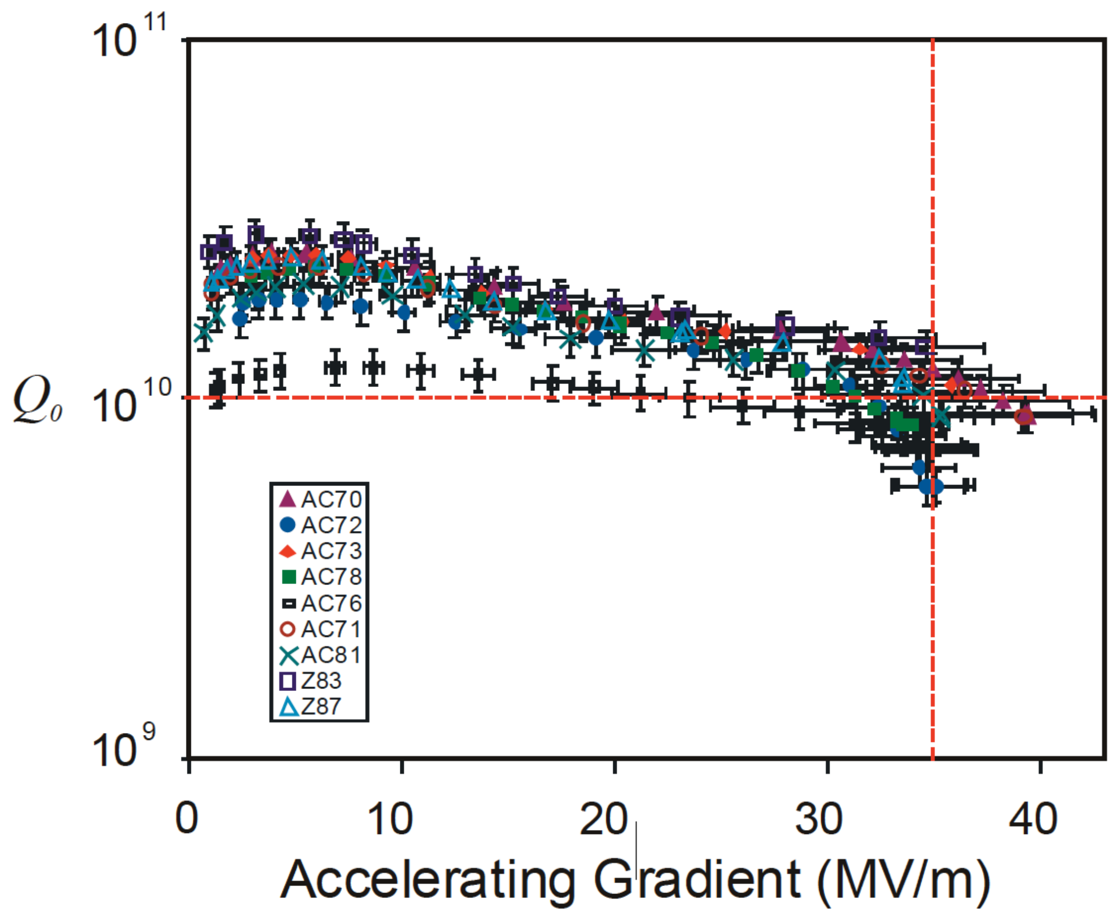
Structure Challenges

Introduction

- You heard all about those, so just a short reminder
- Achieving the gradient is a challenge in both designs
- For ILC the Q-value is crucial
  - can only use structures with good value
  - some structure do not reach the gradient required
- In CLIC the breakdown rate is crucial
  - can kick the beam and prevent luminosity

Super-conducting Cavity Q-Values

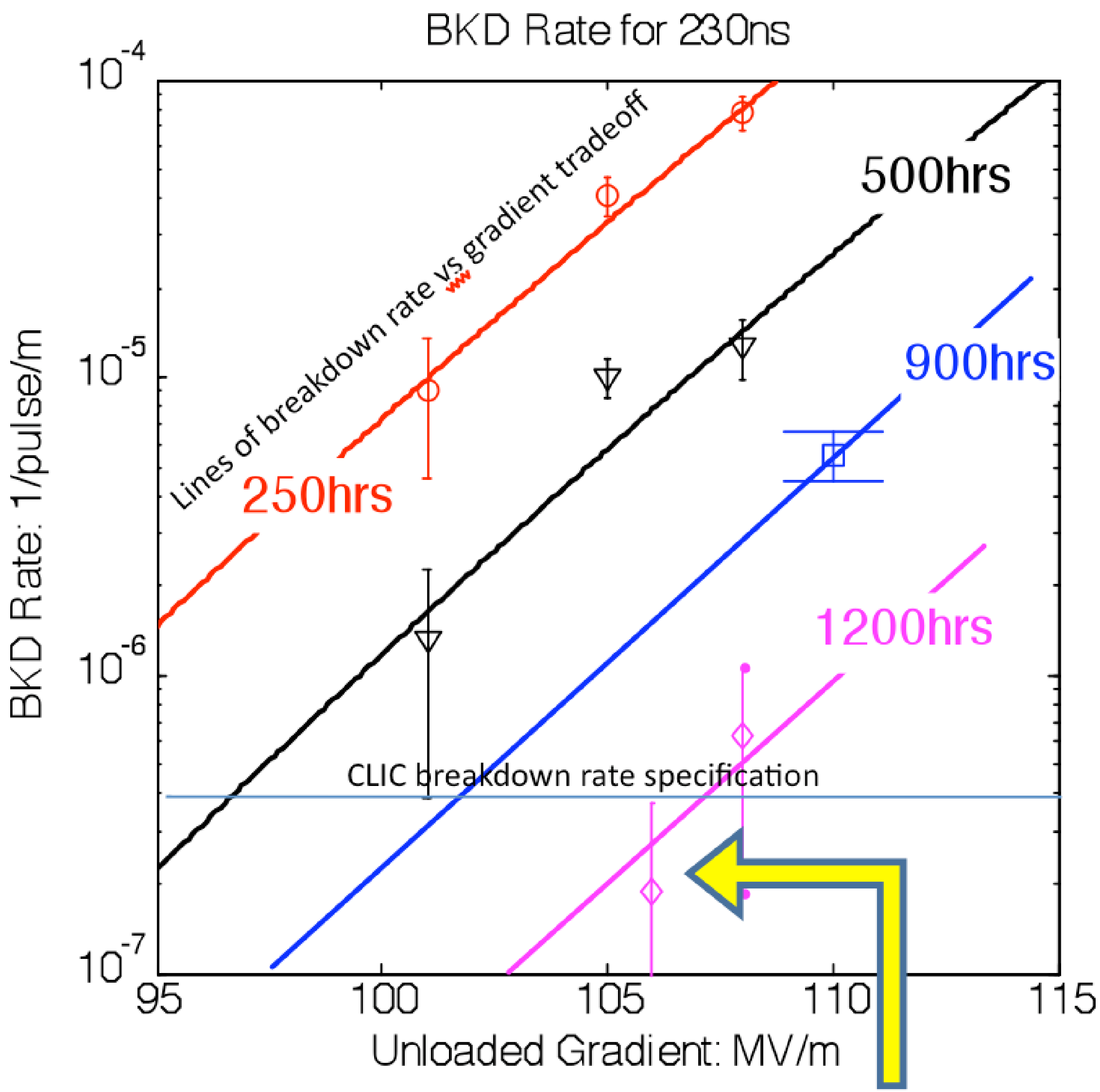
- The Q_0-values of super-conducting cavities can strongly vary from one cavity to the next
  - material quality
- Challenge is to produce enough good cavities
  - fraction of good cavities is relevant for cost
- Too low Q_0 means larger cooling power is required



Breakdown Rate (CLIC)

- Direct limit to breakdown rate
  - 1% luminosity loss budget
  - assuming that a pulse with breakdown leads to no luminosity
  - have 7×10^4 structures per linac

  $\Rightarrow$ breakdown rate $0.01/14 \times 10^4 \approx 0.7 \times 10^{-7}$
- Assumed strategy is to switch off corresponding PETS and slowly go up to power again



Empirical RF Constraints

- To limit the breakdown rate and the severeness of the breakdowns
- The maximum surface field has to be limited

$$\hat{E} < 260\,\mathrm{MV/m}$$

- The temperature rise at the surface needs to be limited

$$\Delta T < 56\,\mathrm{K}$$

- The power flow needs to be limited

  - related to the badness of a breakdown

  empirical parameter is

$$P/(2\pi a)\tau^{\frac{1}{3}} < 18\,\frac{\mathrm{MW}}{\mathrm{mm}}\mathrm{ns}^{\frac{1}{3}}$$

Pulse Length

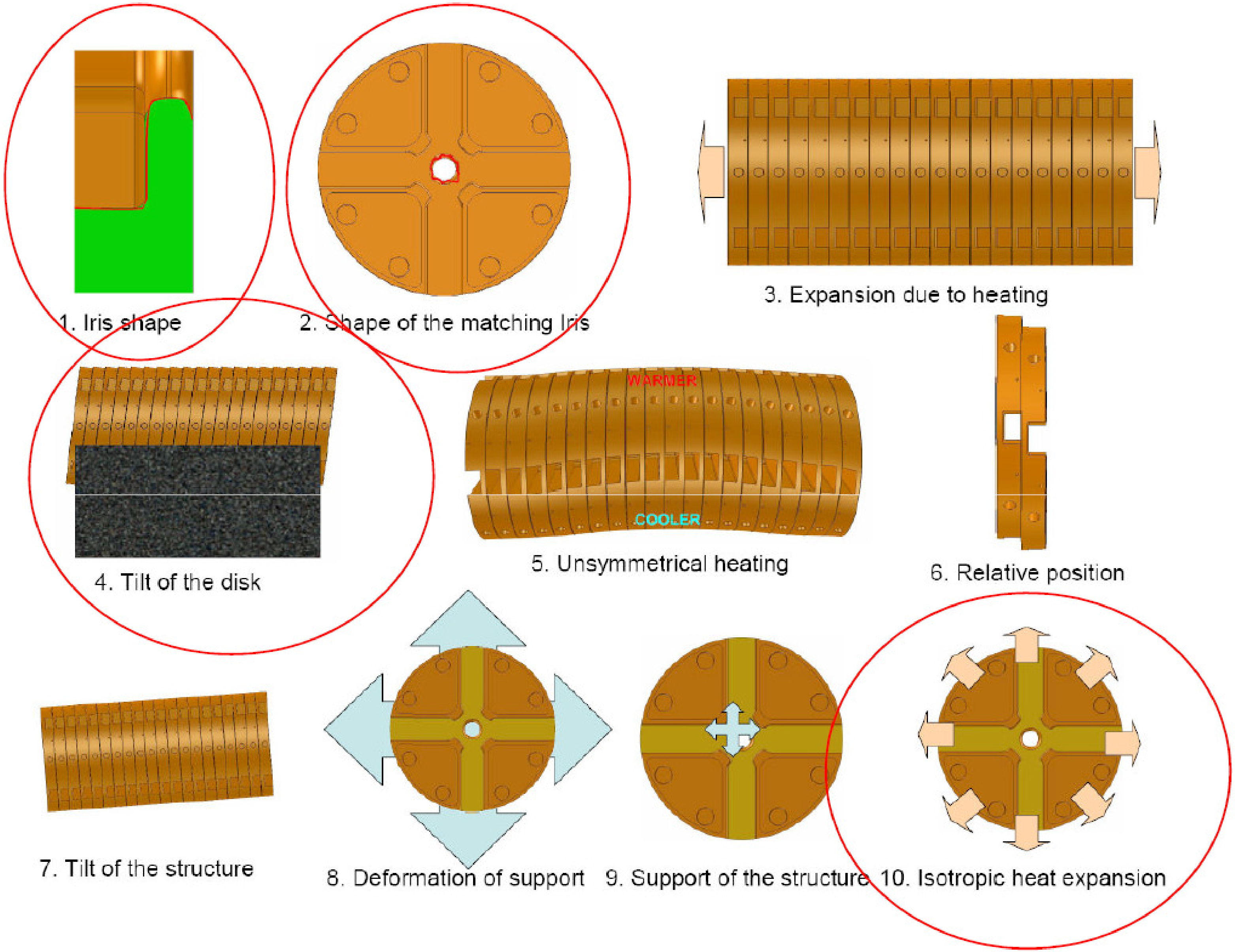
- The breakdown rate p depends on the pulse length τ and the gradient G as (about)

$$p \propto G^{30}\tau^5$$

  Hence, the maximum pulse length and the graidient of a structure are connected

$\Rightarrow$ This gives an upper limit for the acceptable pulse length in each structure for a given gradient

Imperfections from the Structure (CLIC)



Parameter Optimisation

A not so basic thing for linacs. . .

Done for CLIC only

Luminosity

Simplified treatment and approximations used throughout

$$\mathcal{L} = H_D \frac{N^2 f_{rep} n_b}{4\pi\sigma_x\sigma_y}$$

$$\mathcal{L} \propto H_D \frac{N}{\sqrt{\beta_x\epsilon_x}\sqrt{\beta_y\epsilon_y}}\eta P$$

$$\epsilon_x = \epsilon_{x,DR} + \epsilon_{x,BC} + \epsilon_{x,BDS} + \ldots$$

$$\epsilon_y = \epsilon_{y,DR} + \epsilon_{y,BC} + \epsilon_{y,linac} + \epsilon_{y,BDS} + \epsilon_{y,growth} + \epsilon_{y,offset} \ldots$$

$\sigma_{x,y} \propto \sqrt{\beta_{x,y}\epsilon_{x,y}/\gamma}$

$N f_{rep} n_b \propto \eta P$

typically $\epsilon_x \gg \epsilon_y$,
$\beta_x \gg \beta_y$

Fundamental limitations from

- beam-beam: $N/\sqrt{\beta_x\epsilon_x}$, $N/\sqrt{\beta_x\epsilon_x\beta_y\epsilon_y}$
- emittance generation and preservation: $\sqrt{\beta_x\epsilon_x}$, $\sqrt{\beta_y\epsilon_y}$
- main linac RF: η

Potential Limitations

Efficiency η:
depends on beam current that can be transported

- Decrease bunch distance $\Rightarrow$ long-range transverse wakefields in main linac
- Increase bunch charge $\Rightarrow$ short-range transverse and longitudinal wakefields in main linac, other effects
- Increase the RF pulse length $\Rightarrow$ is limited bz the structure, leads to higher drive beam cost

- Horizontal beam size σ_x:
  limit for N/σ_x and $N/(\sigma_x \sigma_y)$ from beam-beam effects
  final focus system can limit achievable σ_x
  damping ring due to generated ϵ_x bunch compressors can increase ϵ_x
- vertical beam size σ_y:
  vertical emittance generated in damping ring
  emittance increase in bunch compressor and main linac
  beam delivery system can limit achievable σ_y
  the need to collide beams can give lower limit on σ_y
  beam-beam effects via the two-stream instability
- Will try to show how to derive $L_{bx}(f, a, \sigma_a, G)$

Beam Size Limit at IP

- The vertical beam size had been $\sigma_y = 1\,\mathrm{nm}$ (BDS)

  $\Rightarrow$ challenging enough, so keep it $\Rightarrow \epsilon_y = 10\,\mathrm{nm}$

- Fundamental limit on horizontal beam size arises from beamstrahlung

  Two regimes exist depending on beamstrahlung parameter

$$\Upsilon = \frac{2}{3}\frac{\hbar\omega_c}{E_0} \propto \frac{N\gamma}{(\sigma_x + \sigma_y)\sigma_z}$$

  $\Upsilon \ll 1$: classical regime, $\Upsilon \gg 1$: quantum regime

  At high energy and high luminosity $\Upsilon \gg 1$

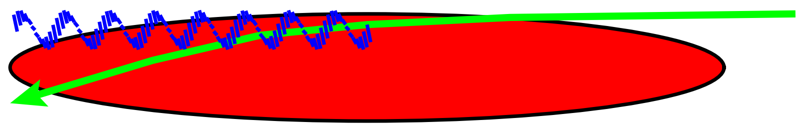
$$\mathcal{L} \propto \Upsilon\sigma_z/\gamma P\eta$$

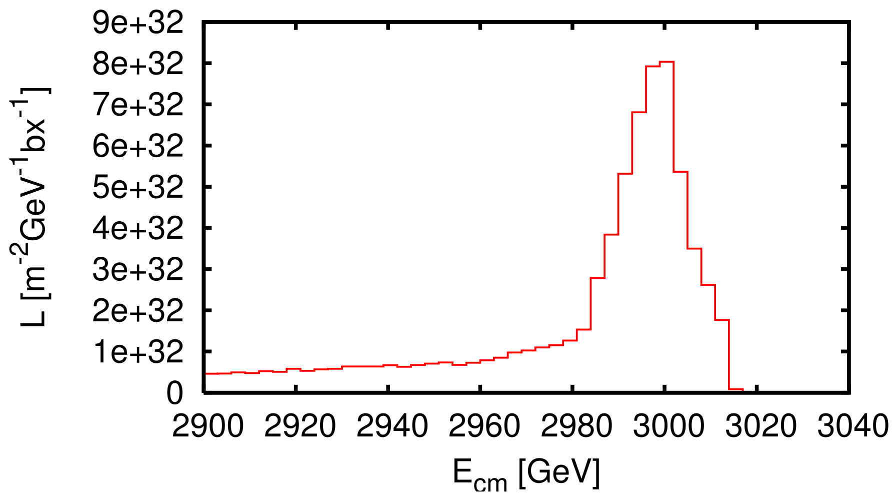
  $\Rightarrow$ partial suppression of beamstrahlung

  $\Rightarrow$ coherent pair production

  In CLIC $\langle\Upsilon\rangle \approx 6$, $N_{coh} \approx 0.1N$

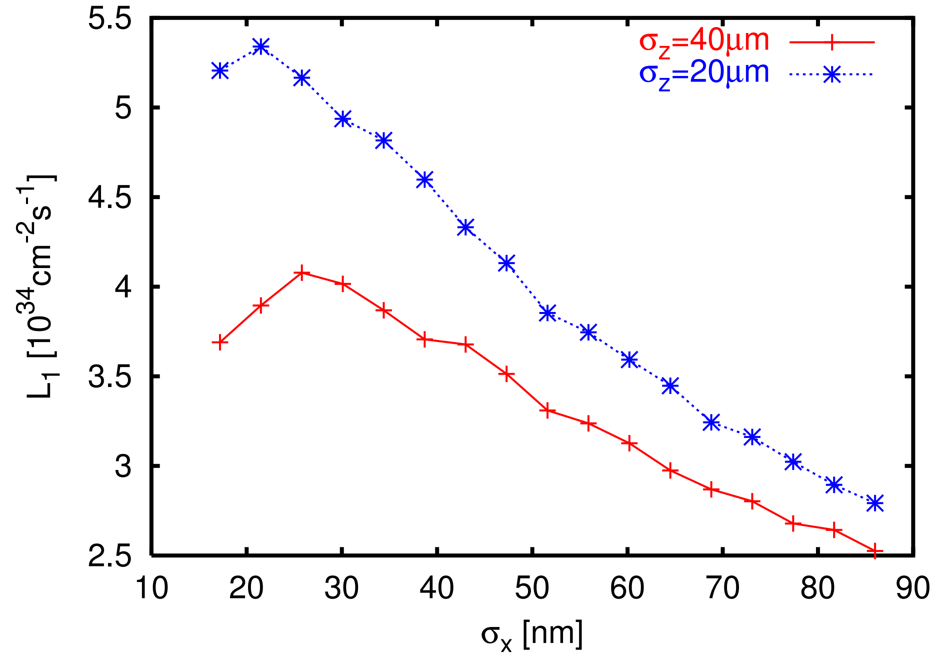
  $\Rightarrow$ somewhat in quantum regime

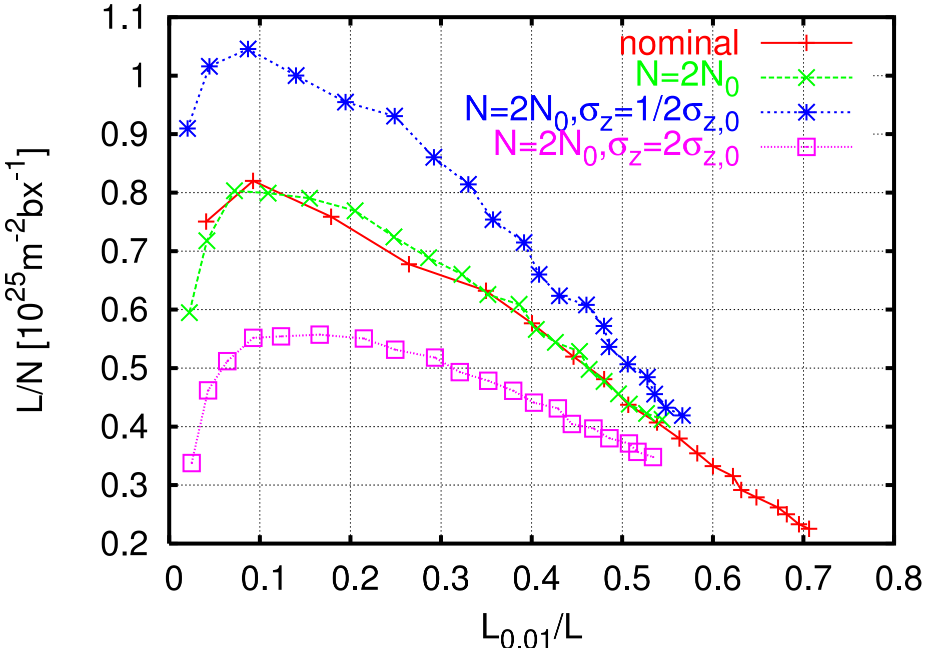




$\Rightarrow$ Use luminosity in peak as figure of merit

Luminosity Optimisation at IP





Total luminosity for $\Upsilon \gg 1$

$$\mathcal{L} \propto \frac{N}{\sigma_x}\frac{\eta}{\sigma_y} \propto \frac{n_\gamma^{3/2}}{\sqrt{\sigma_z}}\frac{\eta}{\sigma_y}$$

large n_γ $\Rightarrow$ higher $\mathcal{L}$ $\Rightarrow$ degraded spectrum

chose n_γ, e.g. maximum $L_{0.01}$ or $L_{0.01}/L = 0.4$ or ...

$$\mathcal{L}_{0.01} \propto \frac{\eta}{\sqrt{\sigma_z}\sigma_y}$$

Other Beam Size Limitations

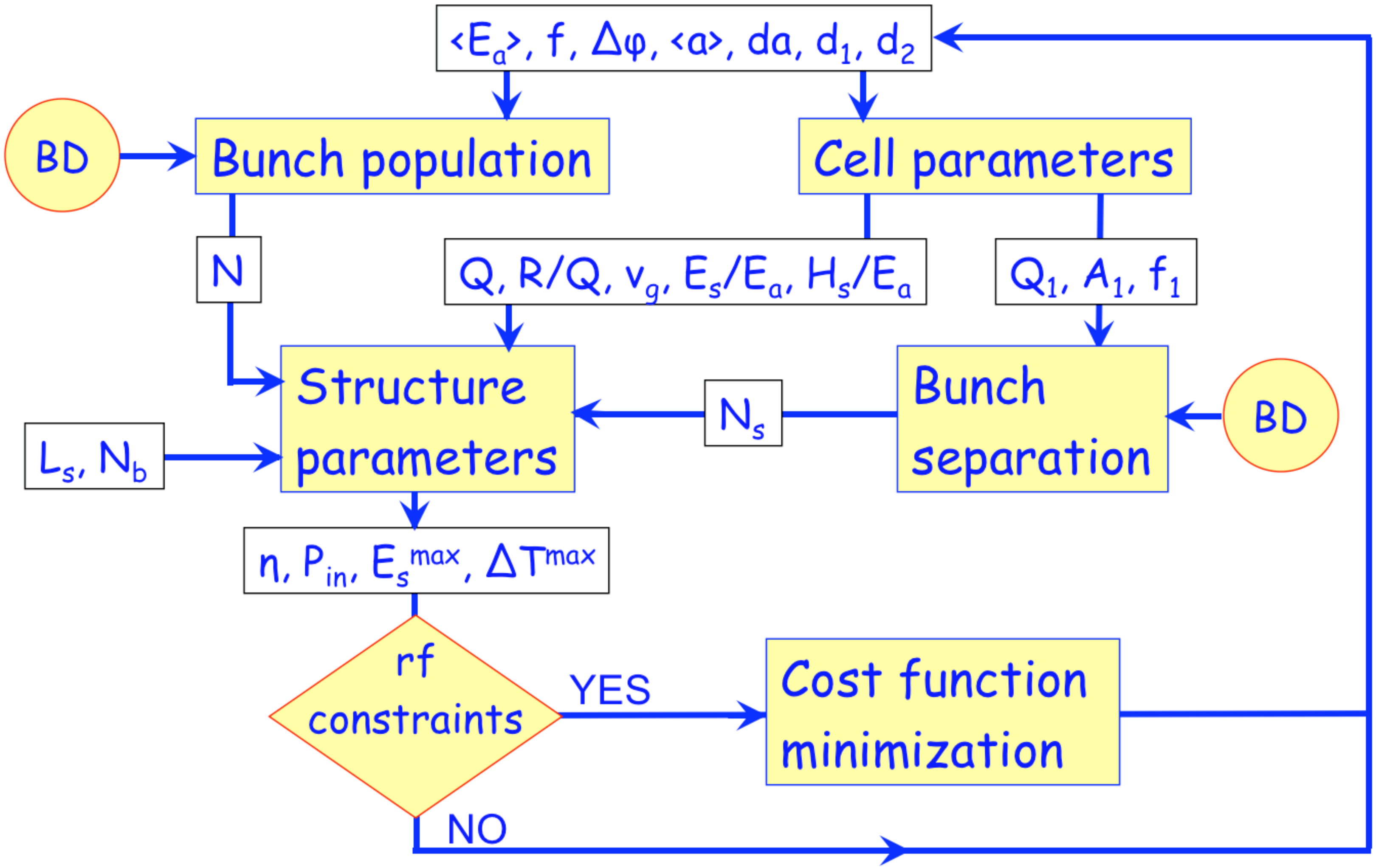
- Final focus system squeezes beams to small sizes with main problems:
  - beam has energy spread (RMS of $\approx 0.35\%$) $\Rightarrow$ avoid chromaticity
  - synchrotron radiation in bends $\Rightarrow$ use weak bends $\Rightarrow$ long system
  - radiation in final doublet (Oide Effect)
- Large $\beta_{x,y} \Rightarrow$ large nominal beam size
- Small $\beta_{x,y} \Rightarrow$ large distortions
- Beam-beam simulation of nominal case: effective $\sigma_x \approx 40\,\mathrm{nm}$, $\sigma_y \approx 1\,\mathrm{nm}$

$\Rightarrow$ lower limit of $\sigma_x \Rightarrow$ for small N optimum n_γ cannot be reached

  - new FFS reaches $\sigma_x \approx 40\,\mathrm{nm}$, $\sigma_y \approx 1\,\mathrm{nm}$

- Assume that the transverse emittances remain the same
  - not strictly true
  - emittance depends on charge in damping ring (e.g $\epsilon_x(N = 2\times10^9) = 450\,\mathrm{nm}$, $\epsilon_x(N = 4\times10^9) = 550\,\mathrm{nm}$)

Work Flow



‹Ea›, f, Δφ, ‹a›, da, d1, d2
BD
Bunch population
Cell parameters
N
Q, R/Q, vg, Es/Ea, Hs/Ea
Q1, A1, f1
Structure parameters
Ns
Bunch separation
BD
Ls, Nb
η, Pin, Es max, ΔTmax
rf constraints
YES
Cost function minimization
NO

Beam Dynamics Work Flow

- Optimisation keeping the main linac beam dynamics tolerances at the original level
  - do not change the lattice
- Minimum spot size at IP is dominated by BDS and damping ring
  - adjust N/σ_x for large bunch charges to respect beam-beam limit
- For each of the different values of f, a/λ and G find $\sigma_z(N)$
  - respecting final RMS energy spread to be $\sigma_E/E = 0.35\%$ and running 12° off-crest
- Choose N such that $2NW_\perp(\sigma_z(N))$ is acceptable (i.e. old value)
- All the single bunch parameters are now fixed

  Need to chose pulse length and repetion rate

  They are linked by the luminosity goal
- We like to chose a repetion rate that is a harmonic or subharmonic of the grid frequency

  This minisises electric and magnetic interference

How to Choose the Pulse Lenght

- Longer pulses are more efficient

  ⇒ efficiency reduces the cost and increases the acceptance of a project

- But they require more RF energy per pulse

  ⇒ higher cost for storage of energy in modulators

- Longer trains of bunches are more constly to produce

  Note: in ILC the number of bunches is very large, tis requires a large damping ring and can drive the cost

- In CLIC we have a clear limit of the pulse length for a given gradient

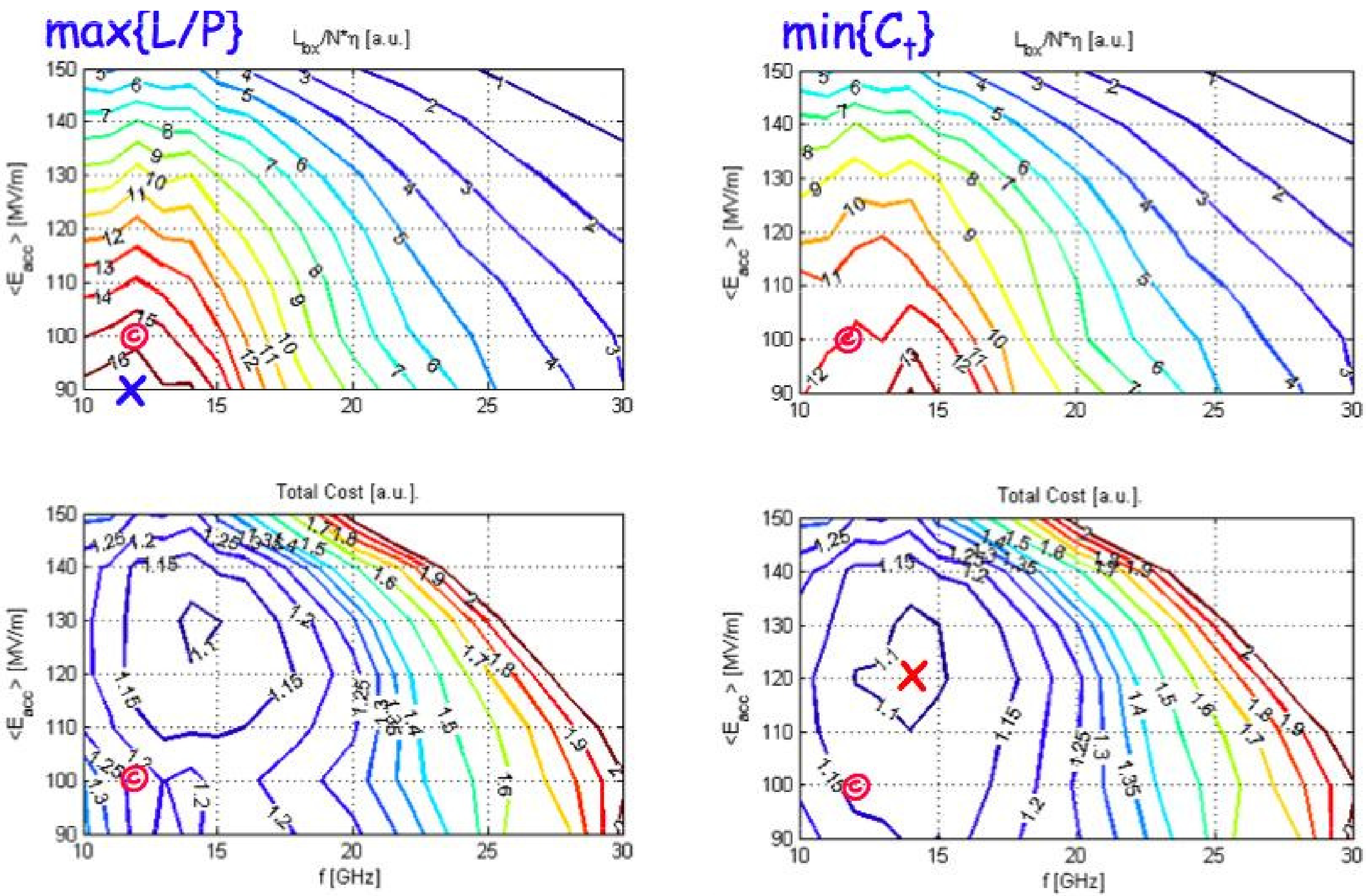
  lower gradients allow for longer pulses but increase the cost since the linac will be longer

- There is some impact of the pulse length on the detector

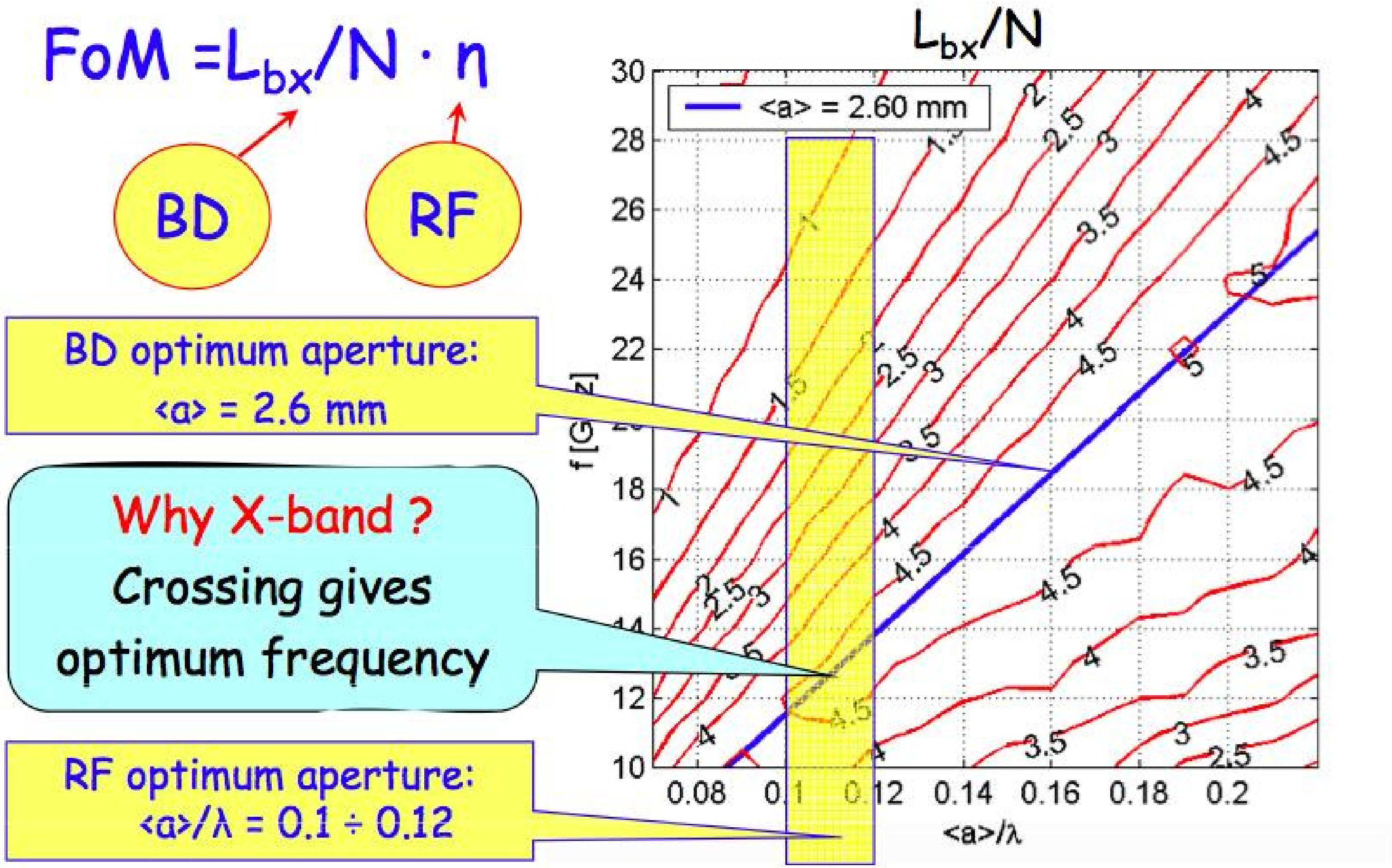
⇒ The choice of pulse length is somewhat involved

  for CLIC we chose the one which gves the lowest cost for each combination of a specific structure and gradient

Results



Results 2



FoM =L$_{bx}$/N · η
BD
RF
BD optimum aperture:
<a> = 2.6 mm
Why X-band ?
Crossing gives
optimum frequency
RF optimum aperture:
<a>/λ = 0.1 ÷ 0.12
L$_{bx}$/N
<a> = 2.60 mm
f [GHz]
<a>/λ

Thanks

- Many thanks to you for listening and to the people who helped me to prepare this lecture
  - with advice
  - with plots

Erik Adli, Alexej Grudiev, Erk Jensen, Jochem Snuverink, Igor Syratchev, Rolf Wegner, Walter Wuensch, Riccardo Zennaro, Frank Zimmermann

Energy and Phase Stability

Requirements

- The final energy needs to be accurately known for physics
  - measurement
- The final energy needs to be stable for physics
  - large energy variations would also cause luminosity loss due to limited BDS band-width
  - need to control final energy
- The emittance needs to be preserved in presence of static imperfections
  - differences between the actual and the assumed lattice can cause emittance growth
  - need to control energy profile
- The emittance needs to be preserved in presence dynamic imperfections
  - the energy profile needs to be stable
  - kicks due to cavity tilts need to be controlled
- Beam timing errors lead to luminosity loss
  - need to control bunch compressor RF stability

Main Linac RF Noise Sources (ILC)

- Lorentz force detuning
  - systematic from pulse to pulse
  - is largely corrected using piezo tuners in feed-forward
- Microphonics
  - unpredictable
  - corrected by klystron-based (or piezo-based) feedback
- Klystron amplitude and phase jitter
  - corrected by klystron based feedback
- Beam current variation
  - measure beam current at damping ring and use feed-forward for klystrons
- Feedback noise
  - measurement noise
  - feedback amplifies at some frequencies
- Jitter of timing reference
  - impacts feedback systems

Low Level RF Controls

- The low level RF control ties the RF phase to a timing reference and adjusts the gradient
- For each cavity one measures
  - field amplitude and phase
  - input power
  - reflected power
- As correctors are used
  - piezo tuners in each cavity
  - stepping motors
  - klystron amplitude and phase
- One needs a beam timing feedback
- The klystron-based feedback acts on the vector sum of all cavity gradients in a unit
- The sensors are calibrated measuring the field with and without beam
  - the field induced by the beam can be calculated
- Input and reflected power per cavity is measured
- Beam current is measured at damping ring and used for feed-forward

Final Energy Static Error

- We can expect systematic errors in the acceleration along the main linac
  - coherent calibration errors of amplitude and phase measurement in all RF units
  - random calibration errors of amplitude and phase in each RF unit
- The beam energy will be measured with the spectrometer and the detector
  - very high precision (10^{-4}, actually it will be precisely the "relevant energy")
  - can remove coherent calibration errors
- We are left with random calibration errors

$\Rightarrow$ they can cause emittance growth

- Typical parameters are accuracies of 1% and 1°

$\Rightarrow$ should specify that this is acceptable (some work has been already done)

for 1.5% random acceleration error per unit, DFS still works

$\Rightarrow$ should identify our limit

Final Energy Stability

- This is fundamental physics requirement

  $\Rightarrow$ has to be achieved by the control system

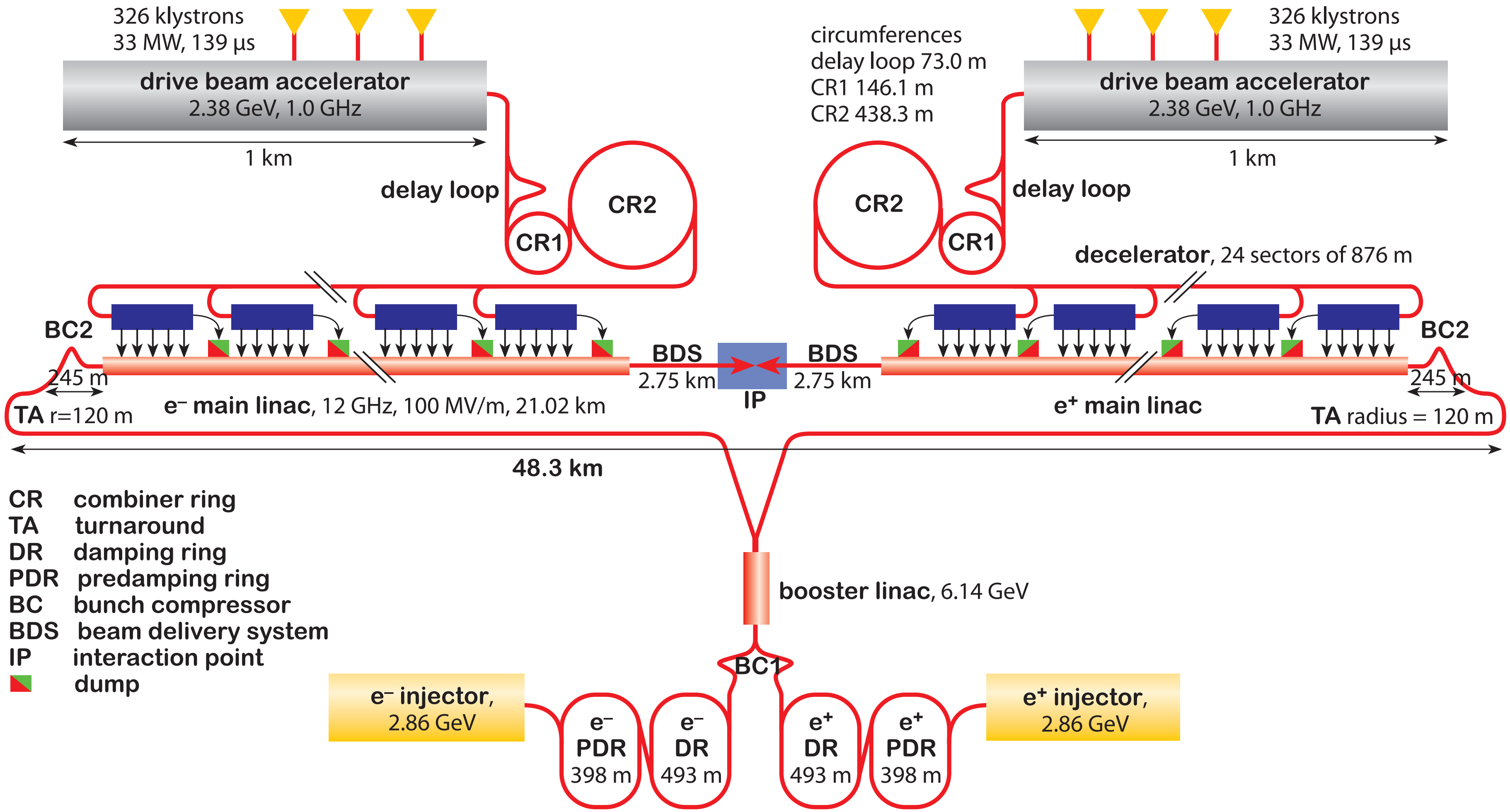
  $\Rightarrow$ let us try to see if this is the tightest tolerance
- Aim for 0.07% energy stability (RDR)
  - but for four error sources, should be reviewed
- Tolerance for coherent errors along main linac are
  - $\sigma_\phi \approx 0.4^\circ$
  - $\sigma_G = 0.07\%$
- Tolerance for independent errors per RF unit along main linac are about 16-times larger
  - $\sigma_\phi = 5.6^\circ$
  - $\sigma_G = 1\%$
- Phase tolerances depend on average RF phase used
- We would expect to have better stability but let us check if we do need it
- Check requirement of single cavity

CLIC RF Jitter Tolerance

- CLIC has similar limits for energy jitter than ILC
  - also luminosity loss is a concern
- Life is a bit more difficult since one drive beam complex powers the main linac
  - phase jitter coherent along each decelerator
  - component is coherent along the whole main linac
- Drive beam is produced at $1\,\mathrm{GHz}$

  $\Rightarrow$ relative phase jitter is amplified by factor 12
- Mitigation strategy is to
  - stabilise drive beam accelerator current and RF
  - correct the phase at final turn-around

CLIC Layout


326 klystrons
33 MW, 139 μs
drive beam accelerator
2.38 GeV, 1.0 GHz
1 km
delay loop
CR2
CR1
circumferences
delay loop 73.0 m
CR1 146.1 m
CR2 438.3 m
326 klystrons
33 MW, 139 μs
drive beam accelerator
2.38 GeV, 1.0 GHz
1 km
delay loop
CR2
CR1
decelerator, 24 sectors of 876 m
BC2
245 m
TA r=120 m
e⁻ main linac, 12 GHz, 100 MV/m, 21.02 km
BDS
2.75 km
IP
BDS
2.75 km
e⁺ main linac
BC2
245 m
TA radius = 120 m
48.3 km
booster linac, 6.14 GeV
BC1
e⁻ injector,
2.86 GeV
e⁻
PDR
398 m
e⁻
DR
493 m
e⁺
DR
493 m
e⁺
PDR
398 m
e⁺ injector,
2.86 GeV
CR combiner ring
TA turnaround
DR damping ring
PDR predamping ring
BC bunch compressor
BDS beam delivery system
IP interaction point
dump

Feed-forward at Final Turn-Around

- Final feed-forward shown

  ultima ratio

  - requires timing reference (FP6)
  - phase measurement/prediction (FP7)
  - tuning chicane (FP7, PSI)

- Measure phase and change of phase at BC1
- Adjust BC2 with kicker to compensate error
- One could also measure phase and energy at BC1
- Missing will be kicker and amplifier